

# PLANNING BOARD MEETING

Tuesday, January 23, 2024 at 6:00 PM

Town Hall - 41 South Main Street Randolph, MA 02368

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## AGENDA

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Pursuant to the temporary provisions pertaining to the Open Meeting Law, public bodies may continue holding meetings remotely without a quorum of the public body physically present at a meeting location until March 31, 2025. The public is invited to participate in the meeting in person, via telephone or computer.

- A. Call to Order - Roll Call**
- B. Chairperson Comments**
- C. Approval of Minutes**
  - 1.** Minutes of 12/12/2023
- D. Public Speaks**
- E. Public Hearings**
  - 1.** Scanlon Drive - Site Plan, Design and Stormwater Review (6:30 PM)
- F. Old/Unfinished Business**
- G. New Business**
  - 1.** Discussion about potential renovations to 334 Center Street
  - 2.** Subdivision - Perry Estates - Request for Extension
- H. Staff Report**
  - \*Active Subdivision Review
  - \*Active Project Review
  - \*Upcoming Projects
- I. Board Comments**
- J. Adjournment**  
Notification of Upcoming Meeting Dates  
  
Feb 13 and 27  
Mar 12 and 26

**File Attachments for Item:**

1. Minutes of 12/12/2023



# PLANNING BOARD MEETING

Tuesday, December 12, 2023 at 6:00 PM

Town Hall - 41 South Main Street Randolph, MA 02368

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## MINUTES

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Pursuant to the temporary provisions pertaining to the Open Meeting Law, public bodies may continue holding meetings remotely without a quorum of the public body physically present at a meeting location until March 31, 2025. The public is invited to participate in the meeting via telephone, computer, or in person.

### A. Call to Order - Roll Call

Chairman Plizga called the meeting to order at 6:02 PM.

PRESENT

Alexandra Alexopoulos  
Tony Plizga  
Nereyda Santos-Pina  
Peter Taveira  
Lou Sahlu

### B. Chairperson Comments

None

### C. Approval of Minutes

#### 1. Minutes of 11-28-2023

The Board approved the minutes of November 28, 2023, as presented.

Motion made by Alexopoulos, Seconded by Sahlu to approve the minutes of November 28, 2023 as presented.

Voting Yea: Alexopoulos, Plizga, Santos-Pina, Sahlu  
Voting Abstaining: Taveira

### D. Public Speaks

Kristen Baker of 29 Commercial Street in Braintree asked to speak in reference to 217 Mill Street. The Board asked Ms. Baker to wait for the Public Hearing to open to comment.

Amy Hubert Maferrer, the attorney for the Buyer of 217 Mill Street also wished to speak but will hold off until the Public Hearing.

Hearing no other comments from the public, Chairman Plizga closed the public portion of the meeting.

## E. Public Hearings

### 1. Subdivision - Mill Street (continuation 6:15pm)

Chairman Plizga asked Planner Tyler for a brief overview of the meeting on November 28. The Board discussed the design challenges of the proposed waterline for the 4-lot subdivision. The layout of the waterline does not loop as required by the Board's regulations. There was a discussion as to how it could be modified to improve it. The applicant's engineer Mr. Burke has drawn a new sketch for review by the Planning Board and DPW.

Mr. Burke, the engineer for the project was present, however, Mr. Sun, the agent for the applicant was not present, despite the request and reminder from the Planner to attend.

Planner Tyler read correspondence that she sent (via email) to the Planning Board, the applicant and the applicant's engineer on December 4. The correspondence stated "The Town's Engineer has reviewed the latest run for the proposed water line that will serve the Mill Street subdivision at the request of the Planning Board. He has reached the same conclusion as with the previous proposal designs. The proposed layout results in a substandard water distribution system that does not meet the Town's requirements for a looped system. While the proposal has revised the water line layout to improve the 180 degree turn in the line, it remains curved with water service beginning and stopping at the mainline on Mill Street. This is not anticipated to minimize any water quality issues and remains problematic with potentials for issues that would not be anticipated in a system with no curves. Further, permitting this type of substandard system could require the Town to invest time and resources above and beyond normal actions or costs to address any failures of the system once the subdivision is complete. The Randolph Planning Board subdivision regulations regarding water utilities are as follows...(pg 43 of the regulations). Planner also indicated in her correspondence that the applicant must attend this meeting.

Chairman Plizga asked Mr. Burke to present to the Board in the applicant's absence. Since the last meeting Mr. Burke revised the water line which widened the space between the tap. Mr. Burke stated that he strongly disagrees with the Town Engineer's assessment and hoped they could have had a discussion in order to work toward a resolution. He feels that water quality isn't an issue and that the head loss for a dead-end would be at a minimum. Mr. Burke pointed out that there are currently several dead-end lines that exist in the Town and would like to proceed with system as originally designed with the possibility of a future easement over to the neighboring water line.

Chairman Plizga invited Attorney Amy Hubert Masferrer to speak on behalf of the buyer. Ms. Masferrer feels with a housing shortage the benefit of adding housing far outweighs the minimal risk of adding this type of waterline. She contacted the abutting neighbors regarding a small easement - some did not respond, others had concerns over the disruption to their lawn.

Chairman Plizga followed up to Mr. Burke's comments about existing dead-end line in the Town. He feels history, although important, doesn't always matter as they have to go by the current rules and regulations of the Town. As for water quality, Chairman Plizga feels it has been an issue for a long time in Randolph. He respects the Town engineer's opinion on the matter and has to take into consideration the opinion of the former DPW Superintendent, as well.

Chairman Plizga asked if they have exhausted all efforts to obtain an easement over to Prospect. Ms. Masferrer replied that yes, they received correspondence back in July that the request for easement at 54 Prospect Ave was denied. Ms. Masferrer replied back to assure them that they would make all restoration to their landscaping and received no reply. She reached out to all the abutting neighbors which was unsuccessful, much to their surprise. It was explained to the abutters that full restoration would be made, their water pressure would likely improve and were offered compensation for the easement. They are currently at a standstill.

Mr. Burke feels that this project, even with a dead-end, has the potential to assist with water quality in that area and could be achieved by eliminating a portion of the the water main on Mill Street where the new road will go by having it loop up into the new roadway and back down again. He feels there are answers to this with some potential design changes, but never had the opportunity to discuss them with the Engineer. Mr. Burke feels a situation like this (relying on a easement) gives abutters a significant amount of power with almost undue leverage in the development of someone's private property.

Chairman Plizga asked how far apart the water taps are on Mill Street. Mr. Burke said about 40 feet. Chairman Plizga recalled from the last meeting trying to make them about 100 feet apart? Mr. Burke explained that he thought he had more frontage, so it is only 40 feet, but could possibly stretch it to 60 feet changing the bends and fittings. He believes if they removed the section of main along Mill street between the taps you would essentially have a looped main. Mr. Burke would have to make sure that section of the main has no tap servicing any of the neighbors. Chairman Plizga understands what Mr. Burke is saying, but that was not what was presented to the Town Engineer. Mr. Burke replied that it was explained in the email he sent as an option. He feels there are several options in trying to correct this and wanted to have an opportunity to discuss them with the engineer. Chairman Plizga pointed out that a meeting was never requested by Mr. Burke.

Chairman Plizga opened the discussion up to the Board members. Mrs. Alexopoulos cannot believe that an easement over to Prospect was not possible and wonders if the abutter shared their concern with Ms. Masferrer? Mrs. Santos-Pina worries about setting precedence with by allowing a dead-end water line and is relying on the Town Engineers comments. Mr. Taveira feels it is an unfortunate circumstance but agrees with Mrs. Santos-Pina about setting precedence.

Chairman Plizga noted that the applicant is still not on the meeting and only the applicant can request a continuation. Therefore, the chair would like to make a motion to close the public hearing. At this time, he does not feel comfortable asking for another continuation as the applicant disregarded the Board's request for him to appear. Mrs. Alexopoulos seconded for discussion. On discussion, by closing the public hearing we would not be able to accept any new information. Our decision will be based on what we have in front of us, both from the engineer and from the Town side.

Motion made by Plizga, Seconded by Alexopoulos to close the public hearing  
Voting Yea: Alexopoulos, Plizga, Santos-Pina, Taveira, Sahlu

Chairman Plizga will move into deliberation. Planner Tyler advised the Chairman that the Board has 90 days to deliberate once the public hearing is closed. Chair is prepared to make a motion to deny the Mill Street subdivision.

On discussion, Chairman Plizga noted they have been through this a number of times and seem to be at a dead-end. Chairman confirmed with the Planner that they could resubmit the project for consideration. Planner Tyler noted that she will file the decision with the Town Clerk within 14 days. That initiates an appeal period for anyone aggrieved by the decision to file an appeal. Mrs. Santos-Pina wanted to clarify that the applicant could come back after this is denied. Planner Tyler replied yes, there is no restriction.

Motion made by Plizga, Seconded by Sahlu to deny the Mill Street subdivision as presented on the Decelle-Burke-Sala drawing package dated April 10, 2023 and revised drawing excerpt depicting proposed alternative water supply layout received via email dated November 28, 2023. The denial is based on the water supply system shown on these drawings, as it does not meet the Planning Board Subdivision Rules and Regulations, specifically Section X "Specification for Construction", subsection E3 "Water."

Voting Yea: Alexopoulos, Plizga, Santos-Pina, Taveira, Sahlu

## F. Old/Unfinished Business

None

## G. New Business

### 1. Subdivision - Pham Estates - Request for Certificate of Completion

The Pham Estates subdivision was approved in 2019 for single lot subdivision that created Mary Lee Way. The project has been constructed and the owner is requesting a release and a certificate of completion.

Chairman Plizga asked Planner Tyler to go through Form N (Final Certificate of Completion) which has a checklist of items on page two for the Board to review and fill in before signing the document.

1. Constructed with approved waivers? YES
2. Constructed with approved field changes? NO
3. Constructed with unapproved field changes? NO
4. Form J - Inspection Sign-Off received? YES, Inspected by Town Engineer, Jean Pierre-Louis.
5. Conveyance of easements and utilities has been received: YES
6. Binder course subjected to one winter prior to application of final course? YES

7. Drainage and utilities exposed to one additional winter season after installation

8. Trees and landscaping exposed to one winter season? N/A

9. Street name is Mary Lee Way and is to remain a private way.

After reviewing Form N, Chairman Plizga requested a motion to approve the Final Certificate of Completion.

Motion made by Taveira, Seconded by Sahlu to approve Form N - Final Certificate of Completion for Pham Estates at Mary Lee Way, as discussed.

Voting Yea: Alexopoulos, Plizga, Santos-Pina, Taveira, Sahlu

Planner Tyler requested the Board sign-off on the Form F - 2, to release the covenant.

Motion made by Plizga, Seconded by Alexopoulos to release the covenant Form F-2 as presented.

Voting Yea: Alexopoulos, Plizga, Santos-Pina, Taveira, Sahlu

Planner will have the forms endorsed and recorded.

## 2. Planning Board Roles for 2024

Chairman Plizga opened the discussion up for nominations for Planning Board Chair. Mrs. Alexopoulos made a motion for Mr. Plizga to be Chair in calendar year 2024. Chairman Plizga asked if there were any other nominations for Chair? Hearing none, the Board proceeded to take a vote.

Motion made by Alexopoulos, Seconded by Taveira for Mr. Plizga to be Chair in calendar 2024.

Voting Yea: Alexopoulos, Santos-Pina, Taveira, Sahlu

Voting Abstaining: Plizga

Chairman Plizga moved to nominate Mrs. Alexopoulos as vice-chair that was seconded by Mr. Taveira that was *withdrawn*.

Chairman Plizga made a motion to nominate Mr. Taveira as vice-chair, seconded by Mrs. Alexopoulos. Mr. Taveira *declined*.

The Board had a brief discussion about the details of going without a vice-chair. Mrs. Alexopoulos agreed to take the position.

Motion made by Plizga, Seconded by Taveira to nominate Alexandra Alexopoulos as vice-chair.

Voting Yea: Alexopoulos, Plizga, Santos-Pina, Taveira, Sahlu

Mrs. Santos-Pina will be resigning from the Planning Board due to personal reasons. Mrs. Santos-Pina said she enjoyed the experience tremendously. The Board offered her well wishes.

## H. Staff Report

### Planning Board Forms

Planner will add this to the next agenda for discussion. Planner Tyler made some modifications to the forms related to performance guarantees that will be sent to the Board for review.

### **Active Subdivision Review**

Planning Department is still reviewing subdivision files to identify what remains outstanding.

### Hampton Court Subdivision

Planner will be reviewing this file to determine if it is complete. Both the property owner and developer feel it is complete, but there seems to be some outstanding items such as as-builts etc. Also, one lot is still not constructed with no curb cut.

### Trim Way & Toby Lane

Recorded the plan with land court. Needs to install a street sign.

### **Active Project Review**

#### Mazzeo Drive (Splash Car Wash)

Waiting for an opening date.

#### Allen Street (Convenience Store)

No update. Chairman Plizga noticed blacktop in parking lot.

#### 647 North Main Street (Daycare)

Finalizing site items. Awaiting Mass DOT approval for the light.

#### 19 Highland Avenue (Taj Estates)

Outstanding site items remain that are known and agreed upon prior to completion.

#### 34 Scanlon Drive (Yankee Bus Lines)

Demo work has started. Still waiting for finalization of stormwater utilities. Weston and Sampson (peer reviewer) is working with the project engineer on some changes. They will be coming back to Planning Board to review some minor changes to the plans.

#### Short Street (Bar)

Planner received a draft set of plans without application or fees. Planner reached out to the owner's attorney and has not hear back yet. There is a lot line issue that will need to be worked out that could impact a Planning Board decision.

### **Upcoming Projects**

#### Lantana/Lombardo's property

In January the Board will review plans draft plans for the proposed development of the Lantana property and lots along Scanlon Drive. The plans are for light-industrial manufacturing - not customer based developments or residential. They are within the

approved uses for that district and will need an ANR to consolidate some lots resulting in some non-conforming lots. One of the non-conforming lots will be for an existing cell tower, the other will be parking for the DCR trailhead. Discussions are taking place with the Conservation Commission regarding storm water, DCR regarding the trailhead parking and DOT due to the proximity to off-ramps. Applicant intends to go to Town Council to discontinue/abandon Billings Way and to Norfolk County to discontinue/abandon part of High Street to make the project they have envisioned work. Their goal is to come before the Board for a Public Hearing on January 23.

#### Road Safety Audit with Mass DOT

Planner walked along Route 28 near Route 128 to review road safety issues with Police Sergeant Andrews, Fire Chief of Operations Frew, and Mass DOT. They reviewed detailed reporting on accidents before walking the area to discuss trouble spots. Mass DOT will be compiling a report.

#### Planning Department News

Planning Department is working on a procedural manual of how meetings operate etc. in anticipation for a new Planning Board member.

Planner received a call from a property owner that wants to have an informal discussion at the January 23 meeting about some changes to their business property.

The Board had a brief discussion about when/or if an executive session may be required.

Chairman Plizga thanked Planner Michelle Tyler for all her help and patience in explaining different subjects and answering questions for the Board.

#### **I. Board Comments**

None

#### **J. Adjournment**

Notification of Upcoming Meeting Dates

January 9, 2024

January 23, 2024

February 13, 2024

February 27, 2024

March 12, 2024

Meeting adjourned at 7:27 PM.

Motion made by Taveira, Seconded by Alexopoulos to adjourn the meeting at 7:27 PM.  
Voting Yea: Alexopoulos, Plizga, Santos-Pina, Taveira, Sahlu

**File Attachments for Item:**

1. Scanlon Drive - Site Plan, Design and Stormwater Review (6:30 PM)

|                          |   |
|--------------------------|---|
| <b>Account Number:</b>   | 663354  |
| <b>Customer Name:</b>    | Randolph Planning Director  |
| <b>Customer Address:</b> | Randolph Planning Director<br>41 South Main St<br>Randolph MA 02368 |
| <b>Contact Name:</b>     | Randolph Planning Director  |
| <b>Contact Phone:</b>    | 7819610936  |
| <b>Contact Email:</b>    |   |
| <b>PO Number:</b>        | Austrino, Jen   |

|                           |            |
|---------------------------|------------|
| <b>Date:</b>              | 01/03/2024 |
| <b>Order Number:</b>      | 9706617    |
| <b>Prepayment Amount:</b> | \$ 0.00    |

|                          |         |
|--------------------------|---------|
| <b>Column Count:</b>     | 1.0000  |
| <b>Line Count:</b>       | 44.0000 |
| <b>Height in Inches:</b> | 0.0000  |

**Print**

| <b>Product</b>             | <b>#Insertions</b> | <b>Start - End</b>      | <b>Category</b> |
|----------------------------|--------------------|-------------------------|-----------------|
| NEO QUI The Patriot Ledger | 2                  | 01/06/2024 - 01/13/2024 | Public Notices  |
| NEO wickedlocal.com        | 2                  | 01/06/2024 - 01/13/2024 | Public Notices  |

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| Total Cash Order Confirmation Amount Due | \$134.64 |
| Service Fee 3.99%                        | \$5.37   |
| Cash/Check/ACH Discount                  | -\$5.37  |
| Payment Amount by Cash/Check/ACH         | \$134.64 |
| Payment Amount by Credit Card            | \$140.01 |

|                                  |                 |
|----------------------------------|-----------------|
| <b>Order Confirmation Amount</b> | <b>\$134.64</b> |
|----------------------------------|-----------------|

## **Ad Preview**

Section E, Item1.

### **HEARING 01/23/24 LEGAL NOTICE Public Hearing**

The Randolph Planning Board and Department of Public Works (stormwater authority) will open a public hearing on Tuesday, January 23, 2024 at 6:30pm on the petition by Scanlon Suburban LLC, 486 and 490 High QOZB, LLC, and 6 Billings QOZB, LLC for site plan and design review for phased construction to demolish existing on-site structures, install stormwater management systems and utilities in conjunction with the construction of new buildings with associated grading, landscaping and site amenities. The parcel is located in the Blue Hill River Highway District and subject to consolidation of parcels and road discontinuances to meet zoning requirements.

This meeting is conducted via ZOOM with public participation via telephone, computer or in person. The link to join the meeting is on the Town of Randolph calendar. Plans and materials may be viewed in the office of the Town Clerk at 41 South Main Street Randolph during regular business hours.

AD# 9706617  
PL 01/06 & 01/13/2024



Randolph Plann

Section E, Item1.

Town Hall

41 South Main Street

Randolph, MA 02368

781.961.0936

## NOTICE OF PUBLIC HEARING

Dear Property Owner

This letter is being sent to let you know a public hearing has been scheduled about a project near your property. You received this notice because records from the Randolph Assessor's Office indicate you own property near the site. Your attendance at this meeting is not required but your participation and input are an important part of the review process. A decision regarding the approval or denial of the proposal may be made at the conclusion of this hearing.

The meeting will be conducted with remote participation by ZOOM or in person at Town Hall. The link to join the meeting is posted to the Town's website [www.townofrandolph.com](http://www.townofrandolph.com) on the Planning Board webpage AND the meeting calendar no less than 48 hours before the meeting date.

Detailed plans and specifications for this project may be viewed at the office of the Town Clerk at 41 South Main Street, Randolph, MA during normal business hours.

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### HEARING TIME & LOCATION

6:30pm

Tuesday, January 23, 2024

Town Hall – Washington Room

41 South Main Street

Randolph, MA 02368

Attendance is via computer or telephone using ZOOM or in person at Town Hall.

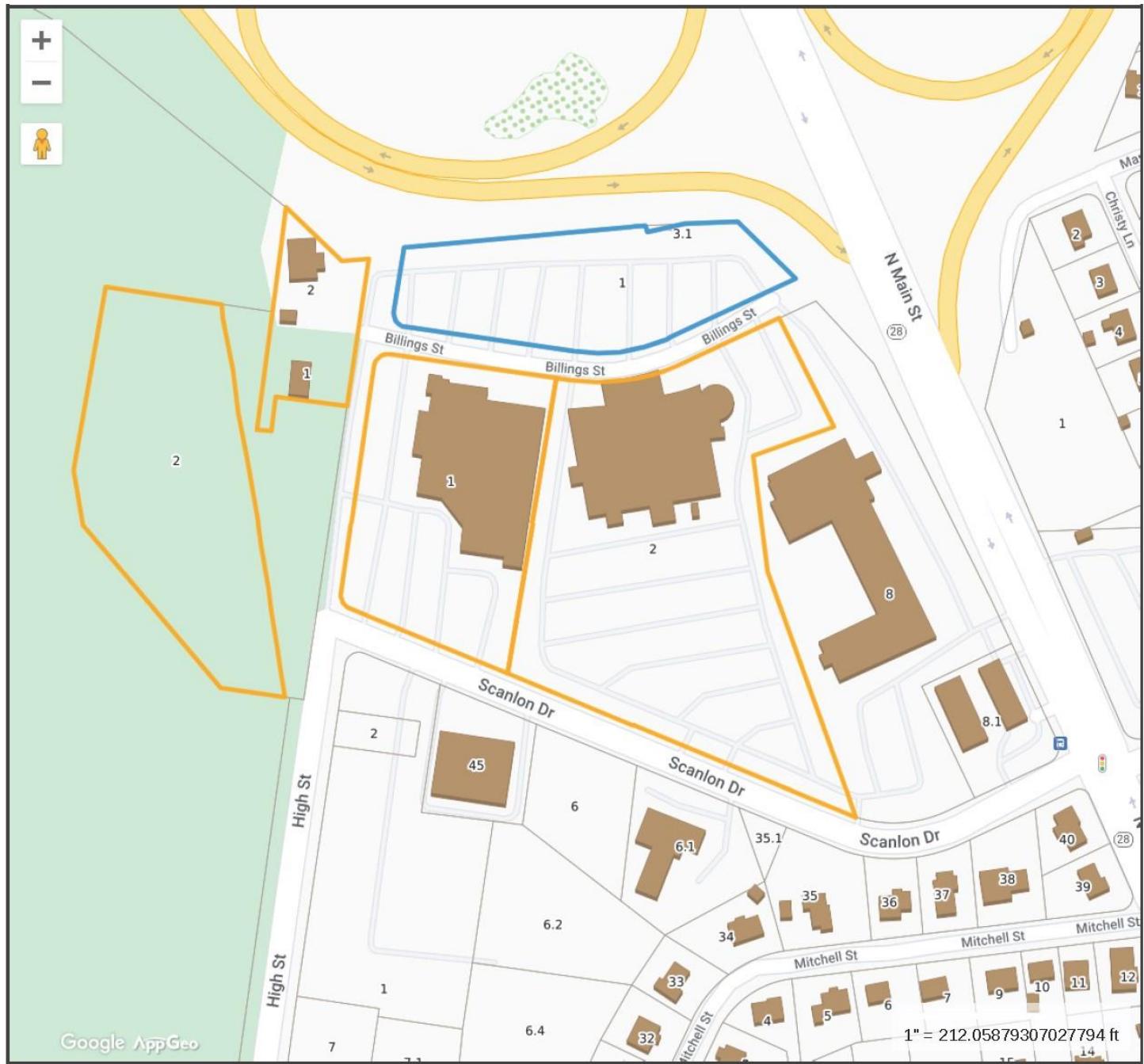
### PROPOSAL DESCRIPTION AND LOCATION

The petitioner seeks **site plan and design review** for phased construction to demolish existing on-site structures, install stormwater management systems and utilities in conjunction with the construction of new buildings with associated grading, landscaping and site amenities. The parcels are located on High Street, Scanlon Drive and Billings Street in the Blue Hill River Highway District and subject to consolidation of parcels and road discontinuances to meet zoning requirements.

*See reverse for map.*

### PETITIONER

Scanlon Suburban, LLC; 486 and 490 High QOZB, LLC; and 6 Billings QOZB, LLC  
800 Boylston Street, 30<sup>th</sup> Floor  
Boston, MA 02199



December 20, 2023

Ms. Michelle Tyler, Director of Planning  
Town of Randolph Planning Board  
41 South Main Street  
Randolph, MA 02368

Re: **Site Plan Design & Review**  
Proposed Development North of Scanlon Drive  
43 Scanlon Drive  
Randolph, MA 02368  
VERTEX Project No. 78000

Dear Ms. Tyler and Members of the Planning Board:

On behalf of the Applicant and pursuant to the Site plan & Design Review Regulations by Planning Board for the Town of Randolph, The Vertex Companies LLC (VERTEX) is pleased to submit the items outlined below for the Proposed Development North of Scanlon Drive (Randolph North Development) as part of the Site plan Design & Review process.

The design team for this project is led by Stantec Architecture & Engineering P.C., of Boston, MA. Civil Engineering services are being provided by The Vertex Companies, LLC of Weymouth, MA. Stantec Architecture & Engineering P.C. of Boston, MA is also providing landscape architectural design for this project.

The project consists of the demolition of the existing onsite structures and construction of two (2) new buildings. In addition to the new structures, work will include site grading, utilities, stormwater management facilities, and site amenities. The structures will be accessed via new curb cuts on Scanlon Drive and High Street.

Included in this submission are the following materials:

- Three (3) copies of the Town of Randolph Planning Department Application for Site Plan & Design Review;
- Three (3) copies of the plans entitled *Site Development Plans for Proposed Development North of Scanlon Drive*, prepared by The Vertex Companies, LLC and dated December 26, 2023;
- Three (3) copies of Architectural Plans prepared by Stantec Architecture & Engineering P.C.;
- Three (3) copies of the Planting Plan prepared by Stantec Architecture & Engineering P.C.;

- Three (3) copies of the plan entitled *RAMP N – Parcelage Legend* prepared by the Owner;
- Three (3) copies of the plan entitled *ANR Plan of Land – High Street and Scanlon Drive – Randolph, MA* prepared by CHA and dated December 19, 2023;
- Three (3) copies of the plan entitled *Billings Street Discontinuance Plan of Land – Billings Street – Randolph, MA* prepared by CHA;
- Three (3) copies of the plan entitled *High Street, Randolph, MA* prepared by CHA and dated September 29, 2023;
- Three (3) copies of the figure entitled *Fire Truck Exhibit* prepared by The Vertex Companies, LLC and dated December 12, 2023;
- Three (3) copies of the Stormwater Management Report prepared by The Vertex Companies, LLC and dated December 26, 2023;
- Three (3) copies of the Operations & Maintenance Manual prepared by The Vertex Companies, LLC and dated December 26, 2023;
- Three (3) copies of the report entitled *Randolph North Development – Traffic Impact Study* prepared by Howard Stein Hudson and dated December 2023;
- Three (3) copies of the Certified Abutters list;
- Three (3) copies of *Memorandum in Support of Application for Site Plan & Design Review*;
- Check for filing fee

We appreciate your consideration of this project and respectfully request the review of the included project materials. Please feel free to contact us if you have any questions or concerns.

Sincerely,

The Vertex Companies, Inc.



Andrew B. Street, PE  
Senior Project Manager – Civil Engineering

**To:** Town of Randolph Planning Board, Planning Department, Building Department, Conservation Commission (the “**Reviewing Authorities**”)

**From:** Scanlon Suburban LLC, 486 and 490 High QOZB, LLC, and 6 Billings QOZB, LLC (the “**Applicants**”)

**Property Addresses:** 43 Scanlon Drive, 6 Billings Street, 493 High Street, 486 High Street, 490 High Street, and unnumbered High Street, of Randolph, MA (collectively, the “**Properties**”)

**Plans:** Existing conditions drawings, discontinuation plans, consolidation plans, proposed site plans (including infrastructure), and conceptual exterior renderings, attached to this memorandum (the “**Plans**”)

**Re:** Site Plan & Design Review, Proposed Maxim Crane Regional HQ & Technical Industrial Building

**First Hearing Date:** January 9, 2023

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**Memorandum In Support of Application  
For Site Plan & Design Review**

**Application for Site Plan & Design Review**

Applicants submit this memorandum in support of their application (the “**Application**”) for Tier 3 Site Plan & Design Review under Section 200-90 of the Town of Randolph Zoning Ordinance. The Applicants are the owners or the current owner’s contracts purchaser of the Properties.

It is the intent of the Applicants, or their successors in title, to consolidate and develop the Properties for four (4) independent uses described below. As part of the consolidation of the Properties, the Applicant intends to simultaneously work with the Town of Randolph to discontinue Billings Street and work with Norfolk County to discontinue the northern portion of High Street.

Applicants would request that the Town of Randolph consider this Application as a “Masterplan” design for a two (2) Phase Development for Property A and Property B as described below.

**Property A**

The Applicants, wish to develop 486 High Street, 490 High Street, a portion of 43 Scanlon Drive, a portion of unnumbered High Street, a portion of 493 High Street, a portion of 6 Billings Street, and a portion of High Street (the “**Maxim Site**”), depicted as “**Property A**” on the Plans, as the regional corporate maintenance and operations headquarters for Maxim Crane Works LP (“**Maxim**”), the largest operator of tower and crawler cranes in the United States.

*Description of Development Plan*

As shown on the Plans, the intended development of the Maxim Site is comprised of newly constructed facility space containing maintenance, warehousing, and office space, for approximately 68,000 square feet, within two (2) buildings located on 43 Scanlon Drive, thirty-seven (37) employee parking spaces, an exterior laydown yard, and ancillary fueling depot.

*Proposed Operations*

The Maxim Site will be fenced and secured at all times for safety and security. Property A will be principally used for (i) storage (interior warehousing and exterior laydown) of new building components, (ii) maintenance and staging of the crawler and tower crane fleet, (iii) supporting office space, (iv) parking, and (v) and laydown of crane components. On-site business hours, during which most staff [roughly thirty (30) on-site employees] will be present, will be between 6:00 AM – 7:00 PM. Occasionally crawler cranes and components of tower cranes may arrive and depart from the Maxim Site outside of those hours.

Essentially all maintenance and upkeep of the fleet will happen within the 65,000 square foot building, which will also house the offices, field operator resource areas, and warehousing mentioned above. The remainder of Property A will be dedicated to yard space, an ancillary fueling area, and parking for employees.

Maxim will diligently monitor and work to mitigate any disturbances caused by noise or light pollution. Maxim's effective monitoring at its existing facilities is evidenced by the fact that there have been no citations for such disturbances. The proposed Maxim Site has been designed to be harmonious with its surroundings. By performing maintenance within the building, utilizing full-perimeter opaque fencing, and providing lush foliage to buffer the yard from the abutters, the few activities occurring in the yard of the Maxim Site are expected to be inconspicuous to outside parties.

#### *Maxim Crane Works LP*

Maxim is the largest provider of cranes and crane services in the United States with almost 3,000 employees, spanning across over 60 locations from coast to coast. Maxim was established in 1994 and has stabilized over 30 locations for its operations since. The Applicants are looking forward to a long-term landlord/tenant relationship with Maxim and anticipate that Maxim will meaningfully contribute to Randolph for the span of its 20-year lease.

In the Spring of 2022, Maxim approached the Applicant expressing interest in the Property A. Maxim had been looking to consolidate an existing portfolio of leased spaces spread throughout the Boston metropolitan area into one facility that could accomplish all of its needs for the foreseeable future, and Property A is where Maxim saw an opportunity to accomplish just that. Maxim's New England regional headquarters, formerly Shaughnessy Crane headquarters, has been located in South Boston for the past 66 years. Maxim has established a deep history and meaningful relationships within the City of Boston. Over time its operation has outgrown its existing facilities. Thus, Maxim now wishes to establish a new corporate home that is conveniently accessible and close to Boston. Maxim and its affiliates across the nation pride themselves on being courteous neighbors and active participants in their communities. The group makes significant contributions to charities on local, regional and national scales, and is currently looking to expand an active Emergency Solutions Grants Program. The majority of Maxim's philanthropy at the local and regional level where they donate or directly engage with the community through events. Maxim's contribution to the tax base in terms of property tax and excise tax will be significant.

#### *Design Strategy*

The layout has been tailored to the intended operations for Maxim Site. The program, consisting of both interior and exterior uses, situates the building between the paved laydown yard and the public face in order to buffer the streetscape from more function-forward uses, such as exterior storage and crane staging. The laydown yard is bounded on 4 of its 5 sides by forested portions of the Blue Hills Reservation. On top of said natural buffering, a tall, opaque fence will surround the entirety of the laydown yard, with gated openings exclusively at the entryway. The proposed building will be no more than two stories to the roof ridge, allowing the structure to be characteristic with its surroundings and conceal the majority of the yard activity from the streetscape. Interior uses occurring inside this building would include all maintenance activity related to cranes, rack-based storage, and office/dispatch areas. Due to the low occupancy levels typical to Maxim operations, the design team elected to provide the minimum parking count required by code.

## Property B

### *Description of Development Plan*

As a second phase to the proposed development of the Properties, the Applicants, wish to develop a portion of a portion of 43 Scanlon Drive, a portion of 6 Billings Street, a portion of 493 High Street, and a portion of Billings Street, depicted as “**Property B**” on the Plans, as either a Current Good Manufacturing Practice (cGMP) facility or another technical industrial use of approximately an approximately 180,000 square foot building. Property B suitable for warehousing, production, and office space, as well as parking for up to two hundred sixty-nine (269) vehicles.

The Applicants plan to commence development of Property B while simultaneously fielding interest from prospective end-users. The day-to-day operations of a cGMP or technical industrial facility customarily involve all on site activity taking place during working hours (8:00 AM – 6:00 PM Monday through Friday). Employees generally arrive between 8:00 AM – 10:00 AM and depart between 4:00 PM – 6:00 PM, and the site is designed to park up to two hundred sixty-nine (269) vehicles for employees. The site is designed to provide viable traffic flow and loading. As noted above, these uses are intended to include **production** of goods, lab and research, warehousing, office, and other support space. Due to the nature of the business of end users in the high-end industrial market, most prospective end-users are solely interested in striking deals with projects that are under construction or have permits in hand. The Applicants have set out to design a site that can accommodate either a large single user or two medium-sized users, both with parking ratios or roughly 1.5 spaces per 1,000 square feet.

## Property C

“**Property C**”, as depicted on the Plans, is a portion of unnumbered High Street at the intersection of High Street and Scanlon Drive. The intended use of Property C is to establish an easement to DCR for public use of this parcel as the trailhead and a related parking area. The origin of this concept was developed as a part of a land swap agreement between the former owner of unnumbered High Street and DCR. The initial design was to provide ten (10) dedicated spaces for trailhead parking. This parcel is a portion of the parking lot which was previously used as overflow parking for the Lantana.

## Property D

490 High Street is home to a single cell tower (and its support equipment). In order to maintain operations, the tenant requires access and a small maintenance area. “**Property D**”, as shown on the Plans, is intended to be used as a non-buildable access easement to the cell tower tenant through Property A and B to 490 High Street.

## The Masterplan

### *Masterplan Approach for Property A*

In light of the fact that the Applicants’ have not yet identified the end-use for Property B (defined below), the Applicants desire to proceed with specific approval for Property A, but conditional approval for Property B because an end-user for Property B has not yet been secured. Once a user is secured (by way of lease agreement or otherwise), the Applicants, will reapproach the town with updated, more

detailed plans and specifications that will pertain to the specific operations. Applicant would accept a condition on Site Design Approval for Property B to return to the Planning Board when the final design and use of Property B is identified. The Applicant would however, respectfully request an independent and full approval for the Maxim Site, Property A.

#### *Site Design Strategy*

The Applicant's design strategy is aimed to minimize potential impacts to the nearby neighborhoods while ushering in stable, long-term uses that complement the existing surroundings and the Town of Randolph as a whole. The proposed consolidation of parcels, locations of intended uses, and street discontinuances (of Billings Street and High Street) within the overall masterplan strategy have been based around market conditions and the perceived "highest-and-best-use" for the Properties. Due to the nature of Maxim's use, the pre-existence of the cell tower, and DCR's need for a trailhead, the western half of the site (Properties A, C and D) came together organically, leaving the remainder, Property B, to be designed around a yet to be identified user.

#### **Current Site Uses and Recent History**

##### *6 Billings Street, Lombardo's Events Facility*

The 70,000+ square foot Lombardo's building plans to cease operations after December of 2023. Lombardo's has hosted a myriad of weddings, holiday parties, retirement functions, proms, and conventions for 40 years and has become an integral part of the Randolph landscape since opening in 1983. One of the Applicants, 6 Billings QOZB, LLC, is the contract purchase of the Lombardo's facility with a closing planned in January 2024.

##### *493 High Street, Parking for Lombardo's Events Facility*

The lot located at 493 High Street, across from Lombardo's on the other side of Billings Street, is solely used as a parking lot for Lombardo's, and included under the Lombardo's purchase agreement.

##### *43 Scanlon Drive, The Lantana*

The Lantana, which ceased operations in 2021, operated at 43 Scanlon Drive for nearly 50 years. The property is owned by one of the Applicants, Scanlon Suburban LLC, and now vacant.

##### *Unnumbered High Street, Greenfield Site*

Located directly across from the former Lantana events facility, the lot referred to as unnumbered High Street currently exists as an undeveloped parcel of vegetated land. Formerly owned by DCR as part of the Blue Hills Reservation, the land was conveyed to the prior owner of 43 Scanlon Drive and was approved by the Town of Randolph to be used as overflow parking for the Lantana.

##### *486 High Street, Single Family Home*

A single-family home, abutting unnumbered High Street, has been vacant since the prior tenant relocated in 2022. The site is owned by one of the Applicants, 486 and 490 High QOZB, LLC, and the house on the property has been boarded up and made safe.

##### *490 High Street, A Cell Tower & Laydown Space*

A portion of this parcel is home to a cell tower easement holder, as mentioned above. In addition, historically, the paved lot on this parcel has been used for parking.

### *Billings Street*

Billings Street is a public way under the Town of Randolph's jurisdiction. Its sole use, as it stands today, is to act as frontage for 6 Billings Street. The street branches off of High Street and dead ends just before Route 24.

### *High Street*

The northern most portion of High Street begins at its intersection of Scanlon Drive and is bounded to the north by the Interstate 93 off ramp (exit 5A). This portion of High Street provides access to the High Street parcels listed above and branches into Billings Street.

### **Description of Abutting Properties**

The Properties are abutted by the following: (i) to the north, Route 93 (MassDOT); (ii) to the south, Scanlon Drive; (iii) to the west, Blue Hills Reservation (DCR); and (iv) to the east, the Comfort Inn Hotel and Route 28. The Properties will be heavily landscaped and fenced at their perimeters and have been designed to use existing buffers to screen forward elements of the program.

### **Conclusion**

Maxim and its development team in partnership with the development staff at Core Investments Development LLC (an affiliate of the Applicants), Stantec Architects and the engineering staff of Vertex have worked tirelessly with the Town Planning, Building, Conservation, Administration, and other departments in Randolph to develop a plan and design that would be fully consistent with Randolph Zoning Ordinance Section 200-94 criteria. As outlined above, the Applicants seek specific approval for Property A, and conditional approval for Property B, as Applicants will continue to work with the Town and seek additional approval for Property B as a second phase to the development of these Properties once an end-use has been secured.

On behalf of the Applicants, Maxim, and Core Investments Development LLC, we thank the Board and the Town of Randolph for their assistance and guidance in the Site Plan Review & Design Approval process and ask that the Board act favorably upon the Application and grant Site Plan & Design Approval.

The Applicants look forward to our hearing before the Board on January 9, 2024.

## TOWN OF RANDOLPH PLANNING DEPARTMENT

**APPLICATION FOR  
SPECIAL PERMIT ~ AND/OR ~ SITE PLAN & DESIGN REVIEW**

|   |   |  |  |
|---|---|--|--|
| <b>Project Type</b>                                   | Tier 1 Review (administrative)  | <input type="checkbox"/> In-Law Apartment<br><input type="checkbox"/> Two-Family Dwelling<br><input type="checkbox"/> Special Permit |  |
|   | Tier 2 Review   |  |  |
|   | <input checked="" type="checkbox"/> Tier 3 Site Plan/Design Review  |  |  |
| <b>Assessor Parcel ID<br/><i>map-block-parcel</i></b> | 1-A-1; 1-B-2; 2-C-1.438; 2-C-2.2; 2-B-1.LA  | <b>Norfolk County Registry of Deeds</b>  | <i>Book&amp; Page or Land Court Cert #</i> |
| <b>Parcel Address</b>                                 | High Street; Blue Hills Reservation; 43 Scanlon Drive; 6 Billings Street; 493 High Street   |  |  |
| <b>Current Use</b>                                    | Commercial and vacant land  |  |  |
| <b>Zoning District</b>                                | Blue Hills River Highway  | <b>Size of Parcel</b>  | 13.18 acres (combined)                     |
| <b>Project Description</b>                            | Project includes the demolition of the existing onsite structures and construction of two new buildings with associated grading, utilities, stormwater management facilities, landscaping and site amenities.   |  |  |
|   | <p><b>Are there wetlands on the parcel or within 300 feet of the construction?</b> <input checked="" type="radio"/> YES <input type="radio"/> NO<br/> <i>If yes – file with the Conservation Commission</i></p> <p><b>Is land disturbance &gt; 5,000 square feet?</b> <input checked="" type="radio"/> YES <input type="radio"/> NO<br/> <i>If yes – file a stormwater permit with DPW</i></p> <p><b>Does the proposed use increase pollutant loads?</b> <input checked="" type="radio"/> YES <input type="radio"/> NO<br/> <i>If yes – file a stormwater permit with DPW</i></p> <p><b>Is structure &gt; 100 years old?</b> <input checked="" type="radio"/> YES <input type="radio"/> NO<br/> <i>If yes – file with the Historic Commission</i></p> |  |  |

|                         |  |        |                              |    |     |       |
|-------------------------|--|--------|------------------------------|----|-----|-------|
| <b>Applicant Name</b>   | Scanlon Suburban LLC, 486 and 490 High QOZB, LLC , and 6 Billings QOZB, LLC  |        |                              |    |     |       |
| <b>Contact person</b>   | Art Campbell   |        |                              |    |     |       |
| <b>Applicant Status</b> | <input checked="" type="radio"/> Owner <input type="radio"/> Tenant <input type="radio"/> Licensee <input type="radio"/> Buyer <input type="radio"/> Other _____ |        |                              |    |     |       |
| <b>Address</b>          | 800 Boylston Street, 30th Floor  |        |                              |    |     |       |
|                         | CITY   | Boston | STATE                        | MA | ZIP | 02199 |
| <b>Phone</b>            | 617-428-8000   | Email  | acambell@coreinvestments.com |    |     |       |

\*If property owner is not the Applicant, authorization from the owner is required\*

|                       |                     |         |                          |    |     |       |
|-----------------------|---------------------|---------|--------------------------|----|-----|-------|
| <b>Surveyor</b>       | CHA                 |         |                          |    |     |       |
| <b>Contact person</b> | William Dorgan, PLS |         |                          |    |     |       |
| <b>Address</b>        | 141 Longwater Drive |         |                          |    |     |       |
|                       | CITY                | Norwell | STATE                    | MA | ZIP | 02061 |
| <b>Phone</b>          | 781-982-5400        | Email   | wdorgan@chasolutions.com |    |     |       |

|                       |  |              |                       |    |            |       |  |
|-----------------------|--|--------------|-----------------------|----|------------|-------|--|
| <b>Engineer</b>       | The Vertex Companies, LLC              |              |                       |    |            |       |  |
| <b>Contact person</b> | Andrew Street, PE                      |              |                       |    |            |       |  |
| <b>Address</b>        | 100 North Washington Street, Suite 302 |              |                       |    |            |       |  |
|                       | <b>CITY</b>                            | Boston       | <b>STATE</b>          | MA | <b>ZIP</b> | 02114 |  |
| <b>Phone</b>          | 781-400-6882                           | <b>Email</b> | astreet@vertexeng.com |    |            |       |  |

|                       |   |              |                                  |    |            |       |  |
|-----------------------|---|--------------|----------------------------------|----|------------|-------|--|
| <b>Property Owner</b> | Scanlon Suburban LLC, 486 and 490 High QOZB, LLC , and 6 Billings QOZB, LLC |              |                                  |    |            |       |  |
| <b>Address</b>        | 800 Boylston Street   |              |                                  |    |            |       |  |
|                       | <b>CITY</b>   | Boston       | <b>STATE</b>                     | MA | <b>ZIP</b> | 02199 |  |
| <b>Phone</b>          | 9082394642  | <b>Email</b> | acampbell@coreinvestmentsinc.com |    |            |       |  |

For any application for a **Special Permit**, the applicant shall submit additional documentation to support:

- That the proposed use is in harmony with the general purpose and intent of the Town's ordinances;
- That the proposed use is in an appropriate location and is not detrimental to the neighborhood and does not significantly alter the character of the zoning district;
- Adequate and appropriate facilities will be provided for the proper operation of the proposed use;
- That the proposed use would not be detrimental or offensive to the adjoining zoning districts and neighboring properties due to the effects of lighting, odors, smoke, noise, sewage, refuse materials or other visual nuisances;
- That the proposed use would not cause undue traffic congestion in the immediate area.

I hereby certify, under the pains and penalties of perjury, that the information contained in this application is true, accurate and complete to the best of my knowledge and belief. I agree to abide by the Randolph Zoning Ordinances and complete construction of the project in accordance with said rules and any conditions of the Planning Board.



Applicant Signature

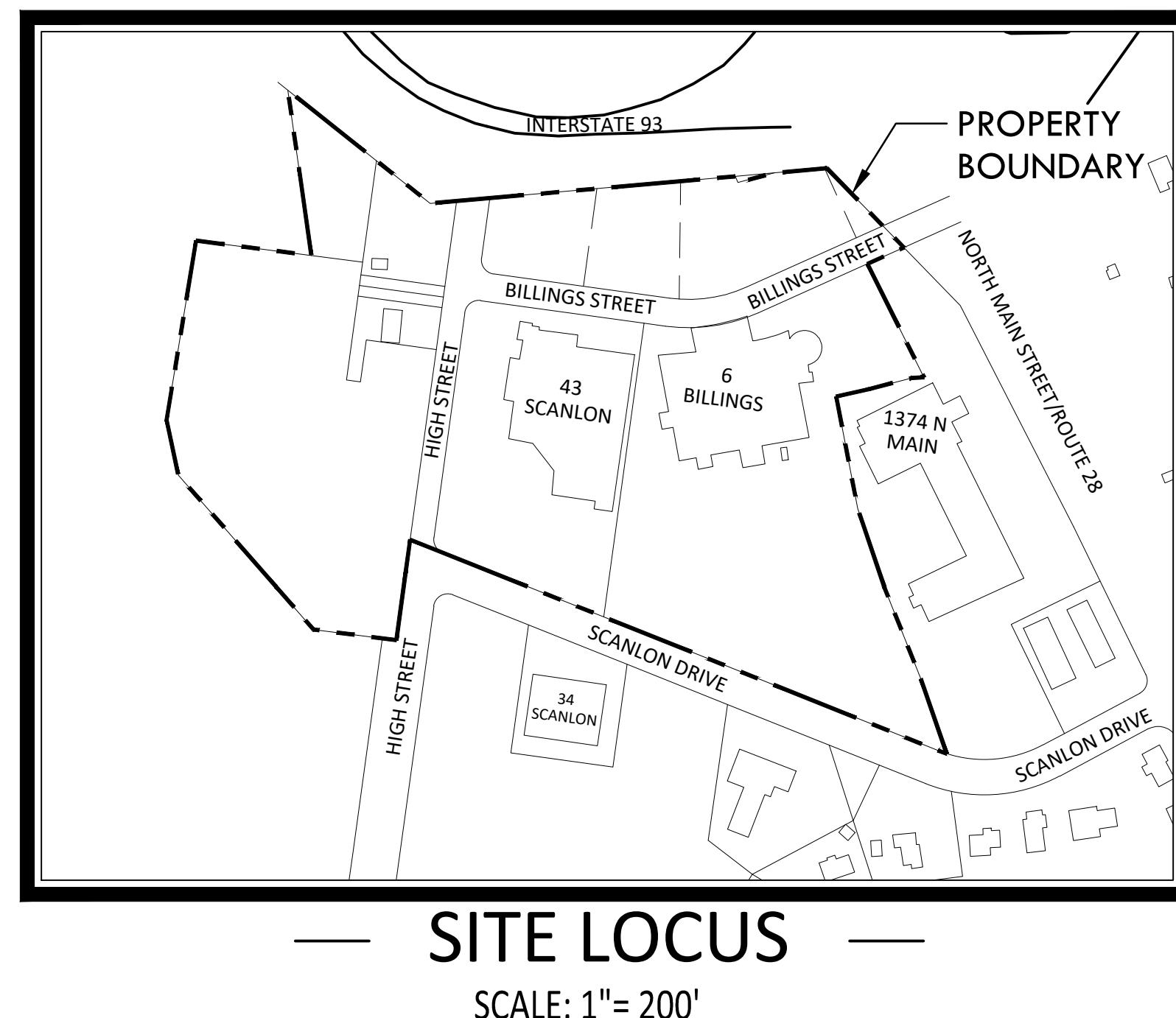
12-19-23

Date

**VERTEX<sup>®</sup>**  
400 Libbey Parkway  
Weymouth, MA 02189  
Main: 781.952.6000  
VERTEXENG.COM

# SITE DEVELOPMENT PLANS FOR PROPOSED DEVELOPMENT NORTH OF SCANLON DRIVE

Submitted to the: Town of Randolph



|  |   |   |
|--|---|---|
| ● <b>OWNER</b><br><hr/>  | ● <b>CIVIL ENGINEER</b><br>THE VERTEX COMPANIES, LLC.<br>400 Libbey Parkway<br>Weymouth, MA 02189                         | ● <b>TRAFFIC ENGINEER</b><br>HOWARD STEIN HUDSON ENGINEERS + PLANNERS<br>11 BEACON STREET, SUITE 1010<br>BOSTON, MA 02108 |
| ● <b>ARCHITECT</b><br>STANTEC ARCHITECTURE & ENGINEERING P.C.<br>40 WATER STREET, 3RD FLOOR<br>BOSTON, MA 02109  | ● <b>LANDSCAPE ARCHITECT</b><br>STANTEC ARCHITECTURE & ENGINEERING P.C.<br>40 WATER STREET, 3RD FLOOR<br>BOSTON, MA 02109 | ● <b>PERMITTING SPECIALIST</b><br>VHB, INC.<br>99 HIGH STREET, 13TH FLOOR<br>BOSTON, MA 02110                             |
| ● <b>MECHANICAL, ELECTRICAL, PLUMBING &amp; FIRE PROTECTION ENGINEER</b><br>CONSENTINI CONSULTING ENGINEERING<br>100 FEDERAL STREET, 6TH FLOOR<br>BOSTON, MA 02110 | ● <b>STRUCTURAL ENGINEER</b><br>DESIMONE CONSULTING ENGINEERS<br>31 MILK STREET, SUITE 1016<br>BOSTON, MA 02109           | ● <b>GEOTECHNICAL ENGINEER</b><br>MCPHAIL ENGINEERS<br>2269 MASSACHUSETTS AVENUE<br>CAMBRIDGE, MA 02140                   |

## SHEET INDEX

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- C1.0 OVERALL EXISTING CONDITIONS AND DEMOLITION PLAN
- C1.1 EXISTING CONDITIONS AND DEMOLITION PLAN 1
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- C2.0 OVERALL SITE IMPROVEMENTS PLAN
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- C6.1 SITE DETAILS 1
- C6.2 SITE DETAILS 2
- C6.3 SITE DETAILS 3
- C6.4 SITE DETAILS 4
- C6.5 SITE DETAILS 5



**REFERENCE**

1. EXISTING CONDITION AND PROPERTY INFORMATION PROVIDED BY CHA CONSULTING, INC. IN APRIL OF 2022.

**GENERAL NOTES**

- THE STATE OF MASSACHUSETTS STANDARD SPECIFICATIONS FOR HIGHWAYS AND BRIDGES 1995 EDITION AND THE SUPPLEMENTAL SPECIFICATIONS 2002 EDITION, OR LATEST REVISION, AND THE MASSACHUSETTS STANDARD DETAILS AND TOWN OF RANDOLPH STANDARD DETAILS AND CONSTRUCTION STANDARDS ARE MADE A PART HEREOF AS FULLY AND COMPLETELY AS IF ATTACHED HERETO. THE 1995 EDITION OF THE STANDARD SPECIFICATIONS AND THE 2002 EDITION OF THE SUPPLEMENTAL SPECIFICATIONS MAY BE OBTAINED AT THE MASSACHUSETTS DEPARTMENT OF TRANSPORTATION.
- THE CONTRACTOR SHALL MAKE ALL NECESSARY CONSTRUCTION NOTIFICATIONS AND APPLY FOR AND OBTAIN ALL NECESSARY CONSTRUCTION PERMITS, PAY ALL FEES AND POST ALL BONDS ASSOCIATED WITH THE SAME, AND COORDINATE WITH THE OWNER AND THE ENGINEER. THE CONTRACTOR IS REQUIRED TO FILE ANY DOCUMENTS REQUIRED BY NPDES GENERAL PERMIT OR PUBLIC WORKS ORDER OF CONDITIONS APPLICABLE TO THE SITE.
- THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR JOB SITE SAFETY. THE CONTRACTOR SHALL PROVIDE TEMPORARY FENCING AND/OR BARRIERS AROUND ALL OPEN EXCAVATED AREAS, AND CONDUCT ALL WORK IN ACCORDANCE WITH OSHA STANDARDS AND TOWN OF RANDOLPH REQUIREMENTS.
- AFTER THE INSTALLATION OF THE EROSION CONTROLS, THE CONTRACTOR SHALL NOTIFY THE PUBLIC WORKS IN WRITING AT LEAST 48 HOURS PRIOR TO THE START OF ANY WORK.
- IF ANY DEVIATION OR ALTERATION OF THE WORK PROPOSED ON THESE DRAWINGS IS REQUIRED, THE CONTRACTOR SHALL IMMEDIATELY CONTACT AND COORDINATE WITH THE ENGINEER, THE OWNER AND TOWN OF RANDOLPH PUBLIC WORKS OR THEIR AGENT.
- ANY AREA OUTSIDE OF THE LIMIT OF WORK THAT IS DISTURBED SHALL BE RESTORED TO ITS ORIGINAL CONDITION AT NO COST TO THE OWNER.
- ALL EXISTING CONDITIONS SHOWN SHALL BE CONSIDERED APPROXIMATE AND ARE BASED ON THE BEST INFORMATION AVAILABLE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFYING THAT THE PROPOSED IMPROVEMENTS SHOWN ON THE PLANS DO NOT CONFLICT WITH ANY KNOWN EXISTING OR OTHER PROPOSED IMPROVEMENTS. IF ANY CONFLICTS ARE DISCOVERED, THE CONTRACTOR SHALL NOTIFY THE OWNER, THE ENGINEER AND TOWN OF RANDOLPH PUBLIC WORKS OR THEIR AGENT PRIOR TO INSTALLATION OF ANY PORTION OF THE SITE WORK WHICH WOULD BE AFFECTED. NO FIELD ADJUSTMENTS IN THE LOCATION OF SITE ELEMENTS SHALL BE MADE WITHOUT THE ENGINEERS, AND TOWN OF RANDOLPH PUBLIC WORKS OR THEIR AGENT APPROVAL.
- ALL UTILITIES LOCATION AND ELEVATION SHOWN SHALL BE CONSIDERED APPROXIMATE ONLY, BEFORE COMMENCING SITE WORK IN ANY AREA, CONTACT "DIG SAFE" AT 1-888-244-7233 AND ALL UTILITY COMPANIES NOT COVERED BY "DIG SAFE". TO ACCURATELY LOCATE UNDERGROUND UTILITIES, ANY DAMAGE TO EXISTING UTILITIES OR STRUCTURES AS SHOWN ON THE PLANS SHALL BE THE CONTRACTOR'S RESPONSIBILITY. COSTS OF SUCH DAMAGE SHALL BE THE CONTRACTOR'S RESPONSIBILITY. NO EXCAVATION SHALL BE DONE UNTIL COMPANIES ARE PROPERLY NOTIFIED IN ADVANCE. NOTE THAT NOT ALL EXISTING UNDERGROUND UTILITIES ARE SHOWN. IT IS THE CONTRACTORS RESPONSIBILITY TO CONTACT ALL RESPECTIVE UTILITY COMPANIES TO VERIFY AND LOCATE EXISTING UTILITIES.
- ALL WORK WITHIN THE RIGHT OF WAY SHALL CONFORM TO TOWN OF RANDOLPH DEPARTMENT OF PUBLIC WORKS REQUIREMENTS, AND MASSACHUSETTS STANDARD SPECIFICATIONS FOR HIGHWAYS AND BRIDGES 1995 EDITION AND THE 2002 EDITION OF THE SUPPLEMENTAL SPECIFICATIONS, OR LATEST REVISIONS TO BOTH.
- PAVEMENT MARKINGS ARE TO BE WATERBORNE AND CONFORM TO THE SPECIFICATIONS.
- PRIOR TO THE PLACEMENT OF THE FINAL COAT OF PAVEMENT, ALL EXISTING PAVEMENT IS TO BE SWEEP CLEAN AND ASPHALT EMULSION TACK COAT IS TO BE APPLIED.
- ALL CURB RAMPS SHALL HAVE DETECTABLE WARNING MATS IN ACCORDANCE WITH MASSACHUSETTS ARCHITECTURAL ACCESS BOARD (MAAB) GUIDELINES. DETECTABLE WARNING PANELS SHALL BE CAST IRON, SEE SPECIFICATION SECTION 32 13 12.
- IN AREAS CALLED OUT AS SIDEWALK FINISHES ARE DETAILED ON THE LANDSCAPE PLANS.
- CONTRACTOR TO INSTALL A VISUAL BARRIER SCREENING COVERING THE CHAIN LINK FENCE WITH A MINIMUM 85% OPACITY. CONTRACTOR TO INSTALL THE SCREENING ACCORDING TO MANUFACTURER'S RECOMMENDATIONS.
- IN ADDITION TO TYPICAL DESIGN STANDARDS, THE CONSTRUCTION GATE/FENCE SUPPORT SYSTEM (POOTS, UPRIGHTS, RODS, RAILS, TIES, FOUNDATIONS, ETC.) SHALL BE DESIGNED FOR A LATERAL WIND PRESSURE WITH THE FENCE ASSUMED TO BE SOLID I.E., WITHOUT PENETRATIONS. CONTRACTOR SHALL SUBMIT CALCULATIONS STAMPED BY A MA REGISTERED PROFESSIONAL ENGINEER DEMONSTRATING THE DESIGN TO BE IN COMPLIANCE WITH ALL LOADS NOTED AND THE STATE BUILDING CODE.
- WORK DEPICTED ON THE CIVIL AND LANDSCAPE PLANS (C-SERIES AND L-SERIES) SHALL BE FURNISHED AND INSTALLED BY THE SITE CONTRACTOR UNLESS OTHERWISE NOTED.

**DEMOLITION NOTES**

- ALL DEMOLITION SHALL BE COORDINATED WITH THE OWNER PRIOR TO START OF WORK.
- PAVEMENT DEMOLITION SHALL BE SAW CUT AND DISPOSED OF PROPERLY. WHERE NEW PAVEMENT ABUTS EXISTING, CONTRACTOR SHALL PROVIDE CLEAN SAW CUT WITH A 2' OVERLAP OF NEW TOP COURSE OVER ADJACENT EXISTING BASE COURSE.
- ALL UTILITIES REMOVED FROM THE SITE SHALL BE REMOVED ALL THE WAY TO THE MAIN LINE, UNLESS OTHERWISE NOTED ON THE PLANS, WITH ANY ASSOCIATED TEES AND FITTINGS REMOVED AND REPLACED WITH A NEW SECTION OF PIPE.
- THE CONTRACTOR SHALL COORDINATE ALL DEMOLITION OF STRUCTURES, PAVEMENT AND CONCRETE MATERIALS, AND UTILITIES WITH APPROPRIATE PROPOSED SITE, GENERAL, AND UTILITY DRAWINGS.
- THE CONTRACTOR SHALL REMOVE ALL UNSUITABLE SOILS IN ACCORDANCE WITH THE RECOMMENDATIONS OF THE GEOTECHNICAL REPORT FOR THE PROPOSED SITE.

**STORMWATER MAINTENANCE**

- PRETREATMENT MAINTENANCE SHOULD BE PERFORMED AT LEAST TWICE A YEAR, AND IDEALLY, SEDIMENT SHOULD BE REMOVED FROM PRETREATMENT BMP'S AFTER EVERY MAJOR STORM. THE SYSTEMS SHOULD BE INSPECTED AFTER THE FIRST SEVERAL RAINFALL EVENTS, AFTER ALL MAJOR STORMS, AND ON REGULAR BI-ANNUAL SCHEDULED DATES IDENTIFIED DEFICIENCIES SHALL BE CORRECTED IMMEDIATELY. THE CONTRACTOR SHALL SUBMIT INSPECTION REPORTS AT LEAST EVERY TWO WEEKS TO TOWN OF RANDOLPH PUBLIC WORKS (VIA E-MAIL, HAND DELIVERED OR FAX).
- PRETREATMENT BMP'S SHOULD BE INSPECTED AND CLEANED DURING THE REGULAR SCHEDULED INSPECTIONS. WATER QUALITY INLETS SHOULD BE CLEARED OF ACCUMULATED SEDIMENT, LEAVES, AND DEBRIS AT EACH REGULAR INSPECTION, AND MORE FREQUENTLY WHERE APPROPRIATE. INLET AND OUTLET PIPES SHOULD BE CHECKED FOR CLOGGING.
- RAIN GARDENS SHOULD BE CLEANED OF TRASH MONTHLY. REMOVE WEED GROWTH FROM MULCHED BEDS AND RIVER STONE AREAS MONTHLY. HERBACEOUS PLANT MATERIAL SPECIFIED FOR THE RAIN GARDEN AREAS SHOULD BE CUT BACK ONCE IN THE LATE FALL OR EARLY SPRING BEFORE NEW GROWTH DEVELOPS. SHRUBS AND TREES SHOULD BE MONITORED TO ENSURE PROPER AND HEALTHY GROWTH. OUTLET STRUCTURES SHALL BE CLEARED OF DEBRIS. ANY EROSION SHOULD BE NOTED. PLANTING BEDS SHOULD HAVE A FRESH LAYER OF MULCH ADDED EACH SPRING.

**SURVEY NOTES**

- INFORMATION SHOWN HEREON IS THE RESULT OF AN ON-THE-GROUND SURVEY PERFORMED BY CHA CONSULTING, INC. IN APRIL OF 2022.
- ALL DEED REFERENCES ARE TO NORFOLK COUNTY REGISTRY OF DEEDS UNLESS OTHERWISE NOTED.
- LOCUS OWNER OF RECORD:

  - RANDOLPH REALTY TRUST II DEED BOOK 2798 PAGE 53 PARCEL ID: 02-B-1-LA
  - RANDOLPH REALTY TRUST I DEED BOOK 27628, PAGE 53 PARCEL ID: 02-B-1-LA

- TOPOGRAPHY, CONTOURS AND BENCHMARKS ARE BASED ON THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88). TEMPORARY BENCHMARKS, REFERENCED TO THE DATUM ARE INDICATED ON THE SURVEY. IN THE EVENT THAT BENCHMARKS (TBMs), ESTABLISHED FOR THIS PROJECT ARE PUBLISHED ON THE SURVEY ARE DESTROYED, NOT RECOVERABLE OR A DISCREPANCY IS FOUND, THE USER SHOULD NOTIFY THIS FIRM IN WRITING PRIOR TO COMMENCING OR CONTINUING ANY WORK.
- THE PROJECT AREA IS LOCATED IN FLOOD ZONES "X" (AREAS OF MINIMAL FLOODING) AS SHOWN ON FLOOD INSURANCE RATE MAP FOR NORFOLK COUNTY, COMMUNITY PLAN NUMBER 502012002404, EFFECTIVE DATE JULY 17, 2012.
- LOCATION OF SUBSURFACE UTILITIES SHOWN HEREON ARE APPROXIMATE AND ADDITIONAL UTILITIES MAY EXIST THAT ARE NOT SHOWN ON THIS PLAN. LOCATIONS ARE COMPILED FROM UTILITY PLANS OF RECORD AND DIG-SAFE FIELD MARKINGS. RIM AND INVERT INFORMATION HAS BEEN COMPILED AND FIELD VERIFIED WHERE POSSIBLE. THIS INFORMATION IS NOT TO BE USED FOR CONSTRUCTION. PRIOR TO ANY CONSTRUCTION, CONTACT DIG-SAFE (811) TO FIELD VERIFY LOCATION OF ALL UTILITIES.
- PLAN REFERENCES:

- LAND COURT PLAN 49215 PLAN BOOK 382 PAGE 570 PLAN BOOK 437 PAGE 117
  - PLAN BOOK 541 PAGE 682 PLAN BOOK 480 PAGE 645 PLAN BOOK 67 PAGE 3227
  - PLAN BOOK 491 PAGE 153 PLAN BOOK 499 PAGE 667 PLAN BOOK 4709 PAGE 407
  - PLAN BOOK 221 PAGE 83 PLAN BOOK 498 PAGE 667 PLAN BOOK 499 PAGE 669
  - PLAN BOOK 699 PAGE 700 PLAN BOOK 4842 PAGE 385 PLAN BOOK 435 PAGE 354
  - PLAN BOOK 230 PAGE 164 PLAN BOOK 204 PAGE 1072-1076 PLAN BOOK 4707 PAGE 50
  - PLAN BOOK 596 PAGE 30 PLAN BOOK 480 PAGE 645 PLAN BOOK 5116 PAGE 585
  - PLAN BOOK 253 PAGE 91 PLAN BOOK 694 PAGE 99
8. THE WORD "CERTIFY" IS UNDERSTOOD TO BE AN EXPRESSION OF PROFESSIONAL OPINION BY THE LAND SURVEYOR WHICH IS BASED ON HIS BEST KNOWLEDGE, INFORMATION AND BELIEF, FORMULATED IN ACCORDANCE WITH COMMONLY ACCEPTED PROCEDURES CONSISTENT WITH APPLICABLE STANDARDS OF PRACTICE, AND AS SUCH IT CONSTITUTES NEITHER A GUARANTEE NOR WARRANTY, EITHER EXPRESS OR IMPLIED. THE CERTIFICATIONS SHOWN ARE NOT CERTIFICATIONS TO THE TITLE OR OWNERSHIP OF THE PROPERTIES.
9. THE LOCUS PARCEL IS LOCATED IN THE TOWN OF RANDOLPH BLUE HILL RIVER HIGHWAY DISTRICT (BRHD) AND RESIDENTIAL SINGLE FAMILY HIGH DENSITY DISTRICT (RSFHD) AS DEFINED BY THE TOWN OF RANDOLPH ZONING MAP.

**EROSION AND SEDIMENTATION CONTROL NOTES**

- SOIL EROSION AND SEDIMENTATION CONTROLS SHALL BE PROVIDED IN ACCORDANCE WITH THE "MASSACHUSETTS SOIL EROSION AND SEDIMENT CONTROL HANDBOOK" THE NPDES GENERAL PERMIT FOR STORMWATER DISCHARGE FROM CONSTRUCTION ACTIVITY AND THE NOTES AND DETAILS SHOWN IN THIS PLAN SET.
- CONTRACTOR SHALL BE RESPONSIBLE FOR FILING THE STORMWATER POLLUTION PREVENTION PLAN AND ANY NECESSARY DOCUMENTS REQUIRED BY THE NPDES GENERAL PERMIT.
- DUST SHALL BE CONTROLLED BY WATERING OR OTHER APPROVED METHODS AS NECESSARY, OR AS DIRECTED BY THE OWNER OR ENGINEER.
- THE CONTRACTOR SHALL SCHEDULE HIS/HER WORK TO ALLOW THE FINISHED SUB GRADE ELEVATIONS TO DRAIN PROPERLY WITHOUT PONDING. SPECIFICALLY, ALLOW WATER TO ESCAPE WHERE PROPOSED CURB MAY RETAIN RUNOFF PRIOR TO APPLICATION OF SURFACE PAVING. PROVIDE TEMPORARY POSITIVE DRAINAGE, AS REQUIRED, TO STABILIZED DISCHARGE POINTS. CONTRACTOR IS RESPONSIBLE FOR ALL TEMPORARY UTILITY CONNECTIONS.
- THE CONTRACTOR SHALL MAINTAIN A SUFFICIENT RESERVE OF VARIOUS EROSION CONTROL MATERIALS ONSITE AT ALL TIMES FOR EMERGENCY PURPOSES.
- ANY DEWATERING WASTE WATERS PUMPED FROM EXCAVATIONS SHALL BE CONVEYED BY HOSE TO AN UPLAND AREA AND DISCHARGED INTO HAYBALE ENCLOSURES OR SEDIMENTATION BAGS OUTSIDE ALL WETLAND AND WETLAND BUFFER AREAS AS REQUIRED.
- CONSTRUCTION SITE WASTE MATERIALS SHALL BE PROPERLY CONTAINED ONSITE AND DISPOSED OFF SITE IN ACCORDANCE WITH ALL APPLICABLE LOCAL AND STATE REGULATIONS.
- ALL DISTURBED OR EXPOSED SOIL SURFACES SHALL BE TEMPORARILY STABILIZED AFTER EACH WORK DAY WITH HAY, STRAW, MULCH OR ANY OTHER PROTECTIVE COVERING AND/OR METHOD APPROVED BY THE U.S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE.
- ALL DRAINAGE STRUCTURES SHALL BE CLEARED OF ACCUMULATED SEDIMENT PRIOR TO ACCEPTANCE OF FINAL PROJECT.
- THE CONTRACTOR SHALL MAINTAIN SURFACE DRAINAGE DURING CONSTRUCTION. STORMWATER SHALL BE MAINTAINED AWAY FROM WORK SITES WHILE PREVENTING EROSION.
- CONTRACTOR IS RESPONSIBLE FOR INSTALLING AND MAINTAINING NECESSARY TEMPORARY EROSION CONTROL MEASURES.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR ESTABLISHING OR INSTALLING ALL TEMPORARY SEDIMENT AND EROSION CONTROLS AS SHOWN ON THESE PLANS AND SHALL MAINTAIN ALL EROSION CONTROL MEASURES AS NECESSARY DURING THE ENTIRE CONSTRUCTION PERIOD.
- TEMPORARY DIVERSION SWALES SHALL BE PROVIDED AS NECESSARY TO DIRECT RUNOFF TO THE SEDIMENT BASINS DURING CONSTRUCTION.
- ANTI-TRACKING PADS AND WHEEL WASH STATIONS SHALL BE PROVIDED AT ALL POINTS OF EGRESS AND INGRESS AND SHALL BE MAINTAINED TO LIMIT TRACKING OR FLOWING OF SEDIMENT ONTO PUBLIC ROADS AND INTO THE REST OF THE SITE.
- EROSION CONTROL BARRIERS SHALL BE INSTALLED AS SHOWN ON THE EROSION CONTROL PLAN PRIOR TO COMMENCEMENT OF CONSTRUCTION OPERATIONS. CONTRACTOR SHALL NOTIFY IN WRITING TOWN OF RANDOLPH PUBLIC WORKS PRIOR TO THE START OF ANY WORK.
- SOIL EROSION AND SEDIMENTATION CONTROL MEASURES SHALL BE INSPECTED AND MAINTAINED ON A WEEKLY BASIS AND AFTER EACH STORM EVENT OF 0.25 INCH OR GREATER DURING CONSTRUCTION TO ENSURE CHANNELS, DITCHES AND PIPES ARE CLEAR OF DEBRIS AND THAT THE EROSION CONTROL BARRIERS ARE INTACT. IDENTIFIED DEFICIENCIES SHALL BE CORRECTED IMMEDIATELY. THE CONTRACTOR SHALL SUBMIT INSPECTION REPORTS AT LEAST EVERY TWO WEEKS TO TOWN OF RANDOLPH PUBLIC WORKS (VIA E-MAIL, HAND DELIVERED OR FAX).
- THE CONTRACTOR SHALL CLEAN AND MAINTAIN EROSION CONTROL BARRIER WHEN SEDIMENT ACCUMULATES TO ONE HALF THE HEIGHT OF THE HAYBALES OR ONE THIRD THE HEIGHT OF SILT FENCE. MATERIAL COLLECTED FROM THE SILTATION BARRIERS SHALL BE REMOVED AS NECESSARY AND DISPOSED IN AN UPLAND AREA.
- INSTALLATION OF THE EROSION CONTROL BARRIERS AS ILLUSTRATED IS INTENDED TO REPRESENT THE MINIMUM SEDIMENTATION CONTROL FACILITIES NECESSARY TO MEET ANTICIPATED SITE CONDITIONS. ADDITIONAL EROSION CONTROL MEASURES SHALL BE IMPLEMENTED AS CONDITIONS WARRANT OR AS DIRECTED BY THE OWNER OR OWNER'S REPRESENTATIVE.
- REQUIRED SEDIMENTATION CONTROL FACILITIES MUST BE PROPERLY ESTABLISHED, CLEARLY VISIBLE AND IN OPERATION PRIOR TO INITIATING ANY LAND CLEARING ACTIVITY AND/OR OTHER CONSTRUCTION RELATED WORK. SUCH FACILITIES SHALL REPRESENT THE LIMIT OF WORK. WORKERS SHALL BE INFORMED THAT NO CONSTRUCTION ACTIVITY IS TO OCUR BEYOND THE LIMIT OF WORK AT ANY TIME THROUGHOUT THE CONSTRUCTION PERIOD.
- CATCH BASINS AND STORM DRAIN INLETS SHALL BE PROTECTED WITH INLET PROTECTION WITHIN LIMITS OF DISTURBANCE.
- THE CONTRACTOR SHALL NOT REMOVE ANY HAYBALES, SILT FENCE OR OTHER EROSION CONTROLS UNTIL THE CONTRIBUTING DRAINAGE AREA HAS BEEN PERMANENTLY STABILIZED.
- RIP-RAP OR OTHER ENERGY DISSIPATORS SHALL BE USED WHERE NECESSARY TO PREVENT SCOUR.
- NO STORAGE OF MATERIAL INCLUDING BUT NOT LIMITED TO COMPOST OR GRASS CLIPPINGS WITHIN 100' WETLAND BUFFER.
- SHOULD ANY EROSION OR SEDIMENTATION CONTROL MEASURES FAIL, IMMEDIATE ATTENTION SHALL BE GIVEN BY THE CONTRACTOR TO CORRECTING THE FAILURE AND TO RECTIFYING ANY ADVERSE IMPACT FROM THE FAILURE. THE COMMISSION AND ENGINEER MUST BE NOTIFIED WITHIN 24 HOURS OF THE FAILURE.

**GRADING AND UTILITY NOTES**

- ALL WORK PERFORMED AND ALL MATERIALS FURNISHED SHALL CONFORM WITH THE LINES AND GRADES ON THE PLANS AND SITE WORK SPECIFICATIONS, UNLESS OTHERWISE DIRECTED.
- AT ALL LOCATIONS WHERE EXISTING CURBING OR PAVEMENT ABUT NEW CONSTRUCTION, THE EDGE OF THE EXISTING CURB OR PAVEMENT SHALL BE SAW CUT TO A CLEAN, SMOOTH EDGE. BLEND NEW PAVEMENT AND CURBS SMOOTHLY INTO EXISTING BY MATCHING LINES, GRADES AND JOINTS.
- ALL EXISTING AND PROPOSED UTILITY COVERS, GRATES, ETC. SHALL BE ADJUSTED TO BE FLUSH WITH THE SURROUNDING SURFACE OR PAVEMENT FINISH GRADE OF THIS CONTRACT. RIM ELEVATIONS OF STRUCTURES AND MANHOLES ARE APPROXIMATE. FINAL ELEVATIONS ARE TO BE SET FLUSH AND CONSISTENT WITH THE PROPOSED FINAL GRADES.
- THE CONTRACTOR SHALL MAKE ALL ARRANGEMENTS FOR THE ALTERATION OF PRIVATE UTILITIES BY THE UTILITY COMPANIES, AS REQUIRED.
- WHERE AN EXISTING UTILITY IS FOUND TO CONFLICT WITH THE PROPOSED WORK, THE LOCATION, ELEVATION AND SIZE OF THE UTILITY SHALL BE ACCURATELY DETERMINED WITHOUT DELAY BY THE CONTRACTOR AND THE INFORMATION FURNISHED TO THE ENGINEER, AND TOWN OF RANDOLPH PUBLIC WORKS OR THEIR AGENT.
- THE CONTRACTOR SHALL PROTECT ALL UNDERGROUND DRAINAGE, SEWER AND UTILITY FACILITIES FROM EXCESSIVE VEHICULAR LOADS DURING CONSTRUCTION. ANY DAMAGE TO THESE FACILITIES RESULTING FROM CONSTRUCTION LOADS WILL BE RESTORED TO ORIGINAL CONDITION AT NO COST TO THE OWNER.
- DURING CONSTRUCTION OPERATIONS, THE CONTRACTOR SHALL PROTECT EXISTING UTILITIES BY PROVIDING TEMPORARY SUPPORTS OR SHEETING AS REQUIRED AT NO ADDITIONAL COST TO THE OWNER.
- EXCAVATION REQUIRED WITHIN THE PROXIMITY OF EXISTING UTILITY LINES SHALL BE DONE BY HAND. CONTRACTOR SHALL REPAIR ANY DAMAGE TO EXISTING UTILITY LINES OR STRUCTURES INCURRED DURING CONSTRUCTION OPERATIONS AT NO COST TO THE OWNER.
- PITCH EVENLY BETWEEN SPOT GRADES. ALL PAVED AREAS MUST PITCH TO DRAIN AT A MIN. OF 1/8" PER FOOT UNLESS SPECIFIED.
- CONTRACTOR SHALL BE RESPONSIBLE FOR SUBMITTING THE MASSACHUSETTS DEPARTMENT OF ENVIRONMENTAL PROTECTION SEWER EXTENSION/CONNECTION COMPLIANCE CERTIFICATION WITHIN SIXTY (60) DAYS OF THE SEWER INSTALLATION.
- SITE GRADES SHALL CONFORM WITH ADA AND MAAB REQUIREMENTS.
- ALL TRANSITIONS BETWEEN GROUND COVERING MATERIALS SHALL BE SMOOTH AND MEET 521 CMR 20.10 REQUIREMENTS.
- ALL PLUMBING/MECHANICAL UTILITIES WITHIN 10 FEET OF THE BUILDING ARE SHOWN ON THE PLUMBING/MECHANICAL PLANS.
- CONTRACTOR IS REQUIRED TO APPLY FOR, OBTAIN, AND PAY ALL FEES ASSOCIATED WITH CONSTRUCTION PHASE PERMITS. PERMITS MAY INCLUDE, BUT NOT LIMITED TO:
  - NPDES CONSTRUCTION GENERAL PERMIT
  - TOWN OF RANDOLPH STREET OPENING PERMIT

**LAYOUT NOTES**

- ALL LINES ARE PERPENDICULAR OR PARALLEL TO THE LINES FROM WHICH THEY ARE MEASURED UNLESS OTHERWISE INDICATED.
- DIMENSIONS OF PARKING SPACES AND DRIVEWAYS ARE FROM FACE OF CURB TO FACE OF CURB UNLESS OTHERWISE NOTED.
- ACCESSIBLE RAMPS SHALL BE PER THE (ADA) ACCESSIBILITY AND (MAAB) GUIDELINES AND INCLUDE DETECTABLE WARNING MATS. DETECTABLE WARNING PANELS SHALL BE CAST IRON, SEE SPECIFICATION SECTION 32 13 12.

**EXISTING LEGEND**

- LOCUS PROPERTY LINE
- INTERNAL PROPERTY LINE
- ABUTTER PROPERTY LINE
- EASEMENT LINE
- ZONING
- INDEX CONTOUR
- INTERMEDIATE CONTOUR
- SPOT ELEVATION
- WATER LINE
- EDGE OF WOODS
- EDGE OF SCRUB BRUSH
- STONEWALL
- FENCE
- GUARDRAIL
- UNDERGROUND SEWER LINE
- UNDERGROUND DRAIN LINE
- UNDERGROUND WATER LINE
- UNDERGROUND GAS LINE
- UNDERGROUND ELECTRIC LINE
- OVER HEAD WIRE
- WETLAND LINE
- ROAD/PARKING STRIPES
- CONCRETE
- BUILDING
- EDGE OF PAVEMENT
- CURB LINE
- ZONING LINE
- FEMA LINE
- 100 FT. WETLAND BUFFER
- WETLAND EDGE
- DRILL HOLE
- CONCRETE BOUND WITH DRILL HOLE
- STONE BOUND WITH DRILL HOLE
- UNKNOWN MANHOLE
- ELECTRIC MANHOLE
- ELECTRIC CONDUIT
- ELECTRIC HAND HOLE
- UTILITY POLE
- LIGHT POLE
- GUY WIRE
- TELEPHONE/CABLE MANHOLE
- TELEPHONE/CABLE HAND HOLE
- TELEPHONE/CABLE PEDESTAL
- GAS VALVE
- GAS METER
- SEWER MANHOLE
- DRAIN MANHOLE
- CATCH BASIN
- TOP OF HOOD
- TOP OF WATER
- INVERT
- VENT
- HYDRANT
- WATER VALVE
- WATER SHUT OFF
- WELL
- IRRIGATION CONTROL VALVE
- AIR CONDITIONER AND AG HEATING
- SIGN
- CONIFEROUS TREE
- DECIDUOUS TREE
- SHRUB
- WETLAND FLAG
- BOLLARD
- TEST PIT
- TEST BORING
- FLAG POLE
- ROCK
- EOP
- EDGE OF PAVEMENT
- CCB
- CAPE COD BERM
- GC
- SLOPE GRANITE CURB
- XW
- CROSS WALL
- CRW
- CONCRETE HEADWALL
- WDF
- WOOD FENCE
- CLF
- CHAIN LINK FENCE
- PRF
- POST & RAIL FENCE
- MHR
- METAL HANDRAIL
- HCPR
- HANDI-CAP RAMP
- CCP
- CONCRETE PAD
- M
- METAL
- WGR
- WOOD GUARDRAIL
- UBB
- UPPER BONNET BOLT
- ADA
- AMERICANS WITH DISABILITIES ACT
- MAAB
- MASSACHUSETTS ARCHITECTURAL ACCESS BOARD
- BMPS
- BEST MANAGEMENT PRACTICES

**PROPOSED LEGEND**

- CURBING(TYPE)
- EDGE OF PAVEMENT
- RETAINING WALL
- INTERMEDIATE CONTOUR
- INDEX CONTOUR
- SPOT ELEVATION
- W
- S
- D
- G
- DR
- CB
- HS
- AD / YD
- O
- SMH
- WG
- SF
- LO

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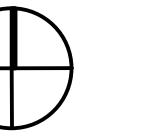
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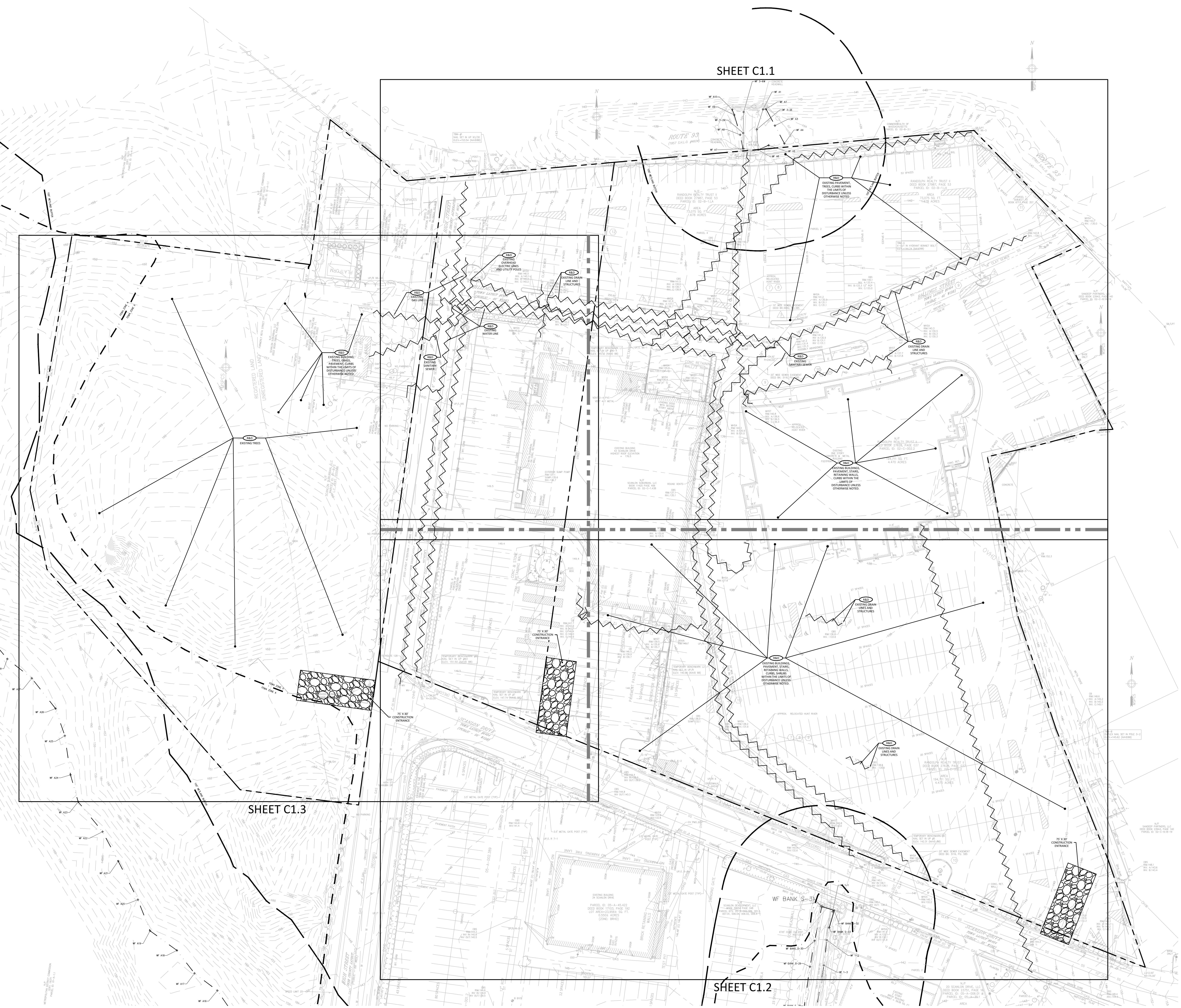
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Project No. 78000  
GENERAL NOTES AND  
LEGEND

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SCALE: 1" = 40'

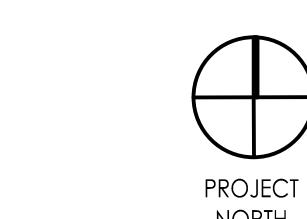
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# OVERALL EXISTING CONDITIONS AND DEMOLITION PLAN

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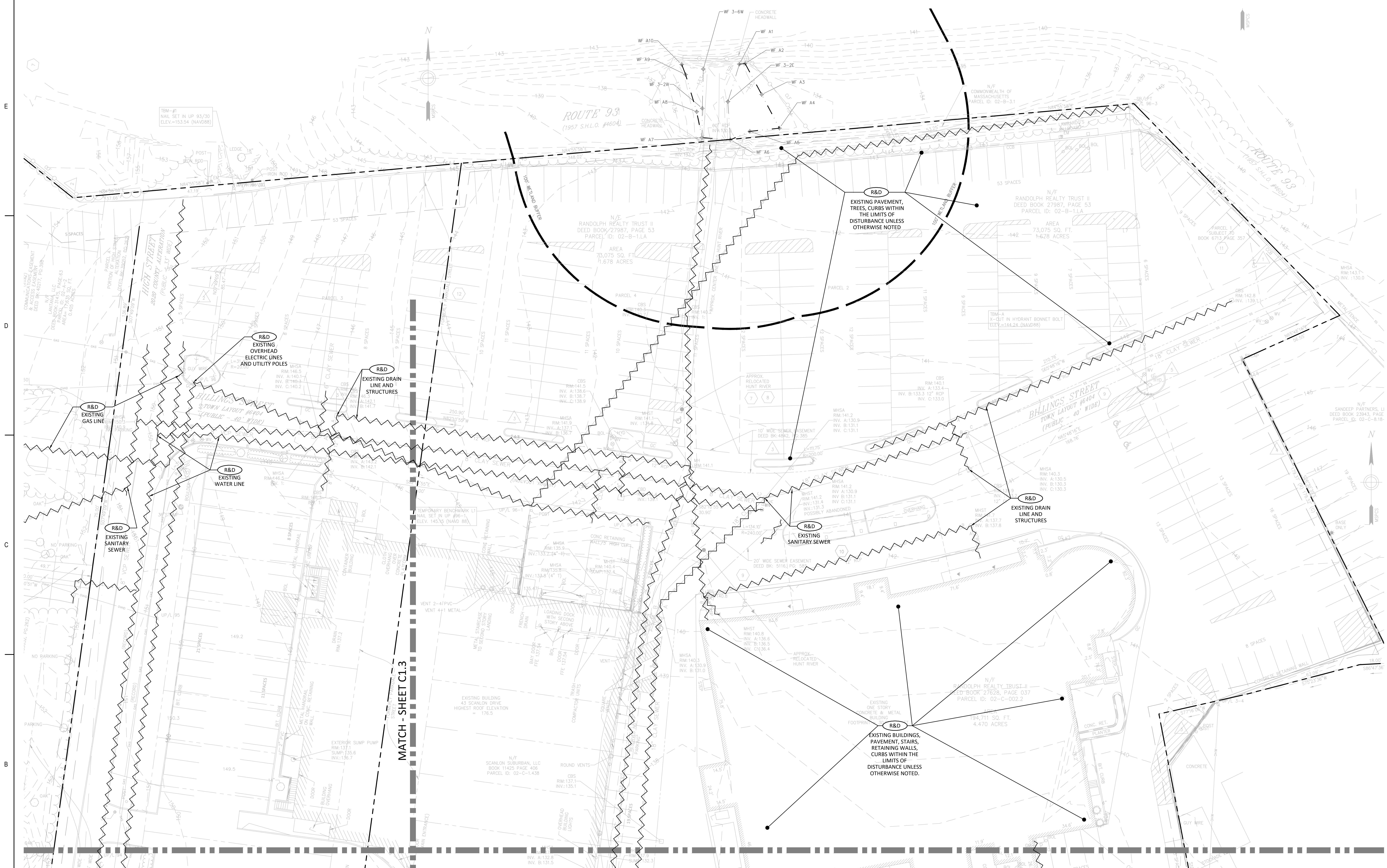


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| 2 DESIGN DEVELOPMENT | 2023.7.15 |
| SCHEMATIC DESIGN     | 2023.7.10 |
| Issued/Revision      | YYYYMMDD  |

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NOT FOR  
CONSTRUCTION**

Scale AS NOTED  
 Project No. 78000  
**EXISTING CONDITIONS  
AND DEMOLITION  
PLAN 1**

**C1.1**



- NOTES:**
- EXISTING UTILITY INFORMATION SHOWN HEREON IS BASED UPON PREVIOUS DESIGN DRAWINGS AND RECORD INFORMATION. LOCATIONS, SIZES, AND DEPTHS OF UTILITIES HAVE NOT BEEN SURVEYED IN THE FIELD. ADDITIONAL SITE SURVEY IS ONGOING.
  - DEMOLITION OF EXISTING BUILDING AND SITE FEATURES SHOWN ON SHEETS C1.1 THROUGH C1.3 ARE INCLUSIVE OF ALL PHASES. PROPOSED DEMOLITION ACTIVITIES SHOWN ON THESE SHEETS ARE NOT INTENDED TO INDICATE THE PHASE IN WHICH THEY OCCUR. SEE PHASING DRAWINGS FOR DEMOLITION SPECIFIC TO PHASING.
  - THE EROSION AND SEDIMENTATION CONTROLS SHOWN ON THE PLANS ARE INTENDED TO REPRESENT THE MINIMUM CONTROLS NECESSARY TO MEET ANTICIPATED SITE CONDITIONS. ADDITIONAL MEASURES SHALL BE IMPLEMENTED AS CONDITIONS WARRANT OR AS DIRECTED BY THE OWNER OR OWNER'S REPRESENTATIVE.
  - INSTALL EROSION CONTROLS DOWNSTREAM OF ANY DISTURBED AREAS TO REDUCE POTENTIAL FOR EROSION. CONTRACTOR SHALL INDICATE LOCATIONS OF EROSION CONTROLS FOR REVIEW WITH GENERAL CONTRACTOR AND OWNER'S REPRESENTATIVE PRIOR TO COMMENCING DISTURBANCE. THE DEMOLITION IS PROPOSED TO BE CONDUCTED IN PHASES. EROSION CONTROLS SHALL BE RELOCATED AS NECESSARY DURING EACH PHASE.
  - INSTALL CHAIN LINK FENCE TREE PROTECTION DETAIL AT THE LOCATIONS SHOWN ON THE PLAN TO PROTECT EXISTING TREES SPECIFICALLY INDICATED ON THE PLAN. LAYOUT OF FENCE SHALL BE REVIEWED AND APPROVED BY THE LANDSCAPE ARCHITECT. TREE PROTECTION SHALL BE MAINTAINED THROUGHOUT ALL PHASES OF CONSTRUCTION.
  - ALL EXISTING DRAINAGE AND SEWER SHALL BE MAINTAINED OR REROUTED AS NECESSARY UNTIL PERMANENT PIPING IS INSTALLED.
  - ELECTRICAL DEMOLITION IS SHOWN FOR INFORMATION ONLY. REFER TO ELECTRICAL PLANS FOR COMPLETE EXTENT OF ELECTRICAL DEMOLITION.
  - PROVIDE INLET PROTECTION AT ALL EXISTING DRAINAGE INLETS.
  - ALL ITEMS TO BE REMOVED AND STOCKPILED SHALL BE COORDINATED WITH OWNER FOR STOCKPILE LOCATIONS. AT THIS TIME, THE OWNER HAS NOT IDENTIFIED ITEMS FOR STOCKPILE.
  - ALL ITEMS MARKED FOR RE-USE SHALL BE STOCKPILED ONSITE, PROTECTED AND RE-INSTALLED AS SHOWN ON THE LANDSCAPE PLANS.

- DRAINAGE FEATURES AND UTILITIES TO BE MAINTAINED UNLESS OTHERWISE NOTED.
- TOTAL AREA OF DISTURBANCE: 13.18 ACRES.
- CONTRACTOR TO REESTABLISH BENCHMARKS IN ALTERNATE LOCATION PRIOR TO CONSTRUCTION.
- CONTRACTOR SHALL COORDINATE CLEARING OF ALL ABUTTER ENCROACHMENTS WITH THE OWNER PRIOR TO CONSTRUCTION. IT IS NOT EXPECTED THAT ENCROACHMENTS WILL BE ENCOUNTERED ON THIS SITE.
- INSTALL CONSTRUCTION ENTRANCE AT ALL ENTRY/EXIT POINT FOR VEHICULAR TRAFFIC FOR EACH PHASE OF THE PROJECT. LOCATION TO BE DETERMINED BY PHASING. IT SHALL BE ASSUMED THAT TWO (2) WILL BE NECESSARY THROUGHOUT CONSTRUCTION.
- ALL EARTH DISTURBANCE SHALL BE CONDUCTED IN ACCORDANCE WITH THE PROJECT SPECIFICATIONS.
- ACTIVE UTILITY LINES (INCLUDING SEWER, WATER, AND DRAINAGE). CONTRACTOR SHALL PROVIDE 1 WEEK NOTIFICATION FOR ANY POSSIBLE DISRUPTION OF SERVICE TO OWNER, OWNER'S PROJECT MANAGER AND ARCHITECT; PROVIDE NOTIFICATION FOR CONNECTING, DISCONNECTING, TURNING ON OR TURNING OFF ANY SERVICE WHICH MAY AFFECT OWNER'S OPERATIONS.
- CONTRACTOR SHALL PROVIDE 72 HOUR (3 WORKING DAYS) NOTICE TO LOCAL FIRE DEPARTMENT OF DISRUPTIONS.
- DISTURBANCE ON ACTIVE GAS LINES SHALL BE COORDINATED WITH UTILITY PROVIDER.
- THE CONTRACTOR SHALL CONFIRM LOCATION AND ELEVATION OF THE EXISTING DRAINAGE MANHOLES AND PIPES INDICATED. IT SHALL BE ASSUMED THAT AN ADDITIONAL 6' OF PIPE WILL NEED TO BE REMOVED AND DISPOSED.
- ANY UNFORESEEN UNDERGROUND TRANSIT PIPE OR OTHER UNFORESEEN HAZARDOUS MATERIAL SHALL BE ABATED IN ACCORDANCE WITH THE SPECIFICATIONS AND ALL LOCAL, STATE AND FEDERAL REGULATIONS.
- CONTRACTOR SHALL COMPLY WITH ALL LEED REQUIREMENTS FOR DEMOLITION.
- ALL EXISTING MANHOLES OR CATCH BASINS TO REMAIN SHALL BE ADJUSTED TO FINISHED GRADE ELEVATION.

- ALL EXISTING UTILITIES WITHIN TREE PROTECTION AREAS NOT SCHEDULED FOR RE-USE SHALL BE CUT, CAPPED, AND ABANDONED IN PLACE.
- DEMOLITION WORK SHOWN ON THIS SHEET IS INDEPENDENT OF PROJECT PHASING OR SEQUENCING. CONTRACTOR SHALL BE RESPONSIBLE FOR SEQUENCING ALL WORK AS OUTLINED IN THE PROJECT SPECIFICATIONS.
- CONTRACTOR SHALL SCHEDULE PRECONSTRUCTION MEETING WITH ARCHITECT, LANDSCAPE ARCHITECT, CIVIL ENGINEER, STRUCTURAL ENGINEER, AND OWNER'S REPRESENTATIVE PRIOR TO DEMOLITION OF EXISTING SERVICE AREA TO CONFIRM EXTENT OF DEMOLITION AND SAWCUT LOCATIONS.
- PERIMETER EROSION CONTROL SHALL BE PROVIDED.

0' 20' 40' 60'  
SCALE: 1" = 20'



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MATCH - SHEET C

NOTES

1. EXISTING UTILITY INFORMATION SHOWN HEREON IS BASED UPON PREVIOUS DESIGN DRAWINGS AND RECORD INFORMATION. LOCATIONS, SIZES, AND DEPTHS OF UTILITIES HAVE NOT BEEN SURVEYED IN THE FIELD. ADDITIONAL SITE SURVEY IS ONGOING.
  2. DEMOLITION OF EXISTING BUILDING AND SITE FEATURES SHOWN ON SHEETS C1.1 THROUGH C1.3 ARE INCLUSIVE OF ALL PHASES. PROPOSED DEMOLITION ACTIVITIES SHOWN ON THESE SHEETS ARE NOT INTENDED TO INDICATE THE PHASE IN WHICH THEY OCCUR. SEE PHASING DRAWINGS FOR DEMOLITION SPECIFIC TO PHASING.
  3. THE EROSION AND SEDIMENTATION CONTROLS SHOWN ON THE PLANS ARE INTENDED TO REPRESENT THE MINIMUM CONTROLS NECESSARY TO MEET ANTICIPATED SITE CONDITIONS. ADDITIONAL MEASURES SHALL BE IMPLEMENTED AS CONDITIONS WARRANT OR AS DIRECTED BY THE OWNER OR OWNER'S REPRESENTATIVE.
  4. INSTALL EROSION CONTROLS DOWNSTREAM OF ANY DISTURBED AREAS TO REDUCE POTENTIAL FOR EROSION. CONTRACTOR SHALL INDICATE LOCATIONS OF EROSION CONTROLS FOR REVIEW WITH GENERAL CONTRACTOR AND OWNER'S REPRESENTATIVE PRIOR TO COMMENCING DISTURBANCE. THE DEMOLITION IS PROPOSED TO BE CONDUCTED IN PHASES. EROSION CONTROLS SHALL BE RELOCATED AS NECESSARY DURING EACH PHASE.
  5. INSTALL CHAIN LINK FENCE TREE PROTECTION PER DETAIL AT THE LOCATIONS SHOWN ON THE PLAN TO PROTECT EXISTING TREES SPECIFICALLY INDICATED ON THE PLAN. LAYOUT OF FENCE SHALL BE REVIEWED AND APPROVED BY THE LANDSCAPE ARCHITECT. TREE PROTECTION SHALL BE MAINTAINED THROUGHOUT ALL PHASES OF CONSTRUCTION.
  6. ALL EXISTING DRAINAGE AND SEWER SHALL BE MAINTAINED OR REROUTED AS NECESSARY UNTIL PERMANENT PIPING IS INSTALLED.
  7. ELECTRICAL DEMOLITION IS SHOWN FOR INFORMATION ONLY. REFER TO ELECTRICAL PLANS FOR COMPLETE EXTENT OF ELECTRICAL DEMOLITION.
  8. PROVIDE INLET PROTECTION AT ALL EXISTING DRAINAGE INLETS.
  9. ALL ITEMS TO BE REMOVED AND STOCKPILED SHALL BE COORDINATED WITH OWNER FOR STOCKPILE LOCATIONS. AT THIS TIME, THE OWNER HAS NOT IDENTIFIED ITEMS FOR STOCKPILE.
  10. ALL ITEMS MARKED FOR RE-USE SHALL BE STOCKPILED ONSITE, PROTECTED AND RE-INSTALLED AS SHOWN ON THE LANDSCAPE PLANS.
  11. DRAINAGE FEATURES AND UTILITIES TO BE MAINTAINED UNLESS OTHERWISE NOTED.
  12. TOTAL AREA OF DISTURBANCE: 13.18 ACRES.
  13. CONTRACTOR TO REESTABLISH BENCHMARKS IN ALTERNATE LOCATION PRIOR TO CONSTRUCTION.
  14. CONTRACTOR SHALL COORDINATE CLEARING OF ALL ABUTTER ENCROACHMENTS WITH THE OWNER PRIOR TO CONSTRUCTION. IT IS NOT EXPECTED THAT ENCROACHMENTS WILL BE ENCOUNTERED ON THIS SITE.
  15. INSTALL CONSTRUCTION ENTRANCE AT ALL ENTRY/EXIT POINT FOR VEHICULAR TRAFFIC FOR EACH PHASE OF THE PROJECT. LOCATION TO DETERMINED BY PHASING. IT SHALL BE ASSUMED THAT TWO (2) WILL BE NECESSARY THROUGHOUT CONSTRUCTION.
  16. ALL EARTH DISTURBANCE SHALL BE CONDUCTED IN ACCORDANCE WITH THE PROJECT SPECIFICATIONS.
  17. ACTIVE UTILITY LINES (INCLUDING SEWER, WATER, AND DRAINAGE), CONTRACTOR SHALL PROVIDE 1 WEEK NOTIFICATION FOR ANY POSSIBLE DISRUPTION OF SERVICE TO OWNER, OWNER'S PROJECT MANAGER AND ARCHITECT; PROVIDE NOTIFICATION FOR CONNECTING, DISCONNECTING, TURNING ON OR TURNING OFF ANY SERVICE WHICH MAY AFFECT OWNER'S OPERATIONS.
  18. CONTRACTOR SHALL PROVIDE 72 HOUR (3 WORKING DAYS) NOTICE TO LOCAL FIRE DEPARTMENT OF DISRUPTIONS.
  19. DISTURBANCE ON ACTIVE GAS LINES SHALL BE COORDINATED WITH UTILITY PROVIDER.
  20. THE CONTRACTOR SHALL CONFIRM LOCATION AND ELEVATION OF THE EXISTING DRAINAGE MANHOLES AND PIPES INDICATED. IT SHALL BE ASSUMED THAT AN ADDITIONAL 60 FEET OF PIPE WILL NEED TO BE REMOVED AND DISPOSED.
  21. ANY UNFORESEEN UNDERGROUND TRANSIT PIPE OR OTHER UNFORESEEN HAZARDOUS MATERIAL SHALL BE ABATED IN ACCORDANCE WITH SPECIFICATIONS AND ALL LOCAL, STATE AND FEDERAL REGULATIONS.
  22. CONTRACTOR SHALL COMPLY WITH ALL LEED REQUIREMENTS FOR DEMOLITION.
  23. ALL EXISTING MANHOLES OR CATCH BASINS TO REMAIN SHALL BE ADJUSTED TO FINISHED GRADE ELEVATION.

24. ALL EXISTING UTILITIES WITHIN TREE PROTECTION AREAS NOT SCHEDULED FOR RE-USE SHALL BE CUT, CAPPED, AND ABANDONED IN PLACE.

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  25. DEMOLITION WORK SHOWN ON THIS SHEET IS INDEPENDENT OF PROJECT PHASING OR SEQUENCING. CONTRACTOR SHALL BE RESPONSIBLE FOR SEQUENCING ALL WORK AS OUTLINED IN THE PROJECT SPECIFICATIONS.
  26. CONTRACTOR SHALL SCHEDULE PRECONSTRUCTION MEETING WITH ARCHITECT, LANDSCAPE ARCHITECT, CIVIL ENGINEER, STRUCTURAL ENGINEER, AND OWNER'S REPRESENTATIVE PRIOR TO DEMOLITION OF EXISTING SERVICE AREA TO CONFIRM EXTENT OF DEMOLITION AND SAWCUT LOCATIONS.
  27. PERIMETER EROSION CONTROL SHALL BE PROVIDED.

# **PRELIMINARY NOT FOR CONSTRUCTION**

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| <b>EXISTING CONDITIONS<br/>AND DEMOLITION<br/>PLAN ?</b> |          |

# C1.2



## NOTES:

1. EXISTING UTILITIES SHOWN HEREON IS BASED UPON PREVIOUS DESIGN DRAWINGS AND RECORD INFORMATION. LOCATIONS, SIZES, AND DEPTHS OF UTILITIES HAVE NOT BEEN SURVEYED IN THE FIELD. ADDITIONAL SITE SURVEY IS ONGOING.

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3. THE EROSION AND SEDIMENTATION CONTROLS SHOWN ON THE PLANS ARE INTENDED TO REPRESENT THE MINIMUM CONTROLS NECESSARY TO MEET ANTICIPATED SITE CONDITIONS. ADDITIONAL MEASURES SHALL BE IMPLEMENTED AS CONDITIONS WARRANT OR AS DIRECTED BY THE OWNER OR OWNER'S REPRESENTATIVE.

4. INSTALL EROSION CONTROLS DOWNSTREAM OF ANY DISTURBED AREAS TO REDUCE POTENTIAL FOR EROSION CONSTRUCTION. INDICATE LOCATION OF EROSION CONTROLS AGREED WITH GENERAL CONTRACTOR AND OWNER'S REPRESENTATIVE PRIOR TO COMMENCING DISTURBANCE. THE DEMOLITION IS PROPOSED TO BE CONDUCTED IN PHASES. EROSION CONTROLS SHALL BE RELOCATED AS NECESSARY DURING EACH PHASE.

5. INSTALL CHAIN LINK FENCE TREE PROTECTION PER DETAIL AT THE LOCATIONS SHOWN ON THE PLAN TO PROTECT EXISTING TREES SPECIFICALLY INDICATED ON THE PLAN. LAYOUT OF FENCE SHALL BE REVIEWED AND APPROVED BY THE LANDSCAPE ARCHITECT. TREE PROTECTION SHALL BE MAINTAINED THROUGHOUT ALL PHASES OF CONSTRUCTION.

6. ALL EXISTING DRAINAGE AND SEWER SHALL BE MAINTAINED OR REROUTED AS NECESSARY UNTIL PERMANENT PIPING IS INSTALLED.

7. ELECTRICAL DEMOLITION IS SHOWN FOR INFORMATION ONLY. REFER TO ELECTRICAL PLANS FOR COMPLETE EXTENT OF ELECTRICAL DEMOLITION.

8. PROVIDE INLET PROTECTION AT ALL EXISTING DRAINAGE INLETS.

9. ALL ITEMS TO BE REMOVED AND STOCKPILED SHALL BE COORDINATED WITH OWNER FOR STOCKPILE LOCATIONS. AT THIS TIME, THE OWNER HAS NOT IDENTIFIED ITEMS FOR STOCKPILE.

10. ALL ITEMS MARKED FOR RE-USE SHALL BE STOCKPILED ON SITE, PROTECTED AND RE-INSTALLED AS SHOWN ON THE LANDSCAPE PLANS.

11. DRAINAGE FEATURES AND UTILITIES TO BE MAINTAINED UNLESS OTHERWISE NOTED.

12. TOTAL AREA OF DISTURBANCE: 13.18 ACRES.

13. CONTRACTOR TO REESTABLISH BENCHMARKS IN ALTERNATE LOCATION PRIOR TO CONSTRUCTION.

14. CONTRACTOR SHALL COORDINATE CLEARING OF ALL ABUTTER ENCROACHMENTS WITH THE OWNER PRIOR TO CONSTRUCTION. IT IS NOT EXPECTED THAT ENCROACHMENTS WILL BE ENCOUNTERED ON THIS SITE.

15. INSTALL CONSTRUCTION ENTRANCE AT ALL ENTRY/EXIT POINT FOR VEHICULAR TRAFFIC FOR EACH PHASE OF THE PROJECT. LOCATION TO BE DETERMINED BY PHASING. IT SHALL BE ASSUMED THAT TWO (2) WILL BE NECESSARY THROUGHOUT CONSTRUCTION.

16. ALL EARTH DISTURBANCE SHALL BE CONDUCTED IN ACCORDANCE WITH THE PROJECT SPECIFICATIONS.

17. ACTIVE UTILITY LINES (INCLUDING SEWER, WATER, AND DRAINAGE), CONTRACTOR SHALL PROVIDE 1 WEEK NOTIFICATION FOR ANY POSSIBLE DISRUPTION OF SERVICE TO OWNER, OWNER'S PROJECT MANAGER AND ARCHITECT; PROVIDE NOTIFICATION FOR CONNECTING, DISCONNECTING, TURNING ON OR TURNING OFF ANY SERVICE WHICH MAY AFFECT OWNER'S OPERATIONS.

18. CONTRACTOR SHALL PROVIDE 72 HOUR (3 WORKING DAYS) NOTICE TO LOCAL FIRE DEPARTMENT OF DISRUPTIONS.

19. DISTURBANCE ON ACTIVE GAS LINES SHALL BE COORDINATED WITH UTILITY PROVIDER.

20. THE CONTRACTOR SHALL CONFIRM LOCATION AND ELEVATION OF THE EXISTING DRAINAGE MANHOLES AND PIPES INDICATED. IT SHALL BE ASSUMED THAT AN ADDITIONAL 60 FEET OF PIPE WILL NEED TO BE REMOVED AND DISPOSED.

21. ANY UNFORESEEN UNDERGROUND TRANSIT PIPE OR OTHER UNFORESEEN HAZARDOUS MATERIAL SHALL BE ABATED IN ACCORDANCE WITH THE SPECIFICATIONS AND ALL LOCAL, STATE AND FEDERAL REGULATIONS.

22. CONTRACTOR SHALL COMPLY WITH ALL LEED REQUIREMENTS FOR DEMOLITION.

23. ALL EXISTING MANHOLES OR CATCH BASINS TO REMAIN SHALL BE ADJUSTED TO FINISHED GRADE ELEVATION.

24. ALL EXISTING UTILITIES WITHIN TREE PROTECTION AREAS NOT SCHEDULED FOR RE-USE SHALL BE CUT, CAPPED, AND ABANDONED IN PLACE.

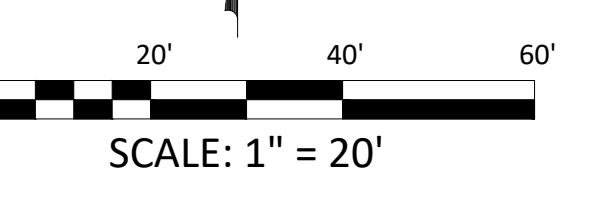
25. DEMOLITION WORK SHOWN ON THIS SHEET IS INDEPENDENT OF PROJECT PHASING OR SEQUENCING. CONTRACTOR SHALL BE RESPONSIBLE FOR SEQUENCING ALL WORK AS OUTLINED IN THE PROJECT SPECIFICATIONS.

26. CONTRACTOR SHALL SCHEDULE PRECONSTRUCTION MEETING WITH ARCHITECT, LANDSCAPE ARCHITECT, CIVIL ENGINEER, STRUCTURAL ENGINEER, AND OWNER'S REPRESENTATIVE PRIOR TO DEMOLITION OF EXISTING SERVICE AREA TO CONFIRM EXTENT OF DEMOLITION AND SAWCUT LOCATIONS.

27. PERIMETER EROSION CONTROL SHALL BE PROVIDED.

MATCH - SHEET C1.1

MATCH - SHEET C1.2

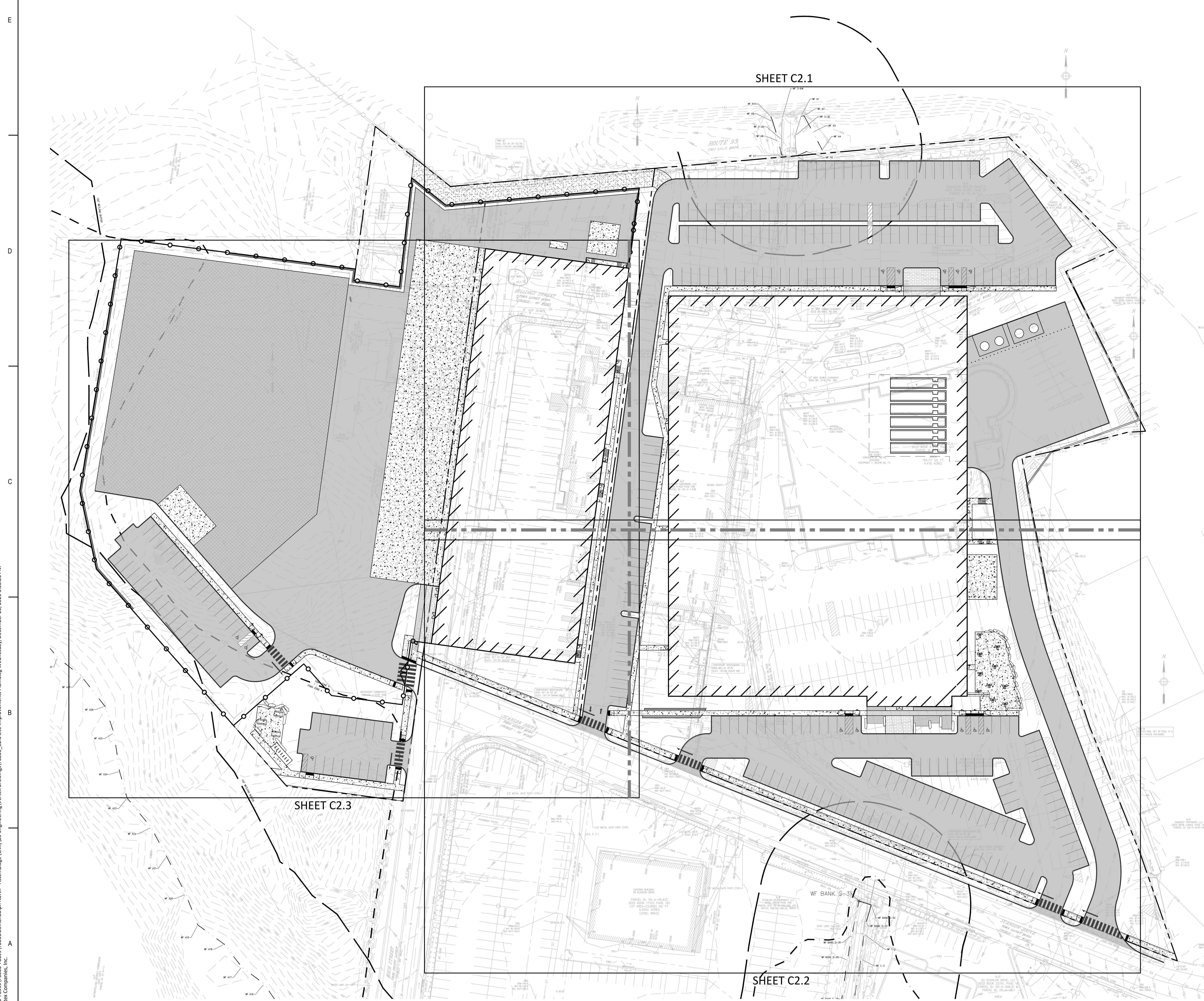


SCALE: 1" = 20'

**PRELIMINARY  
NOT FOR  
CONSTRUCTION**

Scale AS NOTED  
Project No. 78000  
**EXISTING CONDITIONS  
AND DEMOLITION  
PLAN 3**

**C1.3**



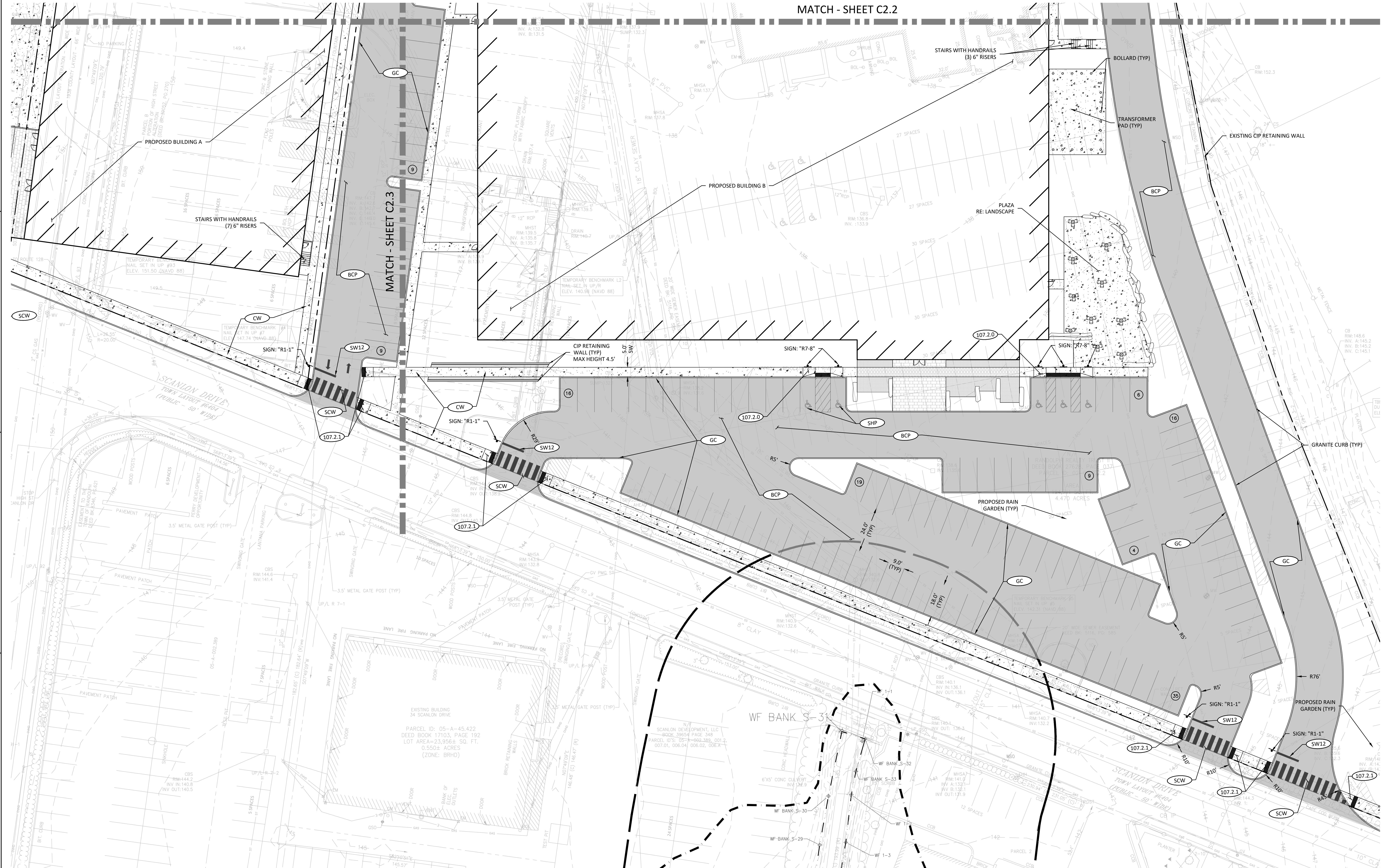




6

Digit/Seal

## MATCH - SHEET C2.2

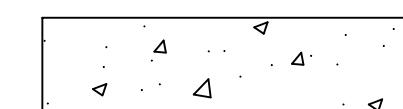


## NOTES:

1. EROSION CONTROL MEASURES SHALL BE IMPLEMENTED FOR THE DURATION OF CONSTRUCTION. AT A MINIMUM, PERIMETER HAY BALES, VEHICLE TRACKING CONTROL, INLET PROTECTION, CONCRETE WASHOUT AREAS AND TEMPORARY SEDIMENTATION BASINS SHOULD BE CONSIDERED
  2. GRANITE CURB SHALL BE PROVIDED IN ALL PARKING AREAS AT THE EDGE OF THE PAVEMENT AND ADJACENT TO SIDEWALKS
  3. CURB, BERM, AND WALKWAY RADII SHALL BE 2 FEET UNLESS NOTED ON PLANS.
  4. WHERE SIDEWALKS INTERSECT CURB LINES, ADA, MAAB COMPLIANT CURB RAMP WITH DETECTABLE WARNING MAT SHALL BE INSTALLED. DETECTABLE WARNING PANELS SHALL BE CAST IRON, SEE SPECIFICATION SECTION 32 13 12.
  5. CURB & GUTTER RELATED DIMENSIONS ARE TO FLOWLINE UNLESS OTHERWISE NOTED.
  6. ALL PAVEMENT MARKINGS ONSITE SHALL BE WATERBOURNE, CONFORMING TO MASSACHUSETTS STANDARD SPECIFICATIONS.
  7. CONCRETE WALKWAY MATERIALS SHOWN FOR CLARITY ONLY. REFER TO LANDSCAPE PLANS FOR ALL WALKWAY MATERIALS, FINISHES, AND SCORING.



**HEAVY-DUTY BITUMINOUS CONCRETE PAVEMENT**  
1.5" FINISH COURSE OVER  
2" BINDER COURSE OVER  
8.5' PROCESSED GRAVEL OVER  
12" COMPACTED SUBGRADE



## SIDEWALK CONCRETE RE: LANDSCAPE FOR CONCRETE



POROUS PAVEMENT  
RE: SITE DETAILS

This architectural elevation drawing depicts a classical column, likely a Corinthian, characterized by its flared base and ornate capital featuring acanthus leaves and volutes. The column is shown in perspective, leaning slightly to the left. A vertical scale bar at the bottom indicates distances of 20', 40', and 60' from left to right.

**PRELIMINARY  
NOT FOR  
CONSTRUCTION**

AS NOTED

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O. 78000

# IMPROVEMENT PLAN 2

C2.2

## NOTES

1. EROSION CONTROL MEASURES SHALL BE IMPLEMENTED FOR THE DURATION OF CONSTRUCTION. AT A MINIMUM, PERIMETER HAY BALES, VEHICLE TRACKING CONTROL, INLET PROTECTION, CONCRETE WASHOUT AREAS AND TEMPORARY SEDIMENTATION BASINS SHOULD BE CONSIDERED
  2. GRANITE CURB SHALL BE PROVIDED IN ALL PARKING AREAS AT THE EDGE OF THE PAVEMENT AND ADJACENT TO SIDEWALKS
  3. CURB, BERM, AND WALKWAY RADII SHALL BE 2 FEET UNLESS NOTED ON PLANS.
  4. WHERE SIDEWALKS INTERSECT CURB LINES, ADA, MAAB COMPLIANT CURB RAMP WITH DETECTABLE WARNING MAT SHALL BE INSTALLED. DETECTABLE WARNING PANELS SHALL BE CAST IRON, SEE SPECIFICATION SECTION 32 13 12.
  5. CURB & GUTTER RELATED DIMENSIONS ARE TO FLOWLINE UNLESS OTHERWISE NOTED.
  6. ALL PAVEMENT MARKINGS ONSITE SHALL BE WATERBOURNE, CONFORMING TO MASSACHUSETTS STANDARD SPECIFICATIONS.
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**HEAVY-DUTY BITUMINOUS CONCRETE PAVEMENT:  
" FINISH COURSE OVER  
BINDER COURSE OVER  
' PROCESSED GRAVEL OVER  
COMPACTED SUBGRADE**

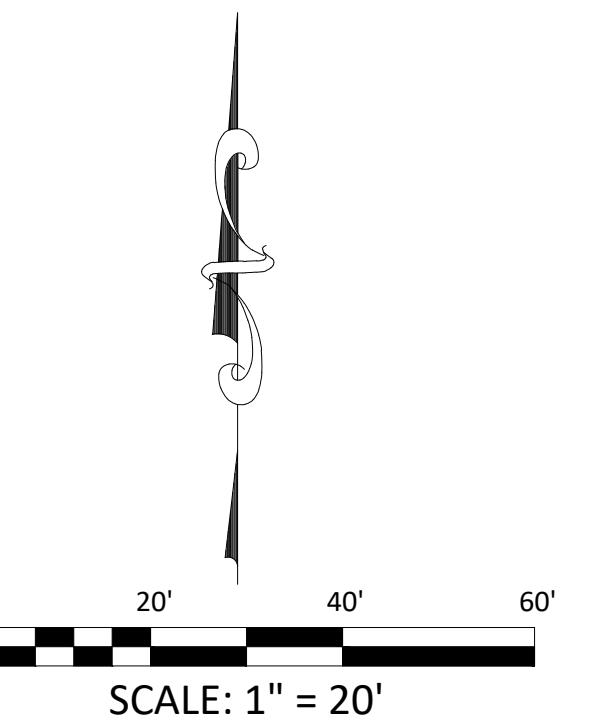
# EWALK CONCRETE LANDSCAPE FOR CONCRETE TYPE

## ROUS PAVEMENT SITE DETAILS

## Notes

MATCH - SHEET C2.1

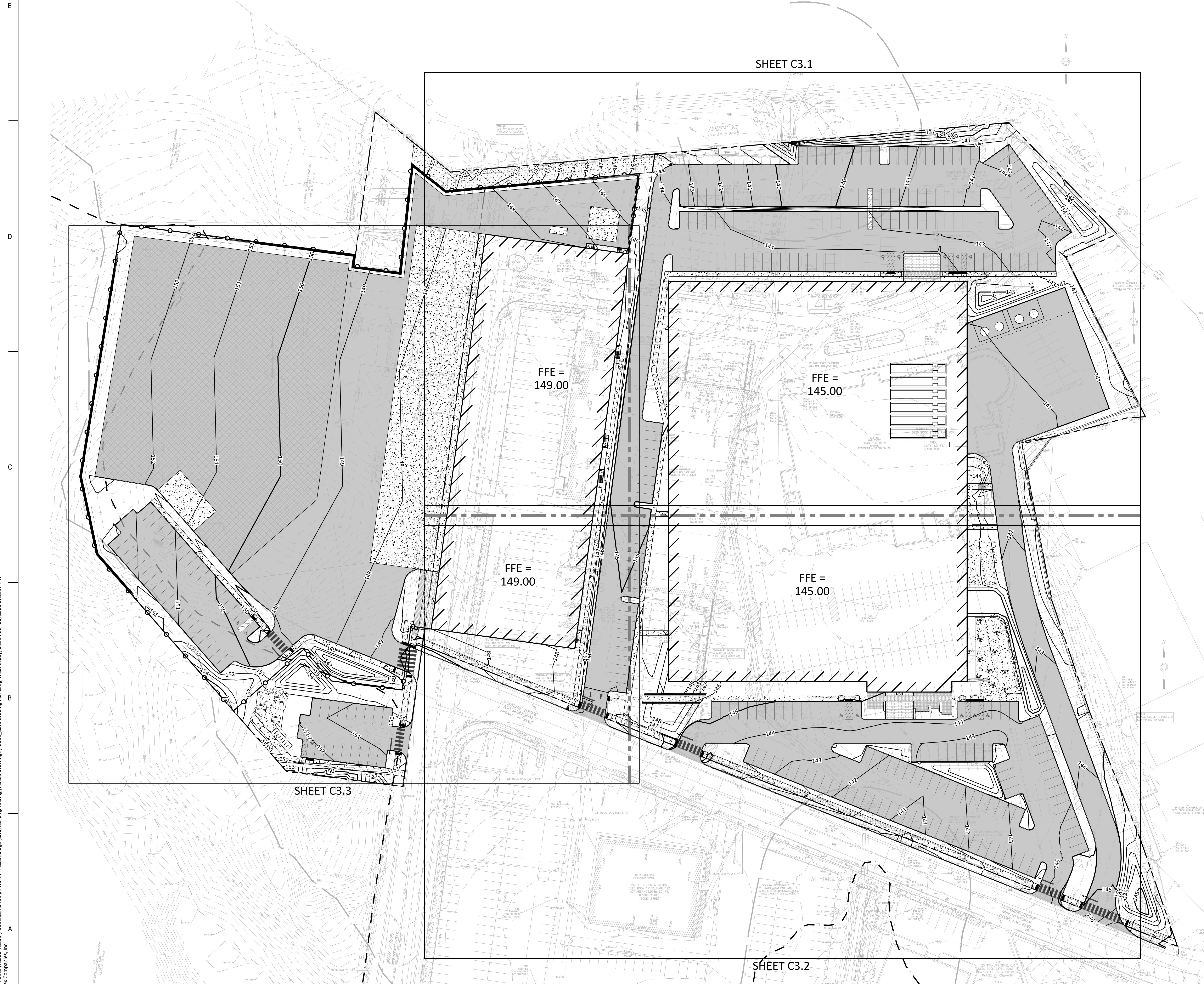
# MATCH - SHEET C2.2



**PRELIMINARY  
NOT FOR  
CONSTRUCTION**

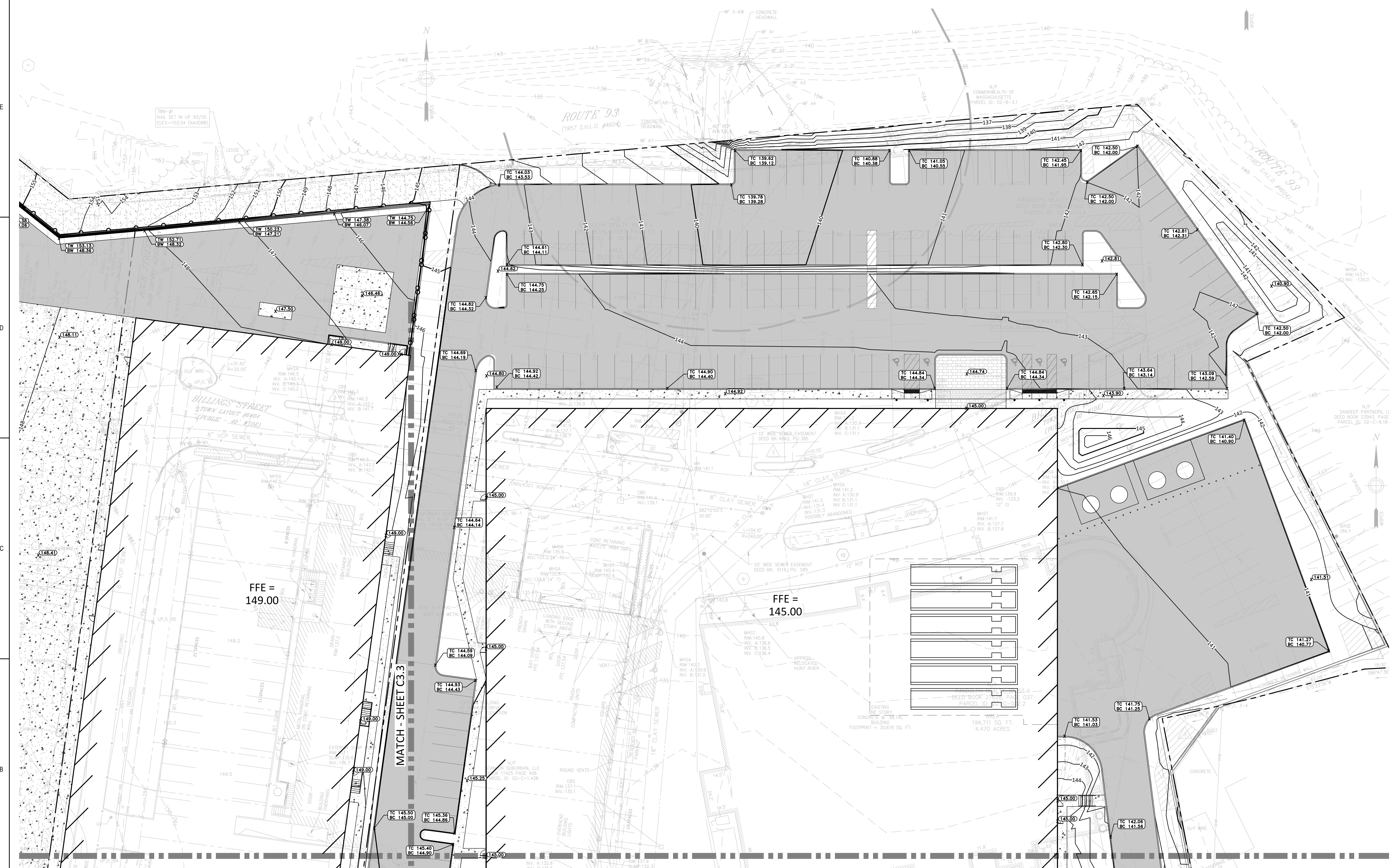
|                                    |          |
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| ale                                | AS NOTED |
| ject No.                           | 78000    |
| <b>SITE IMPROVEMENT<br/>PLAN 3</b> |          |

C2.3





Notes



## NOTES:

1. PITCH EVENLY BETWEEN SPOT GRADES. ALL PAVED AREAS MUST PITCH TO DRAIN AT A MIN. OF 1/8" PER FOOT UNLESS SPECIFIED.
  2. SITE GRADES SHALL CONFORM WITH ADA AND MAAB REQUIREMENTS. IN AREAS WHERE THESE REQUIREMENTS CANNOT BE MET, THE CONTRACTOR SHALL NOTIFY THE ENGINEER IN WRITING FOR RESOLUTION.
  3. ALL TRANSITIONS BETWEEN GROUND COVERING MATERIALS SHALL BE SMOOTH AND MEET 521 CMR 20.10 REQUIREMENTS.
  4. CROSS SLOPES FOR ALL WALKWAYS SHALL NOT EXCEED 2% AND RUNNING SLOPES FOR ALL WALKWAYS SHALL NOT EXCEED 5%.
  5. REFER TO GRADING PLANS FOR ALL GRADING STRUCTURE RIM ELEVATIONS.

ermittlungszeit

**PRELIMINARY  
NOT FOR  
CONSTRUCTION**

scale AS NOTED  
project No. 78000

---

C3 1

C5.1

3

20'      40'      60'

SCALE: 1" = 20'

# C3.1

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40 Water Street  
Boston, MA 02109  
Tel: (617) 234-3100  
[www.stantec.com](http://www.stantec.com)

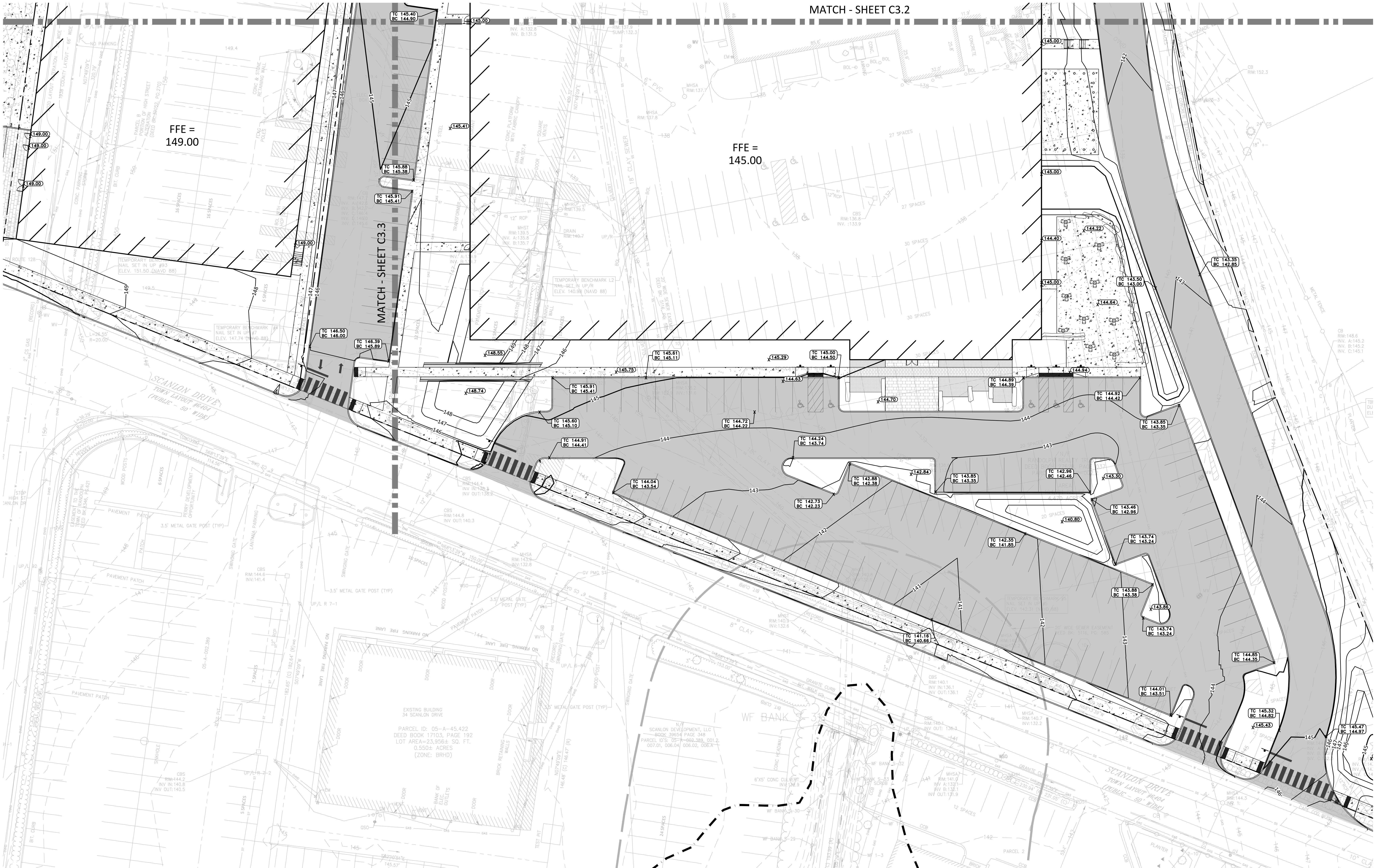
Consultant

**VERTEX**  
The Vertex Companies, LLC.  
400 Libbey Parkway  
Weymouth, MA 02189  
PHONE 781.952.6000  
[www.vertexeng.com](http://www.vertexeng.com)

Key Plan



Notes

**NOTES:**

- PITCH EVENLY BETWEEN SPOT GRADES. ALL PAVED AREAS MUST PITCH TO DRAIN AT A MIN. OF 1/8" PER FOOT UNLESS SPECIFIED.
- SITE GRADES SHALL CONFORM WITH ADA AND MAAB REQUIREMENTS. IN AREAS WHERE THESE REQUIREMENTS CANNOT BE MET, THE CONTRACTOR SHALL NOTIFY THE ENGINEER IN WRITING FOR RESOLUTION.
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- REFER TO GRADING PLANS FOR ALL GRADING STRUCTURE RIM ELEVATIONS.

Issued/Revision

2023.12.15

2023.10.06

YMMJAHZD

Permit/Seal

**PRELIMINARY  
NOT FOR  
CONSTRUCTION**

Scale AS NOTED

Project No. 78000

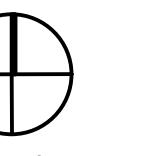
GRADING PLAN 2

0' 20' 40' 60'  
SCALE: 1" = 20'

C3.2



y Plan



Notes

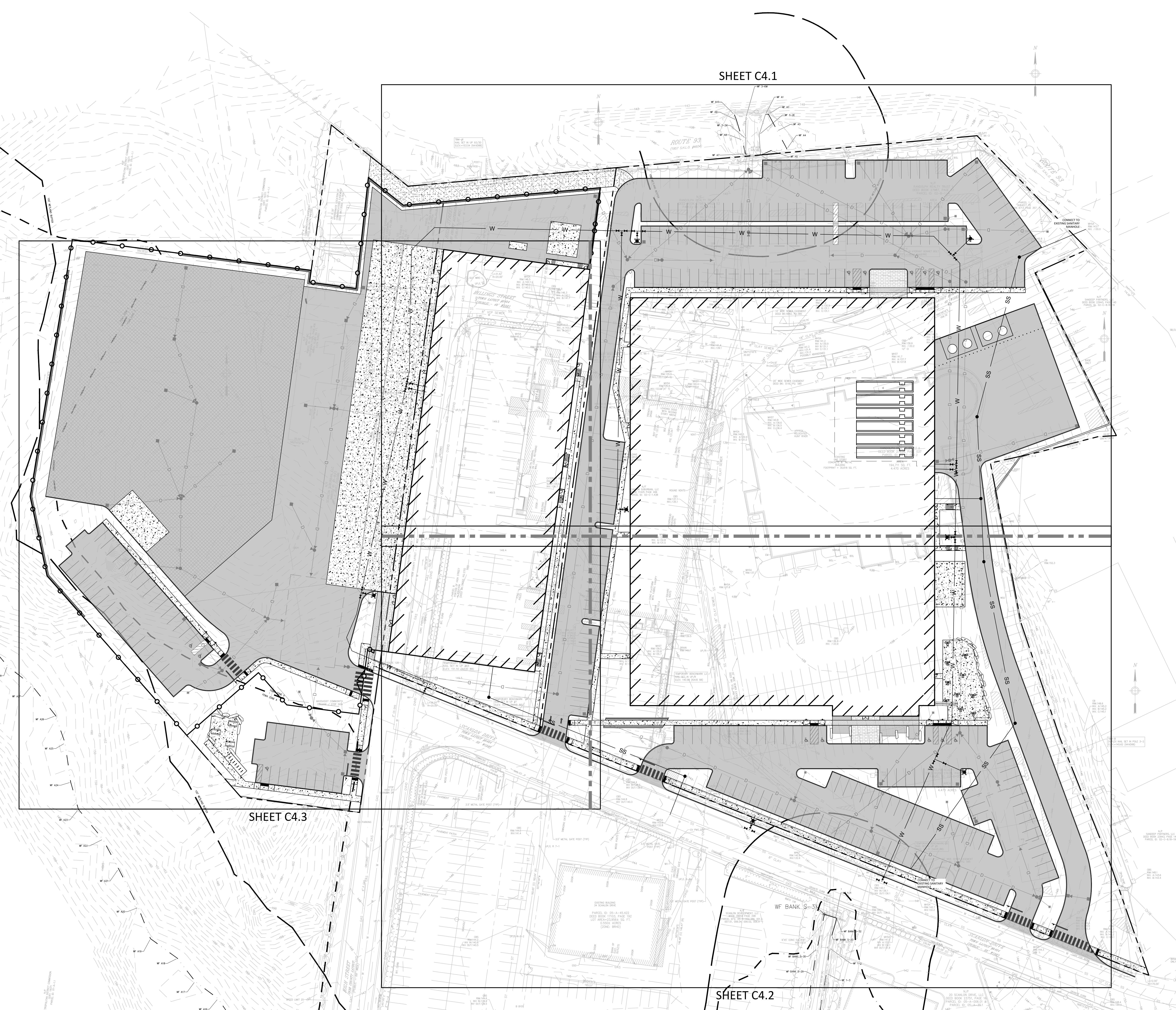
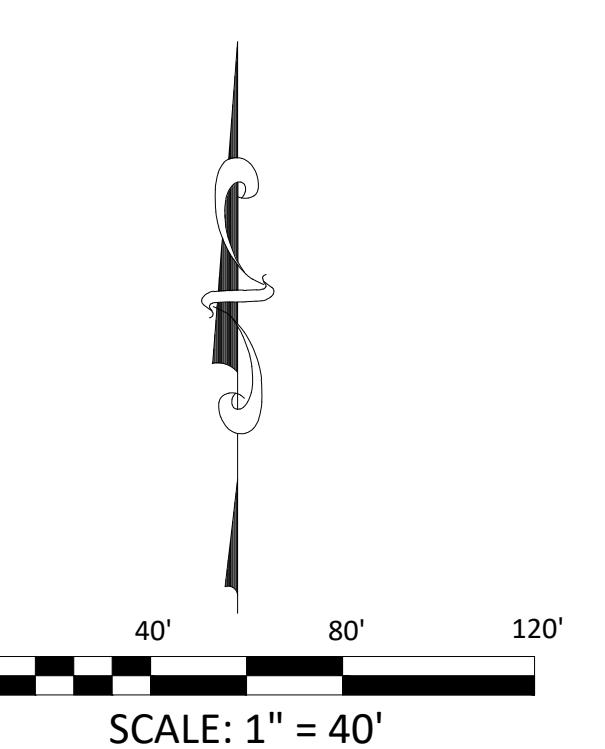
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| DESIGN DEVELOPMENT | 2023.12.15 |
| SCHEMATIC DESIGN   | 2023.10.06 |

Permit/Seal

**PRELIMINARY  
NOT FOR  
CONSTRUCTION**


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| ale                         | AS NOTED |
| object No.                  | 78000    |
| <b>OVERALL UTILITY PLAN</b> |          |

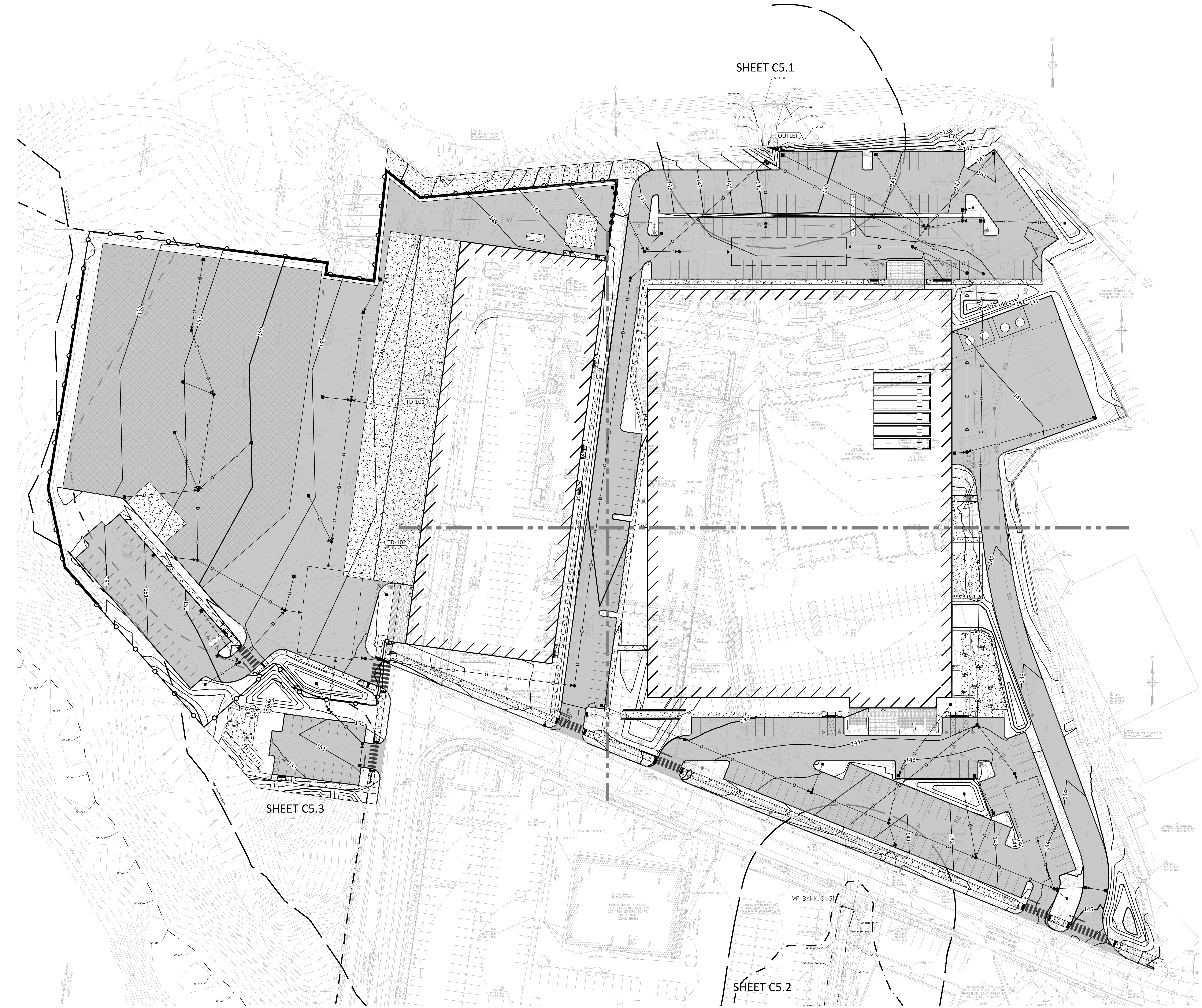
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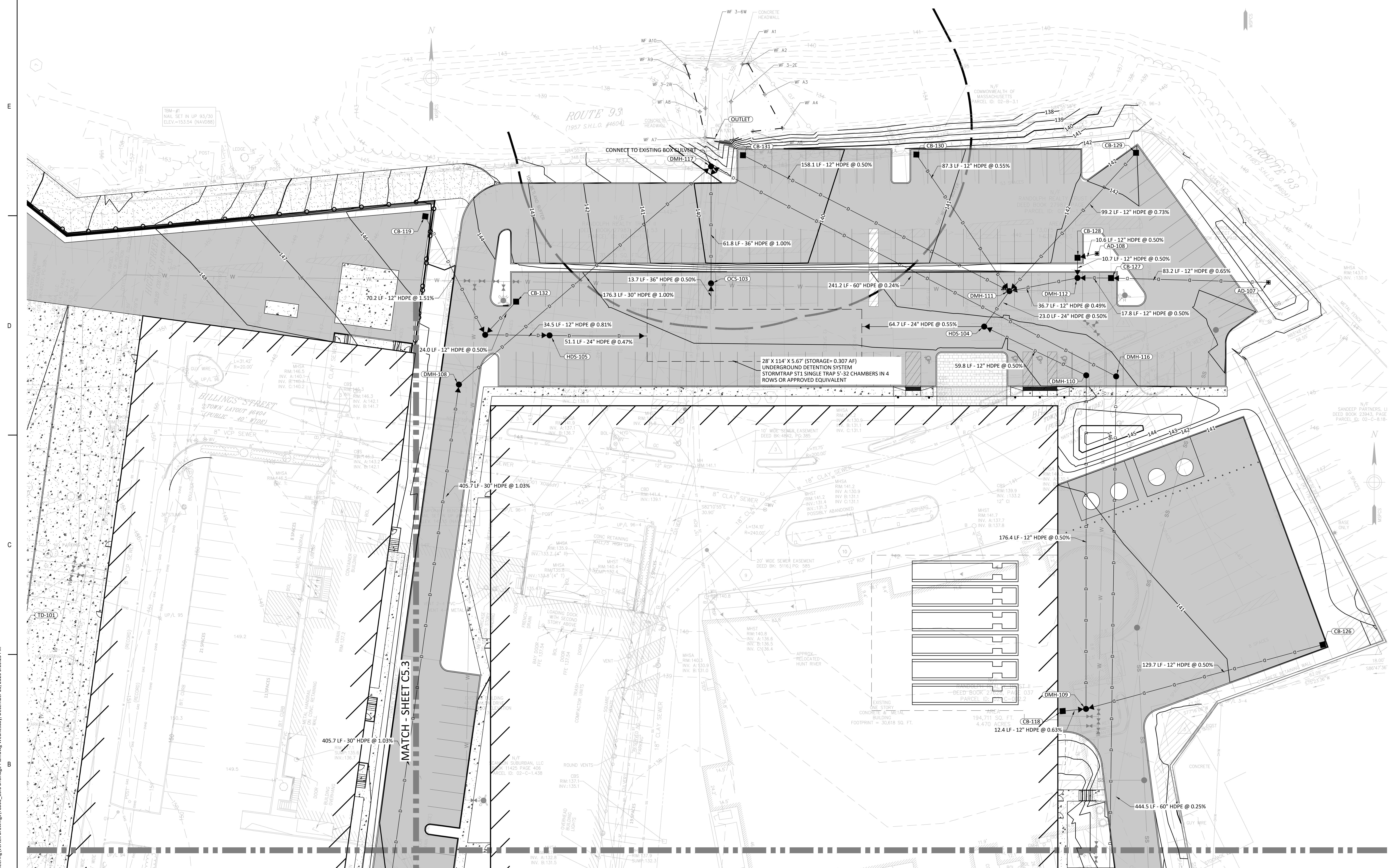








0' 40' 80' 120'  
 SCALE: 1" = 40'




- NOTE:**
- EXISTING UNDERGROUND UTILITY LOCATIONS ARE ESTIMATED. AT THIS TIME EXISTENCE AND CONDITIONS OF UTILITIES HAVE NOT BEEN CONFIRMED.
  - EROSION CONTROL MEASURES SHALL BE IMPLEMENTED FOR THE DURATION OF CONSTRUCTION. AT A MINIMUM, PERIMETER HAY BALES, VEHICLE TRACKING CONTROL, INLET PROTECTION, CONCRETE WASHOUT AREAS AND TEMPORARY SEDIMENTATION BASINS SHOULD BE CONSIDERED.
  - ALL UTILITIES WITHIN THE FOOTPRINT OF PROPOSED BUILDING ADDITIONS SHOULD BE ANTICIPATED TO BE REMOVED AND RELOCATED. SERVICE SHALL BE MAINTAINED TO EXISTING BUILDINGS TO REMAIN FOR THE DURATION OF CONSTRUCTION.
  - ALL EXISTING STRUCTURES TO REMAIN WITHIN THE LIMITS OF WORK SHALL BE ADJUSTED TO FINISH GRADE. SERVICE SHALL BE MAINTAINED TO EXISTING BUILDINGS DURING THE DURATION OF CONSTRUCTION.
  - ALL PRECAST CONCRETE MANHOLES FOR SANITARY AND DRAINAGE SHALL CONFORM TO THE ASTM "SPECIFICATIONS FOR PRECAST REINFORCED CONCRETE MANHOLE SECTIONS," DESIGNATION D478. THE BARREL SHALL BE 4-FOOT WITH A 1-FOOT COLLAR TO PREVENT FLOTATION.
  - ALL DRAIN LINES SHALL BE 12" UNLESS OTHERWISE NOTED. ALL DRAIN LINES SHALL BE RCP UNLESS OTHERWISE NOTED.
  - ALL CATCH BASINS TO BE 4" DIAMETER (UNLESS OTHERWISE NOTED) SHALL CONFORM TO MHD STANDARD DETAIL 202.4.0 AND ALL MANHOLE FRAMES AND COVERS SHALL CONFORM TO 202.6.0 UNLESS OTHERWISE NOTED. CONCRETE ANTI-FLATION COLLARS SHALL BE PROVIDED AT ALL MANHOLES.
  - REINFORCED CONCRETE PIPE AND FLARED ENDS SHALL CONFORM TO THE AASHTO M170 FOR STANDARD STRENGTH REINFORCED CONCRETE CULVERT PIPE FOR CLASS III PIPE, WALL B, OR ASTM C76 FOR REINFORCED CONCRETE CULVERT AND DRAIN PIPE UNLESS NOTED OTHERWISE. PIPE 24 INCHES IN DIAMETER OR SMALLER SHALL BE TONGUE AND GROOVE TYPE. PIPES LARGER THAN 24 INCHES IN DIAMETER SHALL BE TONGUE AND GROOVE OR BELL AND SPIGOT. ALL DRAINAGE PIPING SHALL BE GASKETED.
  - RCP PIPE LOCATED IN VEHICULAR AREAS WITH LESS THAN 6" OF COVER BELOW SUBGRADE ELEVATION SHALL BE CLASS V.
  - CONCRETE VAULT DETENTION SYSTEMS SHALL INCLUDE AN 8" EXTENDED CONCRETE SLAB WITH UNITS ANCHORED INTO SLAB, AND SHALL BE LINED WITH AN IMPERVIOUS LINER.
  - HIGH-DENSITY POLYETHYLENE PIPE AND FITTINGS SHALL BE ADS N-12 IB ST SMOOTH INTERIOR PIPE, ADS N-12 IB ST HIGH CAPACITY LARGE DIAMETER PIPE OR APPROVED EQUIVALENT. JOINTS SHALL BE SOIL-TIGHT AND INCLUDE A RUBBER GASKET ON THE SPIGOT END OF THE PIPE. WHEN INSTALLED INTO THE BELL END, THE JOINT SHALL BE SEALED.
  - MANHOLES OVER 12 FEET IN DEPTH SHALL HAVE A MINIMUM OF 5 FEET INSIDE DIAMETER. ALL MANHOLES SHALL HAVE A SUMP OF AT LEAST 30 INCHES BELOW INVERT OF OUTLET PIPE. RISERS SHALL BE CLAY OR SHALE BRICK, AND SHALL CONFORM TO THE REQUIREMENTS OF AASHTO M 91, GRADE MM OR AS SPECIFIED IN MASSDOT M4.05.
  - ALL CATCH BASINS TO BE 4" DIAMETER (UNLESS OTHERWISE NOTED) SHALL CONFORM TO MHD STANDARD DETAIL 201.4.0 AND ALL CATCH BASIN FRAMES AND GRATES SHALL CONFORM TO 201.6.0 UNLESS OTHERWISE NOTED.
  - ALL CATCH BASINS SHALL HAVE A SUMP OF AT LEAST 48 INCHES (4 FEET) BELOW THE INVERT OF THE OUTLET PIPE, OR OTHERWISE APPROVED BY THE DPW, AND AN INSIDE DIAMETER OF 4 FEET MINIMUM.
  - LIVE LOAD DESIGN FOR CATCH BASINS SHALL BE HS-25. LOADING CATCH BASINS WHICH ARE LIMITED BY HEIGHT SHALL BE INSTALLED WITH A FLAT TOP SLAB, CAST IN PLACE, DESIGNED FOR HS-25 LOADING AND CAST IRON FRAME CAST IN PLACE.
  - MANHOLE FRAMES AND COVERS SHALL BE AT LEAST CLASS 25 CONFORMING TO ASTM A48 STANDARD SPECIFICATION FOR GRAY IRON CASTINGS.
  - CATCH BASIN HOODS SHALL BE USED TO MINIMIZE THE ENTRY OF OIL, GASOLINE, AND DEBRIS INTO DRAINAGE PIPES.
  - WHERE PROPOSED DRAIN LINES CROSS SANITARY OR WATER LINES WITH LESS THAN 15' CLEARANCE, ENCASE BOTH UTILITIES IN FLOWABLE FILL FOR A DISTANCE OF 10' ON EITHER SIDE OF CROSSING. CENTER PIPE LENGTH AT CROSSING. REFER TO CROSSING DETAIL ON SHEET C6. ON DETAIL SHEETS.
  - HYDRODYNAMIC SEPARATORS SHALL BE CONTECH CDS2025-5-C, UNLESS OTHERWISE NOTED, OR APPROVED EQUIVALENT.
  - CONCRETE ANTI-FLATION COLLARS SHALL BE PROVIDED AT ALL MANHOLES IN AREAS OF HIGH GROUNDWATER.

0' 20' 40' 60'

SCALE: 1" = 20'

**PRELIMINARY  
NOT FOR  
CONSTRUCTION**

Scale AS NOTED  
Project No. 78000

**DRAINAGE PLAN 1**

**C5.1**



## NOTE:

- EXISTING UNDERGROUND UTILITY LOCATIONS ARE ESTIMATED. AT THIS TIME EXISTENCE AND CONDITIONS OF UTILITIES HAVE NOT BEEN CONFIRMED
- EROSION CONTROL MEASURES SHALL BE IMPLEMENTED FOR THE DURATION OF CONSTRUCTION, AT A MINIMUM, PERIMETER HAY BALES, VEHICLE TRACKING CONTROL, INLET PROTECTION, CONCRETE WASHOUT AREAS AND TEMPORARY SEDIMENTATION BASINS SHOULD BE CONSIDERED
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- ALL DRAIN LINES SHALL BE 12" UNLESS OTHERWISE NOTED. ALL DRAIN LINES SHALL BE RCP UNLESS OTHERWISE NOTED
- ALL CATCH BASINS TO BE 4' DIAMETER (UNLESS OTHERWISE NOTED) SHALL CONFORM TO MHD STANDARD DETAIL 201.4.0 AND ALL CATCH BASIN FRAMES AND GRATES SHALL CONFORM TO 201.6.0 UNLESS OTHERWISE NOTED
- ALL MANHOLES TO BE 4" DIAMETER (UNLESS OTHERWISE NOTED) AND SHALL CONFORM TO MHD STANDARD DETAIL 202.4.0 AND ALL MANHOLE FRAMES AND COVERS SHALL CONFORM TO 202.6.0 UNLESS OTHERWISE NOTED. CONCRETE ANTI-FLotation COLLARS SHALL BE PROVIDED AT ALL MANHOLES
- REINFORCED CONCRETE PIPE AND FLARED ENDS SHALL CONFORM TO THE AASHTO M170 FOR STANDARD REINFORCED CONCRETE PIPE, CLASS II OR APPROVED EQUIVALENT. PIPE UNLESS OTHERWISE, ALL PIPE 24 INCHES IN DIAMETER OR SMALLER SHALL BE OF THE BELL AND SPIGOT TYPE. PIPES LARGER THAN 24 INCHES IN DIAMETER SHALL BE TONGUE AND GROOVE OR BELL AND SPIGOT. ALL DRAINAGE PIPING SHALL BE GASKETED
- RCP PIPE LOCATED IN VEHICULAR AREAS WITH LESS THAN 6" OF COVER BELOW SUBGRADE ELEVATION SHALL BE CLASS V
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- HYDRODYNAMIC SEPARATORS SHALL BE CONTECH CDS2025-5-C, UNLESS OTHERWISE NOTED, OR APPROVED EQUIVALENT
- CONCRETE ANTI-FLotation COLLARS SHALL BE PROVIDED AT ALL MANHOLES IN AREAS OF HIGH GROUNDWATER

MATCH - SHEET C5.1

MATCH - SHEET C5.2



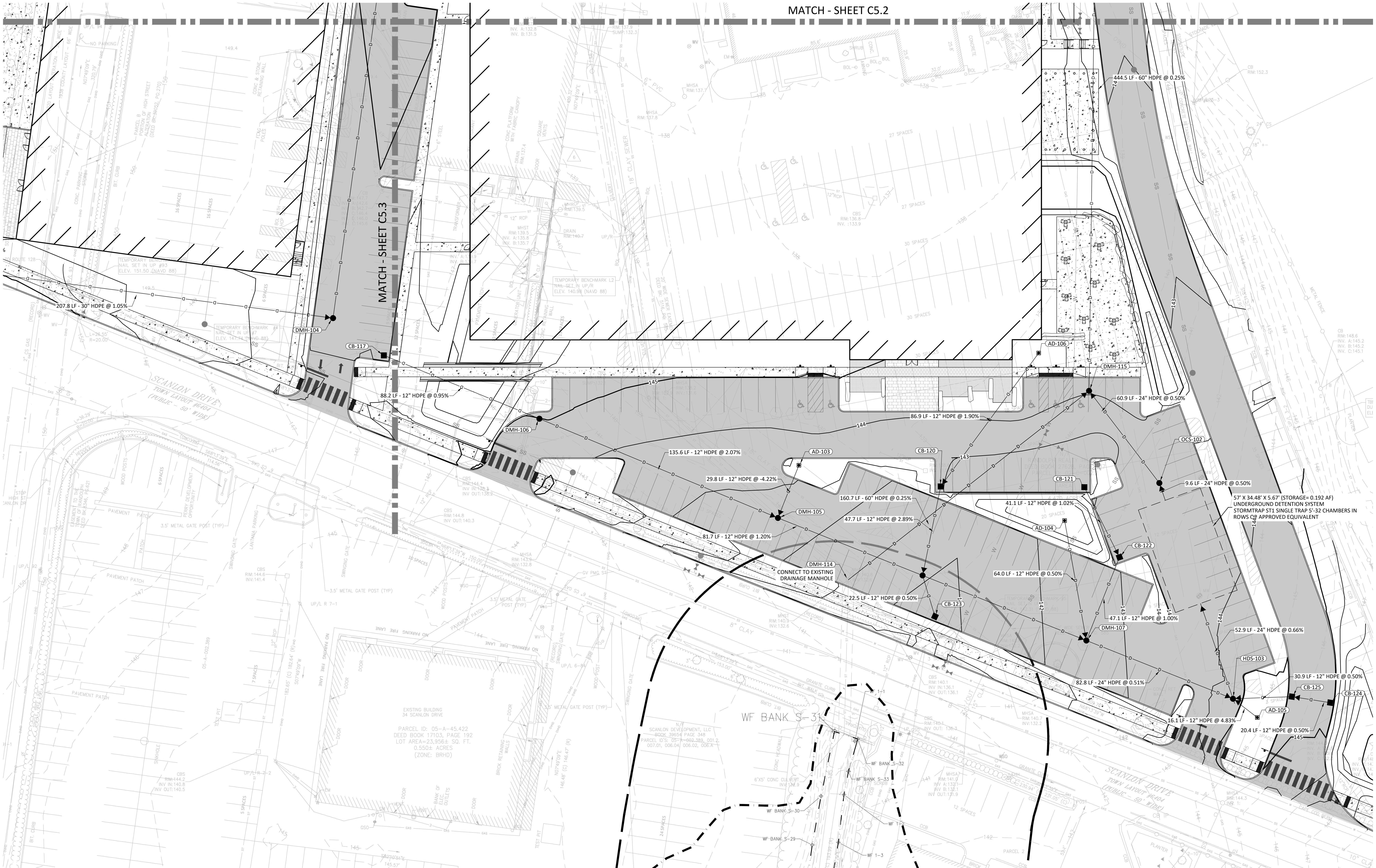
0' 20' 40' 60'

SCALE: 1" = 20'

**PRELIMINARY  
NOT FOR  
CONSTRUCTION**

Scale AS NOTED  
Project No. 78000  
DRAINAGE PLAN 3

**C5.3**

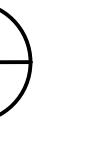


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Consultant

**VERTEX**  
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Key Plan



PROJECT  
NORTH

Notes

2 DESIGN DEVELOPMENT 2023.12.15  
1 SCHEMATIC DESIGN 2023.10.06  
Issued/Revision YYYAHZD

Permit/Seal

PRELIMINARY  
NOT FOR  
CONSTRUCTION

Scale AS NOTED  
Project No. 78000

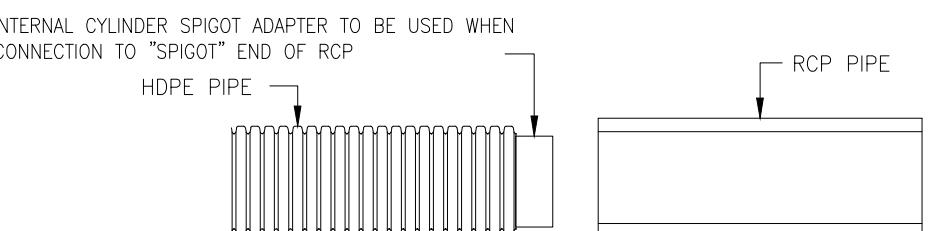
DRAINAGE PLAN 4

C5.4

| Structure Table |   |
|-----------------|---|
| Structure Name  | Structure Details                                   |
| AD-101          | RIM = 151.47<br>INV OUT = 148.43                    |
| AD-102          | RIM = 146.80<br>INV OUT = 144.75                    |
| AD-103          | RIM = 143.65<br>INV OUT = 138.85                    |
| AD-104          | RIM = 140.89<br>INV OUT = 138.75                    |
| AD-105          | RIM = 145.35<br>INV OUT = 143.30                    |
| AD-106          | RIM = 144.98<br>INV OUT = 142.15                    |
| AD-107          | RIM = 140.90<br>INV OUT = 138.85                    |
| AD-108          | RIM = 142.84<br>INV OUT = 140.00                    |
| CB-101          | RIM = 151.27<br>INV OUT = 149.22                    |
| CB-102          | RIM = 151.08<br>INV IN = 148.86<br>INV OUT = 148.76 |
| CB-103          | RIM = 148.70<br>INV OUT = 146.65                    |
| CB-104          | RIM = 151.02<br>INV OUT = 148.97                    |
| CB-105          | RIM = 151.17<br>INV OUT = 149.12                    |
| CB-106          | RIM = 150.00<br>INV OUT = 147.95                    |
| CB-107          | RIM = 151.84<br>INV OUT = 149.79                    |
| CB-108          | RIM = 148.50<br>INV IN = 146.16<br>INV OUT = 145.44 |
| CB-109          | RIM = 148.84<br>INV OUT = 145.98                    |
| CB-110          | RIM = 149.11<br>INV OUT = 147.06                    |
| CB-111          | RIM = 148.74<br>INV OUT = 146.07                    |
| CB-112          | RIM = 150.79<br>INV OUT = 148.74                    |
| CB-113          | RIM = 149.89<br>INV OUT = 147.49                    |
| CB-114          | RIM = 150.35<br>INV OUT = 147.68                    |
| CB-115          | RIM = 150.87<br>INV OUT = 148.82                    |
| CB-116          | RIM = 150.12<br>INV IN = 148.07<br>INV OUT = 147.97 |
| CB-117          | RIM = 145.92<br>INV OUT = 143.76                    |
| CB-118          | RIM = 141.02<br>INV OUT = 138.96                    |
| CB-119          | RIM = 145.17<br>INV OUT = 141.57                    |
| CB-120          | RIM = 143.12<br>INV IN = 140.49<br>INV OUT = 139.73 |
| CB-121          | RIM = 142.24<br>INV OUT = 140.19                    |
| CB-122          | RIM = 143.41<br>INV IN = 139.77<br>INV OUT = 139.67 |
| CB-123          | RIM = 140.68<br>INV OUT = 138.62                    |
| CB-124          | RIM = 144.72<br>INV OUT = 142.67                    |
| CB-125          | RIM = 144.70<br>INV IN = 142.57<br>INV OUT = 142.47 |
| CB-126          | RIM = 140.78<br>INV OUT = 138.73                    |
| CB-127          | RIM = 142.18<br>INV IN = 138.31<br>INV OUT = 138.21 |

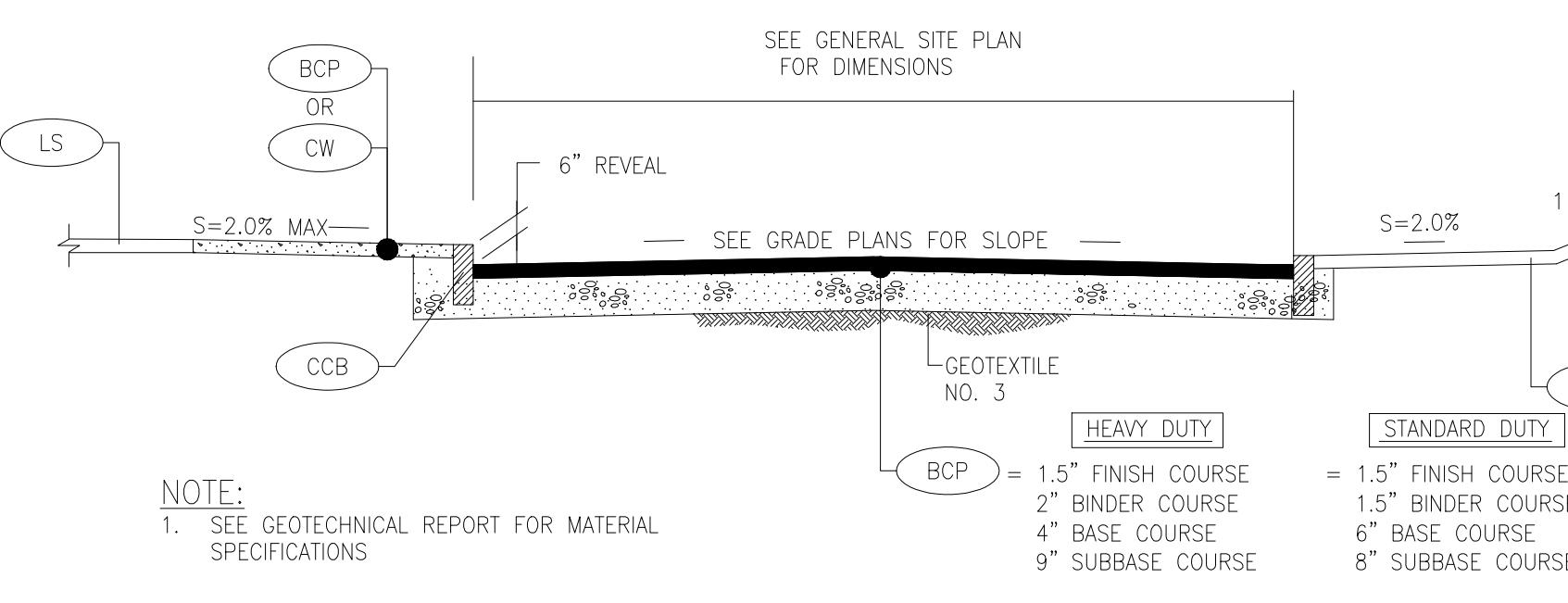
| Structure Table |  |
|-----------------|--|
| Structure Name  | Structure Details  |
| CB-128          | RIM = 142.27<br>INV IN = 139.95<br>INV OUT = 139.85  |
| CB-129          | RIM = 141.99<br>INV OUT = 139.94   |
| CB-130          | RIM = 140.61<br>INV OUT = 138.56   |
| CB-131          | RIM = 140.18<br>INV OUT = 137.13   |
| CB-132          | RIM = 144.31<br>INV OUT = 142.26   |
| DMH-101         | RIM = 150.22<br>INV IN = 147.15<br>INV IN = 147.62<br>INV OUT = 147.05                                       |
| DMH-102         | RIM = 150.78<br>INV IN = 147.85<br>INV IN = 148.73<br>INV IN = 148.72<br>INV IN = 148.50<br>INV OUT = 147.50 |
| DMH-103         | RIM = 148.37<br>INV IN = 144.96<br>INV IN = 145.67<br>INV OUT = 144.86                                       |
| DMH-104         | RIM = 145.71<br>INV IN = 139.88<br>INV OUT = 139.78  |
| DMH-105         | RIM = 143.99<br>INV IN = 140.10<br>INV IN = 139.99<br>INV OUT = 139.89                                       |
| DMH-106         | RIM = 144.99<br>INV IN = 142.92<br>INV OUT = 142.80  |
| DMH-107         | RIM = 142.53<br>INV IN = 137.33<br>INV IN = 139.20<br>INV IN = 138.43<br>INV OUT = 137.23                    |
| DMH-108         | RIM = 144.43<br>INV IN = 135.59<br>INV OUT = 135.61  |
| DMH-109         | RIM = 142.77<br>INV IN = 138.08<br>INV IN = 138.89<br>INV OUT = 137.98                                       |
| DMH-110         | RIM = 143.45<br>INV IN = 137.10<br>INV OUT = 137.00  |
| DMH-111         | RIM = 142.57<br>INV IN = 137.84<br>INV IN = 136.34<br>INV IN = 138.07<br>INV IN = 139.22<br>INV OUT = 136.71 |
| DMH-112         | RIM = 142.30<br>INV IN = 139.79<br>INV IN = 138.12<br>INV OUT = 138.02                                       |
| DMH-113         | RIM = 150.55<br>INV IN = 148.43<br>INV IN = 148.50<br>INV OUT = 148.33                                       |
| DMH-114         | RIM = 141.46<br>INV OUT = 132.60   |
| DMH-115         | RIM = 144.09<br>INV IN = 135.55<br>INV IN = 132.20<br>INV OUT = 132.21                                       |
| DMH-116         | RIM = 143.15<br>INV IN = 131.09<br>INV OUT = 131.10  |
| DMH-117         | RIM = 139.46<br>INV IN = 130.52<br>INV IN = 130.99<br>INV IN = 133.86<br>INV OUT = 130.53                    |
| HDS-101         | RIM = 145.70<br>INV IN = 146.43<br>INV IN = 146.57<br>INV IN = 145.73<br>INV OUT = 144.34                    |
| HDS-102         | RIM = 148.45<br>INV IN = 144.16<br>INV IN = 145.61<br>INV IN = 144.88<br>INV IN = 145.16<br>INV OUT = 144.07 |
| HDS-103         | RIM = 144.57<br>INV IN = 136.80<br>INV IN = 142.32<br>INV IN = 142.52<br>INV OUT = 136.70                    |
| HDS-104         | RIM = 143.31<br>INV IN = 136.60<br>INV IN = 136.70<br>INV OUT = 136.60                                       |
| HDS-105         | RIM = 144.94<br>INV IN = 140.13<br>INV IN = 140.03   |
| HDS-201         | RIM = 151.62<br>INV IN = 147.74<br>INV IN = 144.61<br>INV OUT = 144.51                                       |
| INF-101         | RIM = 145.60<br>INV IN = 144.26  |
| INF-102         | RIM = 144.42<br>INV OUT = 142.24   |
| INF-103         | RIM = 145.35<br>INV IN = 144.25  |
| INF-104         | RIM = 144.90<br>INV IN = 143.79  |
| OCS-101         | RIM = 149.25<br>INV IN = 142.17<br>INV OUT = 142.07  |
| OCS-102         | RIM = 143.42<br>INV IN = 135.95<br>INV OUT = 135.85  |
| OCS-103         | RIM = 143.58<br>INV IN = 135.20<br>INV OUT = 133.61  |





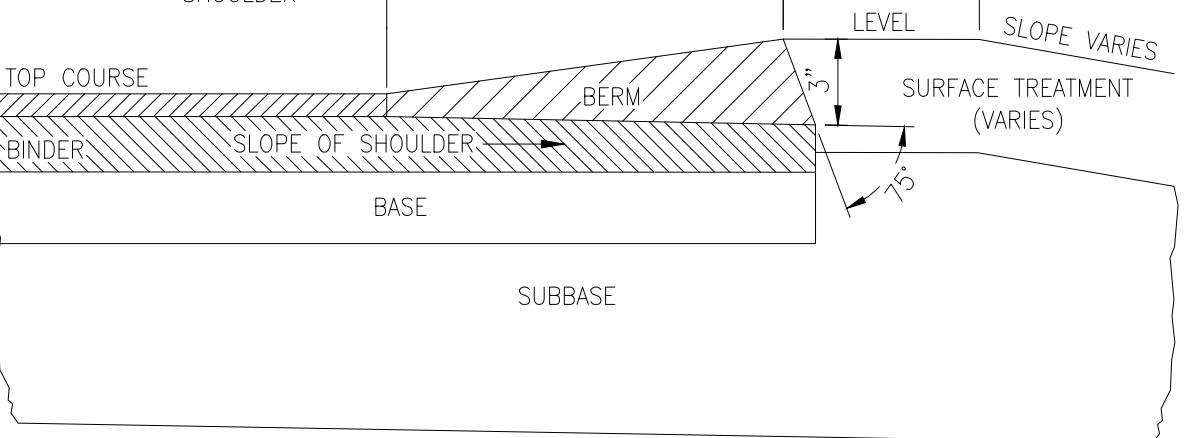
INTERNAL CYLINDER SPIGOT ADAPTER TO BE USED WHEN CONNECTION TO "SPIGOT" END OF RCP  
HOPE PIPE  
RCP PIPE  
FINAL GRADE  
NONWOVEN GEOTEXTILE TYPE 1 TO BE WRAPPED AROUND CONNECTION  
RCP PIPE  
PROVIDE SPACER TO MATCH INVERTS  
  
NOTES:  
1. INTERNAL CYLINDER ADAPTER TO BE WELDED TO HOPE, OUTSIDE DIAMETER TO BE INSERTED INTO INSIDE DIAMETER OF CONCRETE PIPE.  
2. NON-WOVEN GEOTEXTILE TO BE WRAPPED AROUND CONNECTION WITH FULL SEAM OVERLAP TO PROVIDE FULL PROTECTION FROM SOIL INTRUSION.  
3. CONNECTION TO BE MADE IN ACCORDANCE WITH PIPE MANUFACTURER'S REQUIREMENTS.  
4. INTERNAL CYLINDER SPIGOT ADAPTER NOT REQUIRED IF HOPE IS CONNECTED TO "BELL" END OF RCP.

HDPE/RCP PIPE JOINT  
NOT TO SCALE



NOTE:  
1. SEE GEOTECHNICAL REPORT FOR MATERIAL SPECIFICATIONS

TYPICAL BITUMINOUS CONCRETE PAVEMENT SECTIONS  
NOT TO SCALE



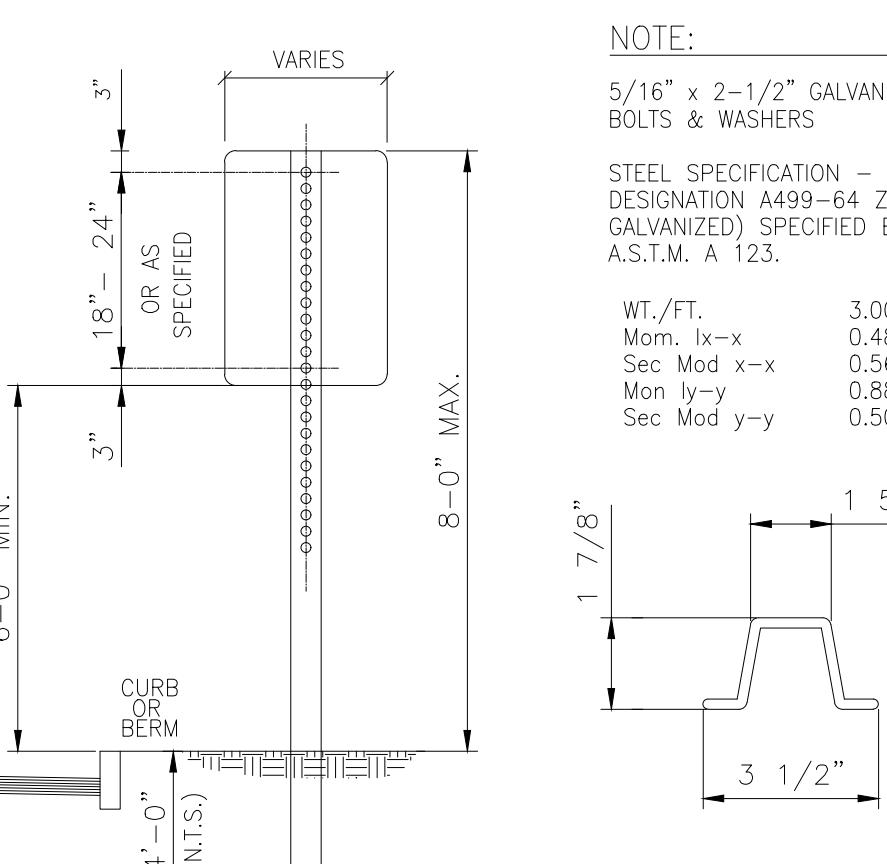
RESERVED PARKING  
VAN  
ACCESSIBLE  
R7-8 (12"x18")  
NOT TO SCALE  
R7-8A  
NOT TO SCALE

NOTE:  
1. ALL HANDICAP PARKING AND SIGNAGE SHALL BE IN CONFORMANCE WITH THE RULES & REGULATIONS OF THE ARCHITECTURAL BARBERS BOARD & ADA.  
2. STRIPING SHOULD BE WHITE IN COLOR

SHP  
HANDICAP PAVEMENT MARKING  
NOT TO SCALE

SHP  
VAN HANDICAP PARKING STALLS @ 90°  
NOT TO SCALE

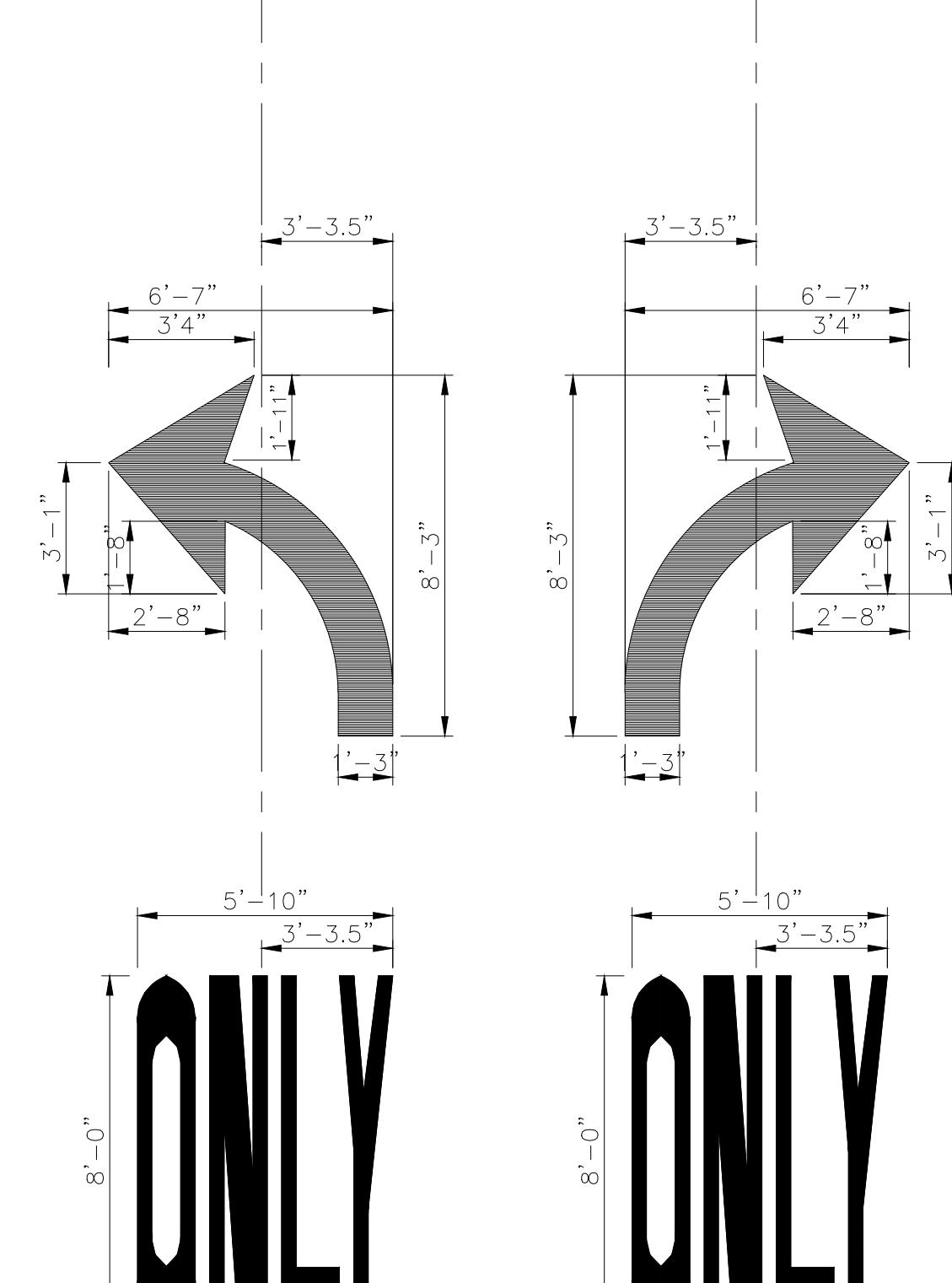
BB  
HOT MIX ASPHALT BERM  
NOT TO SCALE



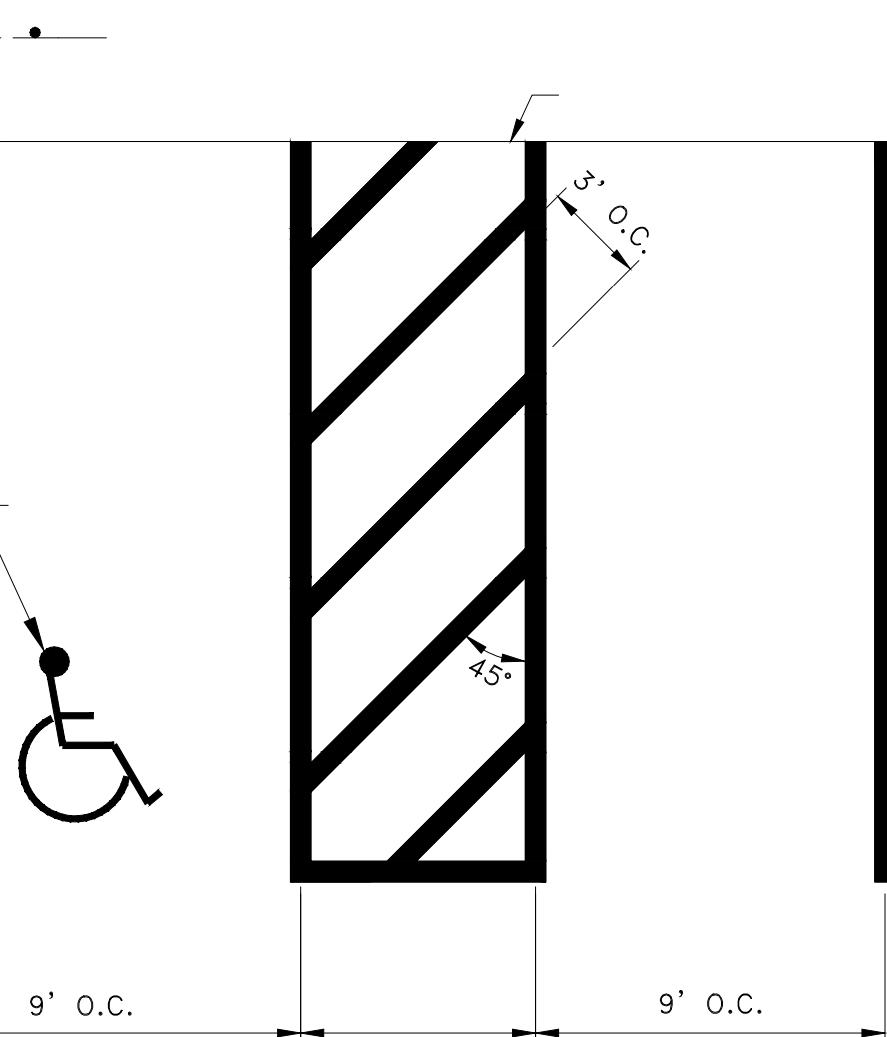
SIGN MOUNTING NOTES:  
1. ALL LAG SCREWS, BOLTS AND WASHERS SHALL BE GALVANIZED 5/16" x 1/2" LONG UNLESS OTHERWISE NOTED.  
2. WASHERS SHALL BE 0.07" THICK. 3. ALL SIGN COLORS, RADII AND BORDERS AS SPECIFIED IN "MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES".

HANDICAP SIGN NOTES:  
1. ALL HANDICAP PARKING AND SIGNAGE SHALL BE IN CONFORMANCE WITH THE RULES & REGULATIONS AS SPECIFIED BY THE AMERICAN DISABILITY ACT (ADA)  
2. SIGN(S) SHALL BE LOCATED SO THEY CANNOT BE OBSCURED BY A VEHICLE PARKED IN THE SPACE.  
3. FOR HANDICAPPED VAN SPACE, USE SIGN AS DETAILED.  
4. FOR HANDICAPPED SPACE FOR AUTOMOBILES, USE ONLY HANDICAPPED PARKING SIGN. (WITHOUT ADDITIONAL "VAN ACCESSIBLE" SIGN)

SIGN MOUNTING DETAIL  
NOT TO SCALE



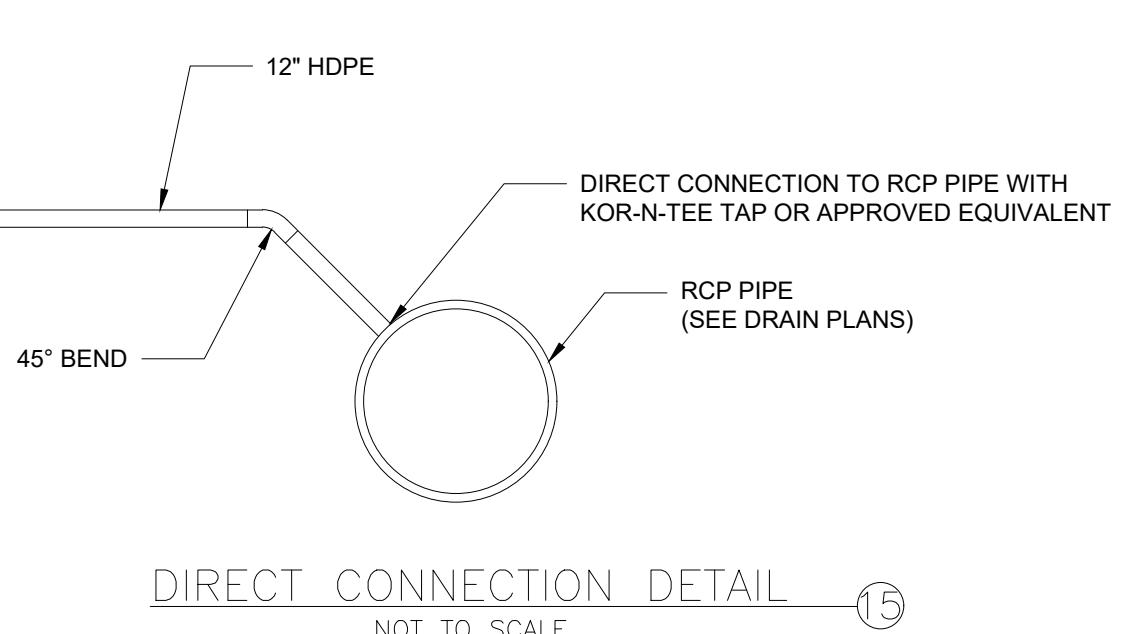
DIRECTIONAL ARROW PAVEMENT MARKINGS  
NOT TO SCALE  
STRIPING SHOULD BE EPOXY RESIN AND WHITE IN COLOR



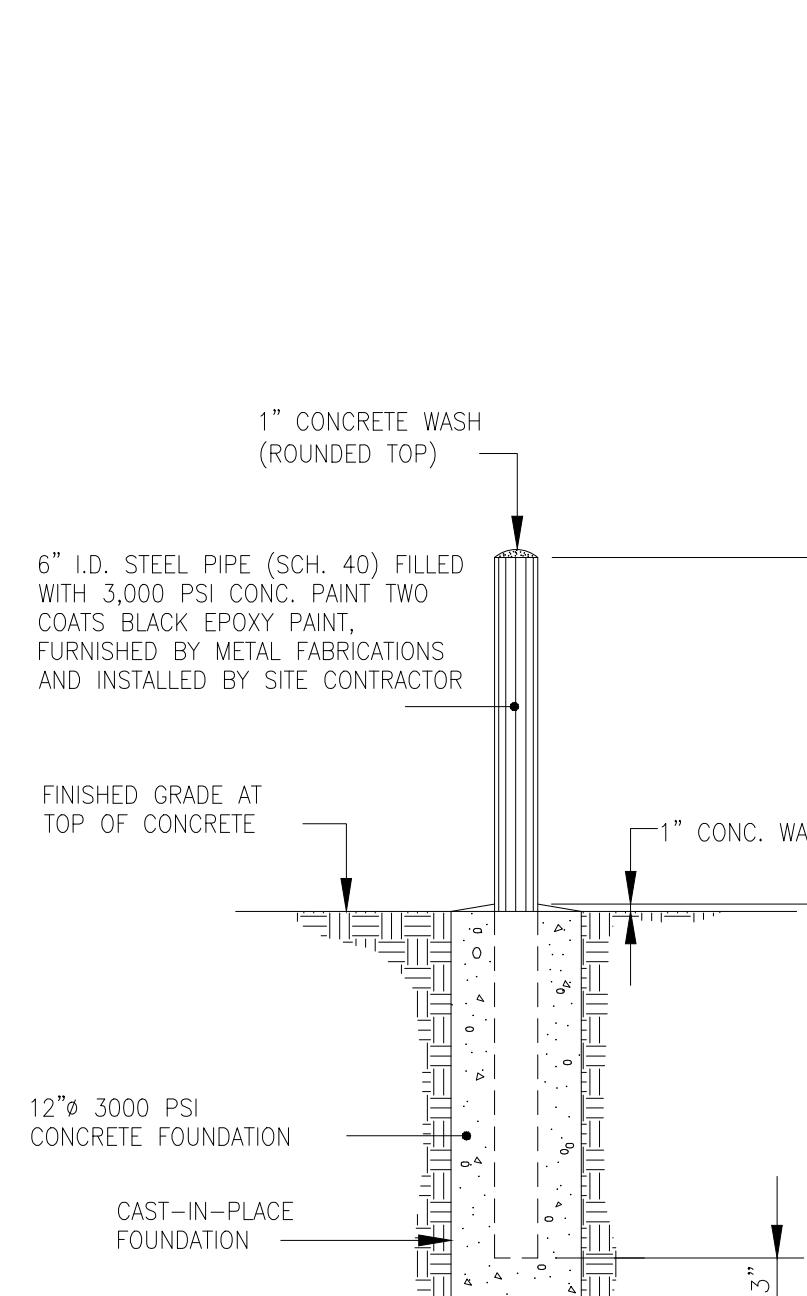
NOTES:  
1. WHERE STALLS ABUT SIDEWALK, PARKING SIGNS SHOULD BE PLACED AT BACK EDGE OF SIDEWALK.  
2. STRIPING SHOULD BE WHITE IN COLOR

NOTES:  
1. TOP SURFACE TO BE DRESSED BY SAW OR TOOL  
2. GRANITE CURB SHALL CONFORM TO M.H.D. STD. SPECIFICATION MATERIALS SECTION M9.04.1 GRANITE CURB, TYPE VAA.

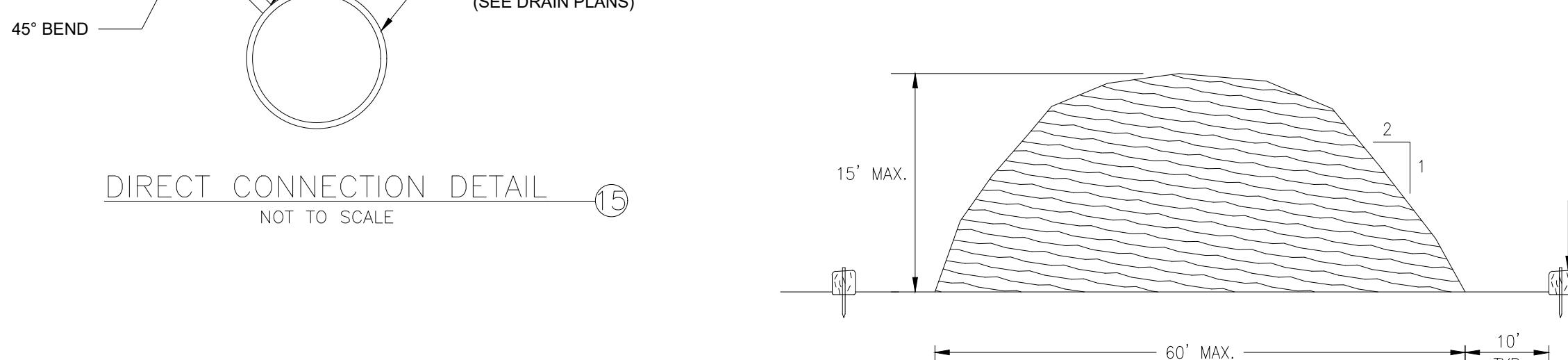
6' GRANITE TRANSITION CURB  
NOT TO SCALE



DIRECT CONNECTION DETAIL  
NOT TO SCALE

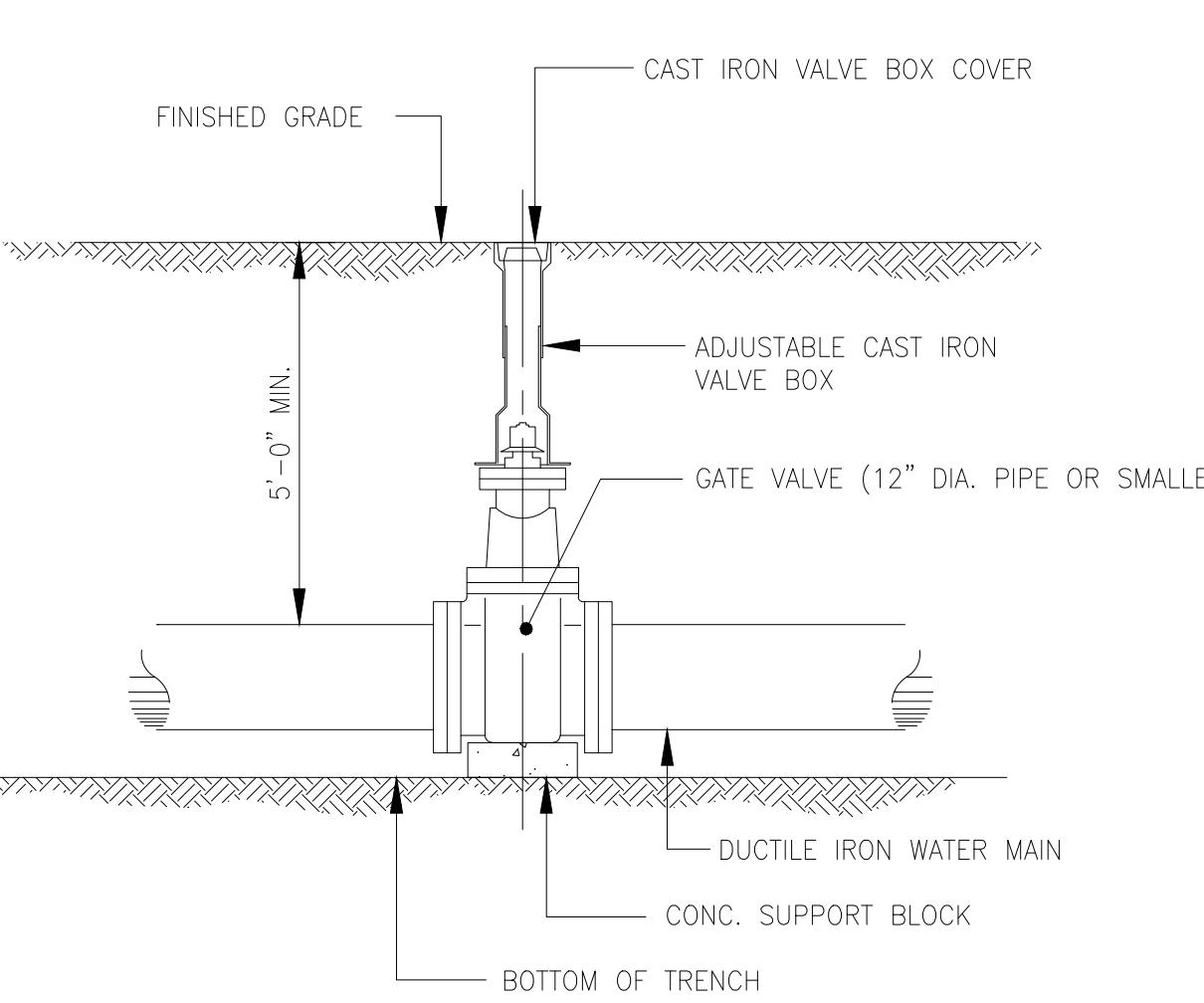


CONCRETE BOLLARD  
NOT TO SCALE

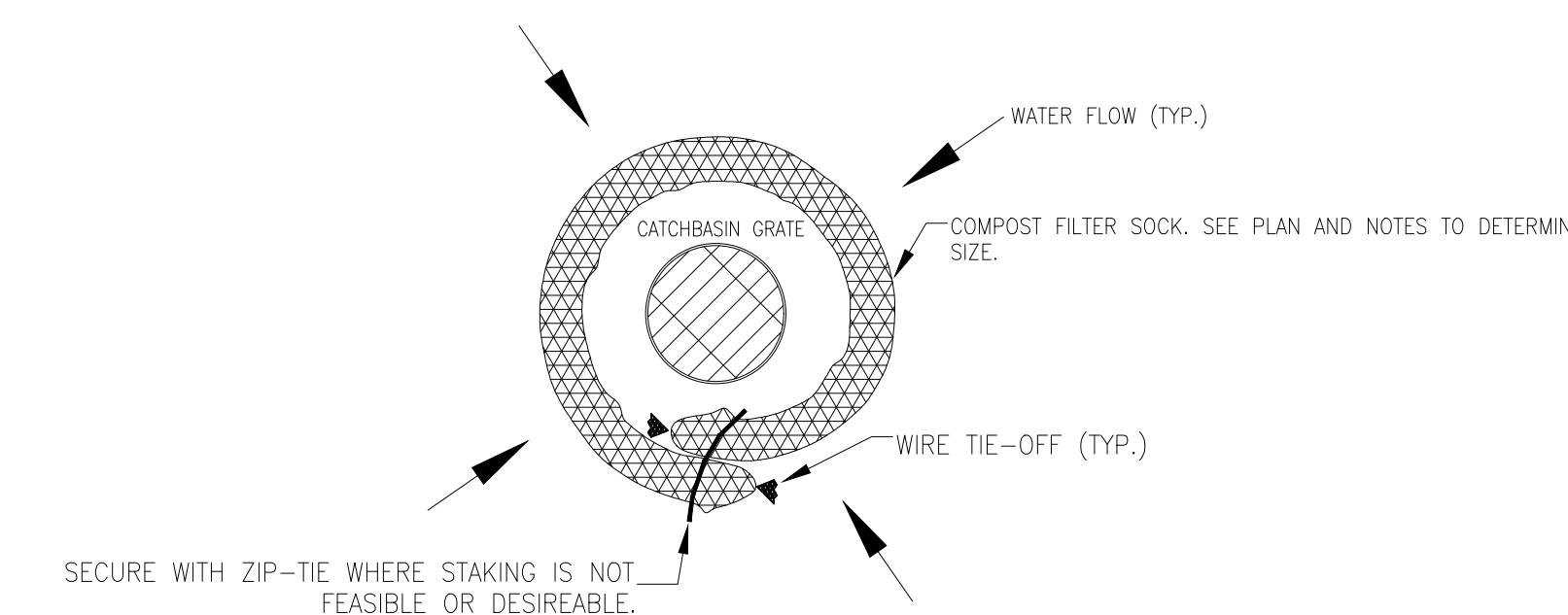


ERODIBLE MATERIAL STOCKPILE  
NOT TO SCALE

NOTE:  
ANY MANUFACTURER'S NAMES AND/OR MODEL NUMBERS IDENTIFIED HEREIN ARE INTENDED TO ASSIST IN ESTABLISHING A GENERAL LEVEL OF QUALITY, CONFIGURATION, FUNCTIONALITY, AND APPEARANCE REQUIRED. THIS IS NOT A PROPRIETARY SPECIFICATION AND IT SHOULD BE NOTED THAT "OR APPROVED EQUIVALENT" APPLIES TO ALL PRODUCTS DENOTED HEREIN. IT IS UNDERSTOOD THAT ALL MANUFACTURERS WILL HAVE MINOR VARIATIONS IN CONFIGURATION, APPEARANCE, AND PRODUCT SPECIFICATION TO ENCOURAGE OPEN AND COMPETITIVE INVOLVEMENT FROM MULTIPLE MANUFACTURERS THAT ARE ABLE TO SUPPLY SIMILAR PRODUCTS.

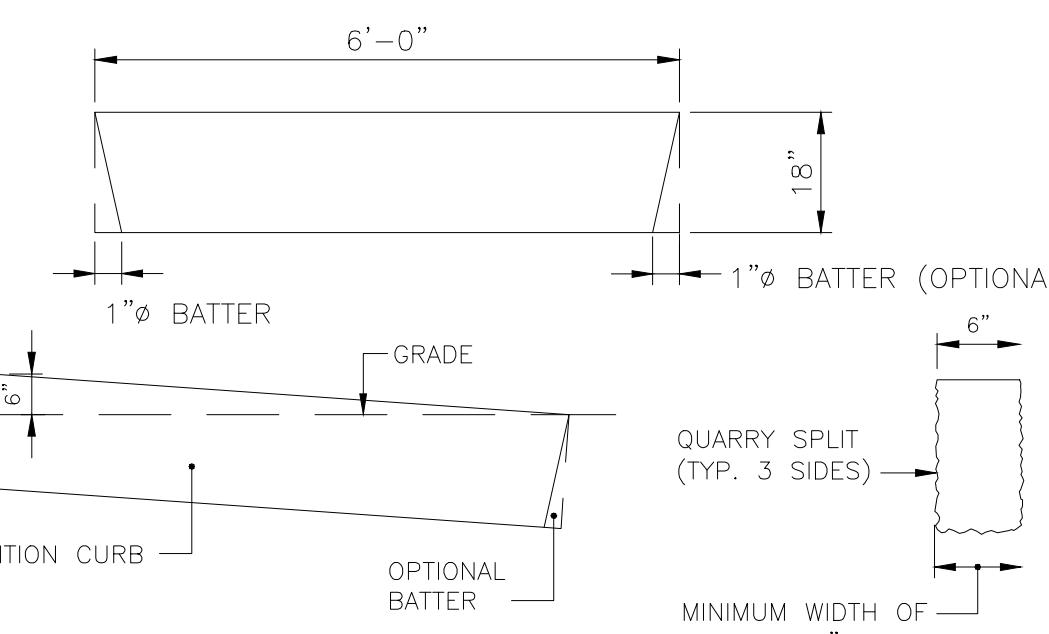


VALVE BOX  
NOT TO SCALE



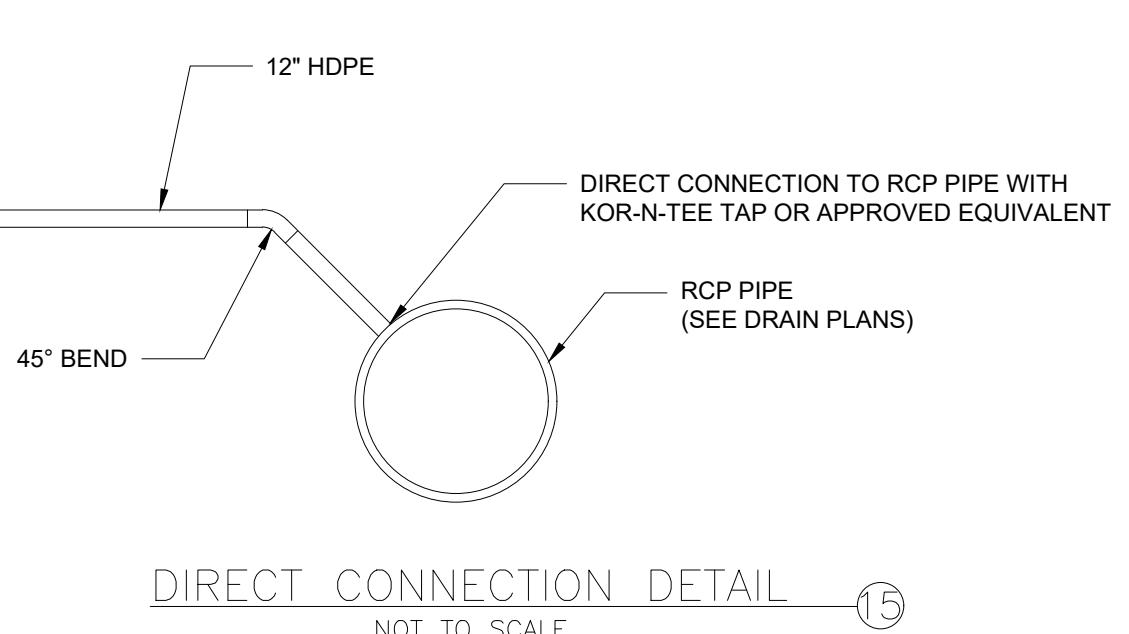
NOTES:  
1. OVERLAP ENDS OF SOCK PER MANUFACTURERS RECOMMENDATIONS - ONE FOOT MINIMUM, 3 FEET MAXIMUM.  
2. USE 8"-12" Dia. SOCK IN CURBSIDE OR TRAFFIC AREA.  
3. USE 12"-18" Dia. SOCK IN NON-TRAFFIC AREA.  
4. INSPECT AND MAINTAIN THROUGHOUT CONSTRUCTION.  
5. SOCK AND COMPOST MATERIAL TO BE REMOVED FROM SITE WHEN CONSTRUCTION IS COMPLETE.

INLET PROTECTION  
NOT TO SCALE

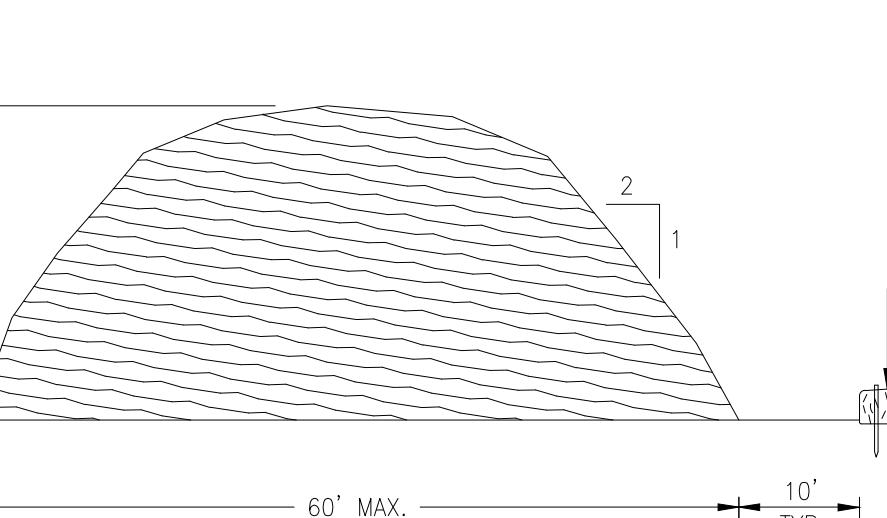


NOTES:  
1. TOP SURFACE TO BE DRESSED BY SAW OR TOOL  
2. GRANITE CURB SHALL CONFORM TO M.H.D. STD. SPECIFICATION MATERIALS SECTION M9.04.1 GRANITE CURB, TYPE VAA.

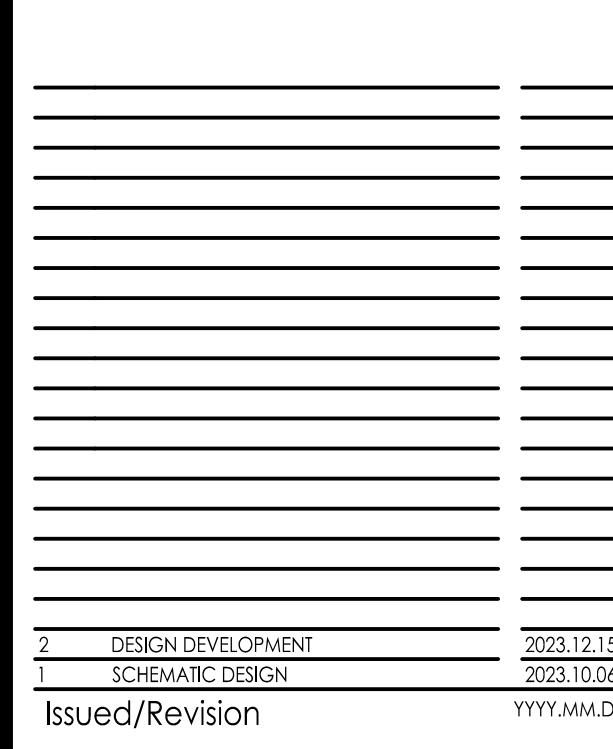
6' GRANITE TRANSITION CURB  
NOT TO SCALE



NOTES:  
1. SEE LANDSCAPE PLANS FOR DECORATIVE BOLLARDS.  
2. SITE CONTRACTOR IS RESPONSIBLE FOR INSTALLING CONCRETE BOLLARDS.



ERODIBLE MATERIAL STOCKPILE  
NOT TO SCALE



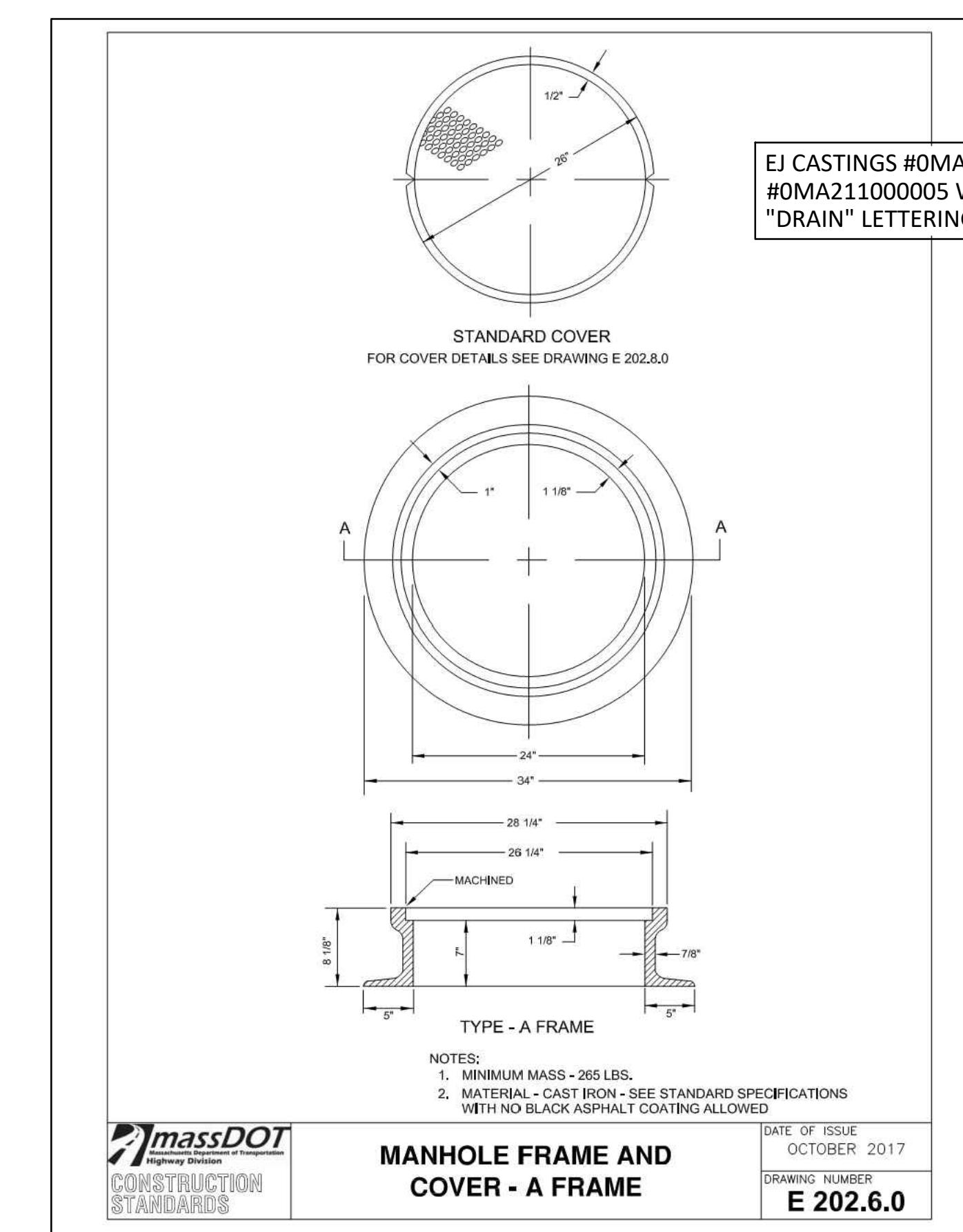
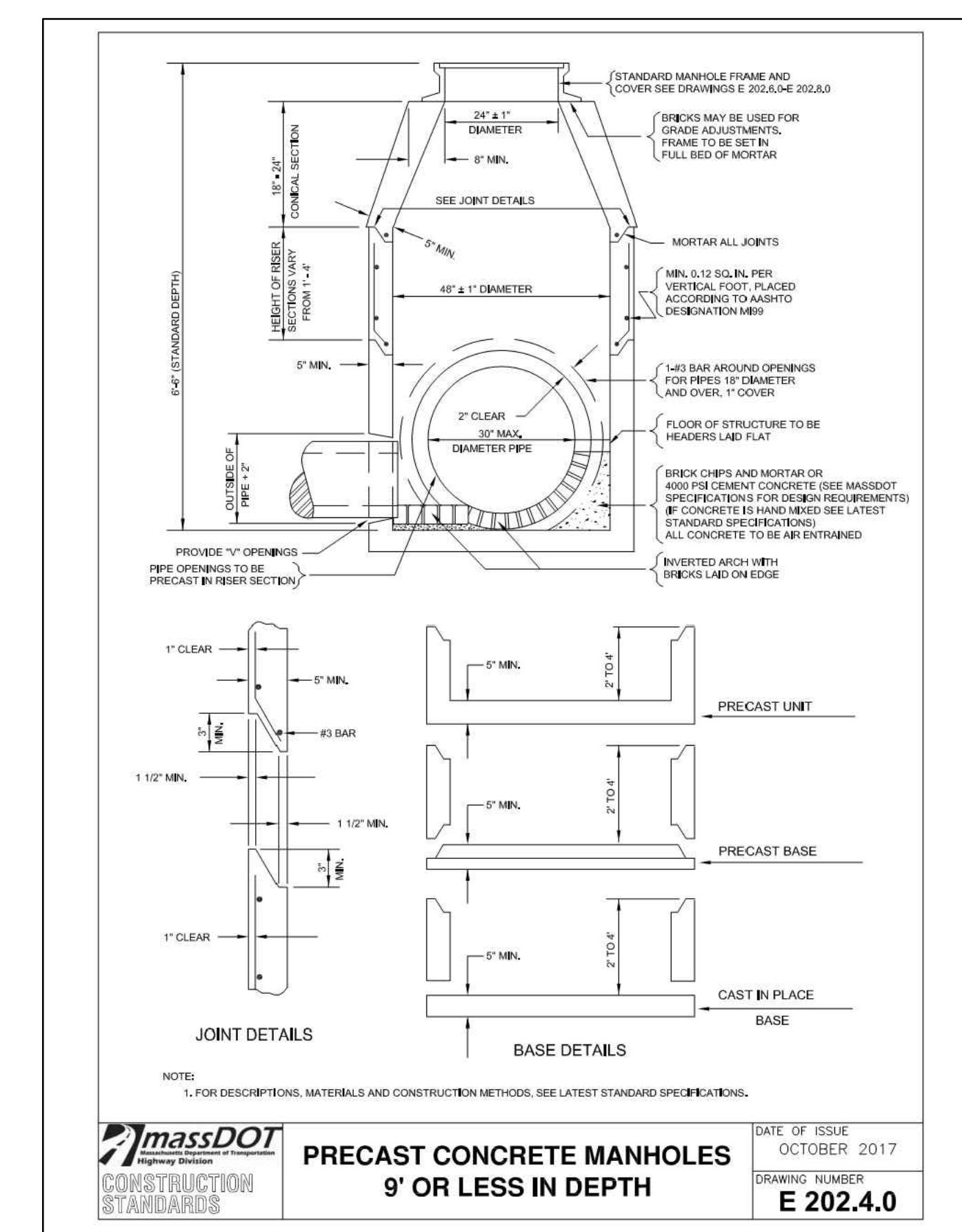
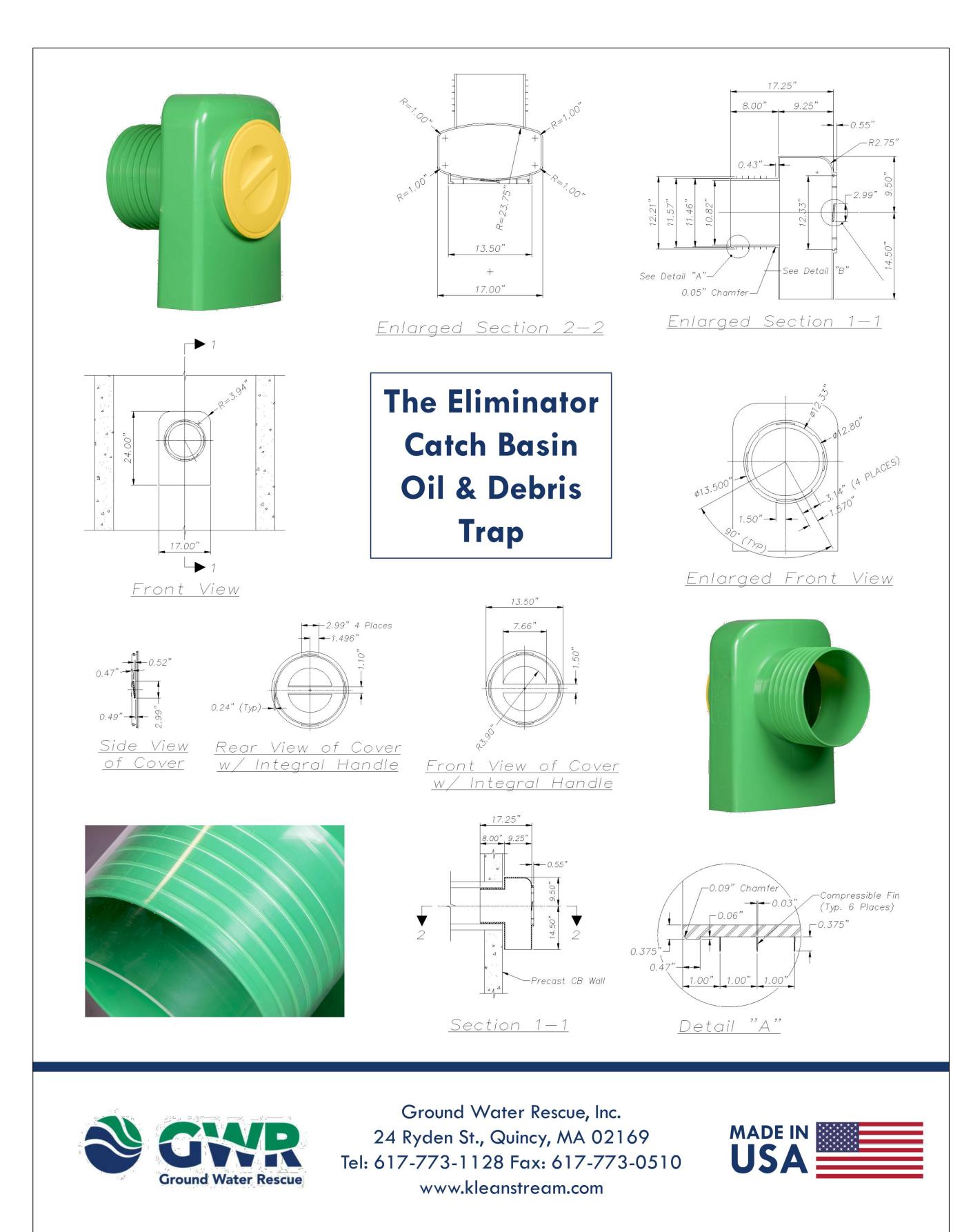
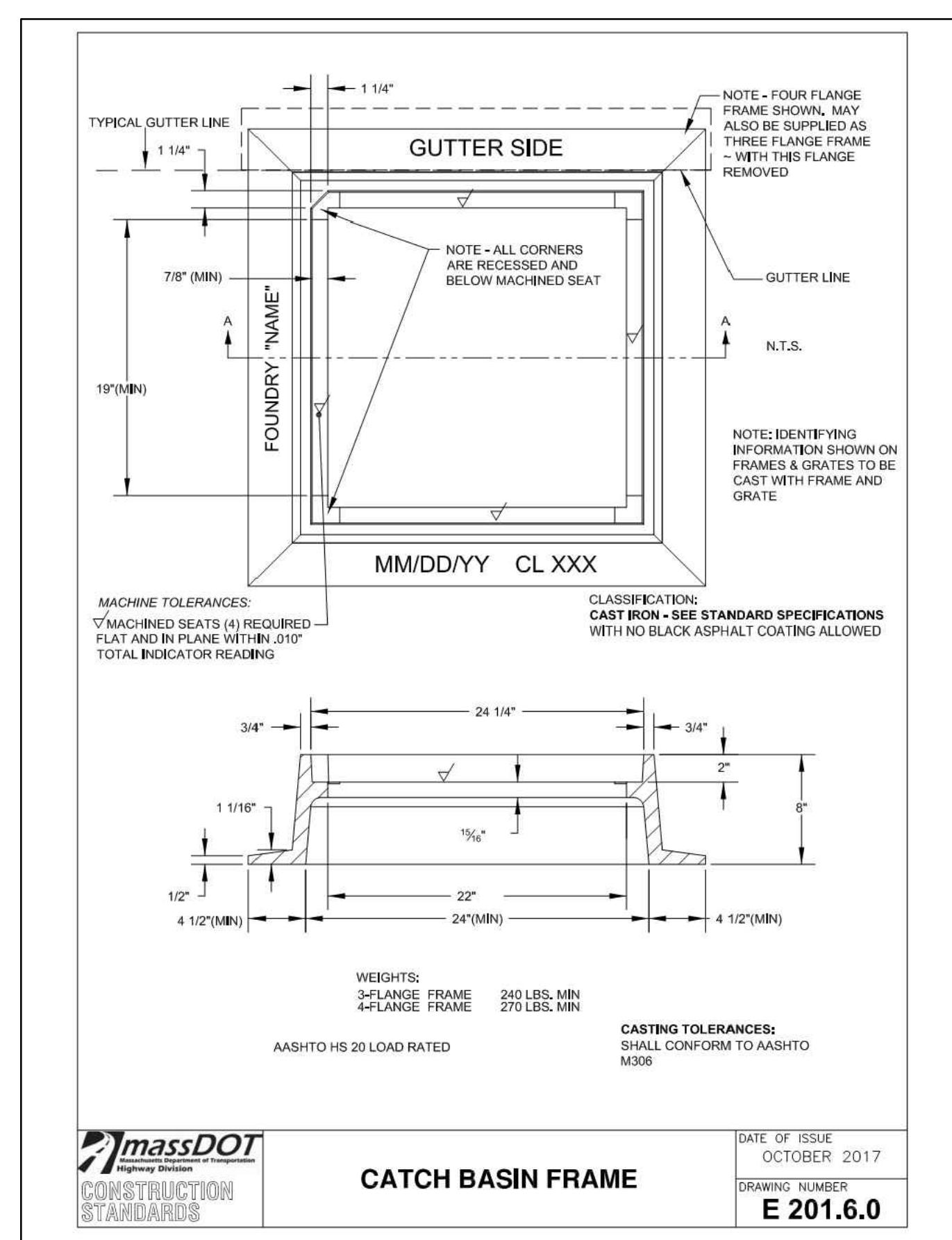
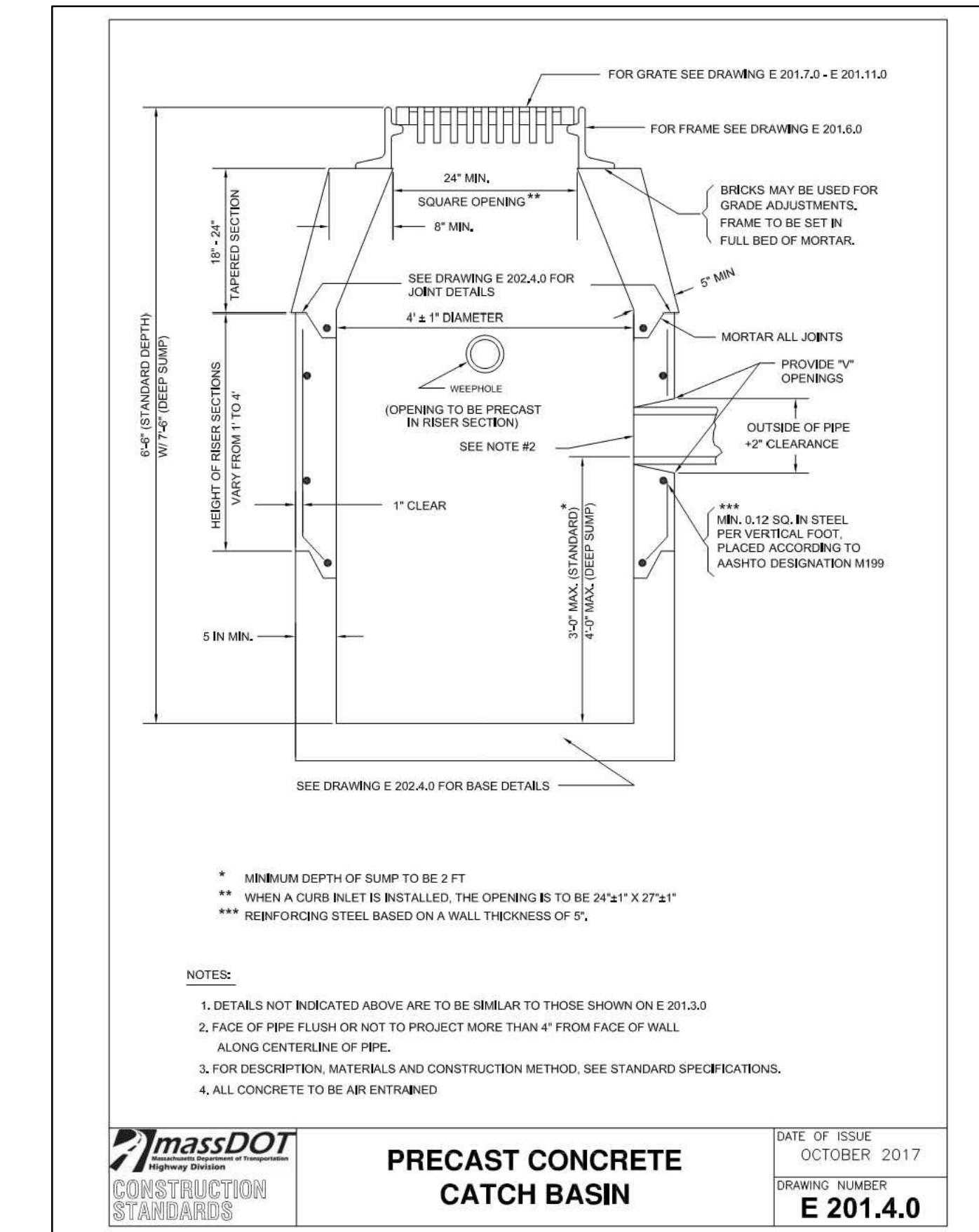
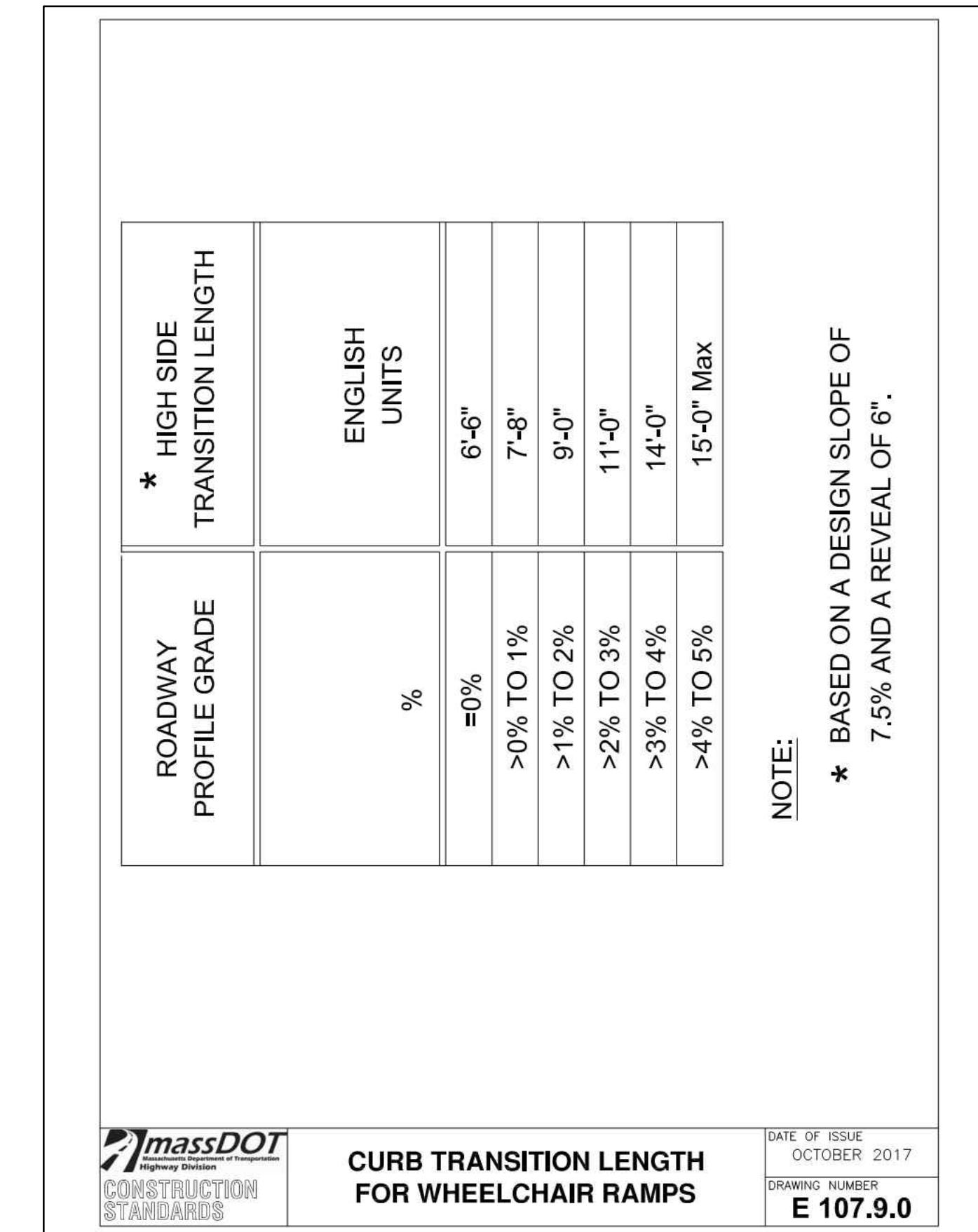
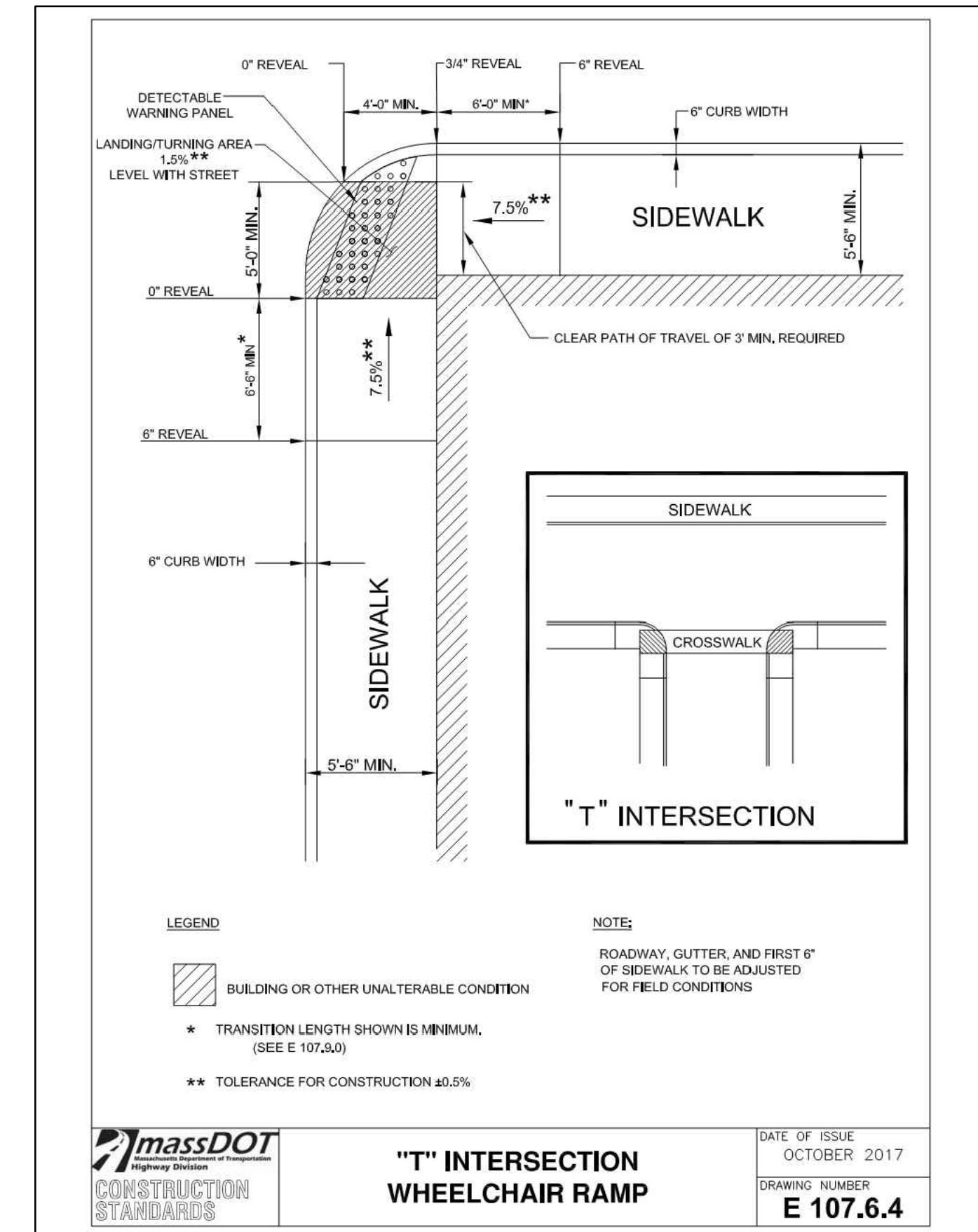
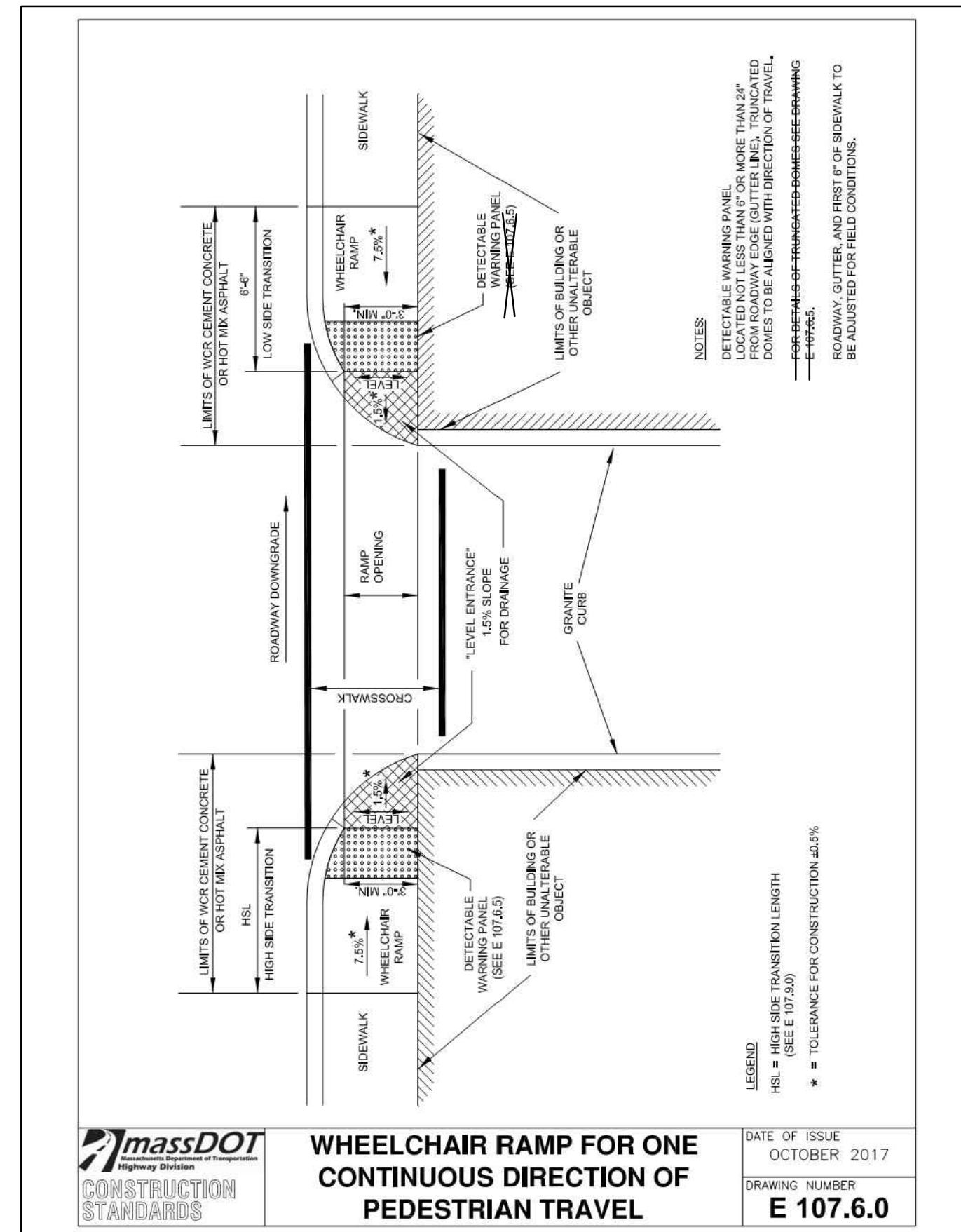
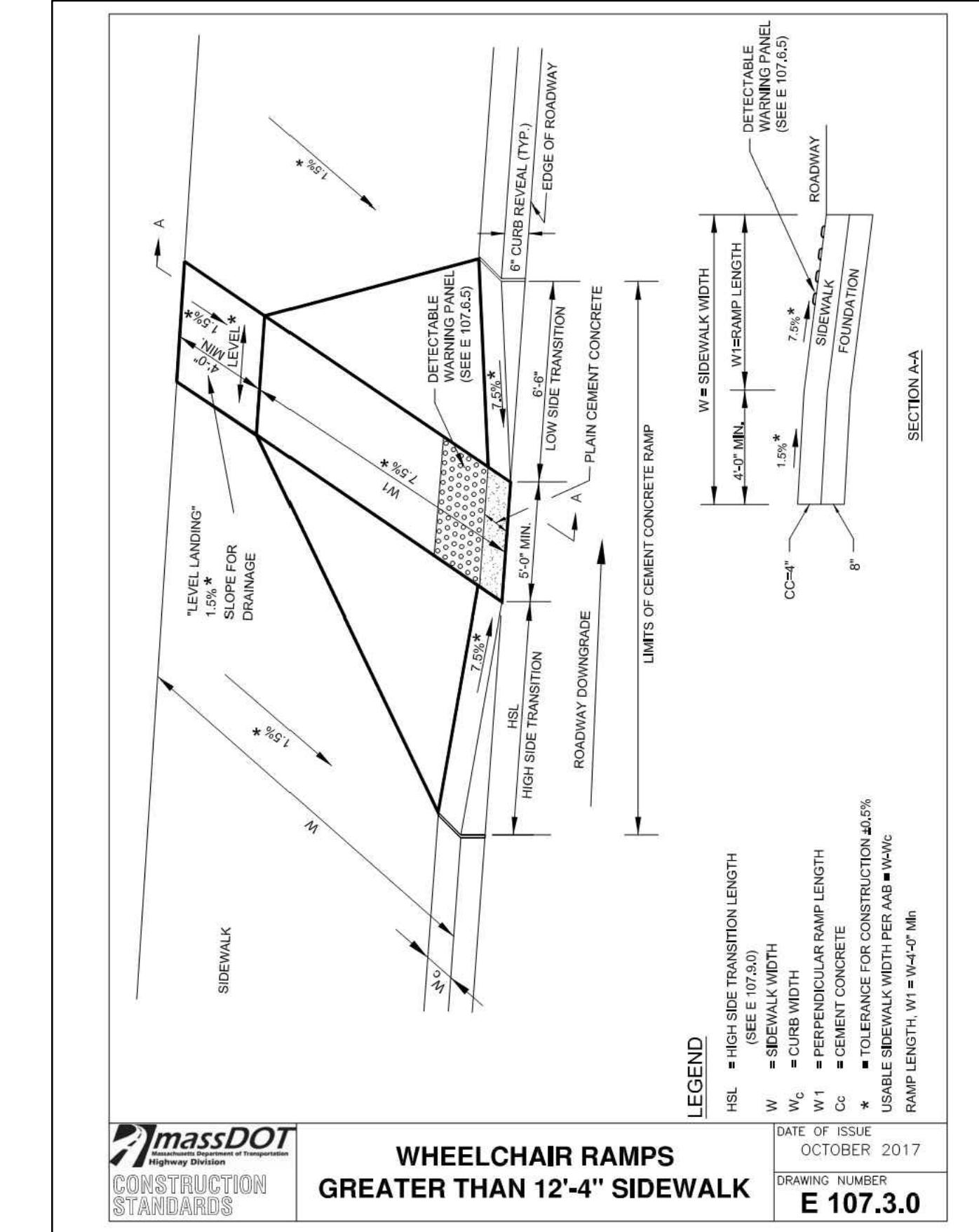
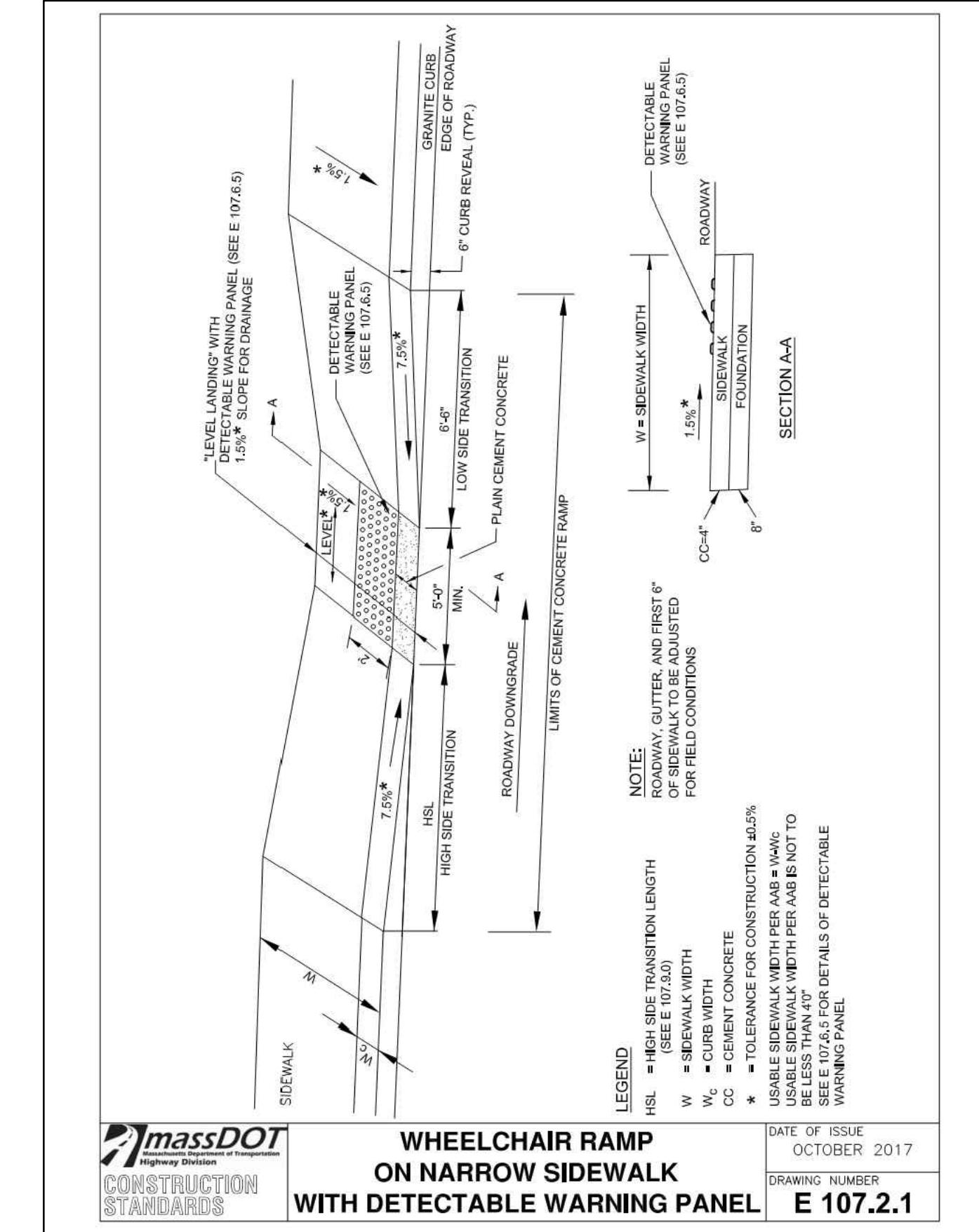
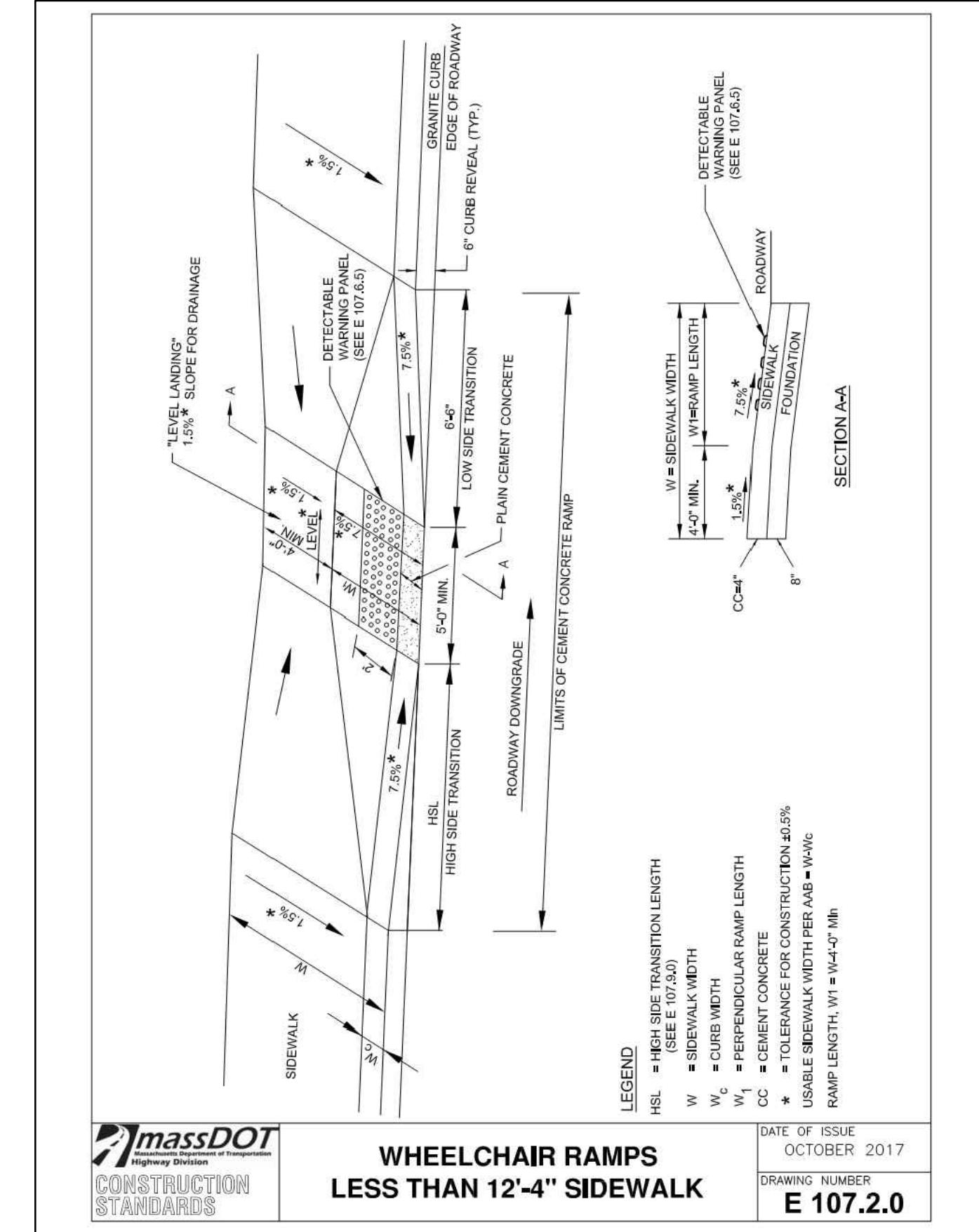
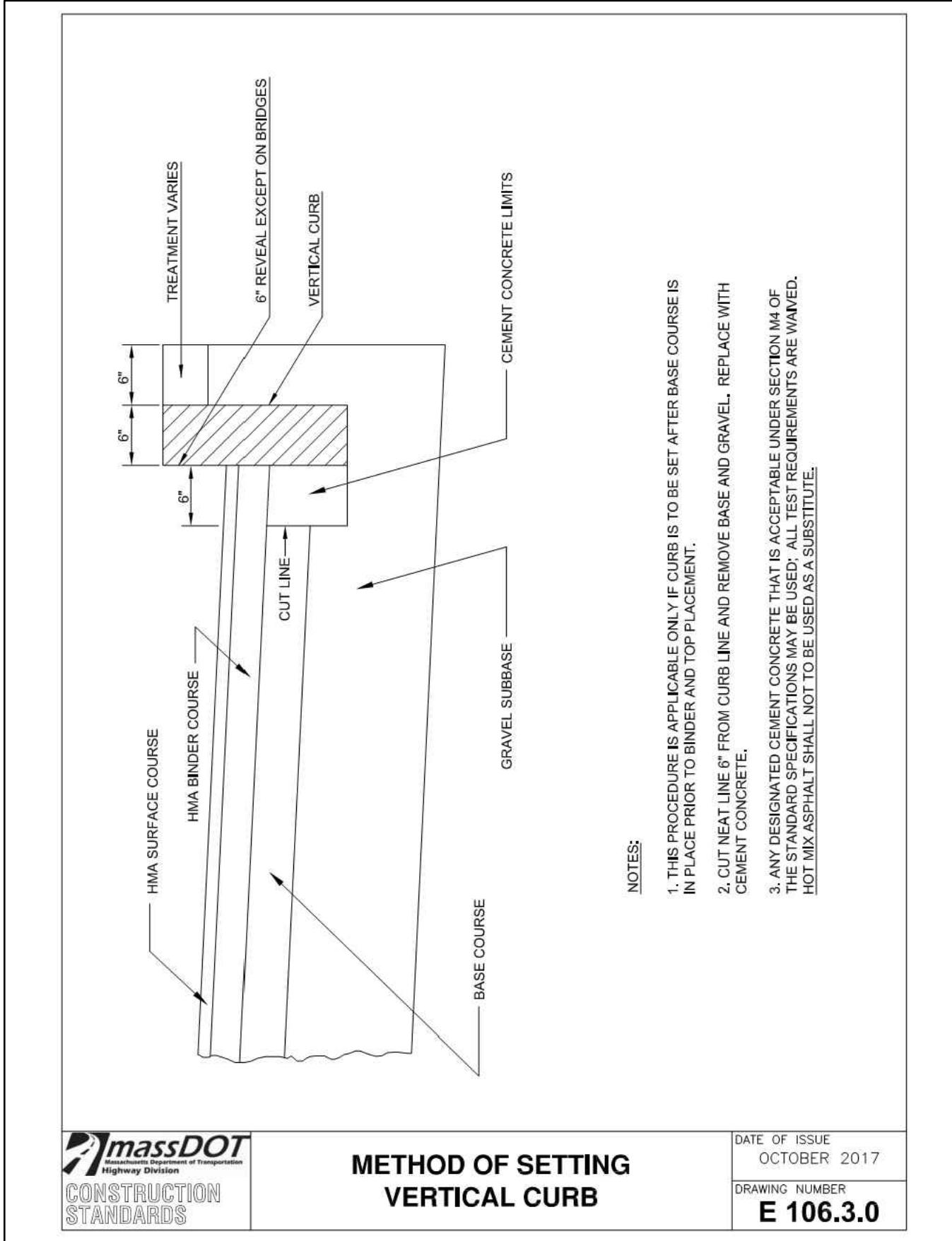
PRELIMINARY  
NOT FOR  
CONSTRUCTION

Scale AS NOTED  
Project No. 78000  
Site Details 1

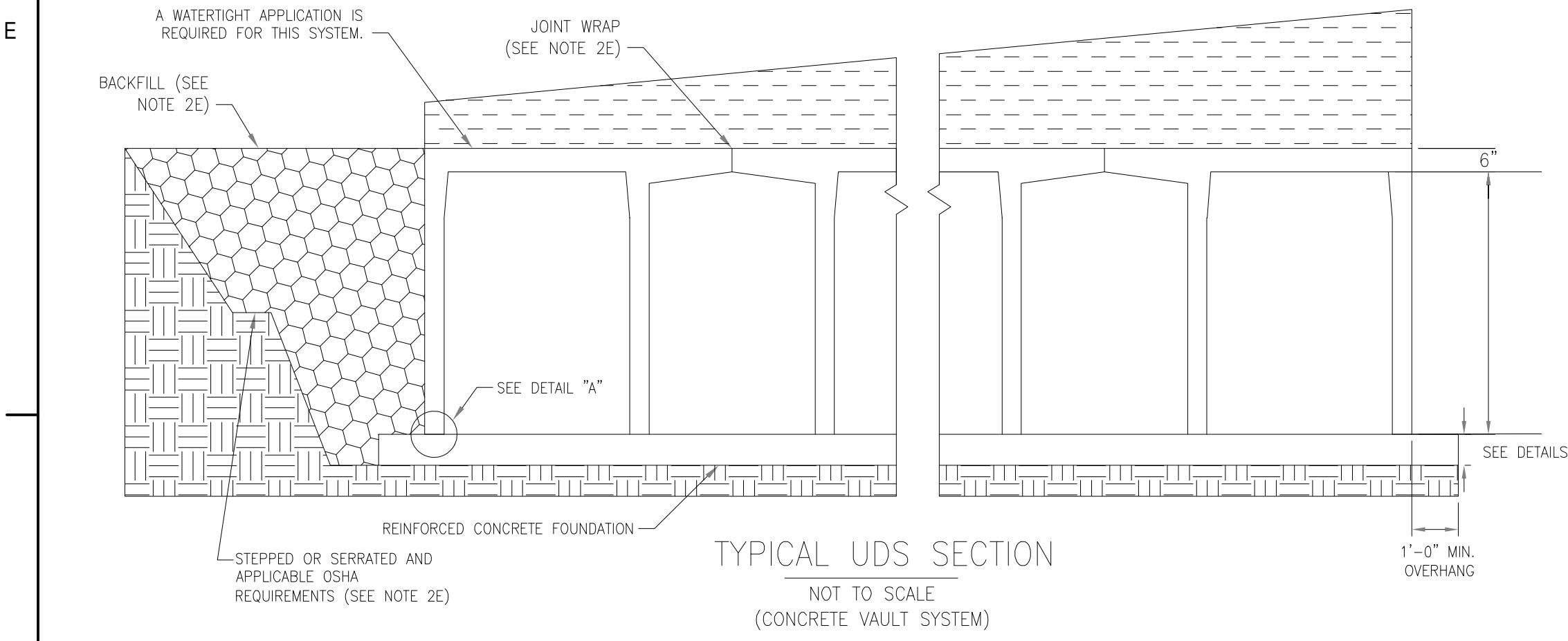
2023.12.15  
2023.12.06  
Issued/Revision  
Permit/Seal

C6.1

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Copyright. 2023 The Vector Company, Inc.



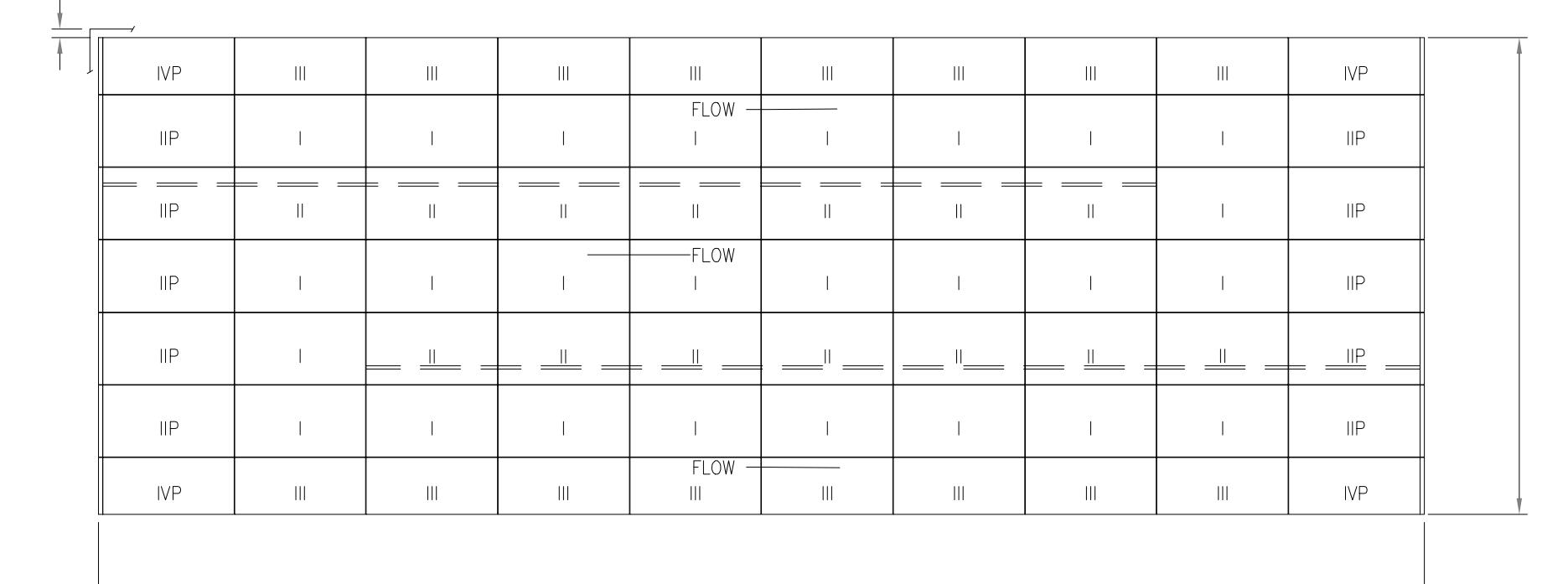
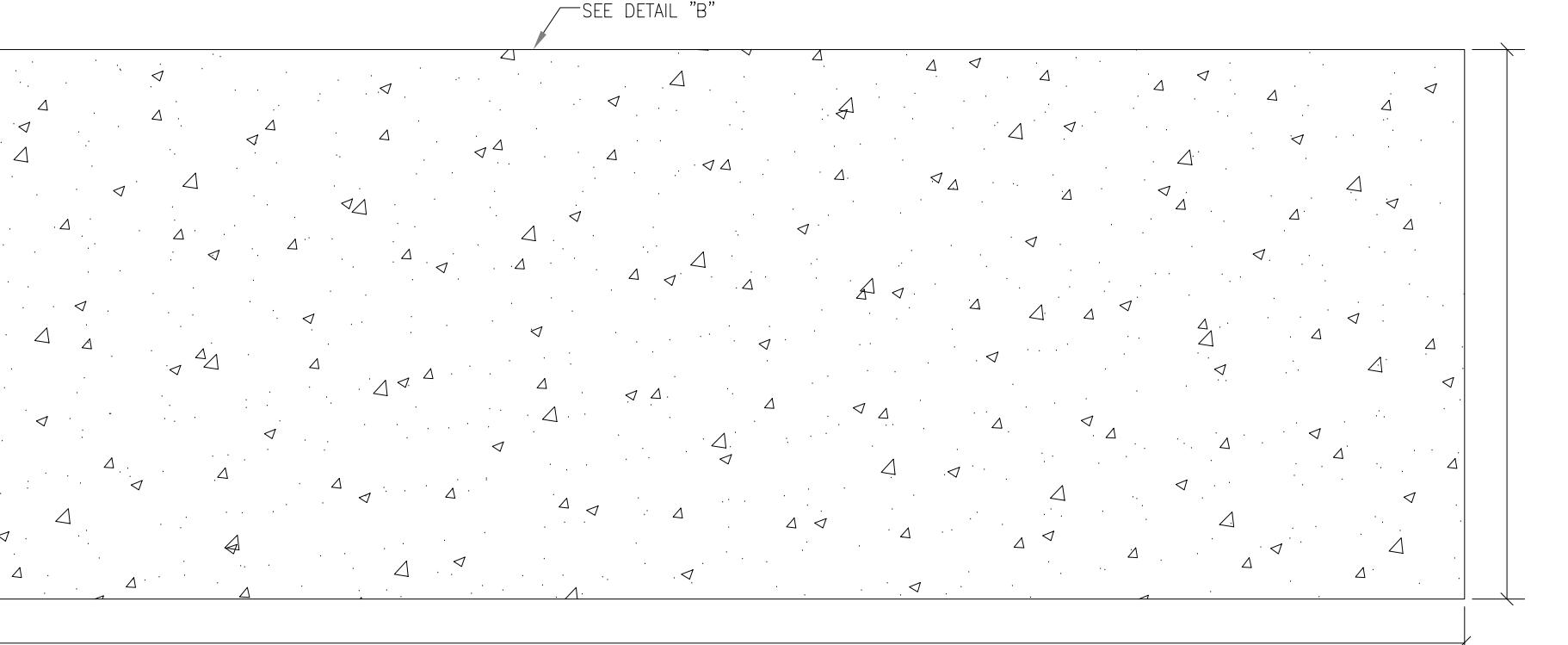



**SYSTEM SPECIFICATION**

- MANUFACTURER SHALL BE STORMTRAP, LLC, UNITED CONCRETE PRODUCTS, CONCRETE SYSTEMS INC, OR APPROVED EQUIVALENT.
- CONTRACTOR SHALL SUBMIT MANUFACTURERS SHOP DRAWINGS, INCLUDING PLANS, ELEVATIONS, SECTIONS, AND DETAILS, INDICATING LAYOUT, DIMENSIONS, FOUNDATION, COVER, AND JOINTS; INDICATE SIZE AND LOCATION OF ROOF OPENINGS AND INLET AND OUTLET PIPE OPENINGS.
- CONTRACTOR SHALL SUBMIT DESIGN CALCULATIONS INCLUDING STORMWATER VOLUME SIZING, STRUCTURAL CALCULATIONS, AND BUOYANCY CALCULATIONS.
- TOTAL COVER: MIN. 2.25" MAX. 3.75" CONSULT MANUFACTURER FOR ADDITIONAL COVER OPTIONS.
- THE SYSTEM SHALL BE WATER TIGHT.
- CONCRETE CHAMBER SHALL BE DESIGNED FOR AASHTO HS-20 HIGHWAY LOADING, MIN. SOIL PRESSURE 2000 PSF.
- ALL DIMENSIONS AND SOIL CONDITIONS, INCLUDING BUT NOT LIMITED TO GROUNDBREAKER AND SOIL BEARING CAPACITY ARE TO BE VERIFIED IN THE FIELD BY OTHERS PRIOR TO UNIT INSTALLATION.
- FOR STRUCTURAL CALCULATIONS THE GROUND WATER TABLE SHALL BE ASSUMED TO BE AT ELEVATION 18.62.
- FOR STRUCTURAL CALCULATIONS THE SOIL DENSITY IS ASSUMED TO BE 120 PCF.
- FOR FLOTATION CALCULATIONS THE GROUND WATER TABLE SHALL BE ASSUMED TO BE AT ELEVATION 18.62.
- SYSTEM VOLUME =

**UNDERGROUND CONCRETE VAULT DETENTION SYSTEM (UDS)**

NOT TO SCALE


**TYPICAL UDS LAYOUT**  
 NOT TO SCALE


## NOTES:

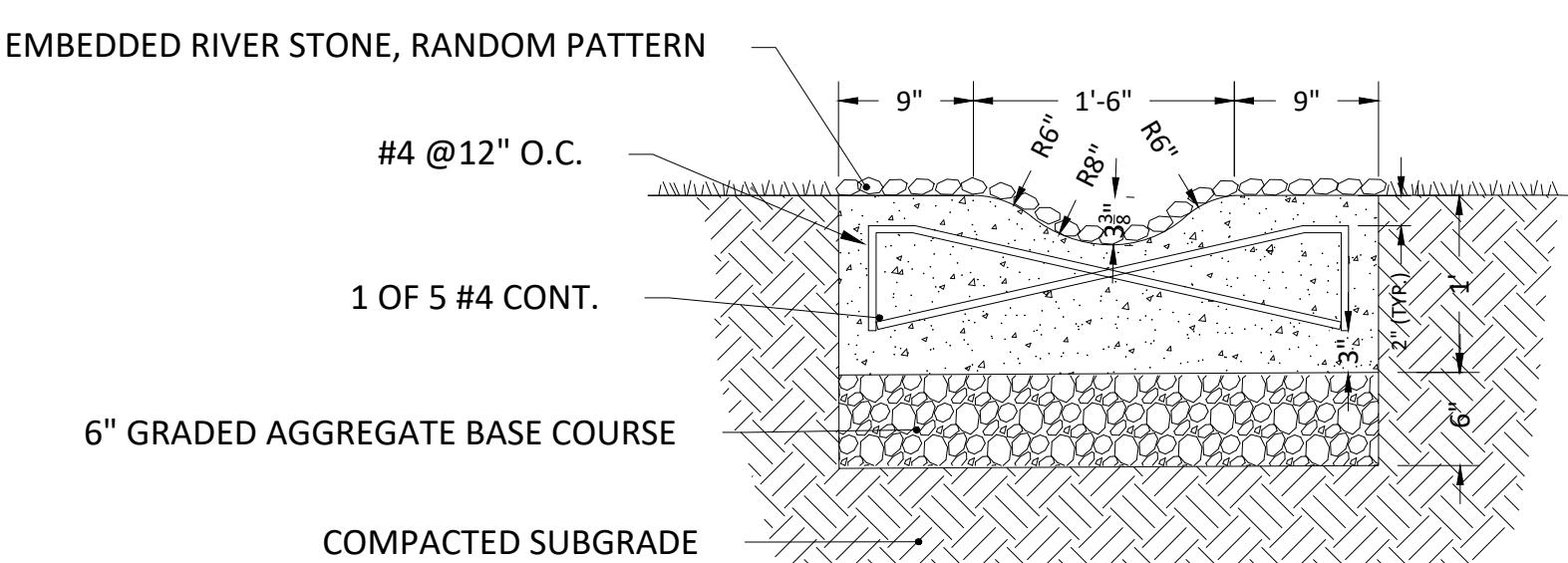
- CONCRETE STRENGTH @ 28 DAYS, 5%-8% ENTRAINED AIR, 4" MAX. SLUMP.
- NET ALLOWABLE SOIL PRESSURE GREATER THAN OR EQUAL TO 2000 PSF.
- SOIL CONDITIONS TO BE VERIFIED ON SITE.
- 1"-0" OVERHANG AROUND EXTERIOR FACE OF UNITS.
- REBAR: ASTM A-615 GRADE 60, BLACK BAR.
- DIMENSION OF FOUNDATION MUST HAVE 1"-0" OVERHANG BEYOND EXTERNAL FACE OF UNITS.
- DIMENSION OF SYSTEM ALLOW FOR A 3/4" GAP BETWEEN EACH UNIT.
- ALL DIMENSIONS TO BE VERIFIED IN THE FIELD.
- THE CONTROL JOINTS CAN BE 16'-0" TO 24'-0" MAX APART.

| MAXIMUM SYSTEM COVER | SLAB THICKNESS | CONCRETE STRENGTH | REINFORCEMENT (BOTH DIRECTIONS) |
|----------------------|----------------|-------------------|---------------------------------|
| 6' - 1"-0"           | 8"             | 4000 psi          | #4 @ 18" o.c.                   |
| >1'-0" - 2'-0"       | 8"             | 4000 psi          | #4 @ 16" o.c.                   |
| >2'-0" - 3'-0"       | 8"             | 4000 psi          | #4 @ 12" o.c.                   |
| >3'-0" - 4'-0"       | 8"             | 4000 psi          | #4 @ 10" o.c.                   |
| >4'-0" - 5'-0"       | 8"             | 4000 psi          | #5 @ 18" o.c.                   |
| >5'-0" - 6'-0"       | 8"             | 4000 psi          | #5 @ 16" o.c.                   |
| >6'-0" - 7'-0"       | 8"             | 4000 psi          | #5 @ 16" o.c.                   |
| >7'-0" - 8'-0"       | 9"             | 4000 psi          | #5 @ 12" o.c.                   |
| >8'-0" - 9'-0"       | 10"            | 4000 psi          | #5 @ 12" o.c.                   |
| >9'-0" - 10'-0"      | 10"            | 4500 psi          | #5 @ 12" o.c.                   |

**TYPICAL UDS FOUNDATION PLAN**

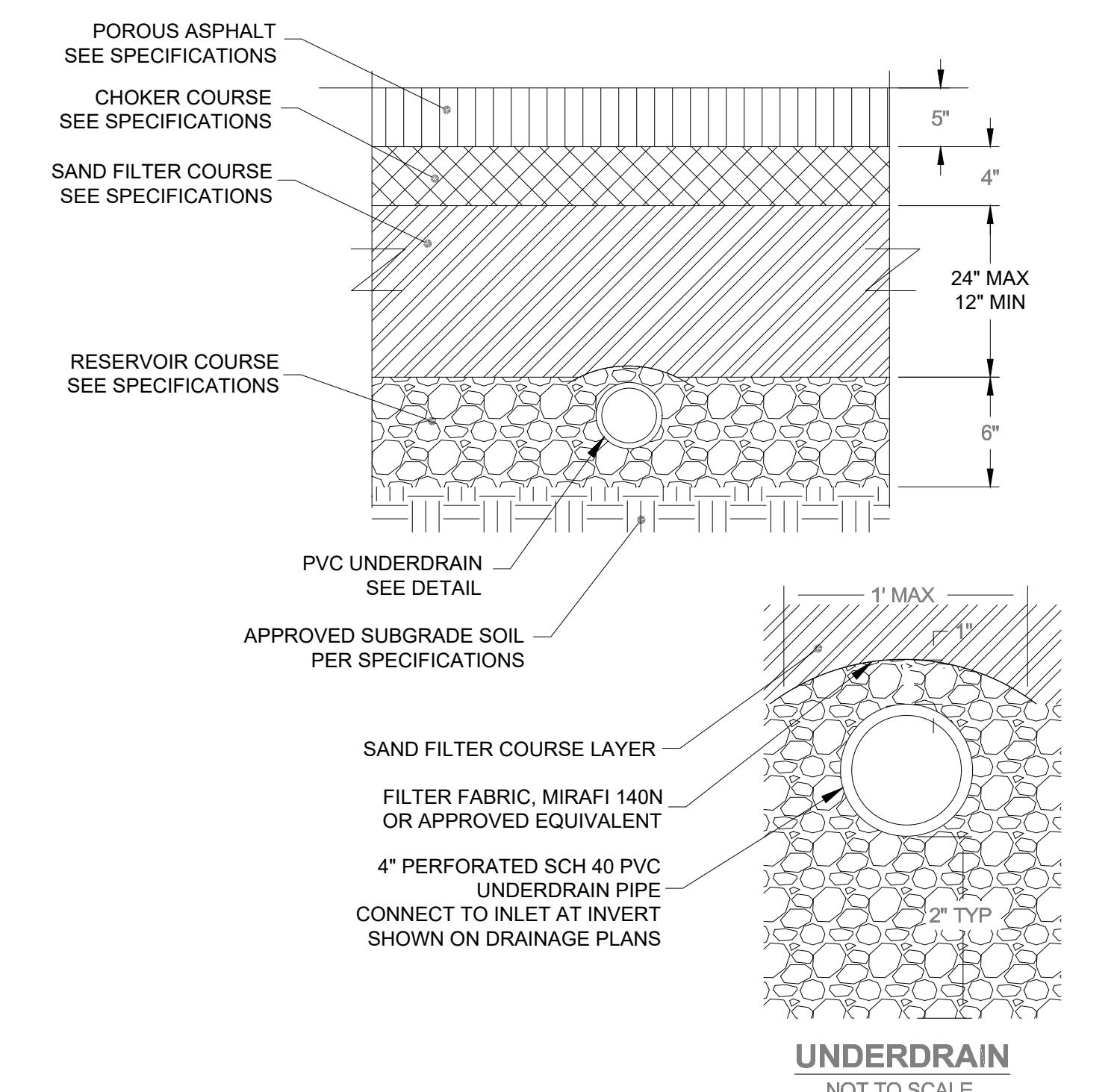
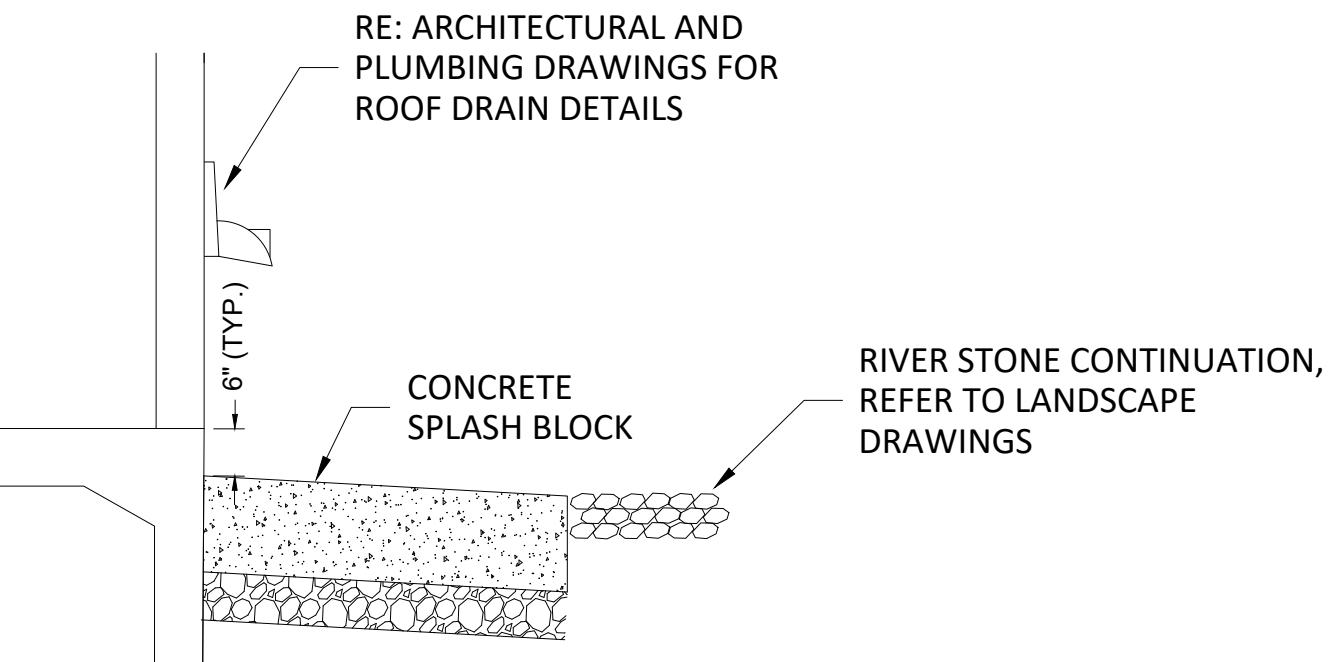
NOT TO SCALE

(CONCRETE VAULT SYSTEM)

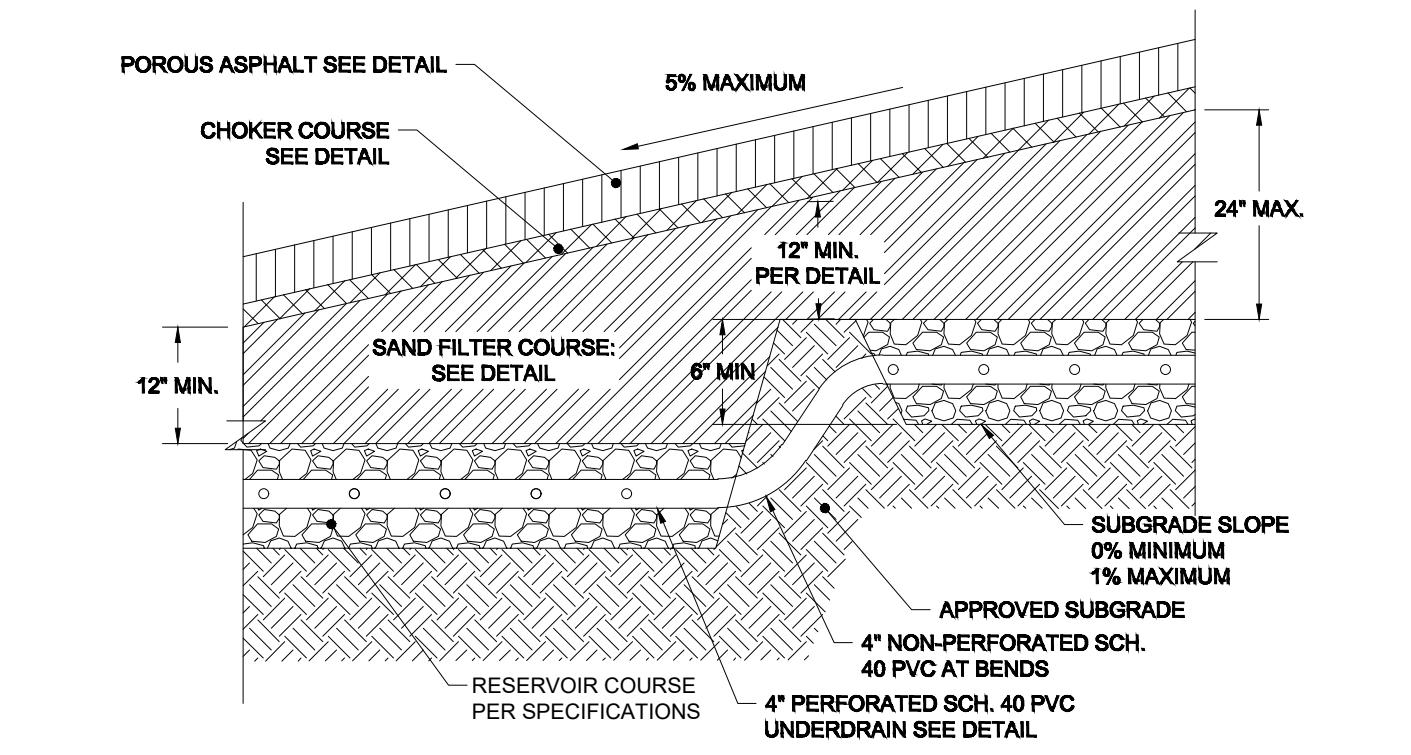

**CONCRETE SPLASH BLOCK**

NOT TO SCALE

\*NOTE: CONTRACTOR SHALL SUBMIT MOCKUP OF SPLASH BLOCK FOR APPROVAL BY THE LANDSCAPE ARCHITECT


**TYPICAL POROUS ASPHALT CROSS-SECTION**

NOT TO SCALE


**POROUS ASPHALT SUBBASE & UNDERDRAIN**

NOT TO SCALE

**PRELIMINARY  
NOT FOR  
CONSTRUCTION**

 Scale AS NOTED  
 Project No. 78000

SITE DETAILS 5

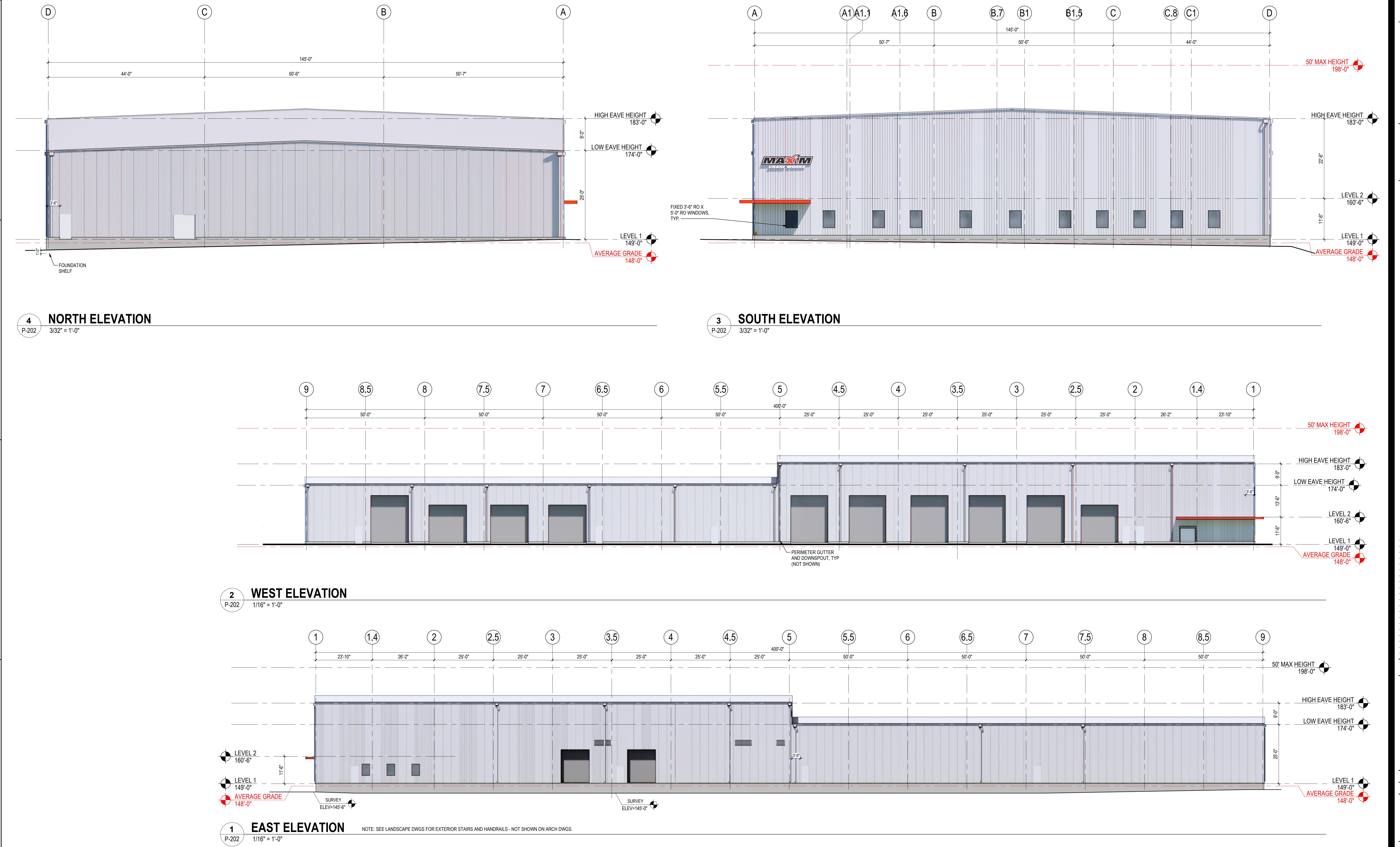
**NOTE:**  
 ANY MANUFACTURER'S NAMES AND/OR MODEL NUMBERS IDENTIFIED HEREIN ARE INTENDED TO ASSIST IN ESTABLISHING A GENERAL LEVEL OF QUALITY, CONFIGURATION, FUNCTIONALITY, AND APPEARANCE REQUIRED. THIS IS NOT A PROPRIETARY SPECIFICATION AND IT SHOULD BE NOTED THAT "OR APPROVED EQUIVALENT" APPLIES TO ALL PRODUCTS DENOTED HEREIN. IT IS UNDERSTOOD THAT ALL MANUFACTURERS WILL HAVE MINOR VARIATIONS IN CONFIGURATION, APPEARANCE, AND PRODUCT SPECIFICATION TO ENCOURAGE OPEN AND COMPETITIVE INVOLVEMENT FROM MULTIPLE MANUFACTURERS THAT ARE ABLE TO SUPPLY SIMILAR PRODUCTS.

**C6.5**

## MATERIAL LEGEND

**INSULATED METAL PANEL - REGAL GRAY  
BOD: METL-SPAN CF FLUTE PROFILE PANELS (42" WIDTH)**

**INSULATED METAL PANEL - REGAL GRAY  
BOD: METL-SPAN CF LIGHT MESA PROFILE PANELS (42" WIDTH)**



c Architecture and Engineering P.C.  
ter Street  
, MA 02109  
(7) 234-3100  
[tantec.com](http://tantec.com)

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
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# **PRELIMINARY NOT FOR CONSTRUCTION**

As indicated  
218421418

# EXTERIOR ELEVATIONS FIGURE A

P-202



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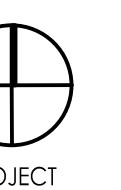
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Consultant

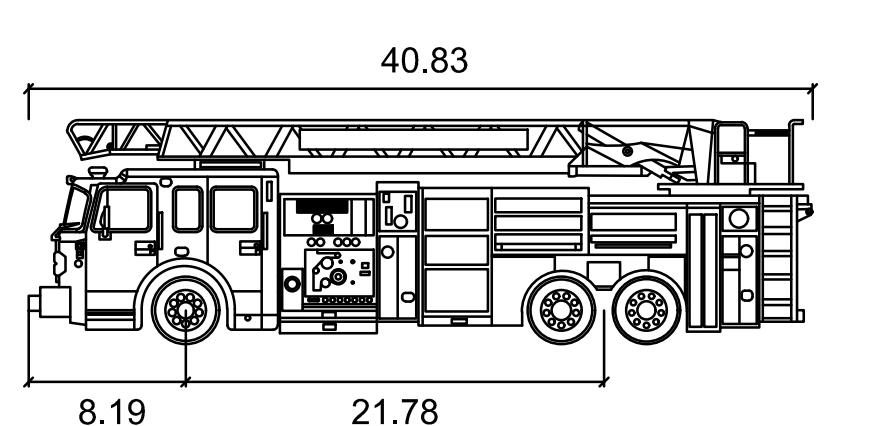
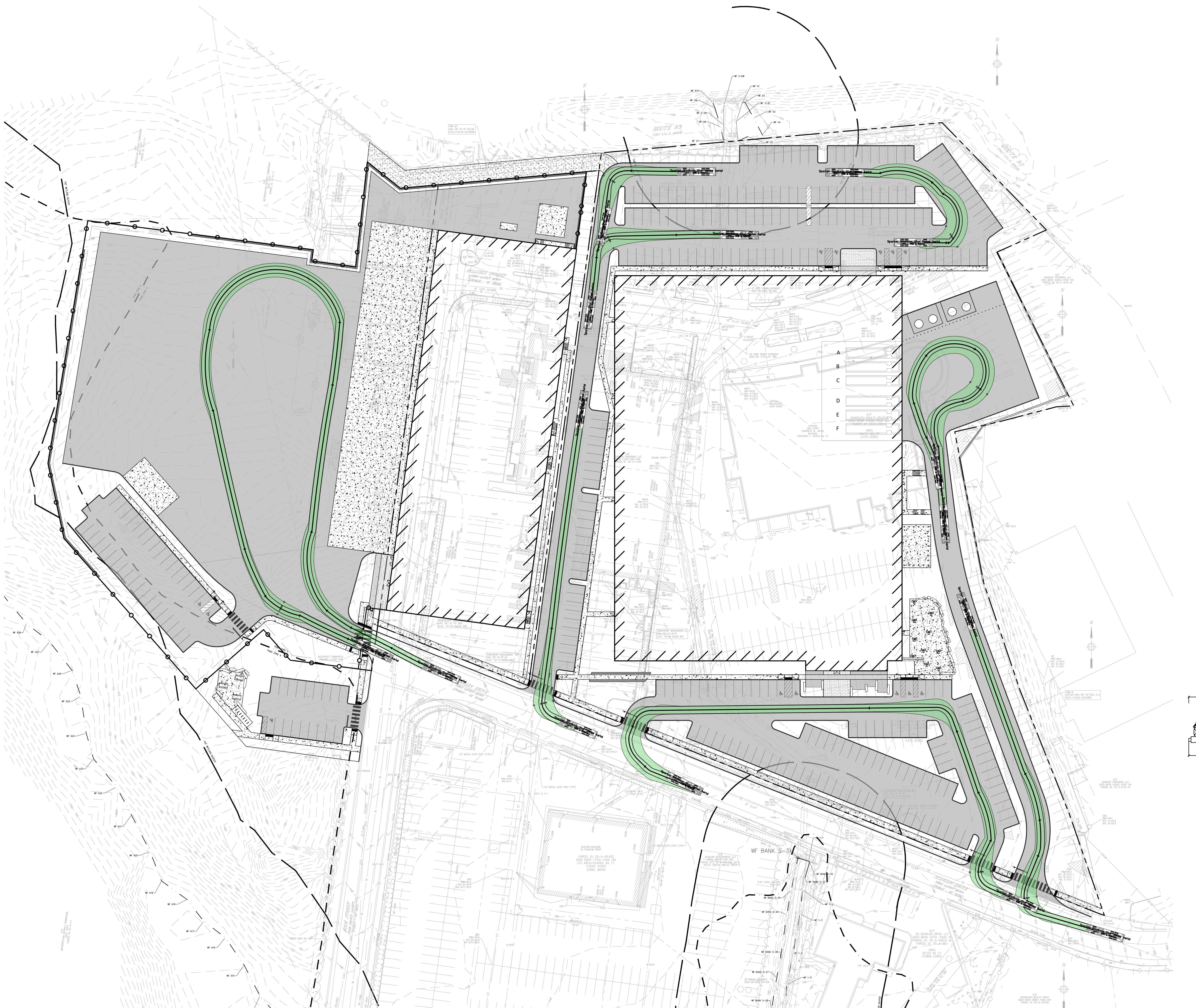
**VERTEX**  
 The Vertex Companies, LLC.  
 400 Libbey Parkway  
 Weymouth, MA 02189  
 PHONE 781.952.6000  
[www.vertexeng.com](http://www.vertexeng.com)

**CORE**  
 INVESTMENTS, INC.

Key Plan



Notes



Spartan Gladiator Star Series Aerial  
feet  
Width : 8.25  
Track : 7.87  
Lock to Lock Time : 6.0  
Steering Angle : 46.3

2 DESIGN DEVELOPMENT  
2023.12.15  
Schematic Design  
2023.10.06  
Issued/Revision  
YMMJAHZD

Permit/Seal

**PRELIMINARY  
NOT FOR  
CONSTRUCTION**

Scale AS NOTED  
Project No. 78000

FIRE TRUCK EXHIBIT

0' 40' 80' 120'  
SCALE: 1" = 40'

**E3.0**

RANDOLPH, MASSACHUSETTS

# Randolph North Redevelopment

## Traffic Impact Study

Prepared for  
**Town of Randolph**

Prepared by  
**Howard Stein Hudson**

Prepared on Behalf of  
**Core Investments Development, Inc**

**December 2023**



**HOWARD STEIN HUDSON**

Engineers + Planners



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Appendix A – Traffic Count Data

Appendix B – MassDOT Seasonal Factors

Appendix C – Crash Data and Worksheets

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# Executive Summary

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This Traffic Impact Study (TIS) presents the comprehensive transportation evaluation completed by **Howard Stein Hudson (HSH)** for the proposed Project, Randolph North Development, located on Scanlon Drive in Randolph, Massachusetts. The study was completed in conformance with the Massachusetts Department of Transportation's (MassDOT's) *Transportation Impact Assessment (TIA) Guidelines*. The study analyzes existing conditions within the Project study area, as well as conditions forecast to be in place under the seven-year planning horizon of 2030.

The site is currently occupied by a two-event venue building, and three parking lots totaling 747 spaces. The Project will consist of demolition of existing venue buildings and construction of two new buildings, one supporting a crane operations tenant that will feature a laydown area to the west of High Street, and another building primarily housing the cGMP uses. Overall, the Project consists of constructing 68,000 square feet (sf) of general office space, 22,000 sf of warehousing space, 75,000 sf of research and development space, and 110,000 sf of cGMP space (Laboratory/current Good Manufacturing Practice) with 326 parking spaces across the development.

Designated loading/service areas for the cGMP building are located at the north edge of the site with parking located at the frontage along Scanlon Drive. The site will also construct a new trailhead and parking lot for the Department of Conservation and Recreation's (DCR's) Blue Hills Reservation near the intersection of High Street and Scanlon Street with approximately 18 parking spaces.

The transportation analysis employed mode use data for the area surrounding the Project site based on U.S. Census data and identifies the number of trips expected to be generated by the Project by mode (walk, bicycle, transit, and vehicle). The Project is expected to generate approximately 242 new vehicle trips, 24 new transit trips, and 6 new walk/bicycle trips during the weekday a.m. peak hour, and 241 new vehicle trips, 23 new transit trips, and 6 new walk/bicycle trips during the weekday p.m. peak hour. The Project is expected to see 184 net new trips for the a.m. peak hour and 171 net new trips during the p.m. peak hour compared to the existing conditions.

A detailed traffic operations analysis was conducted for the following intersections:

- Scanlon Drive/North Main Street (signalized);
- Reed Street/High Street (signalized); and
- Scanlon Drive/High Street (unsignalized).

The Project is expected to have minimal impact on traffic operations at the study area intersections.



# Introduction

---

**Howard Stein Hudson (HSH)** has prepared this Traffic Impact Study (TIS) to determine the potential impacts related to Randolph North redevelopment project (the Project) in Randolph, Massachusetts. The Project consists of constructing approximately 68,000 square feet (sf) of general office space, 22,000 sf of warehousing space, 75,000 sf of research and development space, and 110,000 sf of cGMP space with 324 parking spaces. The site is currently occupied by an event venue, a closed restaurant, and parking lots. **Table 1** presents the program summary of the existing and proposed uses on the site.

**Table 1.** Existing Site and Proposed Building Program

---

| Land Use                 | Proposed   |
|--------------------------|------------|
| cGMP (Manufacturing)     | 110,000 sf |
| Warehousing              | 22,000 sf  |
| General Office           | 68,000 sf  |
| Research and Development | 75,000 sf  |
| Parking Spaces           | 324 spaces |

## Study Area

---

Based on the project traffic demands, proposed site circulation, traffic circulation in this area of the Town, and discussions with the Town of Randolph, the study area includes the following intersection locations:

- Scanlon Drive/North Main Street (signalized);
- Reed Street/High Street (signalized); and
- Scanlon Drive/High Street (unsignalized).

The study area intersection locations are shown on **Figure 1**.

Figure 1. *Study Area*





## Methodology

This TIS follows the Massachusetts Department of Transportation's (MassDOT's) *Transportation Impact Assessment (TIA) Guidelines*, as described below:

- The Existing (2023) Condition analysis includes an inventory of the existing transportation conditions such as traffic characteristics, parking, curb usage, transit, pedestrian circulation, bicycle facilities, loading, and site conditions. Existing counts for vehicles, bicycles, and pedestrians were collected at the study area intersections. Operations at the study area intersections are calculated using Synchro 11.0, which is based on the traffic operational analysis methodology of the Transportation Research Board's (TRB's) *Highway Capacity Manual* (HCM) 6<sup>th</sup> edition.<sup>1</sup>
- The future transportation conditions analyses evaluate potential transportation impacts associated with the Project. The long-term transportation impacts are evaluated for Year 2030, based on a seven-year horizon.
  - The No-build (2030) Condition analysis includes general background traffic growth, traffic growth associated with specific developments (not including this Project), and transportation improvements that are planned in the vicinity of the Project Site.
  - The Build (2030) Condition analysis includes a net increase in traffic volume due to the addition of Project-generated trips. The transportation study identifies expected roadway, parking, transit, pedestrian, and bicycle accommodations, as well as loading capabilities and deficiencies.
  - The Build-Mitigated (2030) Condition includes an analysis of traffic operations in the design year with the implementation of significant roadway or intersection improvements, if applicable.
- The final section of the transportation study summarizes transportation conclusions and identifies potential transportation recommendations.

## Existing (2023) Condition

This section documents the condition of the roadways and intersections located in the study area including geometric layout, lane use, traffic count data, pedestrian and bicycle count data, crash data, and other existing information. Crash analysis was performed using the most recent available data from the MassDOT IMPACT Crash Portal.

<sup>1</sup> Highway Capacity Manual, Sixth Edition; Transportation Research Board; Washington, D.C.; 2016.

## Roadway Descriptions

**Scanlon Drive** is classified as an urban minor arterial under the jurisdiction of the Town of Randolph. It runs east-west between North Main Street to the east and High Street to the west. It is a two-way, two-lane road. On-street parking is not provided on either side of the road. A sidewalk is provided on the south side of the road.

**North Main Street (Route 28)** is classified as an urban principal arterial under Massachusetts Department of Transportation jurisdiction. It runs north-south between the I-93 interchange to the north and South Main Street to the south. Within the study area, it is a two-way, four-lane road. On-street parking is not provided on either side of the road. Sidewalks are generally provided on both sides of the road.

**Reed Street** is classified as an urban minor arterial under the jurisdiction of the Town of Randolph. It runs east-west between North Main Street to the east and Canton Street to the west. It is a two-lane, two-lane road. On-street parking is not provided on either side of the road. Sidewalks are provided on both sides of the road.

**High Street** is classified as an urban minor arterial under the jurisdiction of the Town of Randolph and Norfolk County. It runs north-south between Scanlon Drive to the north and Vine Street to the south. It is a two-way, two-lane road. On-street parking is not provided on either side of the road. A sidewalk is provided on the east side of the road.

**Billings Street** is classified as a local road under the jurisdiction of the Town of Randolph. It runs east-west between High Street and High Street. It is a paper street within the existing site parking lot.

## Intersection Descriptions

**Scanlon Drive/North Main Street/Russ Street** is a four-legged, signalized intersection with four approaches. The Scanlon Drive eastbound approach consists of a shared left-turn/through lane and a shared through/right-turn lane. The Russ Street westbound approach consists of an exclusive left-turn lane and a shared through/right-turn lane. The North Main Street northbound approach consists of an exclusive left-turn lane, a through lane, and a shared through/right-turn lane. The North Main Street southbound approach consists of an exclusive left-turn lane, two through lanes, and an exclusive right-turn lane. Crosswalks are provided at all approaches. Pedestrian ramps are provided at all crossings, but only the ramp at the northeast corner is currently ADA-accessible. On-street parking is not provided along any approach. Pedestrian signal equipment is provided at all crosswalks.



**Reed Street/High Street** is a four-legged, signalized intersection with four approaches. All four approaches consist of a shared left-turn/through/right-turn lane. Crosswalks with pedestrian ramps are provided at all approaches. On-street parking is not provided along any approach. Pedestrian signal equipment is provided at all crosswalks.

**Scanlon Drive/High Street** is a three-legged, unsignalized intersection with three approaches. The Scanlon Drive westbound approach consists of a shared left-turn/right-turn lane. The High Street northbound approach consists of a shared through/right-turn lane. The High Street southbound approach consists of a shared left-turn/through lane. Crosswalks are not provided at any of the approaches. On-street parking is not provided along any approach.

**Scanlon Drive Driveways.** Along Scanlon Drive, there are several driveways that lead to the existing Site as well as adjacent parcels. Starting from High Street and moving east, this includes four driveways for the closed Lantana venue, two driveways for Lombardo's, a shared driveway for Lombardo's and the Comfort Inn Hotel, and a driveway for the Shell gas station.

## Traffic Data Collection

This section summarizes the traffic data that was collected within the study area.

### AUTOMATIC TRAFFIC RECORDER COUNTS

An automatic traffic recorder (ATR) is a device that continuously records the number and class of vehicles on a roadway for a given period. ATR counts were conducted on Park Street for a 48-hour period from Wednesday, September 13, 2023, to Thursday, September 14, 2023. Complete ATR data is included in **Appendix A**. **Table 2** summarizes the existing ATR traffic data, including daily traffic, and peak-hour percentage (K factor). Average vehicular speeds and approximate 85<sup>th</sup> percentile vehicular speeds are included in **Appendix A**. Peak periods are also identified below. **Figure 2**, **Figure 3**, and **Figure 4** show the average daily traffic recorded at each ATR location.

- High Street
  - The a.m. peak was 6:15 a.m. – 7:15 a.m. (770 vehicles).
  - The p.m. peak was 4:30 p.m. – 5:30 p.m. (750 vehicles).
- Scanlon Drive
  - The a.m. peak was 8:15 a.m. – 9:15 a.m. (760 vehicles).
  - The p.m. peak was 4:30 p.m. – 5:30 p.m. (750 vehicles).
- North Main Street
  - The a.m. peak was 8:00 a.m. – 9:00 a.m. (2,400 vehicles).
  - The p.m. peak was 4:15 p.m. – 5:15 p.m. (2,500 vehicles).

**Table 2. Average Weekday Traffic**

| Location                 | ADT           | Heavy Vehicle % | K Factor |
|--------------------------|---------------|-----------------|----------|
| <b>High Street</b>       |               |                 |          |
| <b>Northbound</b>        | 5,033         | 3.1%            | 12%      |
| <b>Southbound</b>        | 4,793         | 2.8%            | 10%      |
| <b>TOTAL</b>             | <b>9,826</b>  |                 |          |
| <b>Scanlon Drive</b>     |               |                 |          |
| <b>Eastbound</b>         | 4,942         | 3.3%            | 11%      |
| <b>Westbound</b>         | 4,762         | 2.9%            | 10%      |
| <b>TOTAL</b>             | <b>9,704</b>  |                 |          |
| <b>North Main Street</b> |               |                 |          |
| <b>Northbound</b>        | 17,318        | 10.3%           | 9%       |
| <b>Southbound</b>        | 19,172        | 4.5%            | 8%       |
| <b>TOTAL</b>             | <b>36,490</b> |                 |          |

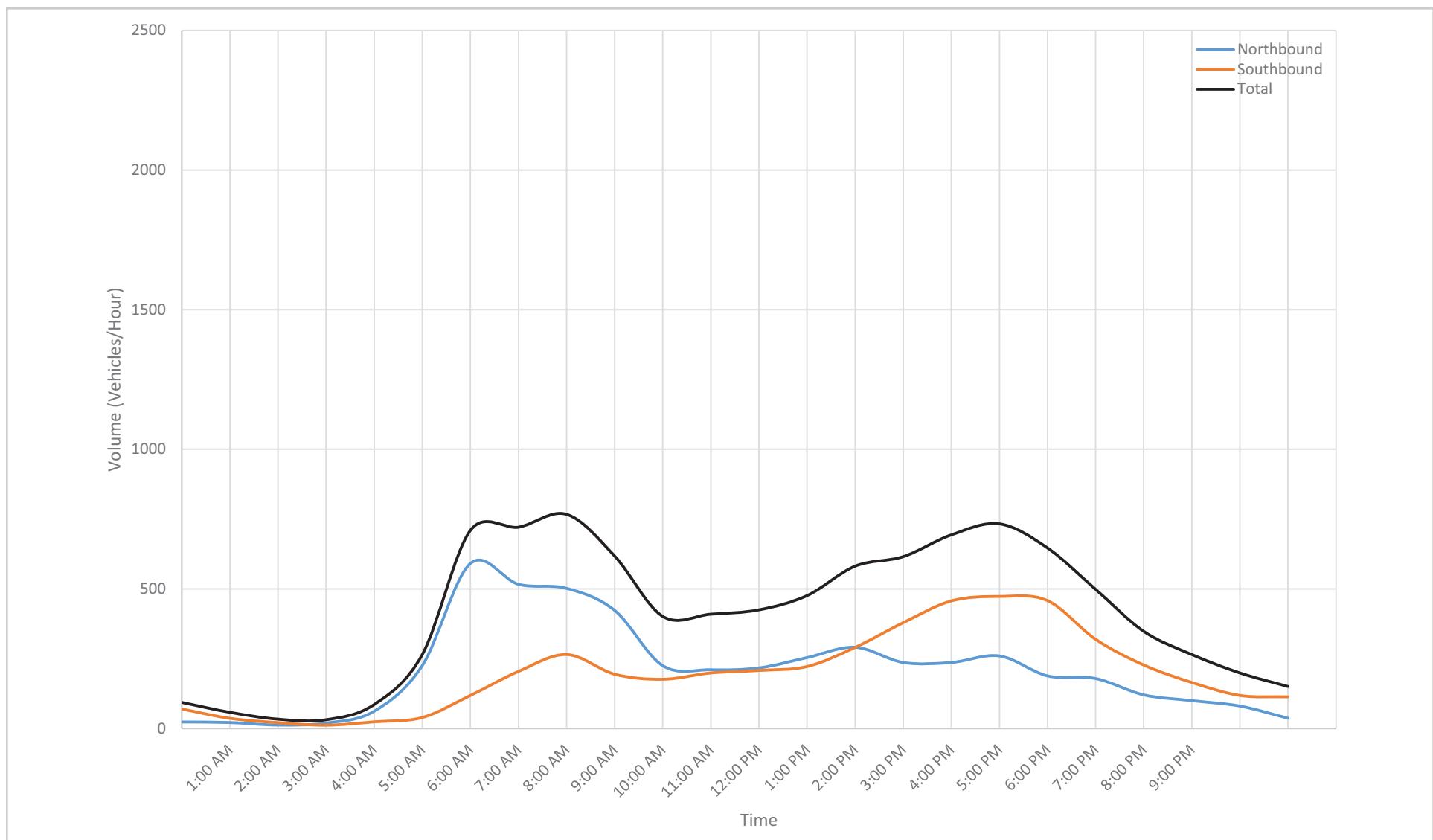
Figure 2. *Average Daily Traffic: High Street, South of Scanlon Drive*

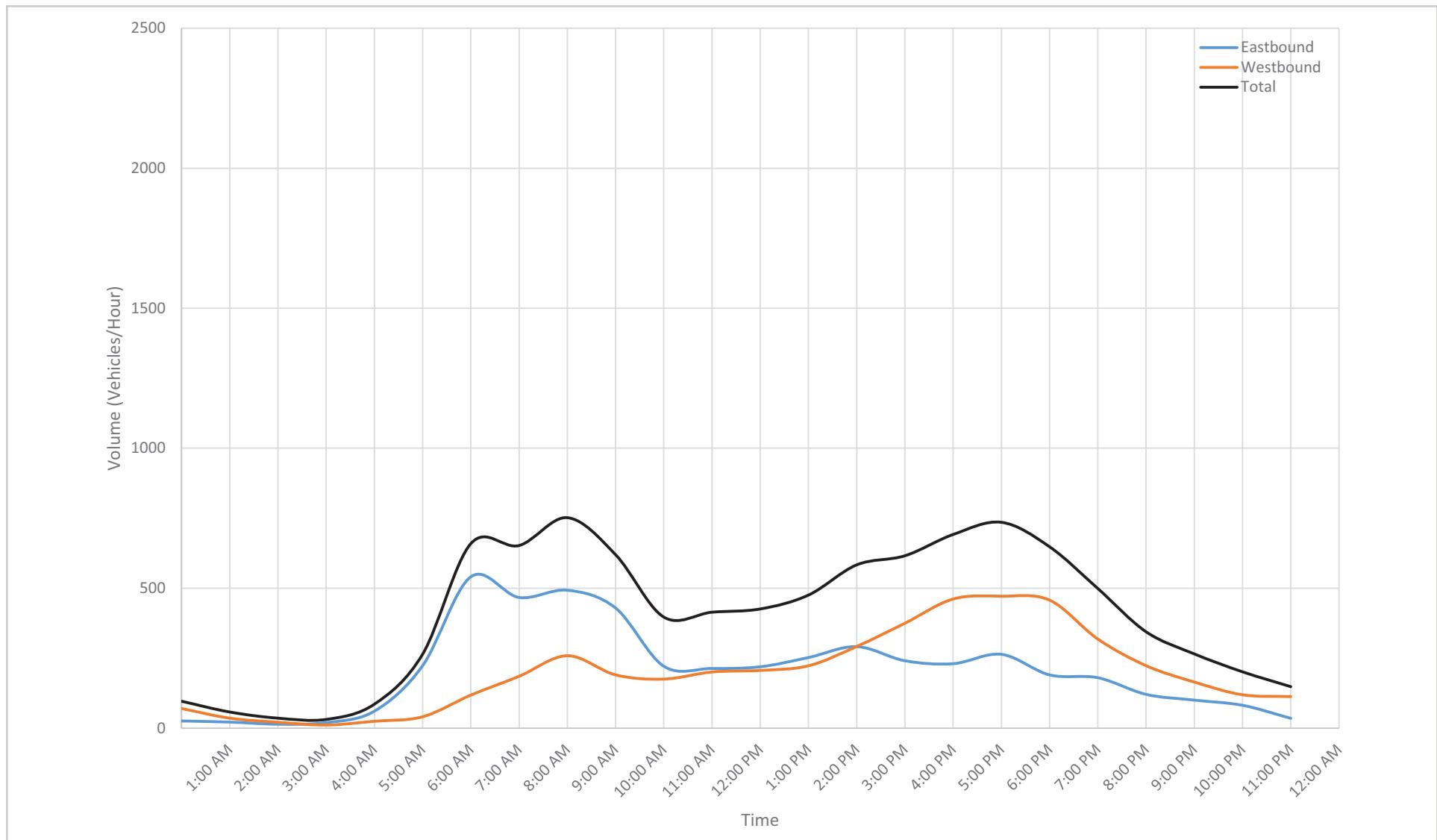
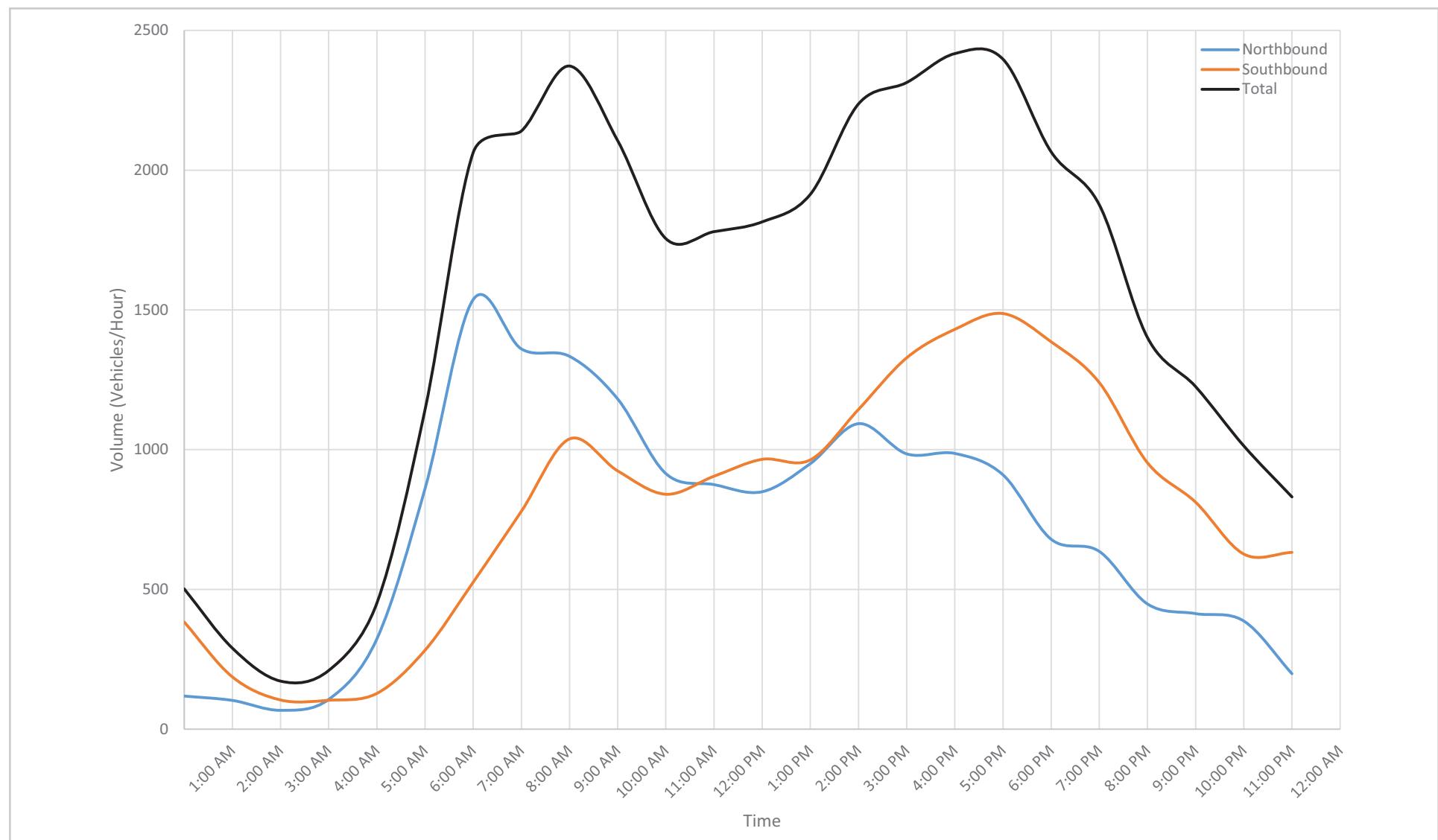
Figure 3. *Average Daily Traffic: Scanlon Drive, East of High Street*

Figure 4. *Average Daily Traffic: North Main Street, North of Scanlon Drive*



## MANUAL TURNING MOVEMENT COUNTS

Manual Turning Movement Counts (TMCs) were recorded from 7:00 – 9:00 a.m. and 4:00 – 6:00 p.m. at the study area intersections and site driveway. The TMCs include vehicle, bicycle, and pedestrian counts. Counts were collected on Wednesday, September 13<sup>th</sup>, 2023, at the study area intersections. The count data indicates that the morning peak hour occurs between 8:00 – 9:00 a.m. and the evening peak hour occurs between 4:30 – 5:30 p.m. Complete traffic count data is provided in **Appendix A**.

## SEASONAL ADJUSTMENT FACTORS

According to MassDOT's Weekday Seasonal Factors Report for urban arterials and collectors, traffic volumes in September are shown to be slightly above average with a seasonal adjustment factor of 0.92. This means that volumes are 8% higher during September than the average for the year. For a more conservative analysis, counts were not adjusted. Seasonal adjustment factors are included in **Appendix B**. **Figure 5** and **Figure 6** show the existing vehicular traffic volumes at the study area intersections and driveways along Scanlon Drive during the morning and evening peak hours. Volumes at adjacent intersections were balanced where appropriate.



Figure 5. Existing (2023) Condition Vehicle Volumes, Weekday a.m. Peak Hour

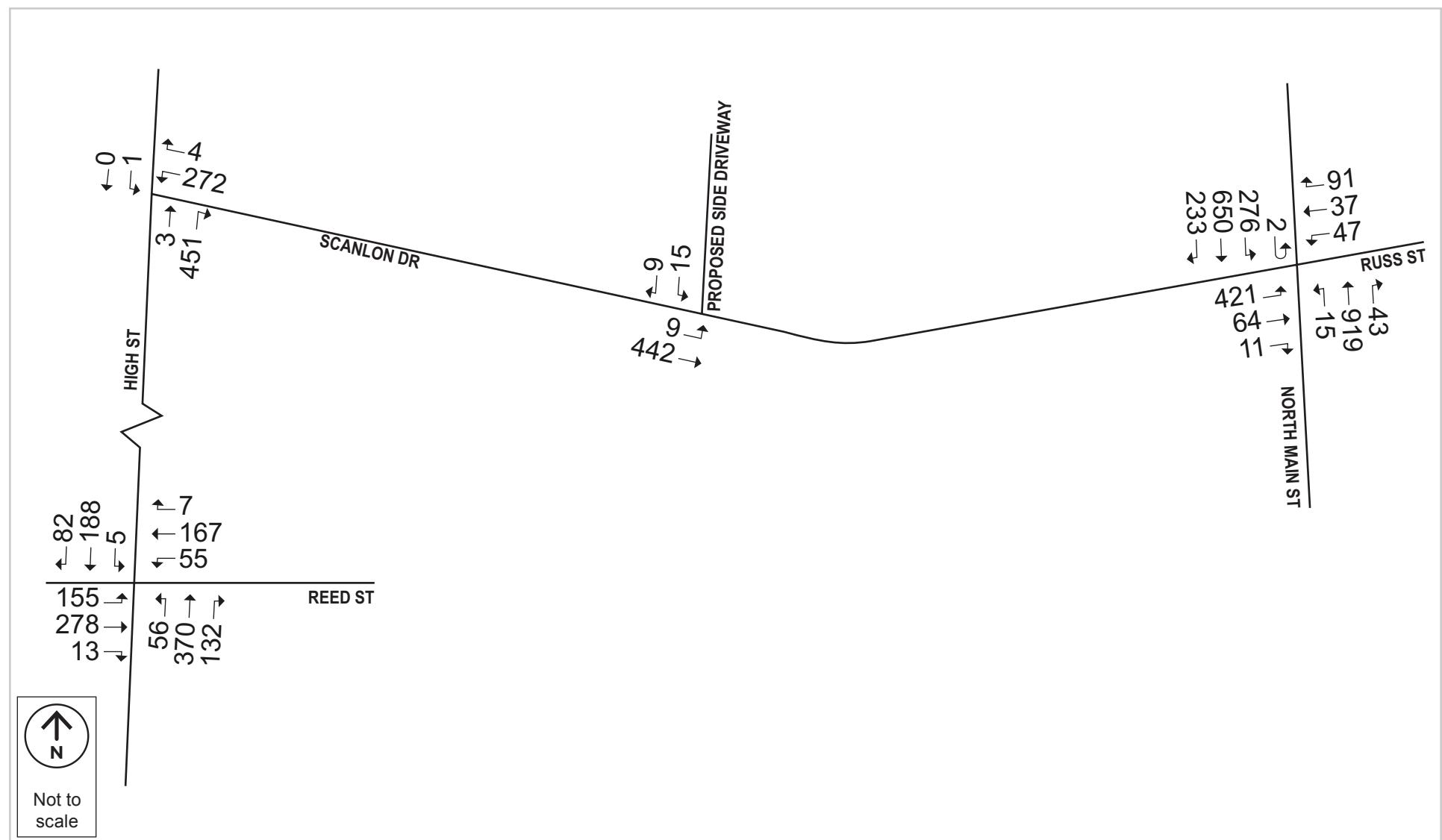
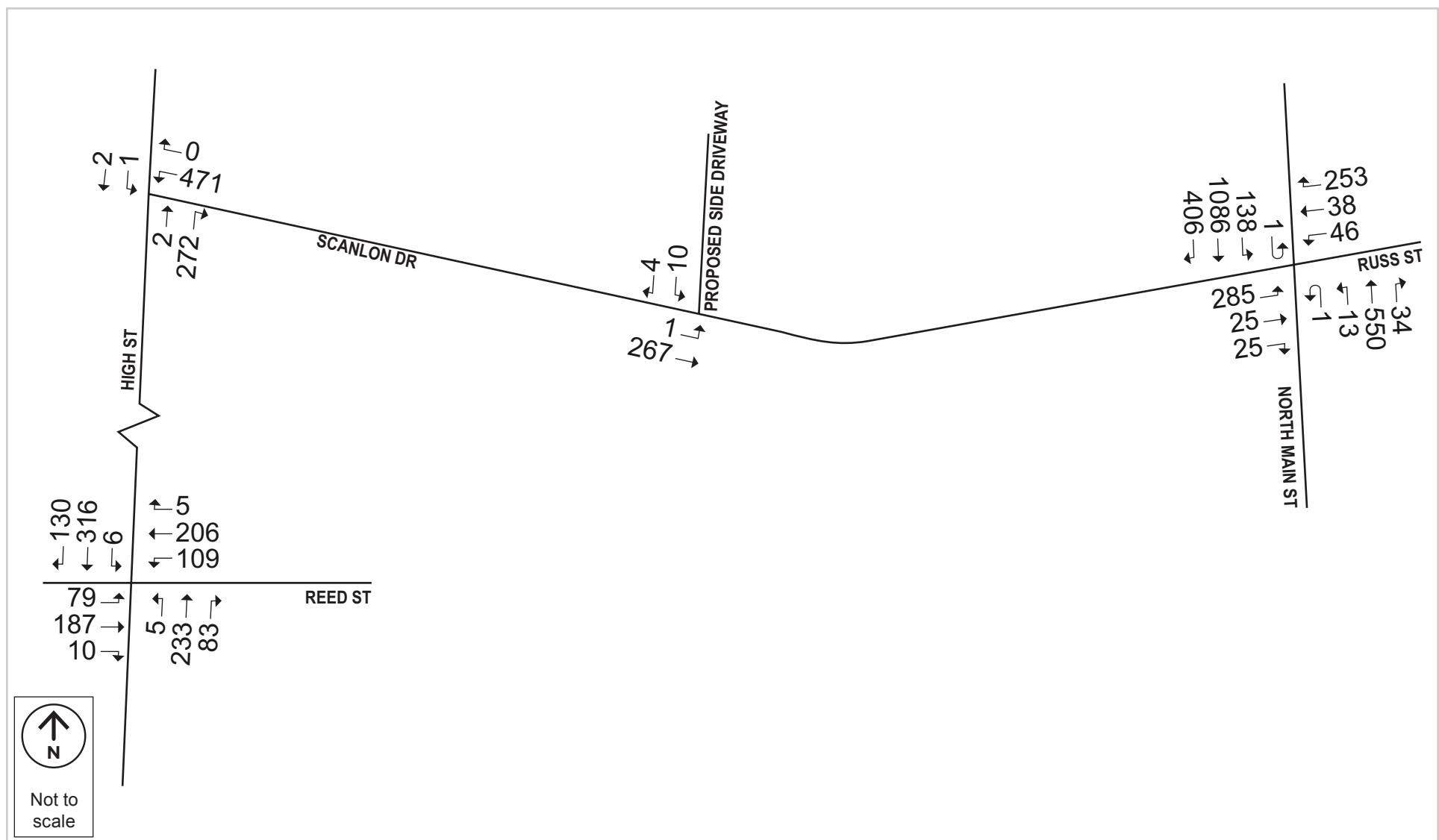


Figure 6. Existing (2023) Condition Vehicle Volumes, Weekday p.m. Peak Hour





## BICYCLE COUNT DATA

Bicycle counts were conducted concurrently with the vehicular traffic data collection. Bicycle activity within the study area was generally low, as shown in **Figure 7**. Cyclists share the road with vehicles on all study area roadways under current conditions.

## PEDESTRIAN COUNT DATA

To determine the amount of pedestrian activity within the study area, pedestrian counts were conducted as part of the traffic data collection at the study area intersections. Counts occurred on a cloudy day with temperatures around 70°F. Pedestrian volumes were highest along North Main Street. The weekday a.m. and p.m. peak hour pedestrian volumes are shown in **Figure 8**.

## Existing Public Transportation

The Massachusetts Bay Transportation Authority (MBTA) and the Brockton Area Transit Authority (BAT) operate buses with stops at the North Main Street at Scanlon Drive bus stop. This bus stop is located an approximately 4-minute (0.2-mile) walk from the Project site. The bus stop is served by MTBA Bus Route 240, which operates between Ashmont and Avon Square; and BAT Bus Route 12, which operates between Ashmont Station and BAT Center hub in Brockton.

Approximately four miles to the south of the site is the Holbrook/Randolph MBTA Station, which is served by the Middleborough/Lakeville Commuter Rail Line. There is also a stop for MBTA Bus Route 240 at this station for potential regional connections.

## Off-street Parking

The existing off-street parking supply was documented at the following parking facilities closest to the Site:

- Lantana - 23 Scanlon Drive Lot (115 spaces);
- Lombardo's Front Lot (approximately 265 spaces); and
- Lombardo's Back Lot (approximately 234 spaces).



Figure 7. Existing (2023) Condition Bicycle Volumes, Weekday a.m. and p.m. Peak Hours

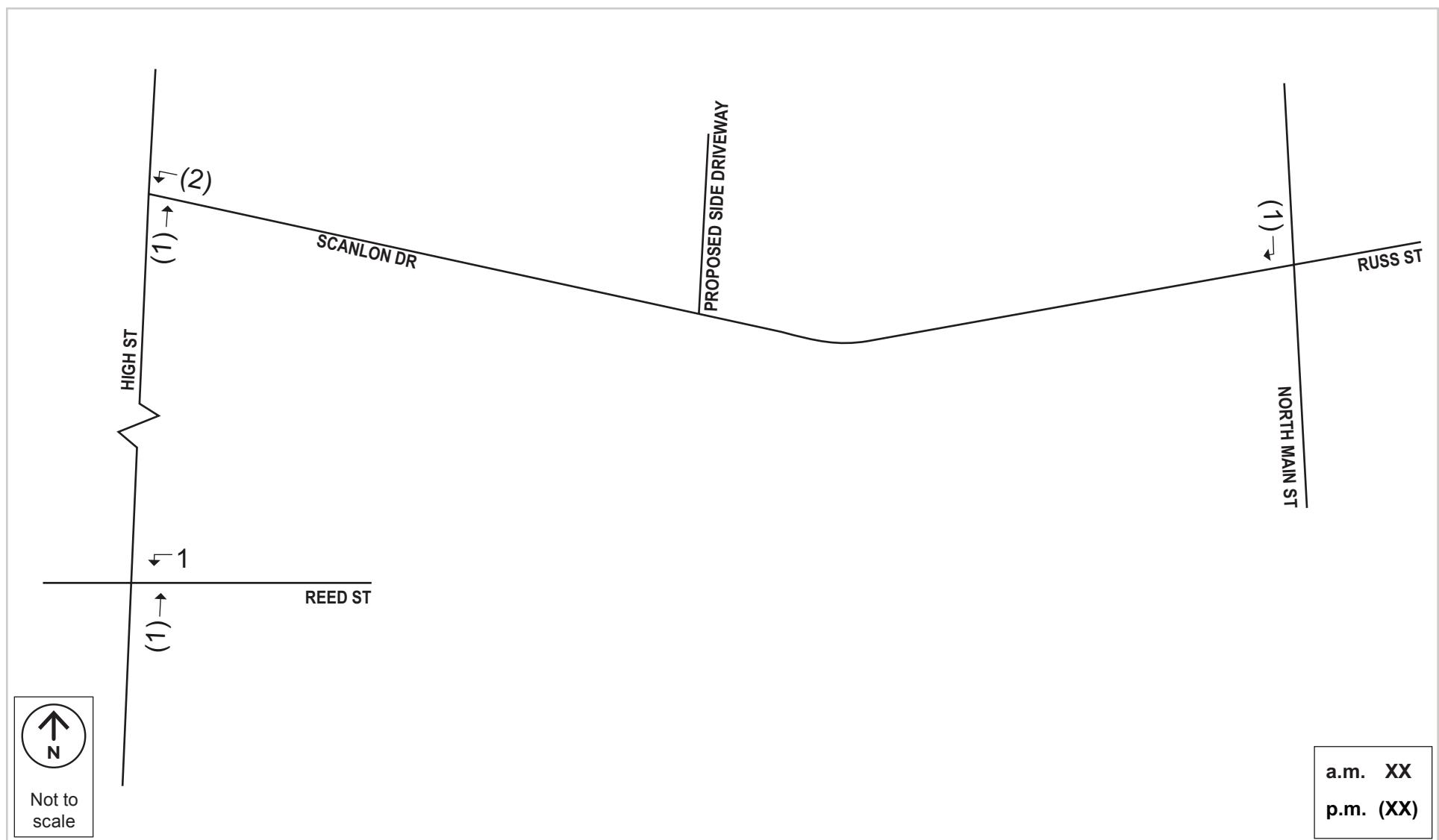
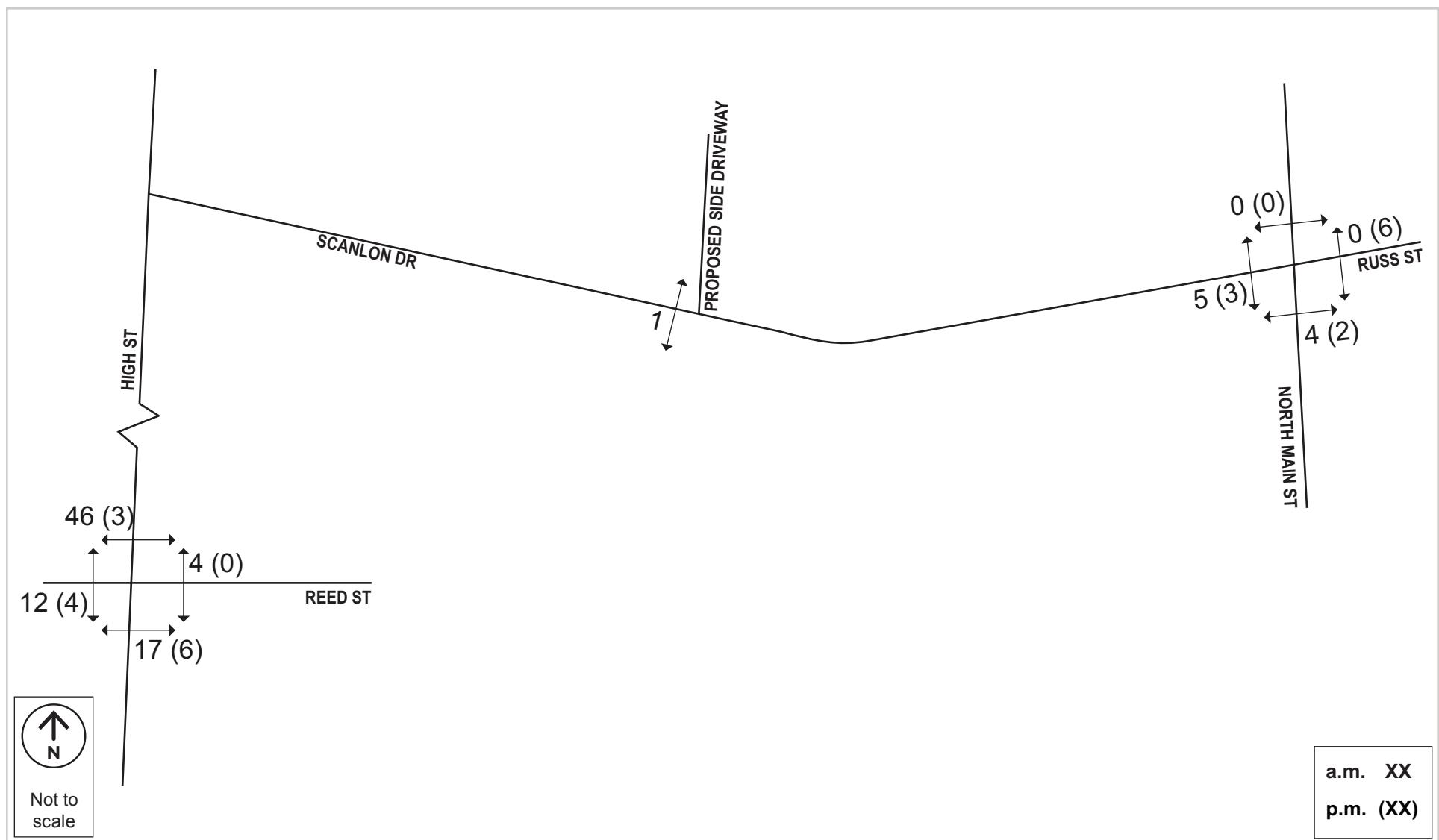




Figure 8. Existing (2023) Condition Pedestrian Volumes, Weekday a.m. and p.m. Peak Hours



## Safety Analysis

HSH performed a safety analysis at all study area intersections to identify and evaluate possible safety issues that exist. Crash data for this corridor was obtained from the MassDOT crash portal database for the most recent period available (2016-2020). **Table 3** summarizes the 86 crashes recorded between 2016 and 2020 at the study area intersections. Most of the crashes reported at the signalized intersection were rear-end crashes (38%) or angle crashes (35%). Two crashes occurred at the study area unsignalized intersections both of which were rear-end crashes. Most crashes were reported with clear weather conditions (62%) and occurred during daylight hours (56%). Most crashes (58%) did not result in any injuries and resulted in property damage only (PDO). No fatalities were recorded. One pedestrian crash was reported.

Crash rates are determined for an intersection based on the number of crashes per million entering vehicles (MEV). The MassDOT District 6 crash rate for signalized intersections is 0.71, and the District 6 crash rate for unsignalized intersections is 0.52. The average crash rates at the signalized intersections are both above the MassDOT District 6 average:

- **Scanlon Drive/North Main Street.** Between 2016 and 2020, 59 crashes occurred at this location. One crash involved a pedestrian. Most (61%) of the crashes occurred during daylight hours. The weather during most (83%) crashes was either clear or cloudy. Based on crash data, crashes often occurred when vehicles had to slow down during heavy traffic. No crashes were fatal.
- **Reed Street/High Street.** Between 2016 and 2020, 25 crashes occurred at this location. No crashes involved pedestrians. Half (48%) of crashes occurred during the night. Over half (56%) of crashes were angle crashes. Crashes were often caused by negligent driving. No crashes were fatal.

Crash data and the crash rate worksheets are provided in **Appendix C**.



Table 3. Crash Data Summary

| Characteristic                | Scanlon Dr/<br>N Main St | Reed St/<br>High St | Scanlon Dr/<br>High St |
|-------------------------------|--------------------------|---------------------|------------------------|
|                               | Signalized               | Signalized          | Unsignalized           |
| <b>Total Crashes</b>          | 59                       | 25                  | 1                      |
| <b>Year</b>                   |                          |                     |                        |
| 2016                          | 19                       | 2                   | 0                      |
| 2017                          | 17                       | 7                   | 1                      |
| 2018                          | 8                        | 6                   | 0                      |
| 2019                          | 10                       | 3                   | 0                      |
| 2020                          | 5                        | 7                   | 0                      |
| <b>Severity</b>               |                          |                     |                        |
| PDO                           | 38                       | 10                  | 1                      |
| Non-fatal Injury              | 19                       | 15                  | 0                      |
| Not Reported                  | 2                        | 0                   | 0                      |
| Fatality                      | 0                        | 0                   | 0                      |
| <b>Crash Type</b>             |                          |                     |                        |
| Angle                         | 15                       | 14                  | 0                      |
| Sideswipe, same direction     | 8                        | 1                   | 0                      |
| Rear-end                      | 26                       | 6                   | 1                      |
| Single vehicle                | 7                        | 0                   | 0                      |
| Head-on                       | 2                        | 3                   | 0                      |
| Sideswipe, opposite direction | 1                        | 0                   | 0                      |
| Not Reported                  | 0                        | 1                   | 0                      |
| <b>Weather</b>                |                          |                     |                        |
| Clear                         | 40                       | 13                  | 0                      |
| Cloudy                        | 9                        | 4                   | 0                      |
| Rain                          | 7                        | 5                   | 1                      |
| Snow                          | 3                        | 1                   | 0                      |
| Sleet/Hail                    | 0                        | 1                   | 0                      |
| Other                         | 0                        | 1                   | 0                      |
| Not Reported                  | 0                        | 0                   | 0                      |

| Characteristic            | Scanlon Dr/<br>N Main St | Reed St/<br>High St | Scanlon Dr/<br>High St |
|---------------------------|--------------------------|---------------------|------------------------|
|                           | Signalized               | Signalized          | Unsignalized           |
| <b>Light Conditions</b>   |                          |                     |                        |
| Daylight                  | 36                       | 11                  | 0                      |
| Dark w/ lighted roadway   | 17                       | 12                  | 1                      |
| Dark w/ unlighted roadway | 0                        | 1                   | 0                      |
| Dark w/ unknown lighting  | 0                        | 1                   | 0                      |
| Dawn                      | 4                        | 0                   | 0                      |
| Dusk                      | 2                        | 0                   | 0                      |
| Not Reported              | 0                        | 0                   | 0                      |
| <b>Hit and Run</b>        | 0                        | 0                   | 0                      |
| <b>Non-motorist</b>       |                          |                     |                        |
| Pedestrian                | 1                        | 0                   | 0                      |
| Bicyclist                 | 0                        | 0                   | 0                      |
| <b>Crash Rate per MEV</b> | 1.00                     | 0.90                | 0.07                   |
| <b>District 6 Average</b> | 0.71                     | 0.71                | 0.52                   |

## No-build (2030) Condition

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The methodology to account for future traffic growth, independent of the Project, consists of two components. The first part of the methodology accounts for general background traffic growth that may be affected by changes in demographics, automobile usage, and automobile ownership. The second part of the methodology identifies any specific planned developments that are expected to affect traffic patterns throughout the study area within the future analysis time horizon.

### Background Growth

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The baseline 2030 traffic volumes have been estimated by applying a 1% annual growth factor to the existing year volumes. The 1% growth rate was determined based on data from 2013 to 2022, collected from a MassDOT continuous count station located along Route 24 (the Fall River Expressway). This data can be found **in Appendix D**. A 1% growth rate is also consistent with the rate used for the adjacent and recently approved 34 Scanlon Drive project.



## Future Development Projects

Within the study area, the following development projects were identified that could impact the traffic patterns throughout the study area:

- **34 Scanlon Drive (Yankee Bus Line Headquarters).** The development consists of a 54,700 square foot (sf) maintenance and repair facility as well as parking areas for approximately 75 buses and staff vehicles. This site is located across from the Project.
- **Hotel Restaurant.** Currently, adjacent to the Comfort Inn hotel there is a site that is not in use but used to operate as a restaurant. Per direction from the Randolph Town Planner, there could be the potential for it to be reopened given recent development in the area, therefore the study conservatively estimated trips for a 200-seat restaurant.
- **Lyons Elementary.** The development consists of a 497-student elementary school that will be built on the site of a different school that has been closed since 2008. This development was reviewed, but analysis showed that its trips did not overlap with the study area.

Project trips from the two background developments noted above that pass through the study area and the annual growth rate of 1% were added to the Existing (2023) Condition to develop the No-Build (2030) Condition. The No-Build (2030) Condition volumes for the morning and evening peak hours are presented in **Figure 9** and **Figure 10**, respectively.



Figure 9. No-build (2030) Condition Vehicle Volumes, Weekday a.m. Peak Hour

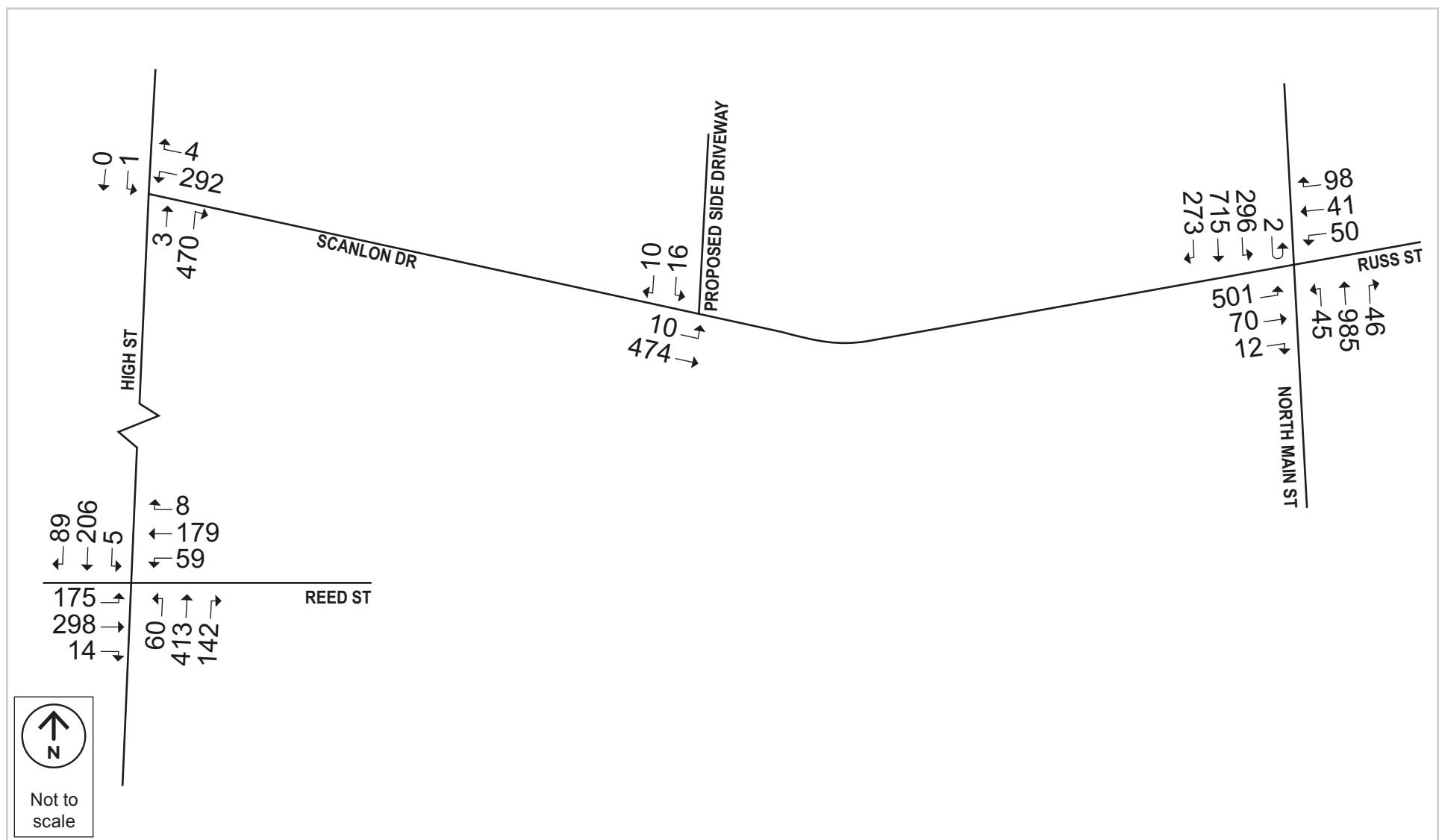
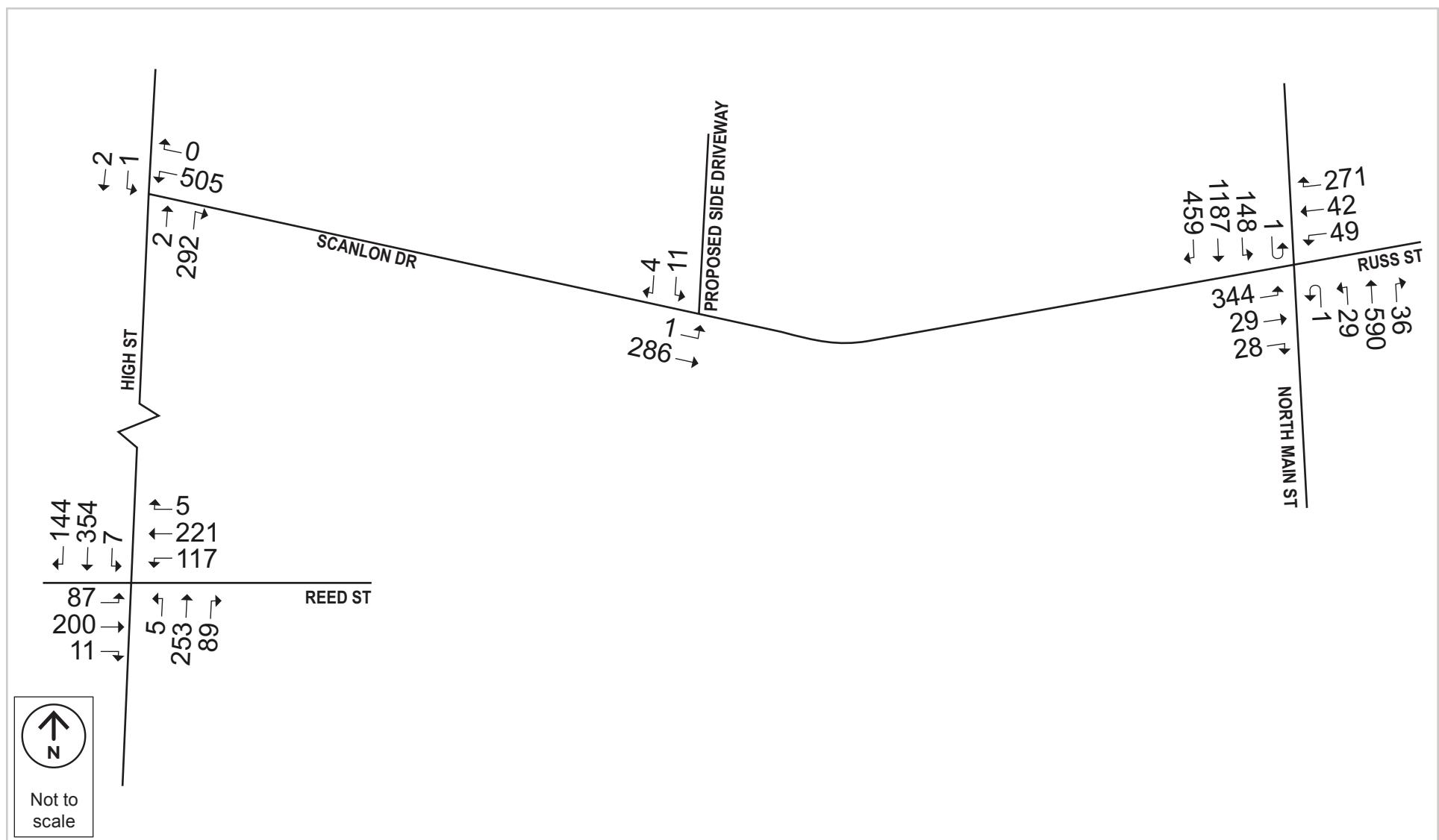




Figure 10. No-build (2030) Condition Vehicle Volumes, Weekday p.m. Peak Hour



# Build (2030) Condition

## Project Description

The Project site, located in Randolph, is bounded by the I-93 interchange ramps to the north, Scanlon Drive to the south, a hotel to the east, and undeveloped land to the west. The existing site is occupied by an event space and an unoccupied second event venue. The Project consists of constructing two buildings, Building A and Building B, which total approximately 68,000 sf of general office space, 110,000 sf of manufacturing space, 75,000 sf of research and development space, and 22,000 sf of warehousing space with 324 parking spaces. The site's front parking lot, which is in front of Building B, consists of 104 spaces and will be accessible by two driveways off Scanlon Drive. Both driveways will be two-way. There will also be a two-way driveway to the west of the front parking lot leading to a parking lot behind Building B. This parking lot will consist of 136 spaces. There will be parking spaces along this driveway consisting of 29 more spaces. Trucks and other service vehicles will use a two-way driveway located to the east of the front parking lot to drive to the service/loading area. Building A will be served by a separate parking lot located to the west of Building A consisting of 35 spaces and features a crane laydown area with access opposite the intersection of High Street at Scanlon Drive. Site access is illustrated on the Site Plan shown in **Figure 11**.

Figure 11. *Site Plan*



## Vehicle Parking

The Town of Randolph Zoning By-Law establishes requirements for off-street parking spaces for new developments. For proposed warehouse/industrial developments, one space is required for every two employees, plus space for every company-owned and -operated vehicle, as well as spaces for customers as determined by the Building Commissioner or Site Plan Administrator. For commercial/business developments, one space is required for each 200 square feet of gross floor area on the first floor of a building, and one space is required for each 400 square feet of gross floor area for subsequent floors, excluding storage area. (Zoning Bylaws Section 200-22). **Table 4** summarizes the required parking spaces as provided by the Town of Randolph's standards.

**Table 4.      *Parking Requirements***

| Development Type            | Spaces per unit<br>(per zoning)   | Units Provided  | Spaces Required |
|-----------------------------|---|---|-----------------|
| <b>Warehouse/Industrial</b> | One space per employee<br>One space per company-owned vehicle                         | 14 truck bays   | -               |
| <b>Commercial/Business</b>  | One space per 200 sf first floor area<br>One space per 400 sf above-first floor area. | 19,355 sf first floor area<br>12,000 sf second floor area | 127 spaces      |

## LOADING/SERVICE

A maintenance bay is located on the southwest side of Building A. The facility will be handling the storage and maintenance of large pieces of construction equipment. A large lot is available to the west of the building for the storage of this equipment. This lot is accessible from an entrance/exit off the intersection of High Street and Scanlon Drive.

Designated loading/service areas are located on the east side of Building B. Loading and service operations such as deliveries, trash pickup, and recycling will occur in the designated loading/service areas. Service vehicles will enter and exit the site from Scanlon Drive on the east side of Building B.

## Trip Generation Methodology

The traffic expected to be generated by the proposed Project was determined based on industry standards. The trip generation estimates were based on data published within the latest Institute of Transportation Engineers (ITE) *Trip Generation Manual*, 11<sup>th</sup> Edition. No direct land use code is



available for the proposed cGMP facility, based on expected building components a mix of manufacturing, general office and research and development center uses were utilized as interpreted by cGMP regulations<sup>2</sup>. No direct land use code is available for the proposed crane operation building, based on expected tenant use a mix of warehousing for crane equipment maintenance and general office for management were utilized in the estimates.

To estimate the number of vehicular trips that will be generated by the project, the following ITE land use codes (LUC) were used:

- ***Land Use Code 140 – Manufacturing.*** A manufacturing facility is an area where the primary activity is the conversion of raw materials or parts into finished products. Size and type of activity may vary substantially from one facility to another. In addition to the actual production of goods, a manufacturing facility typically has an office and may provide space for warehouse, research, and associated functions. The development is a Current Goods Manufacturing Practice (cGMP).
- ***Land Use Code 710 – General Office.*** A general office building is a location where affairs of businesses, commercial or industrial organizations, or professional persons or firms are conducted. An office building houses multiple tenants that can include, as examples, professional services, insurance companies, investment brokers, a banking institution, a restaurant, or other service retailers.
- ***Land Use Code 150 – Warehousing.*** A warehouse is primarily devoted to the storage of materials, but it may also include office and maintenance areas.
- ***Land Use Code 760 – Research and Development Center.*** A research and development center is a facility or group of facilities devoted almost exclusively to research and development activities. The range of specific types of businesses contained in this land use category varies significantly. Research and development centers may contain offices and light fabrication areas.

## MODE SHARE

A mode share is the percentage of trips at a site using various modes of transportation such as vehicle, transit, walking, or biking. The Project mode share was determined using the 2021 American Community Survey (ACS) Means of Transportation to Work (data table B08301) for Census Tract 4202.02, published by the U.S. Census Bureau. Commuting census data includes a percentage of “work from home” responses (9.5%); mode share was adjusted based on commuting

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<sup>2</sup> Current Good Manufacturing Practice (CGMP) Regulations.<https://www.fda.gov/drugs/pharmaceutical-quality-resources/current-good-manufacturing-practice-cgmp-regulations>

travel choices and was proportionally assigned to all other modes. The mode shares are shown in **Table 5**.

**Table 5. Mode Share**

| Mode Type             | Mode Share |
|-----------------------|------------|
| Vehicle               | 91%        |
| Public Transportation | 7%         |
| Bicycle/Walk          | 2%         |
| Total                 | 100%       |

\* Based on U.S. Census 2021: ACS 5-Year Estimates for Means of Transportation to Work for Census Tract 4202.02 (Table B08301).

## PROJECT-GENERATED VEHICLE TRIPS

The unadjusted vehicle trips calculated using the ITE rates described previously were converted to person trips by using vehicle occupancy rates of 1.18 for home-to-work based trips, as published by the Federal Highway Administration (FHWA).<sup>3</sup> **Table 6** presents a summary of the Project-generated person trips assigned to transit trips, bike/walk trips, and adjusted primary vehicle trips for the project based on the mode share distribution applied to the ITE LUCs, and includes daily, a.m. peak hour, and p.m. peak hour trips. Trip generation calculations are provided in **Appendix D**.

**Table 6. Project-generated Person Trips by Mode**

| Time Period               | Direction  | Person Trips |           | Vehicle Trips |
|---------------------------|------------|--------------|-----------|---------------|
|                           |            | Transit      | Walk/Bike | Vehicle       |
| Daily                     | In         | 100          | 30        | 977           |
|                           | <u>Out</u> | <u>100</u>   | <u>30</u> | <u>977</u>    |
|                           | Total      | 200          | 60        | 1,954         |
| Weekday a.m.<br>Peak Hour | In         | 20           | 5         | 197           |
|                           | <u>Out</u> | <u>4</u>     | <u>1</u>  | <u>45</u>     |
|                           | Total      | 24           | 6         | 242           |
|                           | In         | 5            | 1         | 54            |

<sup>3</sup> Summary of Travel Trends: 2017 National Household Travel Survey; FHWA; Washington, D.C.; July 2018



| Time Period               | Direction  | Person Trips |           | Vehicle Trips |
|---------------------------|------------|--------------|-----------|---------------|
|                           |            | Transit      | Walk/Bike | Vehicle       |
| Weekday p.m.<br>Peak Hour | <u>Out</u> | <u>18</u>    | <u>5</u>  | <u>187</u>    |
|                           | Total      | 23           | 6         | 241           |

## EXISTING TRIPS

The sites previous uses included two event venues called Lombardo's and Lantana, and their supporting parking lots. No ITE land use code is available for these style of event venues, so as to estimate existing trips, the land use code for a Hotel was used as it most closely represented the meeting and conference facilities of the previous event venues. Existing trips were estimated to be 948 daily trips with 58 trips during the a.m. peak hour and 70 vehicle trips during the p.m. peak hour. Count data at the site driveway was collected. As shown in **Table 7**, the proposed Project is expected to generate approximately 184 net new vehicle trips during the weekday a.m. peak hour (12 entering and 172 exiting), and 171 net new vehicle trips during the weekday p.m. peak hour (19 entering and 152 exiting). While the net new trip forecasts are presented, given at the time of traffic counts Lantana was closed and Lombardo's was winding down operations, the full Project trips in **Table 7** were used for all traffic analysis scenarios.

*Table 7. Net New Vehicle Trips*

| Time Period                   | Direction    | Existing   | Proposed     | Net New      |
|-------------------------------|--------------|------------|--------------|--------------|
| <b>Weekday Daily</b>          | In           | 474        | 977          | 503          |
|                               | <u>Out</u>   | <u>474</u> | <u>977</u>   | <u>503</u>   |
|                               | <b>Total</b> | <b>948</b> | <b>1,954</b> | <b>1,006</b> |
| <b>Weekday a.m. Peak Hour</b> | In           | 33         | 197          | 12           |
|                               | <u>Out</u>   | <u>25</u>  | <u>45</u>    | <u>172</u>   |
| <b>Weekday p.m. Peak Hour</b> | In           | <u>35</u>  | <u>54</u>    | <u>19</u>    |
|                               | <u>Out</u>   | <u>35</u>  | <u>187</u>   | <u>152</u>   |



## TRIP DISTRIBUTION

The trips generated by the site are expected to be primarily work-based trips. The vehicle trip distribution is based on U.S. Census Journey-to-Work data. The trip distribution for entering and exiting vehicles is illustrated in **Figure 12**. The Project-generated trips were assigned to the parking lot driveways. The Project-generated trips at the study area intersections are shown in **Figure 13**. Project-generated vehicle trips were added to the No-build (2030) Condition vehicle volumes to produce the Build (2030) Condition a.m. and p.m. peak hour vehicle volumes as shown in **Figure 14** and **Figure 15** respectively.

Figure 12. *Trip Distribution*





Figure 13. Project-generated Vehicle Trips, Weekday a.m. and p.m. Peak Hours

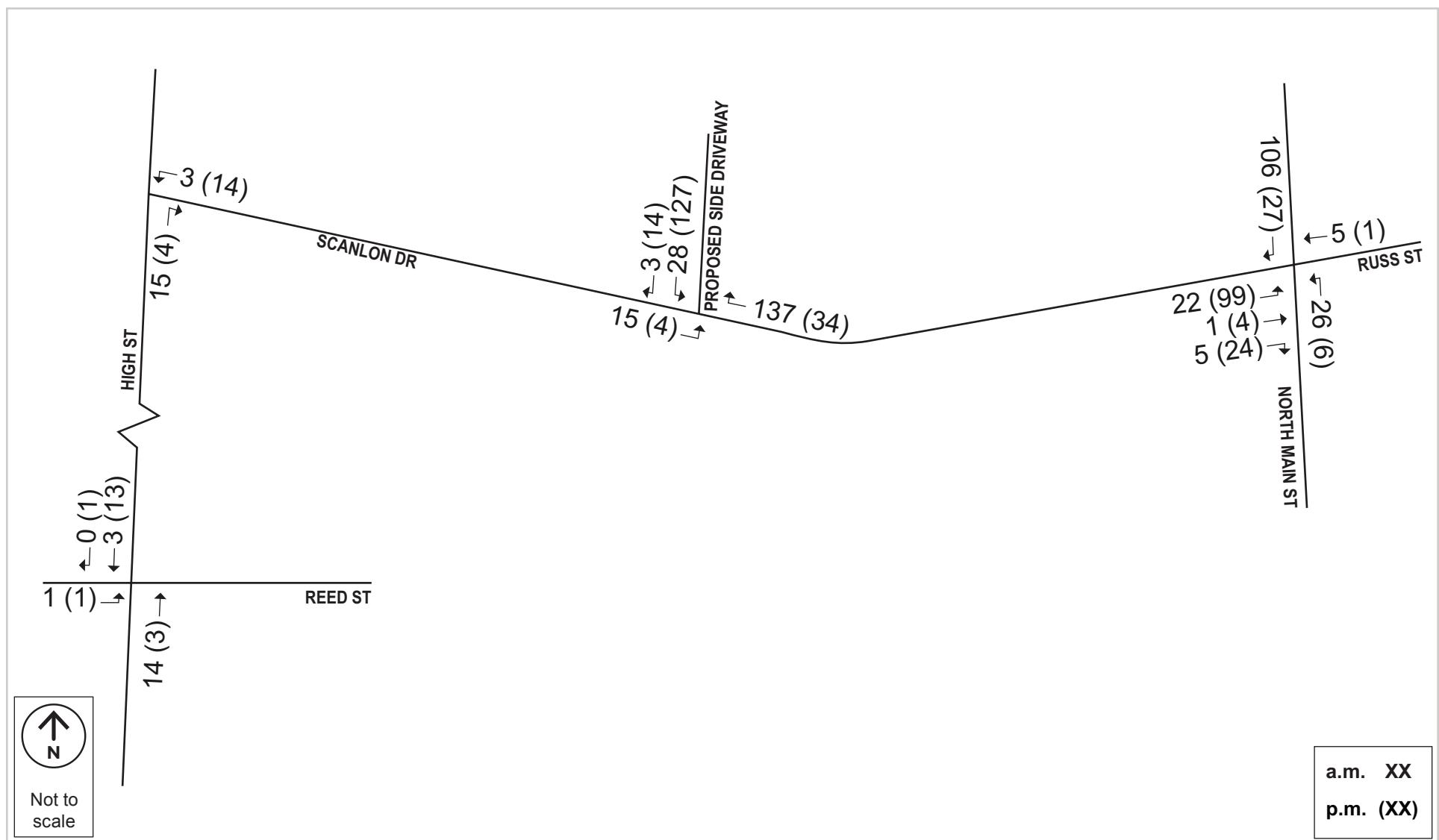


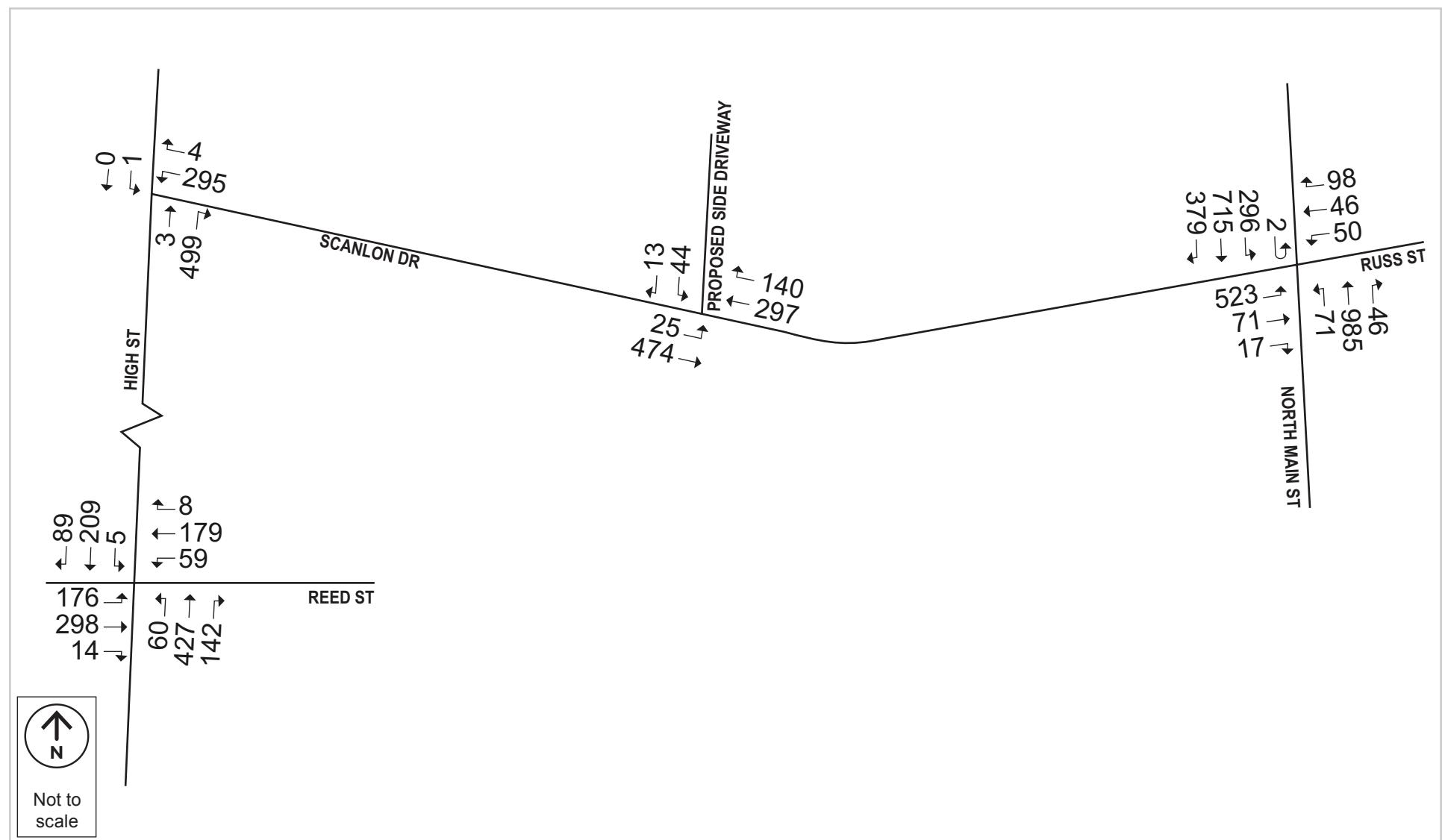
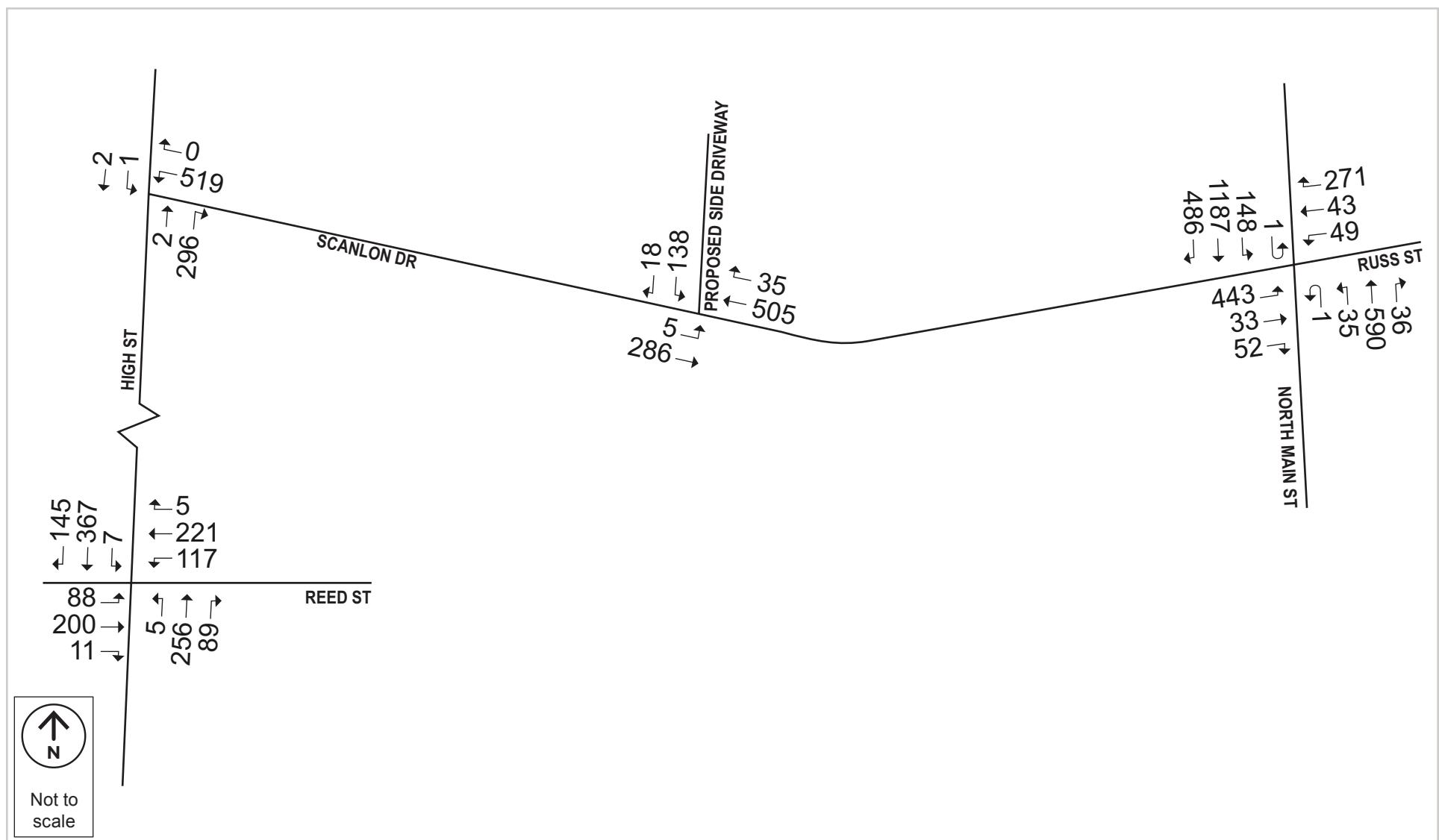
Figure 14. *Build (2030) Condition Vehicle Volumes, Weekday a.m. Peak Hour*

Figure 15. *Build (2030) Condition Vehicle Volumes, Weekday p.m. Peak Hour*





# Transportation Impact Analysis

This section discusses the analysis results for motor vehicle networks. Each section explains the analysis methodology used to evaluate the respective mode and then presents the results.

## Motor Vehicle Operations Analysis

Traffic operations are determined through an analysis of intersection Level of Service (LOS) calculations. LOS at the intersection was calculated using Synchro 11.0, which is based on the traffic operational analysis methodology of the HCM. The LOS and delay (in seconds) are based on intersection geometry and traffic volumes. **Table 8**, an excerpt from the HCM, provides LOS criteria for both signalized and unsignalized intersections. LOS A defines the most favorable condition, with minimum traffic delay. LOS F represents the worst condition, with significant traffic delays. LOS D is generally considered acceptable. However, LOS E or F is often typical for a stop-controlled minor street that intersects a major roadway and does not necessarily indicate that the operations at the intersection are poor or failing.

*Table 8. Level of Service Criteria*

| Level of Service | Average Stopped Delay (sec.) |                            |
|------------------|------------------------------|----------------------------|
|                  | Signalized Intersections     | Unsignalized Intersections |
| A                | 0.0–10.0                     | 0.0–10.0                   |
| B                | 10.1–20.0                    | 10.1–15.0                  |
| C                | 20.1–35.0                    | 15.1–25.0                  |
| D                | 35.1–55.0                    | 25.1–35.0                  |
| E                | 55.1–80.0                    | 35.1–50.0                  |
| F                | >80.0                        | >50.0                      |

In accordance with MassDOT guidelines, the peak 15 minutes of data collected during the peak hour were isolated to calculate the peak-hour factors (PHFs) for each approach. The percentage of heavy vehicles was calculated for each peak hour turning movement. PHFs for No-Build and Build scenarios were changed to 0.92 for all approaches per MassDOT guidelines. **Table 9** and **Table 10** summarize the Existing (2023) Condition, No-build (2030) Condition, and Build (2030) Condition LOS, delay, volume to capacity (v/c) ratio, and queue analysis during the a.m. and p.m. peak hours, respectively. Detailed analysis sheets are provided in **Appendix E**.

Table 9. Capacity Analysis Summary, a.m. Peak Hour

| Intersection/Movement                            | Existing (2023) Condition |           |           |             |        | No-build (2030) Condition |           |           |             |        | Build (2030) Condition |           |           |             |        |
|--|---------------------------|-----------|-----------|-------------|--------|---------------------------|-----------|-----------|-------------|--------|------------------------|-----------|-----------|-------------|--------|
|  | LOS                       | Delay (s) | V/C Ratio | Queues (ft) |        | LOS                       | Delay (s) | V/C Ratio | Queues (ft) |        | LOS                    | Delay (s) | V/C Ratio | Queues (ft) |        |
|  |                           |           |           | 50th %      | 95th % |                           |           |           | 50th %      | 95th % |                        |           |           | 50th %      | 95th % |
| <b>Signalized Intersections</b>                  |                           |           |           |             |        |                           |           |           |             |        |                        |           |           |             |        |
| <b>Reed Street/High Street</b>                   | C                         | 31.9      |           |             |        | C                         | 29.4      |           |             |        | C                      | 32.0      |           |             |        |
| Reed Street Eastbound Left/Through/Right         | C                         | 24.3      | 0.81      | 146         | #264   | C                         | 22.4      | 0.78      | 141         | #294   | C                      | 22.7      | 0.79      | 142         | #295   |
| Reed Street Westbound Left/Through/Right         | B                         | 14.4      | 0.50      | 69          | 100    | B                         | 13.3      | 0.43      | 58          | 111    | B                      | 13.3      | 0.43      | 58          | 111    |
| Reed Street Northbound Left/Through/Right        | D                         | 54.0      | 1.01      | ~218        | #358   | D                         | 48.7      | 0.99      | 207         | #407   | D                      | 55.0      | 1.02      | ~223        | #421   |
| Reed Street Southbound Left/Through/Right        | B                         | 13.9      | 0.45      | 71          | 124    | B                         | 14.1      | 0.47      | 74          | 134    | B                      | 14.3      | 0.48      | 76          | 136    |
| North Main Street/Scanlon Drive/Russ Street      | D                         | 43.5      |           |             |        | D                         | 47.7      |           |             |        | D                      | 51.0      |           |             |        |
| Scanlon Drive Eastbound Left                     | E                         | 69.1      | 0.90      | 202         | #357   | E                         | 75.1      | 0.94      | 229         | #436   | F                      | 90.1      | 0.99      | 246         | #471   |
| Scanlon Drive Eastbound Left/Through/Right       | E                         | 61.7      | 0.86      | 197         | #345   | E                         | 67.4      | 0.90      | 227         | #431   | F                      | 84.1      | 0.98      | 249         | #475   |
| Russ Street Westbound Left                       | E                         | 70.3      | 0.69      | 42          | #91    | E                         | 61.5      | 0.61      | 37          | #103   | E                      | 61.6      | 0.61      | 37          | #103   |
| Russ Street Westbound Through/Right              | F                         | 140.4     | 0.98      | 58          | #149   | F                         | 102.4     | 0.86      | 51          | #185   | F                      | 148.5     | 1.01      | ~62         | #210   |
| N Main Street Northbound U-Turn/Left             | B                         | 18.3      | 0.06      | 5           | 14     | B                         | 17.8      | 0.16      | 14          | 31     | B                      | 18.4      | 0.29      | 25          | 48     |
| N Main Street Northbound Through   Through/Right | C                         | 32.3      | 0.80      | 345         | 431    | D                         | 36.4      | 0.86      | 371         | 461    | D                      | 36.3      | 0.86      | 371         | 461    |
| N Main Street Southbound U-Turn/Left             | F                         | 80.3      | 0.99      | 155         | #353   | F                         | 123.5     | 1.12      | ~218        | #414   | F                      | 123.6     | 1.12      | ~218        | #414   |
| N Main Street Southbound Through   Through       | B                         | 16.8      | 0.46      | 130         | 230    | B                         | 19.9      | 0.54      | 198         | 256    | B                      | 20.0      | 0.54      | 198         | 256    |
| N Main Street Southbound Right                   | A                         | 3.5       | 0.17      | 0           | 19     | A                         | 4.4       | 0.20      | 0           | 20     | A                      | 4.7       | 0.30      | 0           | 24     |
| <b>Unsignalized Intersections</b>                |                           |           |           |             |        |                           |           |           |             |        |                        |           |           |             |        |
| <b>High Street/Scanlon Drive</b>                 |                           |           |           |             |        |                           |           |           |             |        |                        |           |           |             |        |
| Scanlon Drive Eastbound Through/Right            | -                         | -         | -         | -           | -      | -                         | -         | -         | -           | -      | A                      | 8.9       | 0.02      | -           | 0      |
| Scanlon Drive Westbound Left/Right               | C                         | 16.8      | 0.70      | -           | 150    | B                         | 13.3      | 0.60      | -           | 103    |                        |           |           |             |        |
| Scanlon Drive Westbound Left/Through             | -                         | -         | -         | -           | -      | -                         | -         | -         | -           | -      | C                      | 15.7      | 0.57      | -           | 3.7    |
| High Street Northbound Through/Right             | B                         | 14.0      | 0.50      | -           | 70     | B                         | 13        | 0.47      | -           | 63     |                        |           |           |             |        |
| High Street Northbound Left/Right                | -                         | -         | -         | -           | -      | -                         | -         | -         | -           | -      | C                      | 16.1      | 0.68      | -           | 5.3    |
| High Street Southbound Left/Through              | A                         | 8.9       | 0.01      | -           | 0      | A                         | 8.7       | 0.00      | -           | 0      |                        |           |           |             |        |

~ = Volume exceeds capacity, queue is theoretically infinite.

# = 95th percentile volume exceeds capacity; queue may be longer. Queue shown is maximum after 2 cycles.

Grey = Indicates a lane movement that decreased to LOS E or LOS F from the Existing Condition to the No-build Condition or decreased to LOS E or LOS F from the No-build Condition to the Build Condition.

Table 10. Capacity Analysis Summary, p.m. Peak Hour

| Intersection/Movement                            | Existing (2023) Condition |           |           |             |        |     | No-build (2030) Condition |           |             |        |     |           | Build (2030) Condition |             |        |        |        |  |
|--|---------------------------|-----------|-----------|-------------|--------|-----|---------------------------|-----------|-------------|--------|-----|-----------|------------------------|-------------|--------|--------|--------|--|
|  | LOS                       | Delay (s) | V/C Ratio | Queues (ft) |        | LOS | Delay (s)                 | V/C Ratio | Queues (ft) |        | LOS | Delay (s) | V/C Ratio              | Queues (ft) |        | 50th % | 95th % |  |
|  |                           |           |           | 50th %      | 95th % |     |                           |           | 50th %      | 95th % |     |           |                        | 50th %      | 95th % |        |        |  |
| <b>Signalized Intersections</b>                  |                           |           |           |             |        |     |                           |           |             |        |     |           |                        |             |        |        |        |  |
| <b>Reed Street/High Street</b>                   | B                         | 14.5      |           |             |        | B   | 16.2                      |           |             |        | B   | 16.8      |                        |             |        |        |        |  |
| Reed Street Eastbound Left/Through/Right         | B                         | 11.9      | 0.44      | 55          | 106    | B   | 12.4                      | 0.48      | 58          | 112    | B   | 12.       | 0.48                   | 58          | 112    |        |        |  |
| Reed Street Westbound Left/Through/Right         | B                         | 15.4      | 0.61      | 68          | 135    | B   | 16.7                      | 0.65      | 74          | #156   | B   | 16.7      | 0.65                   | 74          | #156   |        |        |  |
| Reed Street Northbound Left/Through/Right        | B                         | 12.9      | 0.52      | 68          | 121    | B   | 13.0                      | 0.53      | 70          | 131    | B   | 13.1      | 0.53                   | 71          | 133    |        |        |  |
| Reed Street Southbound Left/Through/Right        | B                         | 16.7      | 0.69      | 98          | #194   | C   | 20.3                      | 0.78      | 117         | #259   | C   | 21.9      | 0.81                   | 123         | #272   |        |        |  |
| North Main Street/Scanlon Drive/Russ Street      | C                         | 28.3      |           |             |        | D   | 37.4                      |           |             |        | D   | 47.5      |                        |             |        |        |        |  |
| Scanlon Drive Eastbound Left                     | D                         | 39.3      | 0.67      | 107         | 185    | D   | 41.5                      | 0.69      | 138         | 224    | E   | 58.7      | 0.88                   | 211         | #374   |        |        |  |
| Scanlon Drive Eastbound Left/Through/Right       | D                         | 37.1      | 0.62      | 101         | 176    | D   | 38.5                      | 0.63      | 129         | 211    | D   | 48.2      | 0.80                   | 193         | #341   |        |        |  |
| Russ Street Westbound Left                       | D                         | 36.6      | 0.25      | 25          | 67     | D   | 37.4                      | 0.24      | 31          | 68     | D   | 38.2      | 0.23                   | 31          | 68     |        |        |  |
| Russ Street Westbound Through/Right              | D                         | 47.1      | 0.68      | 57          | #197   | E   | 55.7                      | 0.77      | 88          | #241   | E   | 65.2      | 0.84                   | 111         | #275   |        |        |  |
| N Main Street Northbound U-Turn/Left             | C                         | 21.4      | 0.13      | 5           | 17     | C   | 23.8                      | 0.25      | 11          | 29     | C   | 27.1      | 0.34                   | 15          | 35     |        |        |  |
| N Main Street Northbound Through   Through/Right | C                         | 26.2      | 0.58      | 167         | 258    | C   | 28.3                      | 0.63      | 200         | 281    | C   | 31.5      | 0.67                   | 201         | 281    |        |        |  |
| N Main Street Southbound U-Turn/Left             | B                         | 14.4      | 0.42      | 50          | 96     | B   | 15.9                      | 0.48      | 61          | 103    | B   | 18.4      | 0.52                   | 61          | 103    |        |        |  |
| N Main Street Southbound Through   Through       | C                         | 30.3      | 0.87      | 277         | #556   | D   | 51.2                      | 0.99      | ~510        | #646   | E   | 69.8      | 1.05                   | ~512        | #646   |        |        |  |
| N Main Street Southbound Right                   | A                         | 6.4       | 0.29      | 0           | 34     | A   | 7.3                       | 0.33      | 0           | 36     | A   | 7.8       | 0.36                   | 0           | 37     |        |        |  |
| <b>Unsignalized Intersections</b>                |                           |           |           |             |        |     |                           |           |             |        |     |           |                        |             |        |        |        |  |
| <b>High Street/Scanlon Drive</b>                 |                           |           |           |             |        |     |                           |           |             |        |     |           |                        |             |        |        |        |  |
| Scanlon Drive Eastbound Through/Right            | -                         | -         | -         | -           | -      | -   | -                         | -         | -           | -      | A   | 9.1       | 0.09                   | -           | 0.3    |        |        |  |
| Scanlon Drive Westbound Left/Right               | B                         | 11        | 0.42      | -           | 53     | B   | 11.2                      | 0.42      | -           | 53     |     |           |                        |             |        |        |        |  |
| Scanlon Drive Westbound Left/Through             | -                         | -         | -         | -           | -      | -   | -                         | -         | -           | -      | D   | 26.5      | 0.81                   | -           | 8.6    |        |        |  |
| High Street Northbound Through/Right             | C                         | 18.3      | 0.69      | -           | 140    | C   | 21.0                      | 0.75      | -           | 170    |     |           |                        |             |        |        |        |  |
| High Street Northbound Left/Right                | -                         | -         | -         | -           | -      | -   | -                         | -         | -           | -      | B   | 12.0      | 0.45                   | -           | 2.3    |        |        |  |
| High Street Southbound Left/Through              | A                         | 8.9       | 0.02      | -           | 3      | A   | 8.9                       | 0.01      | -           | 0      |     |           |                        |             |        |        |        |  |

~ = Volume exceeds capacity, queue is theoretically infinite.

# = 95th percentile volume exceeds capacity; queue may be longer. Queue shown is maximum after 2 cycles.

Grey = Indicates a lane movement that decreased to LOS E or LOS F from the Existing Condition to the No-build Condition or decreased to LOS E or LOS F from the No-build Condition to the Build Condition.

## EXISTING OPERATIONS ANALYSIS SUMMARY

All study area intersections and approaches operate at acceptable levels of service (LOS D or better) during the a.m. and p.m. peak hours in the Existing (2023) Condition except:

- North Main Street/Scanlon Drive/Russ Street
  - The Scanlon Drive Eastbound movements operate at LOS E during the a.m. peak hour.
  - The Russ Street Westbound Left movement operates at LOS E during the a.m. peak hour.
  - The Russ Street Westbound Through/Right movement operates at LOS F during the a.m. peak hour.
  - The North Main Street Southbound U-Turn/Left movement operates at LOS F during the a.m. peak hour.

## NO-BUILD OPERATIONS ANALYSIS SUMMARY

All study area intersections and approaches continue to operate at the same LOS in the No-build Condition as they do in the Existing (2023) Condition during the a.m. and p.m. peak hours except:

- Reed Street/High Street
  - The Reed Street Southbound movement changes from LOS B to LOS C during the p.m. peak hour.
- North Main Street/Scanlon Drive/Russ Street
  - The Russ Street Westbound Through/Right movement changes from LOS D to LOS E during the p.m. peak hour.
  - The North Main Street Northbound Through movement changes from LOS C to LOS D during the a.m. peak hour.
  - The North Main Street Southbound Through movement changes from LOS C to LOS D during the a.m. peak hour.
- Scanlon Drive/High Street
  - The Scanlon Drive westbound through/right changes from LOS C to LOS B during the a.m. peak hour.

## BUILD OPERATIONS ANALYSIS SUMMARY

All study area intersections and approaches continue to operate at the same LOS in the Build Condition as they do in the No-build Condition during the a.m. and p.m. peak hours except:

- North Main Street/Scanlon Drive/Russ Street
  - The Scanlon Drive Eastbound Left movement changes from LOS E to the LOS F during the a.m. peak hour and from LOS D to LOS E during the p.m. peak hour.



- The Scanlon Drive Eastbound Left/Through/Right movement changes from LOS E to LOS F during the a.m. peak hour.
- The North Main Street Southbound Through movement changes from LOS D to LOS E during the p.m. peak hour.

## Transportation Mitigation

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The Proponent will work with the Town of Randolph to create a Project that provides safe access for vehicle trips, improves the pedestrian environment, and encourages carpooling to reduce single occupancy trips to the Project Site. As a means of supporting the extensive existing DCR trails/paths in the area, the project is proposing to construct a trailhead parking area off High Street with approximately 18 parking spaces. Currently there is no way to easily get access to the trails from this area of Randolph, so this improvement will not only create a formal entrance, but also make this nearby amenity more known and visible.

Adjusting the timings at the North Main Street/Scanlon Drive intersection can allow for the eastbound left movement at Scanlon Drive to remain below a forecasted LOS F during the a.m. peak hour. **Table 11** shows the improvements made by these new signal timings.

**Table 11. Mitigation at North Main Street/Scanlon Drive**

| Movement   | Unmitigated (a.m.) |             |           |             |        | Mitigated (a.m.) |             |           |             |        |
|--|--------------------|-------------|-----------|-------------|--------|------------------|-------------|-----------|-------------|--------|
|  | LOS                | Delay (s)   | V/C Ratio | Queues (ft) |        | LOS              | Delay (s)   | V/C Ratio | Queues (ft) |        |
|  |                    |             |           | 50th %      | 95th % |                  |             |           | 50th %      | 95th % |
| <b>North Main Street/Scanlon Drive</b>           | <b>D</b>           | <b>51.0</b> |           |             |        | <b>D</b>         | <b>49.2</b> |           |             |        |
| Scanlon Drive Eastbound Left                     | F                  | 90.1        | 0.99      | 246         | #471   | E                | 76.6        | 0.94      | 256         | #449   |
| Scanlon Drive Eastbound Left/Through/Right       | F                  | 84.1        | 0.98      | 249         | #475   | E                | 71.2        | 0.93      | 260         | #451   |
| Russ Street Westbound Left                       | E                  | 61.6        | 0.61      | 37          | #103   | E                | 56.3        | 0.53      | 39          | #92    |
| Russ Street Westbound Through/Right              | F                  | 148.5       | 1.01      | ~62         | #210   | F                | 106.1       | 0.89      | 64          | #198   |
| N Main Street Northbound U-Turn/Left             | B                  | 18.4        | 0.29      | 25          | 48     | B                | 19.7        | 0.30      | 27          | 51     |
| N Main Street Northbound Through   Through Right | D                  | 36.3        | 0.86      | 371         | 461    | D                | 39.5        | 0.88      | 389         | 484    |
| N Main Street Southbound U-Turn/Left             | F                  | 123.6       | 1.12      | ~218        | #414   | F                | 138.1       | 1.16      | ~238        | #420   |
| N Main Street Southbound Through   Through       | B                  | 20.0        | 0.54      | 198         | 256    | C                | 21.6        | 0.55      | 210         | 271    |
| N Main Street Southbound Right                   | A                  | 4.7         | 0.30      | 0           | 24     | A                | 5.1         | 0.30      | 0           | 25     |



# Conclusion and Recommendations

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A detailed traffic operations analysis was conducted for the nearby intersections. The Project is expected to have minimal impacts on traffic operations at the study area intersections.). The Project is expected to generate approximately 242 new vehicle trips, 24 new transit trips, and 6 new walk/bicycle trips during the weekday a.m. peak hour, and 241 new vehicle trips, 23 new transit trips, and 6 new walk/bicycle trips during the weekday p.m. peak hour. The Project is expected to see 184 net new trips for the a.m. peak hour and 171 net new trips during the p.m. peak hour compared to the existing conditions. Parking will be reduced to 324 spaces. Placement of loading operations at the back of the site will maintain a welcoming frontage along Scanlon Drive and the extensive landscaping will add much needed green elements to a street that today is overwhelmed by pavement. The Project's construction of a DCR trailhead will support more recreational use of park facilities in the area for residents and new employees of the site.



HOWARD STEIN HUDSON

Engineers + Planners

## Appendix A

### Traffic Count Data

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 1  
 Location: Randolph, MA  
 Street 1: High Street  
 Street 2: Reed Street  
 Count Date: 9/13/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701  
 Office: 978-746-1259  
 DataRequest@BostonTrafficData.com  
 www.BostonTrafficData.com

## PASSENGER CARS & HEAVY VEHICLES COMBINED

|            | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Reed Street Eastbound |      |      |       | Reed Street Westbound |      |      |       |
|------------|------------------------|------|------|-------|------------------------|------|------|-------|-----------------------|------|------|-------|-----------------------|------|------|-------|
| Start Time | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                | Left | Thru | Right | U-Turn                | Left | Thru | Right |
| 7:00 AM    | 0                      | 1    | 88   | 19    | 0                      | 1    | 41   | 12    | 0                     | 54   | 46   | 1     | 0                     | 6    | 35   | 4     |
| 7:15 AM    | 0                      | 2    | 74   | 27    | 0                      | 3    | 55   | 19    | 0                     | 41   | 52   | 0     | 0                     | 19   | 36   | 1     |
| 7:30 AM    | 0                      | 4    | 93   | 32    | 0                      | 4    | 46   | 19    | 0                     | 51   | 76   | 1     | 0                     | 9    | 43   | 2     |
| 7:45 AM    | 0                      | 4    | 82   | 31    | 0                      | 1    | 39   | 17    | 0                     | 35   | 58   | 1     | 0                     | 15   | 52   | 2     |
| 8:00 AM    | 0                      | 17   | 93   | 35    | 0                      | 4    | 50   | 22    | 0                     | 34   | 57   | 0     | 0                     | 11   | 48   | 2     |
| 8:15 AM    | 0                      | 24   | 74   | 20    | 0                      | 0    | 62   | 16    | 0                     | 34   | 70   | 7     | 0                     | 12   | 62   | 2     |
| 8:30 AM    | 0                      | 11   | 83   | 31    | 0                      | 1    | 39   | 25    | 0                     | 49   | 81   | 4     | 0                     | 13   | 27   | 1     |
| 8:45 AM    | 0                      | 4    | 120  | 46    | 0                      | 0    | 37   | 19    | 0                     | 38   | 70   | 2     | 0                     | 19   | 30   | 2     |

|            | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Reed Street Eastbound |      |      |       | Reed Street Westbound |      |      |       |
|------------|------------------------|------|------|-------|------------------------|------|------|-------|-----------------------|------|------|-------|-----------------------|------|------|-------|
| Start Time | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                | Left | Thru | Right | U-Turn                | Left | Thru | Right |
| 4:00 PM    | 0                      | 1    | 44   | 11    | 0                      | 2    | 83   | 30    | 0                     | 20   | 30   | 1     | 0                     | 29   | 45   | 0     |
| 4:15 PM    | 0                      | 4    | 49   | 18    | 0                      | 0    | 97   | 32    | 0                     | 15   | 43   | 2     | 0                     | 26   | 41   | 1     |
| 4:30 PM    | 0                      | 1    | 50   | 19    | 0                      | 0    | 68   | 37    | 0                     | 18   | 51   | 4     | 0                     | 31   | 57   | 0     |
| 4:45 PM    | 0                      | 2    | 51   | 21    | 0                      | 2    | 81   | 29    | 0                     | 21   | 48   | 2     | 0                     | 21   | 50   | 2     |
| 5:00 PM    | 0                      | 1    | 73   | 18    | 0                      | 1    | 86   | 26    | 0                     | 21   | 53   | 3     | 0                     | 27   | 53   | 0     |
| 5:15 PM    | 0                      | 1    | 59   | 25    | 0                      | 3    | 81   | 38    | 0                     | 19   | 35   | 1     | 0                     | 30   | 46   | 3     |
| 5:30 PM    | 0                      | 1    | 42   | 16    | 0                      | 1    | 64   | 37    | 0                     | 21   | 44   | 0     | 0                     | 13   | 38   | 4     |
| 5:45 PM    | 0                      | 3    | 39   | 15    | 0                      | 1    | 77   | 26    | 0                     | 15   | 39   | 2     | 0                     | 25   | 24   | 3     |

| AM PEAK HOUR<br>8:00 AM<br>to<br>9:00 AM | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Reed Street Eastbound |      |      |       | Reed Street Westbound |      |      |       |      |      |
|--|------------------------|------|------|-------|------------------------|------|------|-------|-----------------------|------|------|-------|-----------------------|------|------|-------|------|------|
|  | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                | Left | Thru | Right | U-Turn                | Left | Thru | Right |      |      |
|  | 0                      | 56   | 370  | 132   | 0                      | 5    | 188  | 82    | 0                     | 155  | 278  | 13    | 0                     | 55   | 167  | 7     |      |      |
| PHF<br>HV %                              |                        | 0.82 |      | 0.88  |                        | 0.83 |      | 0.75  |                       | 0.0% | 0.0% | 4.6%  | 2.3%                  | 0.0% | 0.0% | 10.9% | 3.0% | 0.0% |

| PM PEAK HOUR<br>4:30 PM<br>to<br>5:30 PM | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Reed Street Eastbound |      |      |       | Reed Street Westbound |      |      |       |      |      |
|--|------------------------|------|------|-------|------------------------|------|------|-------|-----------------------|------|------|-------|-----------------------|------|------|-------|------|------|
|  | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                | Left | Thru | Right | U-Turn                | Left | Thru | Right |      |      |
|  | 0                      | 5    | 233  | 83    | 0                      | 6    | 316  | 130   | 0                     | 79   | 187  | 10    | 0                     | 109  | 206  | 5     |      |      |
| PHF<br>HV %                              |                        | 0.87 |      | 0.93  |                        | 0.90 |      | 0.91  |                       | 0.0% | 0.0% | 2.1%  | 1.2%                  | 0.0% | 0.0% | 3.7%  | 0.0% | 0.0% |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 1  
 Location: Randolph, MA  
 Street 1: High Street  
 Street 2: Reed Street  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

**HEAVY VEHICLES**

| Start Time | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Reed Street Eastbound |      |      |       | Reed Street Westbound |      |      |       |
|------------|------------------------|------|------|-------|------------------------|------|------|-------|-----------------------|------|------|-------|-----------------------|------|------|-------|
|            | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                | Left | Thru | Right | U-Turn                | Left | Thru | Right |
| 7:00 AM    | 0                      | 0    | 3    | 3     | 0                      | 0    | 0    | 0     | 0                     | 2    | 1    | 0     | 0                     | 1    | 1    | 0     |
| 7:15 AM    | 0                      | 0    | 1    | 1     | 0                      | 0    | 3    | 0     | 0                     | 0    | 2    | 0     | 0                     | 2    | 4    | 0     |
| 7:30 AM    | 0                      | 0    | 4    | 4     | 0                      | 0    | 1    | 0     | 0                     | 2    | 2    | 0     | 0                     | 0    | 0    | 0     |
| 7:45 AM    | 0                      | 0    | 1    | 2     | 0                      | 0    | 0    | 0     | 0                     | 2    | 1    | 0     | 0                     | 0    | 1    | 0     |
| 8:00 AM    | 0                      | 0    | 3    | 0     | 0                      | 0    | 2    | 1     | 0                     | 1    | 1    | 0     | 0                     | 1    | 2    | 0     |
| 8:15 AM    | 0                      | 0    | 4    | 0     | 0                      | 0    | 4    | 0     | 0                     | 0    | 0    | 0     | 0                     | 2    | 1    | 0     |
| 8:30 AM    | 0                      | 0    | 5    | 2     | 0                      | 0    | 4    | 0     | 0                     | 1    | 2    | 0     | 0                     | 1    | 1    | 0     |
| 8:45 AM    | 0                      | 0    | 5    | 1     | 0                      | 0    | 3    | 0     | 0                     | 0    | 1    | 0     | 0                     | 2    | 1    | 0     |

| Start Time | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Reed Street Eastbound |      |      |       | Reed Street Westbound |      |      |       |
|------------|------------------------|------|------|-------|------------------------|------|------|-------|-----------------------|------|------|-------|-----------------------|------|------|-------|
|            | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                | Left | Thru | Right | U-Turn                | Left | Thru | Right |
| 4:00 PM    | 0                      | 0    | 0    | 0     | 0                      | 0    | 4    | 0     | 0                     | 0    | 0    | 0     | 0                     | 0    | 3    | 0     |
| 4:15 PM    | 0                      | 0    | 1    | 0     | 0                      | 0    | 6    | 0     | 0                     | 0    | 2    | 0     | 0                     | 0    | 2    | 0     |
| 4:30 PM    | 0                      | 0    | 2    | 0     | 0                      | 0    | 2    | 0     | 0                     | 0    | 1    | 0     | 0                     | 3    | 0    | 0     |
| 4:45 PM    | 0                      | 0    | 0    | 0     | 0                      | 0    | 1    | 0     | 0                     | 0    | 1    | 0     | 0                     | 1    | 0    | 0     |
| 5:00 PM    | 0                      | 0    | 2    | 0     | 0                      | 0    | 2    | 2     | 0                     | 0    | 0    | 0     | 0                     | 0    | 0    | 0     |
| 5:15 PM    | 0                      | 0    | 1    | 1     | 0                      | 0    | 3    | 0     | 0                     | 0    | 0    | 0     | 0                     | 0    | 0    | 0     |
| 5:30 PM    | 0                      | 0    | 0    | 1     | 0                      | 0    | 1    | 1     | 0                     | 1    | 0    | 0     | 0                     | 0    | 2    | 0     |
| 5:45 PM    | 0                      | 0    | 0    | 0     | 0                      | 0    | 2    | 0     | 0                     | 0    | 0    | 0     | 0                     | 1    | 4    | 0     |

| AM PEAK HOUR<br>8:00 AM<br>to<br>9:00 AM | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Reed Street Eastbound |      |      |       | Reed Street Westbound |      |      |       |
|--|------------------------|------|------|-------|------------------------|------|------|-------|-----------------------|------|------|-------|-----------------------|------|------|-------|
|  | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                | Left | Thru | Right | U-Turn                | Left | Thru | Right |
|  | 0                      | 0    | 17   | 3     | 0                      | 0    | 13   | 1     | 0                     | 2    | 4    | 0     | 0                     | 6    | 5    | 0     |
| PHF                                      | 0.71                   |      |      |       | 0.88                   |      |      |       | 0.50                  |      |      |       | 0.92                  |      |      |       |

| PM PEAK HOUR<br>4:00 PM<br>to<br>5:00 PM | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Reed Street Eastbound |      |      |       | Reed Street Westbound |      |      |       |
|--|------------------------|------|------|-------|------------------------|------|------|-------|-----------------------|------|------|-------|-----------------------|------|------|-------|
|  | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                | Left | Thru | Right | U-Turn                | Left | Thru | Right |
|  | 0                      | 0    | 3    | 0     | 0                      | 0    | 13   | 0     | 0                     | 0    | 4    | 0     | 0                     | 4    | 5    | 0     |
| PHF                                      | 0.38                   |      |      |       | 0.54                   |      |      |       | 0.50                  |      |      |       | 0.75                  |      |      |       |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 1  
 Location: Randolph, MA  
 Street 1: High Street  
 Street 2: Reed Street  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701  
 Office: 978-746-1259  
[DataRequest@BostonTrafficData.com](mailto:DataRequest@BostonTrafficData.com)  
[www.BostonTrafficData.com](http://www.BostonTrafficData.com)

## PEDESTRIANS & BICYCLES

|            | High Street Northbound |      |       |     | High Street Southbound |      |       |     | Reed Street Eastbound |      |       |     | Reed Street Westbound |      |       |     |
|------------|------------------------|------|-------|-----|------------------------|------|-------|-----|-----------------------|------|-------|-----|-----------------------|------|-------|-----|
| Start Time | Left                   | Thru | Right | PED | Left                   | Thru | Right | PED | Left                  | Thru | Right | PED | Left                  | Thru | Right | PED |
| 7:00 AM    | 0                      | 0    | 0     | 1   | 0                      | 0    | 0     | 3   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 1   |
| 7:15 AM    | 0                      | 0    | 0     | 1   | 0                      | 0    | 0     | 1   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 0   |
| 7:30 AM    | 0                      | 0    | 0     | 0   | 0                      | 0    | 0     | 2   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 0   |
| 7:45 AM    | 0                      | 0    | 0     | 0   | 0                      | 0    | 0     | 0   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 0   |
| 8:00 AM    | 0                      | 0    | 0     | 1   | 0                      | 0    | 0     | 10  | 0                     | 0    | 0     | 0   | 1                     | 0    | 0     | 2   |
| 8:15 AM    | 0                      | 0    | 0     | 6   | 0                      | 0    | 0     | 31  | 0                     | 0    | 0     | 5   | 0                     | 0    | 0     | 0   |
| 8:30 AM    | 0                      | 0    | 0     | 9   | 0                      | 0    | 0     | 5   | 0                     | 0    | 0     | 7   | 0                     | 0    | 0     | 2   |
| 8:45 AM    | 0                      | 0    | 0     | 1   | 0                      | 0    | 0     | 0   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 0   |

|            | High Street Northbound |      |       |     | High Street Southbound |      |       |     | Reed Street Eastbound |      |       |     | Reed Street Westbound |      |       |     |
|------------|------------------------|------|-------|-----|------------------------|------|-------|-----|-----------------------|------|-------|-----|-----------------------|------|-------|-----|
| Start Time | Left                   | Thru | Right | PED | Left                   | Thru | Right | PED | Left                  | Thru | Right | PED | Left                  | Thru | Right | PED |
| 4:00 PM    | 0                      | 0    | 0     | 1   | 0                      | 0    | 0     | 0   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 0   |
| 4:15 PM    | 0                      | 0    | 0     | 1   | 0                      | 0    | 0     | 0   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 0   |
| 4:30 PM    | 0                      | 0    | 0     | 3   | 0                      | 0    | 0     | 3   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 0   |
| 4:45 PM    | 0                      | 0    | 0     | 2   | 0                      | 0    | 0     | 0   | 0                     | 0    | 0     | 4   | 0                     | 0    | 0     | 0   |
| 5:00 PM    | 0                      | 1    | 0     | 0   | 0                      | 0    | 0     | 0   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 0   |
| 5:15 PM    | 0                      | 0    | 0     | 1   | 0                      | 0    | 0     | 0   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 0   |
| 5:30 PM    | 0                      | 0    | 0     | 0   | 0                      | 0    | 0     | 0   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 0   |
| 5:45 PM    | 0                      | 0    | 0     | 1   | 0                      | 0    | 0     | 0   | 0                     | 0    | 0     | 0   | 0                     | 0    | 0     | 0   |

| AM PEAK HOUR <sup>1</sup><br>8:00 AM<br>to<br>9:00 AM | High Street Northbound |      |       |     | High Street Southbound |      |       |     | Reed Street Eastbound |      |       |     | Reed Street Westbound |      |       |     |
|---|------------------------|------|-------|-----|------------------------|------|-------|-----|-----------------------|------|-------|-----|-----------------------|------|-------|-----|
|   | Left                   | Thru | Right | PED | Left                   | Thru | Right | PED | Left                  | Thru | Right | PED | Left                  | Thru | Right | PED |
|   | 0                      | 0    | 0     | 17  | 0                      | 0    | 0     | 46  | 0                     | 0    | 0     | 12  | 1                     | 0    | 0     | 4   |

| PM PEAK HOUR <sup>1</sup><br>4:30 PM<br>to<br>5:30 PM | High Street Northbound |      |       |     | High Street Southbound |      |       |     | Reed Street Eastbound |      |       |     | Reed Street Westbound |      |       |     |
|---|------------------------|------|-------|-----|------------------------|------|-------|-----|-----------------------|------|-------|-----|-----------------------|------|-------|-----|
|   | Left                   | Thru | Right | PED | Left                   | Thru | Right | PED | Left                  | Thru | Right | PED | Left                  | Thru | Right | PED |
|   | 0                      | 1    | 0     | 6   | 0                      | 0    | 0     | 3   | 0                     | 0    | 0     | 4   | 0                     | 0    | 0     | 0   |

<sup>1</sup>NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 2  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: High Street  
 Count Date: 9/13/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701  
 Office: 978-746-1259  
 DataRequest@BostonTrafficData.com  
 www.BostonTrafficData.com

## PASSENGER CARS & HEAVY VEHICLES COMBINED

| Start Time | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------------------|------|------|-------|------------------------|------|------|-------|-----------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn    | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0                      | 0    | 4    | 141   | 0                      | 2    | 2    | 0     | 0         | 0    | 0    | 0     | 0                       | 49   | 0    | 1     |
| 7:15 AM    | 0                      | 0    | 0    | 115   | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 52   | 0    | 1     |
| 7:30 AM    | 0                      | 0    | 4    | 102   | 0                      | 0    | 1    | 0     | 0         | 0    | 0    | 0     | 0                       | 55   | 0    | 0     |
| 7:45 AM    | 0                      | 0    | 1    | 117   | 0                      | 0    | 1    | 0     | 0         | 0    | 0    | 0     | 0                       | 54   | 0    | 0     |
| 8:00 AM    | 0                      | 0    | 2    | 105   | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 75   | 0    | 3     |
| 8:15 AM    | 0                      | 0    | 1    | 89    | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 80   | 0    | 1     |
| 8:30 AM    | 0                      | 0    | 0    | 99    | 0                      | 1    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 64   | 0    | 0     |
| 8:45 AM    | 0                      | 0    | 0    | 145   | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 53   | 0    | 0     |

| Start Time | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------------------|------|------|-------|------------------------|------|------|-------|-----------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn    | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0                      | 0    | 0    | 57    | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 121  | 0    | 0     |
| 4:15 PM    | 0                      | 0    | 0    | 65    | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 125  | 0    | 0     |
| 4:30 PM    | 0                      | 0    | 1    | 57    | 0                      | 1    | 2    | 0     | 0         | 0    | 0    | 0     | 0                       | 117  | 0    | 0     |
| 4:45 PM    | 0                      | 0    | 1    | 58    | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 115  | 0    | 0     |
| 5:00 PM    | 0                      | 0    | 0    | 82    | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 127  | 0    | 0     |
| 5:15 PM    | 0                      | 0    | 0    | 75    | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 112  | 0    | 0     |
| 5:30 PM    | 0                      | 0    | 1    | 56    | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 102  | 0    | 0     |
| 5:45 PM    | 0                      | 0    | 0    | 49    | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 127  | 0    | 0     |

| AM PEAK HOUR             | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------------------|------|------|-------|------------------------|------|------|-------|-----------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn    | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 8:00 AM<br>to<br>9:00 AM | 0                      | 0    | 3    | 438   | 0                      | 1    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 272  | 0    | 4     |
| PHF                      | 0.76                   |      |      |       | 0.25                   |      |      |       | 0.00      |      |      |       | 0.85                    |      |      |       |
| HV %                     | 0.0%                   | 0.0% | 0.0% | 3.7%  | 0.0%                   | 0.0% | 0.0% | 0.0%  | 0.0%      | 0.0% | 0.0% | 0.0%  | 0.0%                    | 5.1% | 0.0% | 0.0%  |

| PM PEAK HOUR             | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------------------|------|------|-------|------------------------|------|------|-------|-----------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn    | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:15 PM<br>to<br>5:15 PM | 0                      | 0    | 2    | 262   | 0                      | 1    | 2    | 0     | 0         | 0    | 0    | 0     | 0                       | 484  | 0    | 0     |
| PHF                      | 0.80                   |      |      |       | 0.25                   |      |      |       | 0.00      |      |      |       | 0.95                    |      |      |       |
| HV %                     | 0.0%                   | 0.0% | 0.0% | 2.3%  | 0.0%                   | 0.0% | 0.0% | 0.0%  | 0.0%      | 0.0% | 0.0% | 0.0%  | 0.0%                    | 2.9% | 0.0% | 0.0%  |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 2  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: High Street  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701  
 Office: 978-746-1259  
 DataRequest@BostonTrafficData.com  
 www.BostonTrafficData.com

## HEAVY VEHICLES

| Start Time | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------------------|------|------|-------|------------------------|------|------|-------|-----------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn    | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0                      | 0    | 0    | 5     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 1    | 0    | 0     |
| 7:15 AM    | 0                      | 0    | 0    | 2     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 3    | 0    | 0     |
| 7:30 AM    | 0                      | 0    | 0    | 4     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 1    | 0    | 0     |
| 7:45 AM    | 0                      | 0    | 0    | 4     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 0    | 0    | 0     |
| 8:00 AM    | 0                      | 0    | 0    | 3     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 3    | 0    | 0     |
| 8:15 AM    | 0                      | 0    | 0    | 3     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 5    | 0    | 0     |
| 8:30 AM    | 0                      | 0    | 0    | 6     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 3    | 0    | 0     |
| 8:45 AM    | 0                      | 0    | 0    | 4     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 3    | 0    | 0     |

| Start Time | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------------------|------|------|-------|------------------------|------|------|-------|-----------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn    | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0                      | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 7    | 0    | 0     |
| 4:15 PM    | 0                      | 0    | 0    | 1     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 6    | 0    | 0     |
| 4:30 PM    | 0                      | 0    | 0    | 2     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 3    | 0    | 0     |
| 4:45 PM    | 0                      | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 1    | 0    | 0     |
| 5:00 PM    | 0                      | 0    | 0    | 3     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 4    | 0    | 0     |
| 5:15 PM    | 0                      | 0    | 0    | 1     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 3    | 0    | 0     |
| 5:30 PM    | 0                      | 0    | 0    | 2     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 3    | 0    | 0     |
| 5:45 PM    | 0                      | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 3    | 0    | 0     |

| AM PEAK HOUR<br>8:00 AM<br>to<br>9:00 AM | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------------------|------|------|-------|------------------------|------|------|-------|-----------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn    | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0                      | 0    | 0    | 16    | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 14   | 0    | 0     |
| PHF                                      | 0.67                   |      |      |       | 0.00                   |      |      |       | 0.00      |      |      |       | 0.70                    |      |      |       |

| PM PEAK HOUR<br>4:00 PM<br>to<br>5:00 PM | High Street Northbound |      |      |       | High Street Southbound |      |      |       | Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------------------|------|------|-------|------------------------|------|------|-------|-----------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn                 | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn    | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0                      | 0    | 0    | 3     | 0                      | 0    | 0    | 0     | 0         | 0    | 0    | 0     | 0                       | 17   | 0    | 0     |
| PHF                                      | 0.38                   |      |      |       | 0.00                   |      |      |       | 0.00      |      |      |       | 0.61                    |      |      |       |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 2  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: High Street  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701  
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 www.BostonTrafficData.com

## PEDESTRIANS & BICYCLES

| Start Time | High Street Northbound |      |       | High Street Southbound |      |      | Eastbound |     |      | Scanlon Drive Westbound |       |     |      |      |       |     |
|------------|------------------------|------|-------|------------------------|------|------|-----------|-----|------|-------------------------|-------|-----|------|------|-------|-----|
|            | Left                   | Thru | Right | PED                    | Left | Thru | Right     | PED | Left | Thru                    | Right | PED | Left | Thru | Right | PED |
| 7:00 AM    | 0                      | 0    | 0     | 0                      | 0    | 0    | 0         | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 7:15 AM    | 0                      | 0    | 0     | 0                      | 0    | 0    | 0         | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 7:30 AM    | 0                      | 0    | 0     | 0                      | 0    | 0    | 0         | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 7:45 AM    | 0                      | 0    | 0     | 0                      | 0    | 0    | 0         | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 8:00 AM    | 0                      | 0    | 0     | 0                      | 0    | 0    | 0         | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 08:15 AM   | 0                      | 0    | 0     | 0                      | 0    | 0    | 0         | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 08:30 AM   | 0                      | 0    | 0     | 0                      | 0    | 0    | 0         | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 08:45 AM   | 0                      | 0    | 0     | 0                      | 0    | 0    | 0         | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |

| Start Time | High Street Northbound |      |      | High Street Southbound |        |      | Eastbound |       |        | Scanlon Drive Westbound |      |       |        |      |      |       |
|------------|------------------------|------|------|------------------------|--------|------|-----------|-------|--------|-------------------------|------|-------|--------|------|------|-------|
|            | U-Turn                 | Left | Thru | Right                  | U-Turn | Left | Thru      | Right | U-Turn | Left                    | Thru | Right | U-Turn | Left | Thru | Right |
| 4:00 PM    | 0                      | 0    | 0    | 0                      | 0      | 0    | 0         | 0     | 0      | 0                       | 0    | 0     | 0      | 0    | 0    | 0     |
| 4:15 PM    | 0                      | 0    | 0    | 0                      | 0      | 0    | 0         | 0     | 0      | 0                       | 0    | 0     | 0      | 0    | 0    | 0     |
| 4:30 PM    | 0                      | 0    | 0    | 0                      | 0      | 0    | 0         | 0     | 0      | 0                       | 0    | 0     | 0      | 0    | 0    | 0     |
| 4:45 PM    | 0                      | 1    | 0    | 0                      | 0      | 0    | 0         | 0     | 0      | 0                       | 0    | 0     | 2      | 0    | 0    | 0     |
| 5:00 PM    | 0                      | 0    | 0    | 0                      | 0      | 0    | 0         | 0     | 0      | 0                       | 0    | 0     | 0      | 0    | 0    | 0     |
| 5:15 PM    | 0                      | 0    | 0    | 0                      | 0      | 0    | 0         | 0     | 0      | 0                       | 0    | 0     | 0      | 0    | 0    | 0     |
| 5:30 PM    | 0                      | 0    | 0    | 0                      | 0      | 0    | 0         | 0     | 0      | 0                       | 0    | 0     | 0      | 0    | 0    | 0     |
| 5:45 PM    | 0                      | 0    | 0    | 0                      | 0      | 0    | 0         | 0     | 0      | 0                       | 0    | 0     | 0      | 0    | 0    | 0     |

| AM PEAK HOUR <sup>1</sup> | High Street Northbound |      |      | High Street Southbound |        |      | Eastbound |       |        | Scanlon Drive Westbound |      |       |        |      |      |       |
|---------------------------|------------------------|------|------|------------------------|--------|------|-----------|-------|--------|-------------------------|------|-------|--------|------|------|-------|
|                           | U-Turn                 | Left | Thru | Right                  | U-Turn | Left | Thru      | Right | U-Turn | Left                    | Thru | Right | U-Turn | Left | Thru | Right |
| 8:00 AM<br>to<br>9:00 AM  | 0                      | 0    | 0    | 0                      | 0      | 0    | 0         | 0     | 0      | 0                       | 0    | 0     | 0      | 0    | 0    | 0     |

| PM PEAK HOUR <sup>1</sup> | High Street Northbound |      |      | High Street Southbound |        |      | Eastbound |       |        | Scanlon Drive Westbound |      |       |        |      |      |       |
|---------------------------|------------------------|------|------|------------------------|--------|------|-----------|-------|--------|-------------------------|------|-------|--------|------|------|-------|
|                           | U-Turn                 | Left | Thru | Right                  | U-Turn | Left | Thru      | Right | U-Turn | Left                    | Thru | Right | U-Turn | Left | Thru | Right |
| 4:15 PM<br>to<br>5:15 PM  | 0                      | 1    | 0    | 0                      | 0      | 0    | 0         | 0     | 0      | 0                       | 0    | 0     | 2      | 0    | 0    | 0     |

<sup>1</sup>NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 3A  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #1 combine 2 driveways  
 Count Date: 9/13/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701  
 Office: 978-746-1259  
 DataRequest@BostonTrafficData.com  
 www.BostonTrafficData.com

## PASSENGER CARS & HEAVY VEHICLES COMBINED

| Start Time | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 1    | 142  | 0     | 0                       | 0    | 0    | 50    | 0                       |      |      |       |
| 7:15 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 1    | 117  | 0     | 0                       | 0    | 0    | 53    | 0                       |      |      |       |
| 7:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 100  | 0     | 0                       | 0    | 0    | 55    | 0                       |      |      |       |
| 7:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 120  | 0     | 1                       | 0    | 0    | 54    | 0                       |      |      |       |
| 8:00 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 1          | 0    | 104  | 0     | 0                       | 0    | 0    | 78    | 0                       |      |      |       |
| 8:15 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 90   | 0     | 1                       | 0    | 0    | 81    | 0                       |      |      |       |
| 8:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 1    | 98   | 0     | 0                       | 0    | 0    | 64    | 0                       |      |      |       |
| 8:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 145  | 0     | 0                       | 0    | 0    | 53    | 0                       |      |      |       |

| Start Time | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 56   | 0     | 0                       | 0    | 0    | 122   | 0                       |      |      |       |
| 4:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 65   | 0     | 0                       | 0    | 0    | 125   | 1                       |      |      |       |
| 4:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 1    | 57   | 0     | 0                       | 0    | 0    | 117   | 0                       |      |      |       |
| 4:45 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 58   | 0     | 0                       | 0    | 0    | 115   | 0                       |      |      |       |
| 5:00 PM    | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 0     | 0          | 0    | 82   | 0     | 0                       | 0    | 0    | 127   | 0                       |      |      |       |
| 5:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 74   | 0     | 0                       | 0    | 0    | 113   | 0                       |      |      |       |
| 5:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 57   | 0     | 0                       | 0    | 0    | 102   | 0                       |      |      |       |
| 5:45 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 50   | 0     | 0                       | 0    | 0    | 124   | 0                       |      |      |       |

| AM PEAK HOUR             | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 8:00 AM<br>to<br>9:00 AM | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 1          | 1    | 437  | 0     | 1                       | 0    | 0    | 276   | 0                       |      |      |       |
| PHF                      | 0.00       |      |      |       | 0.00                            |      |      |       | 0.76       |      |      |       | 0.84                    |      |      |       |                         |      |      |       |
| HV %                     | 0.0%       | 0.0% | 0.0% | 0.0%  | 0.0%                            | 0.0% | 0.0% | 0.0%  | 0.0%       | 0.0% | 3.7% | 0.0%  | 0.0%                    | 0.0% | 0.0% | 5.1%  | 0.0%                    | 0.0% | 2.7% | 0.0%  |

| PM PEAK HOUR             | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:15 PM<br>to<br>5:15 PM | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 0     | 0          | 1    | 262  | 0     | 0                       | 0    | 0    | 484   | 1                       |      |      |       |
| PHF                      | 0.00       |      |      |       | 0.25                            |      |      |       | 0.80       |      |      |       | 0.95                    |      |      |       |                         |      |      |       |
| HV %                     | 0.0%       | 0.0% | 0.0% | 0.0%  | 0.0%                            | 0.0% | 0.0% | 0.0%  | 0.0%       | 0.0% | 2.3% | 0.0%  | 0.0%                    | 0.0% | 0.0% | 5.1%  | 0.0%                    | 0.0% | 2.7% | 0.0%  |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 3A  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #1 combine 2 driveways  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

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 DataRequest@BostonTrafficData.com  
 www.BostonTrafficData.com

## HEAVY VEHICLES

| Start Time | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 5    | 0     | 0                       | 0    | 1    | 0     |
| 7:15 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 3    | 0     |
| 7:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 1    | 0     |
| 7:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 0    | 0     |
| 8:00 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 3    | 0     |
| 8:15 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 5    | 0     |
| 8:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 6    | 0     | 0                       | 0    | 3    | 0     |
| 8:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 3    | 0     |

| Start Time | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 0    | 0     | 0                       | 0    | 7    | 0     |
| 4:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 1    | 0     | 0                       | 0    | 5    | 0     |
| 4:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 3    | 0     |
| 4:45 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 0    | 0     | 0                       | 0    | 1    | 0     |
| 5:00 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 4    | 0     |
| 5:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 1    | 0     | 0                       | 0    | 3    | 0     |
| 5:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 3    | 0     |
| 5:45 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 0    | 0     | 0                       | 0    | 3    | 0     |

| AM PEAK HOUR<br>8:00 AM<br>to<br>9:00 AM | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 16   | 0     | 0                       | 0    | 14   | 0     |
| PHF                                      | 0.00       |      |      |       | 0.00                            |      |      |       | 0.67                    |      |      |       | 0.70                    |      |      |       |

| PM PEAK HOUR<br>4:00 PM<br>to<br>5:00 PM | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 16   | 0     |
| PHF                                      | 0.00       |      |      |       | 0.00                            |      |      |       | 0.38                    |      |      |       | 0.57                    |      |      |       |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 3A  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #1 combine 2 driveways  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

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 Office: 978-746-1259  
 DataRequest@BostonTrafficData.com  
 www.BostonTrafficData.com

## PEDESTRIANS & BICYCLES

| Start Time | Northbound |      |       |     | Driveway #1 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|            | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 7:00 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 1   |
| 7:15 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 1   | 0                       | 0    | 0     | 0   |
| 7:30 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 7:45 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 1   | 0                       | 0    | 0     | 0   |
| 8:00 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 08:15 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 08:30 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 1   |
| 08:45 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |

| Start Time | Northbound |      |       |     | Driveway #1 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|            | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 4:00 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 4:15 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 4:30 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 4:45 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 2    | 0     | 0   |
| 5:00 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 5:15 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 5:30 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 5:45 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |

| AM PEAK HOUR <sup>1</sup> | Northbound |      |       |     | Driveway #1 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|---------------------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|                           | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 8:00 AM<br>to<br>9:00 AM  | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 1   |

| PM PEAK HOUR <sup>1</sup> | Northbound |      |       |     | Driveway #1 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|---------------------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|                           | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 4:15 PM<br>to<br>5:15 PM  | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 2    | 0     | 0   |

<sup>1</sup>NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 3B  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #1 combine 2 driveways  
 Count Date: 9/13/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

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## PASSENGER CARS & HEAVY VEHICLES COMBINED

| Start Time | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 142  | 0     | 0                       | 0    | 0    | 50    | 0                       |      |      |       |
| 7:15 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 118  | 0     | 0                       | 0    | 0    | 54    | 0                       |      |      |       |
| 7:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 99   | 0     | 0                       | 0    | 0    | 56    | 0                       |      |      |       |
| 7:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 122  | 0     | 0                       | 0    | 0    | 55    | 0                       |      |      |       |
| 8:00 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 104  | 0     | 0                       | 1    | 0    | 78    | 0                       |      |      |       |
| 8:15 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 92   | 0     | 0                       | 0    | 0    | 82    | 0                       |      |      |       |
| 8:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 97   | 0     | 0                       | 0    | 0    | 63    | 0                       |      |      |       |
| 8:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 145  | 0     | 0                       | 0    | 0    | 54    | 0                       |      |      |       |

| Start Time | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 56   | 0     | 0                       | 0    | 0    | 123   | 0                       |      |      |       |
| 4:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 66   | 0     | 0                       | 0    | 0    | 125   | 0                       |      |      |       |
| 4:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 57   | 0     | 0                       | 0    | 0    | 118   | 0                       |      |      |       |
| 4:45 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 58   | 0     | 0                       | 0    | 0    | 115   | 0                       |      |      |       |
| 5:00 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 82   | 0     | 0                       | 0    | 0    | 127   | 0                       |      |      |       |
| 5:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 73   | 0     | 0                       | 0    | 0    | 112   | 0                       |      |      |       |
| 5:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 57   | 0     | 0                       | 0    | 0    | 102   | 0                       |      |      |       |
| 5:45 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 51   | 0     | 0                       | 0    | 0    | 124   | 0                       |      |      |       |

| AM PEAK HOUR             | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 8:00 AM<br>to<br>9:00 AM | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 438  | 0     | 1                       | 0    | 277  | 0     |                         |      |      |       |
| PHF                      | 0.00       |      |      |       | 0.00                            |      |      |       | 0.76       |      |      |       | 0.85                    |      |      |       |                         |      |      |       |
| HV %                     | 0.0%       | 0.0% | 0.0% | 0.0%  | 0.0%                            | 0.0% | 0.0% | 0.0%  | 0.0%       | 0.0% | 3.7% | 0.0%  | 0.0%                    | 0.0% | 0.0% | 5.1%  | 0.0%                    | 0.0% | 2.7% | 0.0%  |

| PM PEAK HOUR             | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:15 PM<br>to<br>5:15 PM | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0          | 0    | 263  | 0     | 0                       | 0    | 0    | 485   | 0                       |      |      |       |
| PHF                      | 0.00       |      |      |       | 0.00                            |      |      |       | 0.80       |      |      |       | 0.95                    |      |      |       |                         |      |      |       |
| HV %                     | 0.0%       | 0.0% | 0.0% | 0.0%  | 0.0%                            | 0.0% | 0.0% | 0.0%  | 0.0%       | 0.0% | 2.3% | 0.0%  | 0.0%                    | 0.0% | 0.0% | 5.1%  | 0.0%                    | 0.0% | 2.7% | 0.0%  |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 3B  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #1 combine 2 driveways  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

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## HEAVY VEHICLES

| Start Time | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 5    | 0     | 0                       | 0    | 1    | 0     |
| 7:15 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 3    | 0     |
| 7:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 1    | 0     |
| 7:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 0    | 0     |
| 8:00 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 3    | 0     |
| 8:15 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 5    | 0     |
| 8:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 6    | 0     | 0                       | 0    | 3    | 0     |
| 8:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 3    | 0     |

| Start Time | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 0    | 0     | 0                       | 0    | 7    | 0     |
| 4:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 1    | 0     | 0                       | 0    | 5    | 0     |
| 4:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 3    | 0     |
| 4:45 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 0    | 0     | 0                       | 0    | 1    | 0     |
| 5:00 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 4    | 0     |
| 5:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 1    | 0     | 0                       | 0    | 3    | 0     |
| 5:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 3    | 0     |
| 5:45 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 1    | 0     | 0                       | 0    | 3    | 0     |

| AM PEAK HOUR<br>8:00 AM<br>to<br>9:00 AM | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 16   | 0     | 0                       | 0    | 14   | 0     |
| PHF                                      | 0.00       |      |      |       | 0.00                            |      |      |       | 0.67                    |      |      |       | 0.70                    |      |      |       |

| PM PEAK HOUR<br>5:00 PM<br>to<br>6:00 PM | Northbound |      |      |       | Driveway #1 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 7    | 0     | 0                       | 0    | 13   | 0     |
| PHF                                      | 0.00       |      |      |       | 0.00                            |      |      |       | 0.58                    |      |      |       | 0.81                    |      |      |       |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 3B  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #1 combine 2 driveways  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

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 Office: 978-746-1259  
 DataRequest@BostonTrafficData.com  
 www.BostonTrafficData.com

## PEDESTRIANS & BICYCLES

| Start Time | Northbound |      |       |     | Driveway #1 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|            | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 7:00 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 7:15 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 7:30 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 1   |
| 7:45 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 8:00 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 08:15 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 08:30 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 08:45 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |

| Start Time | Northbound |      |       |     | Driveway #1 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|            | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 4:00 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 4:15 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 4:30 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 4:45 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 2    | 0     | 0   |
| 5:00 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 5:15 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 5:30 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 5:45 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |

| AM PEAK HOUR <sup>1</sup> | Northbound |      |       |     | Driveway #1 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|---------------------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|                           | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 8:00 AM<br>to<br>9:00 AM  | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |

| PM PEAK HOUR <sup>1</sup> | Northbound |      |       |     | Driveway #1 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|---------------------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|                           | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 4:15 PM<br>to<br>5:15 PM  | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 2    | 0     | 0   |

<sup>1</sup>NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 4  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #2 combine 2 driveways  
 Count Date: 9/13/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701  
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## PASSENGER CARS & HEAVY VEHICLES COMBINED

| Start Time | Northbound |      |      |       | Driveway #2 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0          | 0    | 0    | 0     | 0                               | 2    | 0    | 0     | 0          | 1    | 142  | 0     | 0                       | 0    | 0    | 50    | 2                       |      |      |       |
| 7:15 AM    | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 2     | 0          | 6    | 111  | 0     | 0                       | 0    | 0    | 53    | 2                       |      |      |       |
| 7:30 AM    | 0          | 0    | 0    | 0     | 0                               | 5    | 0    | 0     | 0          | 2    | 99   | 0     | 0                       | 0    | 0    | 53    | 2                       |      |      |       |
| 7:45 AM    | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 3     | 0          | 4    | 117  | 0     | 0                       | 0    | 0    | 52    | 3                       |      |      |       |
| 8:00 AM    | 0          | 0    | 0    | 0     | 0                               | 4    | 0    | 5     | 0          | 4    | 96   | 0     | 0                       | 0    | 0    | 75    | 1                       |      |      |       |
| 8:15 AM    | 0          | 0    | 0    | 0     | 0                               | 4    | 0    | 1     | 0          | 1    | 103  | 0     | 0                       | 0    | 0    | 83    | 1                       |      |      |       |
| 8:30 AM    | 0          | 0    | 0    | 0     | 0                               | 3    | 0    | 1     | 0          | 3    | 95   | 0     | 0                       | 0    | 0    | 63    | 0                       |      |      |       |
| 8:45 AM    | 0          | 0    | 0    | 0     | 0                               | 4    | 0    | 2     | 0          | 1    | 143  | 0     | 0                       | 0    | 0    | 54    | 1                       |      |      |       |

| Start Time | Northbound |      |      |       | Driveway #2 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 2     | 0          | 0    | 57   | 0     | 0                       | 0    | 0    | 123   | 1                       |      |      |       |
| 4:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 1     | 0          | 1    | 65   | 0     | 0                       | 0    | 0    | 122   | 0                       |      |      |       |
| 4:30 PM    | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 3     | 0          | 0    | 57   | 0     | 0                       | 0    | 0    | 117   | 0                       |      |      |       |
| 4:45 PM    | 0          | 0    | 0    | 0     | 0                               | 3    | 0    | 0     | 0          | 1    | 56   | 0     | 0                       | 0    | 0    | 116   | 0                       |      |      |       |
| 5:00 PM    | 0          | 0    | 0    | 0     | 0                               | 2    | 0    | 1     | 0          | 0    | 81   | 0     | 0                       | 0    | 0    | 126   | 1                       |      |      |       |
| 5:15 PM    | 0          | 0    | 0    | 0     | 0                               | 4    | 0    | 0     | 0          | 0    | 74   | 0     | 0                       | 0    | 0    | 111   | 0                       |      |      |       |
| 5:30 PM    | 0          | 0    | 0    | 0     | 0                               | 2    | 0    | 5     | 0          | 0    | 58   | 0     | 0                       | 0    | 0    | 97    | 3                       |      |      |       |
| 5:45 PM    | 0          | 0    | 0    | 0     | 0                               | 2    | 0    | 1     | 0          | 0    | 51   | 0     | 0                       | 0    | 0    | 123   | 0                       |      |      |       |

| AM PEAK HOUR             | Northbound |      |      |       | Driveway #2 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 8:00 AM<br>to<br>9:00 AM | 0          | 0    | 0    | 0     | 0                               | 15   | 0    | 9     | 0          | 9    | 437  | 0     | 0                       | 0    | 0    | 275   | 3                       |      |      |       |
| PHF                      | 0.00       |      |      |       | 0.67                            |      |      |       | 0.77       |      |      |       | 0.83                    |      |      |       |                         |      |      |       |
| HV %                     | 0.0%       | 0.0% | 0.0% | 0.0%  | 0.0%                            | 0.0% | 0.0% | 0.0%  | 0.0%       | 0.0% | 3.9% | 0.0%  | 0.0%                    | 0.0% | 0.0% | 5.1%  | 0.0%                    | 0.0% | 2.7% | 0.0%  |

| PM PEAK HOUR             | Northbound |      |      |       | Driveway #2 combine 2 driveways |      |      |       | Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------|------|------|-------|---------------------------------|------|------|-------|------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn     | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:15 PM<br>to<br>5:15 PM | 0          | 0    | 0    | 0     | 0                               | 6    | 0    | 5     | 0          | 2    | 259  | 0     | 0                       | 0    | 0    | 481   | 1                       |      |      |       |
| PHF                      | 0.00       |      |      |       | 0.69                            |      |      |       | 0.81       |      |      |       | 0.95                    |      |      |       |                         |      |      |       |
| HV %                     | 0.0%       | 0.0% | 0.0% | 0.0%  | 0.0%                            | 0.0% | 0.0% | 0.0%  | 0.0%       | 0.0% | 2.7% | 0.0%  | 0.0%                    | 0.0% | 0.0% | 2.7%  | 0.0%                    | 0.0% | 2.7% | 0.0%  |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 4  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #2 combine 2 driveways  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

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## HEAVY VEHICLES

| Start Time | Northbound |      |      |       | Driveway #2 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 0     | 0                       | 0    | 5    | 0     | 0                       | 0    | 1    | 0     |
| 7:15 AM    | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 0     | 0                       | 1    | 1    | 0     | 0                       | 0    | 3    | 0     |
| 7:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 1    | 0     |
| 7:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 1    | 2    | 0     | 0                       | 0    | 0    | 0     |
| 8:00 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 3    | 0     |
| 8:15 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 5    | 0     |
| 8:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 6    | 0     | 0                       | 0    | 3    | 0     |
| 8:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 3    | 0     |

| Start Time | Northbound |      |      |       | Driveway #2 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 0    | 0     | 0                       | 0    | 7    | 0     |
| 4:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 5    | 0     |
| 4:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 3    | 0     |
| 4:45 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 0    | 0     | 0                       | 0    | 1    | 0     |
| 5:00 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 4    | 0     |
| 5:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 1    | 0     | 0                       | 0    | 3    | 0     |
| 5:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 3    | 0     |
| 5:45 PM    | 0          | 0    | 0    | 0     | 0                               | 2    | 0    | 0     | 0                       | 0    | 1    | 0     | 0                       | 0    | 3    | 1     |

| AM PEAK HOUR<br>8:00 AM<br>to<br>9:00 AM | Northbound |      |      |       | Driveway #2 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 17   | 0     | 0                       | 0    | 14   | 0     |
| PHF                                      | 0.00       |      |      |       | 0.00                            |      |      |       | 0.71                    |      |      |       | 0.70                    |      |      |       |

| PM PEAK HOUR<br>5:00 PM<br>to<br>6:00 PM | Northbound |      |      |       | Driveway #2 combine 2 driveways |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0          | 0    | 0    | 0     | 0                               | 2    | 0    | 0     | 0                       | 0    | 7    | 0     | 0                       | 0    | 13   | 1     |
| PHF                                      | 0.00       |      |      |       | 0.25                            |      |      |       | 0.58                    |      |      |       | 0.88                    |      |      |       |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 4  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #2 combine 2 driveways  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

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## PEDESTRIANS & BICYCLES

| Start Time | Northbound |      |       |     | Driveway #2 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|            | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 7:00 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 7:15 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 7:30 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 7:45 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 2   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 1   |
| 8:00 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 08:15 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 08:30 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 08:45 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |

| Start Time | Northbound |      |       |     | Driveway #2 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|            | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 4:00 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 4:15 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 1   |
| 4:30 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 4:45 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 2    | 0     | 0   |
| 5:00 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 5:15 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 1   | 0                       | 0    | 0     | 0   |
| 5:30 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 5:45 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 1   |

| AM PEAK HOUR <sup>1</sup> | Northbound |      |       |     | Driveway #2 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|---------------------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|                           | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 8:00 AM<br>to<br>9:00 AM  | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |

| PM PEAK HOUR <sup>1</sup> | Northbound |      |       |     | Driveway #2 combine 2 driveways |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|---------------------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|                           | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 4:15 PM<br>to<br>5:15 PM  | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 0   | 0                       | 2    | 0     | 1   |

<sup>1</sup>NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 5  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #3  
 Count Date: 9/13/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

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## PASSENGER CARS & HEAVY VEHICLES COMBINED

| Start Time | Northbound |      |      |       | Driveway #3 Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0          | 0    | 0    | 0     | 0                      | 1    | 0    | 0     | 0                       | 0    | 140  | 0     | 0                       | 0    | 53   | 2     |
| 7:15 AM    | 0          | 0    | 0    | 0     | 0                      | 2    | 0    | 1     | 0                       | 1    | 112  | 0     | 0                       | 0    | 55   | 3     |
| 7:30 AM    | 0          | 0    | 0    | 0     | 0                      | 1    | 0    | 0     | 0                       | 0    | 110  | 0     | 0                       | 0    | 55   | 4     |
| 7:45 AM    | 0          | 0    | 0    | 0     | 0                      | 4    | 0    | 0     | 0                       | 0    | 119  | 0     | 1                       | 0    | 55   | 3     |
| 8:00 AM    | 0          | 0    | 0    | 0     | 0                      | 2    | 0    | 0     | 0                       | 0    | 108  | 0     | 0                       | 0    | 78   | 9     |
| 8:15 AM    | 0          | 0    | 0    | 0     | 0                      | 3    | 0    | 0     | 0                       | 0    | 106  | 0     | 0                       | 0    | 83   | 4     |
| 8:30 AM    | 0          | 0    | 0    | 0     | 0                      | 3    | 0    | 0     | 0                       | 0    | 100  | 0     | 0                       | 0    | 63   | 3     |
| 8:45 AM    | 0          | 0    | 0    | 0     | 0                      | 1    | 0    | 1     | 0                       | 1    | 145  | 0     | 0                       | 0    | 54   | 1     |

| Start Time | Northbound |      |      |       | Driveway #3 Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0          | 0    | 0    | 0     | 0                      | 1    | 0    | 3     | 0                       | 1    | 57   | 0     | 0                       | 0    | 121  | 5     |
| 4:15 PM    | 0          | 0    | 0    | 0     | 0                      | 1    | 0    | 0     | 0                       | 0    | 65   | 0     | 0                       | 0    | 122  | 2     |
| 4:30 PM    | 0          | 0    | 0    | 0     | 0                      | 3    | 0    | 1     | 0                       | 1    | 56   | 0     | 0                       | 0    | 116  | 2     |
| 4:45 PM    | 0          | 0    | 0    | 0     | 0                      | 3    | 0    | 3     | 0                       | 0    | 59   | 0     | 0                       | 0    | 113  | 1     |
| 5:00 PM    | 0          | 0    | 0    | 0     | 0                      | 7    | 0    | 3     | 0                       | 0    | 82   | 0     | 0                       | 0    | 124  | 2     |
| 5:15 PM    | 0          | 0    | 0    | 0     | 0                      | 3    | 0    | 1     | 0                       | 0    | 78   | 0     | 0                       | 0    | 111  | 8     |
| 5:30 PM    | 0          | 0    | 0    | 0     | 0                      | 3    | 0    | 1     | 0                       | 1    | 59   | 0     | 0                       | 0    | 99   | 3     |
| 5:45 PM    | 0          | 0    | 0    | 0     | 0                      | 3    | 0    | 3     | 0                       | 0    | 52   | 0     | 0                       | 0    | 119  | 1     |

| AM PEAK HOUR             | Northbound |      |      |       | Driveway #3 Southbound |       |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------|------|------|-------|------------------------|-------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn     | Left | Thru | Right | U-Turn                 | Left  | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 8:00 AM<br>to<br>9:00 AM | 0          | 0    | 0    | 0     | 0                      | 9     | 0    | 1     | 0                       | 1    | 459  | 0     | 0                       | 0    | 278  | 17    |
| PHF                      | 0.00       |      |      |       | 0.83                   |       |      |       | 0.79                    |      |      |       | 0.85                    |      |      |       |
| HV %                     | 0.0%       | 0.0% | 0.0% | 0.0%  | 0.0%                   | 33.3% | 0.0% | 0.0%  | 0.0%                    | 0.0% | 3.7% | 0.0%  | 0.0%                    | 0.0% | 5.0% | 11.8% |

| PM PEAK HOUR             | Northbound |      |      |       | Driveway #3 Southbound |       |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------|------|------|-------|------------------------|-------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn     | Left | Thru | Right | U-Turn                 | Left  | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:30 PM<br>to<br>5:30 PM | 0          | 0    | 0    | 0     | 0                      | 16    | 0    | 8     | 0                       | 1    | 275  | 0     | 0                       | 0    | 464  | 13    |
| PHF                      | 0.00       |      |      |       | 0.60                   |       |      |       | 0.84                    |      |      |       | 0.95                    |      |      |       |
| HV %                     | 0.0%       | 0.0% | 0.0% | 0.0%  | 0.0%                   | 12.5% | 0.0% | 0.0%  | 0.0%                    | 0.0% | 2.2% | 0.0%  | 0.0%                    | 0.0% | 2.4% | 7.7%  |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 5  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #3  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701  
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 DataRequest@BostonTrafficData.com  
 www.BostonTrafficData.com

## HEAVY VEHICLES

| Start Time | Northbound |      |      |       | Driveway #3 Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 6    | 0     | 0                       | 0    | 1    | 0     |
| 7:15 AM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 1    | 0     | 0                       | 0    | 3    | 0     |
| 7:30 AM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 1    | 1     |
| 7:45 AM    | 0          | 0    | 0    | 0     | 0                      | 1    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 0    | 0     |
| 8:00 AM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 3    | 0     |
| 8:15 AM    | 0          | 0    | 0    | 0     | 0                      | 2    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 5    | 2     |
| 8:30 AM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 6    | 0     | 0                       | 0    | 3    | 0     |
| 8:45 AM    | 0          | 0    | 0    | 0     | 0                      | 1    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 3    | 0     |

| Start Time | Northbound |      |      |       | Driveway #3 Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 0    | 0     | 0                       | 0    | 7    | 0     |
| 4:15 PM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 5    | 0     |
| 4:30 PM    | 0          | 0    | 0    | 0     | 0                      | 2    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 3    | 1     |
| 4:45 PM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 0    | 0     | 0                       | 0    | 1    | 0     |
| 5:00 PM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 4    | 0     |
| 5:15 PM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 1    | 0     | 0                       | 0    | 3    | 0     |
| 5:30 PM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 4    | 0     |
| 5:45 PM    | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 4    | 1     |

| AM PEAK HOUR<br>8:00 AM<br>to<br>9:00 AM | Northbound |      |      |       | Driveway #3 Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------|------|------|-------|------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn     | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0          | 0    | 0    | 0     | 0                      | 3    | 0    | 0     | 0                       | 0    | 17   | 0     | 0                       | 0    | 14   | 2     |
| PHF                                      | 0.00       |      |      |       | 0.38                   |      |      |       | 0.71                    |      |      |       | 0.57                    |      |      |       |

| PM PEAK HOUR<br>5:00 PM<br>to<br>6:00 PM | Northbound |      |      |       | Driveway #3 Southbound |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------|------|------|-------|------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn     | Left | Thru | Right | U-Turn                 | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0          | 0    | 0    | 0     | 0                      | 0    | 0    | 0     | 0                       | 0    | 9    | 0     | 0                       | 0    | 15   | 1     |
| PHF                                      | 0.00       |      |      |       | 0.00                   |      |      |       | 0.75                    |      |      |       | 0.80                    |      |      |       |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 5  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #3  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

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## PEDESTRIANS & BICYCLES

| Start Time | Northbound |      |       | Driveway #3 Southbound |      |      | Scanlon Drive Eastbound |     |      | Scanlon Drive Westbound |       |     |      |      |       |     |
|------------|------------|------|-------|------------------------|------|------|-------------------------|-----|------|-------------------------|-------|-----|------|------|-------|-----|
|            | Left       | Thru | Right | PED                    | Left | Thru | Right                   | PED | Left | Thru                    | Right | PED | Left | Thru | Right | PED |
| 7:00 AM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 7:15 AM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 1   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 7:30 AM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 1   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 7:45 AM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 8:00 AM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 08:15 AM   | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 08:30 AM   | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 08:45 AM   | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |

| Start Time | Northbound |      |       | Driveway #3 Southbound |      |      | Scanlon Drive Eastbound |     |      | Scanlon Drive Westbound |       |     |      |      |       |     |
|------------|------------|------|-------|------------------------|------|------|-------------------------|-----|------|-------------------------|-------|-----|------|------|-------|-----|
|            | Left       | Thru | Right | PED                    | Left | Thru | Right                   | PED | Left | Thru                    | Right | PED | Left | Thru | Right | PED |
| 4:00 PM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 4:15 PM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 4:30 PM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 4:45 PM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 1    | 0     | 0   |
| 5:00 PM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 5:15 PM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 5:30 PM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |
| 5:45 PM    | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |

| AM PEAK HOUR <sup>1</sup> | Northbound |      |       | Driveway #3 Southbound |      |      | Scanlon Drive Eastbound |     |      | Scanlon Drive Westbound |       |     |      |      |       |     |
|---------------------------|------------|------|-------|------------------------|------|------|-------------------------|-----|------|-------------------------|-------|-----|------|------|-------|-----|
|                           | Left       | Thru | Right | PED                    | Left | Thru | Right                   | PED | Left | Thru                    | Right | PED | Left | Thru | Right | PED |
| 8:00 AM<br>to<br>9:00 AM  | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 0    | 0     | 0   |

| PM PEAK HOUR <sup>1</sup> | Northbound |      |       | Driveway #3 Southbound |      |      | Scanlon Drive Eastbound |     |      | Scanlon Drive Westbound |       |     |      |      |       |     |
|---------------------------|------------|------|-------|------------------------|------|------|-------------------------|-----|------|-------------------------|-------|-----|------|------|-------|-----|
|                           | Left       | Thru | Right | PED                    | Left | Thru | Right                   | PED | Left | Thru                    | Right | PED | Left | Thru | Right | PED |
| 4:30 PM<br>to<br>5:30 PM  | 0          | 0    | 0     | 0                      | 0    | 0    | 0                       | 0   | 0    | 0                       | 0     | 0   | 0    | 1    | 0     | 0   |

<sup>1</sup>NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 6  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #4 (Shell Gas Station)  
 Count Date: 9/13/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

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## PASSENGER CARS & HEAVY VEHICLES COMBINED

| Start Time | Northbound |      |      |       | Driveway #4 (Shell Gas Station) |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0          | 0    | 0    | 0     | 0                               | 9    | 0    | 8     | 0                       | 2    | 133  | 0     | 0                       | 0    | 47   | 5     |
| 7:15 AM    | 0          | 0    | 0    | 0     | 0                               | 10   | 0    | 7     | 0                       | 3    | 110  | 0     | 0                       | 0    | 51   | 1     |
| 7:30 AM    | 0          | 0    | 0    | 0     | 0                               | 5    | 0    | 11    | 0                       | 1    | 117  | 0     | 0                       | 0    | 48   | 4     |
| 7:45 AM    | 0          | 0    | 0    | 0     | 0                               | 5    | 0    | 6     | 0                       | 3    | 119  | 0     | 0                       | 0    | 53   | 3     |
| 8:00 AM    | 0          | 0    | 0    | 0     | 0                               | 10   | 0    | 5     | 0                       | 1    | 112  | 0     | 0                       | 0    | 82   | 3     |
| 8:15 AM    | 0          | 0    | 0    | 0     | 0                               | 13   | 0    | 7     | 0                       | 6    | 91   | 0     | 0                       | 0    | 80   | 4     |
| 8:30 AM    | 0          | 0    | 0    | 0     | 0                               | 17   | 0    | 10    | 0                       | 7    | 108  | 0     | 0                       | 0    | 56   | 3     |
| 8:45 AM    | 0          | 0    | 0    | 0     | 0                               | 13   | 0    | 5     | 0                       | 8    | 132  | 0     | 0                       | 0    | 51   | 6     |

| Start Time | Northbound |      |      |       | Driveway #4 (Shell Gas Station) |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0          | 0    | 0    | 0     | 0                               | 12   | 0    | 4     | 0                       | 1    | 56   | 0     | 0                       | 0    | 124  | 3     |
| 4:15 PM    | 0          | 0    | 0    | 0     | 0                               | 12   | 0    | 2     | 0                       | 2    | 68   | 0     | 1                       | 0    | 121  | 6     |
| 4:30 PM    | 0          | 0    | 0    | 0     | 0                               | 11   | 0    | 8     | 0                       | 3    | 49   | 0     | 0                       | 0    | 110  | 1     |
| 4:45 PM    | 0          | 0    | 0    | 0     | 0                               | 13   | 0    | 12    | 0                       | 1    | 67   | 0     | 0                       | 0    | 103  | 5     |
| 5:00 PM    | 0          | 0    | 0    | 0     | 0                               | 12   | 0    | 14    | 0                       | 2    | 82   | 0     | 0                       | 0    | 112  | 6     |
| 5:15 PM    | 0          | 0    | 0    | 0     | 0                               | 16   | 0    | 6     | 0                       | 3    | 85   | 0     | 0                       | 0    | 113  | 8     |
| 5:30 PM    | 0          | 0    | 0    | 0     | 0                               | 16   | 0    | 4     | 0                       | 3    | 53   | 0     | 0                       | 0    | 99   | 3     |
| 5:45 PM    | 0          | 0    | 0    | 0     | 0                               | 12   | 0    | 7     | 0                       | 3    | 58   | 0     | 0                       | 0    | 112  | 5     |

| AM PEAK HOUR             | Northbound |      |      |       | Driveway #4 (Shell Gas Station) |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 8:00 AM<br>to<br>9:00 AM | 0          | 0    | 0    | 0     | 0                               | 53   | 0    | 27    | 0                       | 22   | 443  | 0     | 0                       | 0    | 269  | 16    |
| PHF                      | 0.00       |      |      |       | 0.74                            |      |      |       | 0.83                    |      |      |       | 0.84                    |      |      |       |
| HV %                     | 0.0%       | 0.0% | 0.0% | 0.0%  | 0.0%                            | 1.9% | 0.0% | 0.0%  | 0.0%                    | 0.0% | 4.5% | 0.0%  | 0.0%                    | 0.0% | 5.9% | 0.0%  |

| PM PEAK HOUR             | Northbound |      |      |       | Driveway #4 (Shell Gas Station) |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--------------------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|                          | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:30 PM<br>to<br>5:30 PM | 0          | 0    | 0    | 0     | 0                               | 52   | 0    | 40    | 0                       | 9    | 283  | 0     | 0                       | 0    | 438  | 20    |
| PHF                      | 0.00       |      |      |       | 0.88                            |      |      |       | 0.83                    |      |      |       | 0.95                    |      |      |       |
| HV %                     | 0.0%       | 0.0% | 0.0% | 0.0%  | 0.0%                            | 3.8% | 0.0% | 0.0%  | 0.0%                    | 0.0% | 2.8% | 0.0%  | 0.0%                    | 0.0% | 2.7% | 0.0%  |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 6  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #4 (Shell Gas Station)  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

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## HEAVY VEHICLES

| Start Time | Northbound |      |      |       | Driveway #4 (Shell Gas Station) |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 7:00 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 5    | 0     | 0                       | 0    | 1    | 0     |
| 7:15 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 3    | 0     |
| 7:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 2    | 0     |
| 7:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 0    | 1     |
| 8:00 AM    | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 3    | 0     |
| 8:15 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 5    | 0     | 0                       | 0    | 7    | 0     |
| 8:30 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 7    | 0     | 0                       | 0    | 3    | 0     |
| 8:45 AM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 3    | 0     |

| Start Time | Northbound |      |      |       | Driveway #4 (Shell Gas Station) |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|------------|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|            | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
| 4:00 PM    | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 0     | 0                       | 0    | 0    | 0     | 0                       | 0    | 6    | 0     |
| 4:15 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 5    | 0     |
| 4:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 4    | 0     | 0                       | 0    | 4    | 0     |
| 4:45 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 0    | 0     | 0                       | 0    | 1    | 0     |
| 5:00 PM    | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 4    | 0     |
| 5:15 PM    | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 0     | 0                       | 0    | 1    | 0     | 0                       | 0    | 3    | 0     |
| 5:30 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 2    | 0     | 0                       | 0    | 4    | 0     |
| 5:45 PM    | 0          | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                       | 0    | 3    | 0     | 0                       | 0    | 4    | 0     |

| AM PEAK HOUR<br>8:00 AM<br>to<br>9:00 AM | Northbound |      |      |       | Driveway #4 (Shell Gas Station) |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0          | 0    | 0    | 0     | 0                               | 1    | 0    | 0     | 0                       | 0    | 20   | 0     | 0                       | 0    | 16   | 0     |
| PHF                                      | 0.00       |      |      |       | 0.25                            |      |      |       | 0.71                    |      |      |       | 0.57                    |      |      |       |

| PM PEAK HOUR<br>5:00 PM<br>to<br>6:00 PM | Northbound |      |      |       | Driveway #4 (Shell Gas Station) |      |      |       | Scanlon Drive Eastbound |      |      |       | Scanlon Drive Westbound |      |      |       |
|--|------------|------|------|-------|---------------------------------|------|------|-------|-------------------------|------|------|-------|-------------------------|------|------|-------|
|  | U-Turn     | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                  | Left | Thru | Right | U-Turn                  | Left | Thru | Right |
|  | 0          | 0    | 0    | 0     | 0                               | 2    | 0    | 0     | 0                       | 0    | 9    | 0     | 0                       | 0    | 15   | 0     |
| PHF                                      | 0.00       |      |      |       | 0.50                            |      |      |       | 0.75                    |      |      |       | 0.94                    |      |      |       |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 6  
 Location: Randolph, MA  
 Street 1: Scanlon Drive  
 Street 2: Driveway #4 (Shell Gas Station)  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

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 www.BostonTrafficData.com

## PEDESTRIANS & BICYCLES

| Start Time | Northbound |      |       |     | Driveway #4 (Shell Gas Station) |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|            | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 7:00 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 7:15 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 7:30 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 1   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 7:45 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 8:00 AM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 08:15 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 08:30 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 08:45 AM   | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |

| Start Time | Northbound |      |       |     | Driveway #4 (Shell Gas Station) |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|            | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 4:00 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 4:15 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 1   |
| 4:30 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 4:45 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 1    | 0     | 0   |
| 5:00 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 5:15 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 5:30 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |
| 5:45 PM    | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |

| AM PEAK HOUR <sup>1</sup> | Northbound |      |       |     | Driveway #4 (Shell Gas Station) |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|---------------------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|                           | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 8:00 AM<br>to<br>9:00 AM  | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 0    | 0     | 0   |

| PM PEAK HOUR <sup>1</sup> | Northbound |      |       |     | Driveway #4 (Shell Gas Station) |      |       |     | Scanlon Drive Eastbound |      |       |     | Scanlon Drive Westbound |      |       |     |
|---------------------------|------------|------|-------|-----|---------------------------------|------|-------|-----|-------------------------|------|-------|-----|-------------------------|------|-------|-----|
|                           | Left       | Thru | Right | PED | Left                            | Thru | Right | PED | Left                    | Thru | Right | PED | Left                    | Thru | Right | PED |
| 4:30 PM<br>to<br>5:30 PM  | 0          | 0    | 0     | 0   | 0                               | 0    | 0     | 0   | 0                       | 0    | 0     | 0   | 0                       | 1    | 0     | 0   |

<sup>1</sup>NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 7  
 Location: Randolph, MA  
 Street 1: North Main Street  
 Street 2: Scanlon Drive & Russ Street  
 Count Date: 9/13/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

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## PASSENGER CARS & HEAVY VEHICLES COMBINED

| North Main Street<br>Northbound |        |      |      |       | North Main Street<br>Southbound |      |      |       |        | Scanlon Drive<br>Eastbound |      |       |        |      | Russ Street<br>Westbound |       |  |
|---------------------------------|--------|------|------|-------|---------------------------------|------|------|-------|--------|----------------------------|------|-------|--------|------|--------------------------|-------|--|
| Start Time                      | U-Turn | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn | Left                       | Thru | Right | U-Turn | Left | Thru                     | Right |  |
| 7:00 AM                         | 0      | 2    | 337  | 9     | 0                               | 27   | 80   | 42    | 0      | 133                        | 6    | 0     | 0      | 6    | 8                        | 43    |  |
| 7:15 AM                         | 0      | 1    | 285  | 7     | 0                               | 29   | 115  | 44    | 0      | 110                        | 8    | 2     | 0      | 13   | 7                        | 18    |  |
| 7:30 AM                         | 0      | 2    | 242  | 8     | 0                               | 59   | 150  | 44    | 0      | 107                        | 12   | 2     | 0      | 10   | 3                        | 28    |  |
| 7:45 AM                         | 0      | 5    | 214  | 18    | 1                               | 62   | 120  | 43    | 0      | 107                        | 14   | 1     | 0      | 4    | 8                        | 16    |  |
| 8:00 AM                         | 0      | 4    | 255  | 11    | 1                               | 66   | 180  | 72    | 0      | 105                        | 16   | 0     | 0      | 6    | 9                        | 20    |  |
| 8:15 AM                         | 0      | 4    | 238  | 12    | 0                               | 63   | 187  | 70    | 0      | 88                         | 13   | 3     | 0      | 14   | 10                       | 20    |  |
| 8:30 AM                         | 0      | 4    | 210  | 5     | 1                               | 76   | 140  | 45    | 0      | 99                         | 20   | 6     | 0      | 14   | 10                       | 33    |  |
| 8:45 AM                         | 0      | 3    | 216  | 15    | 0                               | 71   | 143  | 46    | 0      | 128                        | 15   | 2     | 0      | 13   | 8                        | 18    |  |

| North Main Street<br>Northbound |        |      |      |       | North Main Street<br>Southbound |      |      |       |        | Scanlon Drive<br>Eastbound |      |       |        |      | Russ Street<br>Westbound |       |  |
|---------------------------------|--------|------|------|-------|---------------------------------|------|------|-------|--------|----------------------------|------|-------|--------|------|--------------------------|-------|--|
| Start Time                      | U-Turn | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn | Left                       | Thru | Right | U-Turn | Left | Thru                     | Right |  |
| 4:00 PM                         | 0      | 5    | 158  | 8     | 0                               | 45   | 237  | 109   | 0      | 53                         | 5    | 8     | 0      | 14   | 14                       | 65    |  |
| 4:15 PM                         | 1      | 4    | 168  | 6     | 0                               | 24   | 235  | 105   | 0      | 70                         | 10   | 3     | 0      | 11   | 17                       | 75    |  |
| 4:30 PM                         | 0      | 0    | 151  | 11    | 0                               | 33   | 257  | 102   | 0      | 54                         | 3    | 3     | 0      | 10   | 10                       | 63    |  |
| 4:45 PM                         | 0      | 2    | 116  | 7     | 0                               | 47   | 296  | 96    | 0      | 72                         | 3    | 6     | 0      | 13   | 8                        | 65    |  |
| 5:00 PM                         | 0      | 4    | 140  | 10    | 1                               | 37   | 292  | 103   | 0      | 76                         | 8    | 7     | 0      | 9    | 11                       | 75    |  |
| 5:15 PM                         | 1      | 7    | 143  | 6     | 0                               | 21   | 241  | 105   | 0      | 83                         | 11   | 9     | 0      | 14   | 9                        | 50    |  |
| 5:30 PM                         | 0      | 8    | 163  | 10    | 0                               | 29   | 233  | 89    | 0      | 53                         | 5    | 7     | 0      | 7    | 6                        | 60    |  |
| 5:45 PM                         | 0      | 6    | 99   | 12    | 0                               | 28   | 237  | 99    | 0      | 57                         | 10   | 6     | 0      | 10   | 11                       | 34    |  |

| AM PEAK HOUR<br>8:00 AM<br>to<br>9:00 AM | North Main Street<br>Northbound |             |             |             |             | North Main Street<br>Southbound |              |             |             |             | Scanlon Drive<br>Eastbound |             |             |             |             | Russ Street<br>Westbound |  |  |
|--|---------------------------------|-------------|-------------|-------------|-------------|---------------------------------|--------------|-------------|-------------|-------------|----------------------------|-------------|-------------|-------------|-------------|--------------------------|--|--|
|  | U-Turn                          | Left        | Thru        | Right       | U-Turn      | Left                            | Thru         | Right       | U-Turn      | Left        | Thru                       | Right       | U-Turn      | Left        | Thru        | Right                    |  |  |
|  | <b>0</b>                        | <b>15</b>   | <b>919</b>  | <b>43</b>   | <b>2</b>    | <b>276</b>                      | <b>650</b>   | <b>233</b>  | <b>0</b>    | <b>420</b>  | <b>64</b>                  | <b>11</b>   | <b>0</b>    | <b>47</b>   | <b>37</b>   | <b>91</b>                |  |  |
| PHF                                      | <b>0.90</b>                     |             |             |             | <b>0.91</b> |                                 |              |             | <b>0.85</b> |             |                            |             | <b>0.77</b> |             |             |                          |  |  |
| HV %                                     | <b>0.0%</b>                     | <b>6.7%</b> | <b>4.8%</b> | <b>7.0%</b> | <b>0.0%</b> | <b>2.5%</b>                     | <b>11.7%</b> | <b>6.4%</b> | <b>0.0%</b> | <b>4.0%</b> | <b>6.3%</b>                | <b>9.1%</b> | <b>0.0%</b> | <b>4.3%</b> | <b>0.0%</b> | <b>4.4%</b>              |  |  |

| PM PEAK HOUR<br>4:15 PM<br>to<br>5:15 PM | North Main Street<br>Northbound |             |             |             |             | North Main Street<br>Southbound |             |             |             |             | Scanlon Drive<br>Eastbound |             |             |             |             | Russ Street<br>Westbound |  |  |
|--|---------------------------------|-------------|-------------|-------------|-------------|---------------------------------|-------------|-------------|-------------|-------------|----------------------------|-------------|-------------|-------------|-------------|--------------------------|--|--|
|  | U-Turn                          | Left        | Thru        | Right       | U-Turn      | Left                            | Thru        | Right       | U-Turn      | Left        | Thru                       | Right       | U-Turn      | Left        | Thru        | Right                    |  |  |
|  | <b>1</b>                        | <b>10</b>   | <b>575</b>  | <b>34</b>   | <b>1</b>    | <b>141</b>                      | <b>1080</b> | <b>406</b>  | <b>0</b>    | <b>272</b>  | <b>24</b>                  | <b>19</b>   | <b>0</b>    | <b>43</b>   | <b>46</b>   | <b>278</b>               |  |  |
| PHF                                      | <b>0.87</b>                     |             |             |             | <b>0.93</b> |                                 |             |             | <b>0.87</b> |             |                            |             | <b>0.89</b> |             |             |                          |  |  |
| HV %                                     | <b>0.0%</b>                     | <b>0.0%</b> | <b>3.3%</b> | <b>0.0%</b> | <b>0.0%</b> | <b>0.0%</b>                     | <b>4.3%</b> | <b>3.7%</b> | <b>0.0%</b> | <b>3.7%</b> | <b>0.0%</b>                | <b>0.0%</b> | <b>0.0%</b> | <b>2.3%</b> | <b>0.0%</b> | <b>1.1%</b>              |  |  |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 7  
 Location: Randolph, MA  
 Street 1: North Main Street  
 Street 2: Scanlon Drive & Russ Street  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

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 www.BostonTrafficData.com

## HEAVY VEHICLES

|            | North Main Street<br>Northbound |      |      |       | North Main Street<br>Southbound |      |      |       | Scanlon Drive<br>Eastbound |      |      |       | Russ Street<br>Westbound |      |      |       |
|------------|---------------------------------|------|------|-------|---------------------------------|------|------|-------|----------------------------|------|------|-------|--------------------------|------|------|-------|
| Start Time | U-Turn                          | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                     | Left | Thru | Right | U-Turn                   | Left | Thru | Right |
| 7:00 AM    | 0                               | 0    | 10   | 1     | 0                               | 0    | 6    | 1     | 0                          | 5    | 0    | 0     | 0                        | 0    | 0    | 0     |
| 7:15 AM    | 0                               | 0    | 10   | 0     | 0                               | 0    | 9    | 2     | 0                          | 2    | 0    | 0     | 0                        | 1    | 1    | 0     |
| 7:30 AM    | 0                               | 1    | 14   | 0     | 0                               | 0    | 1    | 1     | 0                          | 2    | 0    | 0     | 0                        | 1    | 0    | 0     |
| 7:45 AM    | 0                               | 1    | 6    | 1     | 0                               | 0    | 11   | 0     | 0                          | 5    | 0    | 0     | 0                        | 0    | 0    | 1     |
| 8:00 AM    | 0                               | 1    | 15   | 1     | 0                               | 1    | 16   | 2     | 0                          | 4    | 1    | 0     | 0                        | 0    | 0    | 1     |
| 8:15 AM    | 0                               | 0    | 13   | 2     | 0                               | 2    | 21   | 7     | 0                          | 3    | 2    | 1     | 0                        | 0    | 0    | 2     |
| 8:30 AM    | 0                               | 0    | 8    | 0     | 0                               | 1    | 23   | 3     | 0                          | 7    | 0    | 0     | 0                        | 2    | 0    | 0     |
| 8:45 AM    | 0                               | 0    | 8    | 0     | 0                               | 3    | 16   | 3     | 0                          | 3    | 1    | 0     | 0                        | 0    | 0    | 1     |

|            | North Main Street<br>Northbound |      |      |       | North Main Street<br>Southbound |      |      |       | Scanlon Drive<br>Eastbound |      |      |       | Russ Street<br>Westbound |      |      |       |
|------------|---------------------------------|------|------|-------|---------------------------------|------|------|-------|----------------------------|------|------|-------|--------------------------|------|------|-------|
| Start Time | U-Turn                          | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                     | Left | Thru | Right | U-Turn                   | Left | Thru | Right |
| 4:00 PM    | 0                               | 0    | 6    | 0     | 0                               | 0    | 6    | 7     | 0                          | 1    | 0    | 0     | 0                        | 0    | 0    | 1     |
| 4:15 PM    | 0                               | 0    | 6    | 0     | 0                               | 0    | 7    | 5     | 0                          | 2    | 0    | 0     | 0                        | 0    | 0    | 1     |
| 4:30 PM    | 0                               | 0    | 3    | 0     | 0                               | 0    | 11   | 4     | 0                          | 4    | 0    | 0     | 0                        | 0    | 0    | 0     |
| 4:45 PM    | 0                               | 0    | 4    | 0     | 0                               | 0    | 17   | 1     | 0                          | 0    | 0    | 0     | 0                        | 1    | 0    | 1     |
| 5:00 PM    | 0                               | 0    | 6    | 0     | 0                               | 0    | 11   | 5     | 0                          | 4    | 0    | 0     | 0                        | 0    | 0    | 1     |
| 5:15 PM    | 0                               | 0    | 2    | 0     | 0                               | 0    | 4    | 2     | 0                          | 2    | 0    | 0     | 0                        | 0    | 0    | 0     |
| 5:30 PM    | 0                               | 1    | 2    | 0     | 0                               | 0    | 3    | 3     | 0                          | 2    | 0    | 0     | 0                        | 0    | 0    | 1     |
| 5:45 PM    | 0                               | 0    | 6    | 0     | 0                               | 0    | 3    | 5     | 0                          | 1    | 1    | 1     | 0                        | 0    | 0    | 0     |

| AM PEAK HOUR<br>8:00 AM<br>to<br>9:00 AM | North Main Street<br>Northbound |      |      |       | North Main Street<br>Southbound |      |      |       | Scanlon Drive<br>Eastbound |      |      |       | Russ Street<br>Westbound |      |      |       |
|--|---------------------------------|------|------|-------|---------------------------------|------|------|-------|----------------------------|------|------|-------|--------------------------|------|------|-------|
|  | U-Turn                          | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                     | Left | Thru | Right | U-Turn                   | Left | Thru | Right |
| PHF                                      | 0                               | 1    | 44   | 3     | 0                               | 7    | 76   | 15    | 0                          | 17   | 4    | 1     | 0                        | 2    | 0    | 4     |
|  | <b>0.71</b>                     |      |      |       | <b>0.82</b>                     |      |      |       | <b>0.79</b>                |      |      |       | <b>0.75</b>              |      |      |       |

| PM PEAK HOUR<br>4:15 PM<br>to<br>5:15 PM | North Main Street<br>Northbound |      |      |       | North Main Street<br>Southbound |      |      |       | Scanlon Drive<br>Eastbound |      |      |       | Russ Street<br>Westbound |      |      |       |
|--|---------------------------------|------|------|-------|---------------------------------|------|------|-------|----------------------------|------|------|-------|--------------------------|------|------|-------|
|  | U-Turn                          | Left | Thru | Right | U-Turn                          | Left | Thru | Right | U-Turn                     | Left | Thru | Right | U-Turn                   | Left | Thru | Right |
| PHF                                      | 0                               | 0    | 19   | 0     | 0                               | 0    | 46   | 15    | 0                          | 10   | 0    | 0     | 0                        | 1    | 0    | 3     |
|  | <b>0.79</b>                     |      |      |       | <b>0.85</b>                     |      |      |       | <b>0.63</b>                |      |      |       | <b>0.50</b>              |      |      |       |

Client: Vannessa Methoxha, EIT  
 Project #: 1329\_1\_HSH  
 BTD #: Location 7  
 Location: Randolph, MA  
 Street 1: North Main Street  
 Street 2: Scanlon Drive & Russ Street  
 Count Date: 13/09/2023  
 Day of Week: Wednesday  
 Weather: Mostly Cloudy, 70°F

# BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701  
 Office: 978-746-1259  
 DataRequest@BostonTrafficData.com  
 www.BostonTrafficData.com

## PEDESTRIANS & BICYCLES

| North Main Street<br>Northbound |      |      |       | North Main Street<br>Southbound |      |      |       | Scanlon Drive<br>Eastbound |      |      |       | Russ Street<br>Westbound |      |      |       |     |
|---------------------------------|------|------|-------|---------------------------------|------|------|-------|----------------------------|------|------|-------|--------------------------|------|------|-------|-----|
| Start Time                      | Left | Thru | Right | PED                             | Left | Thru | Right | PED                        | Left | Thru | Right | PED                      | Left | Thru | Right | PED |
| 7:00 AM                         | 0    | 0    | 0     | 1                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 0                        | 0    | 0    | 0     | 0   |
| 7:15 AM                         | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 0                        | 0    | 0    | 0     | 0   |
| 7:30 AM                         | 0    | 0    | 0     | 1                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 3                        | 0    | 0    | 0     | 1   |
| 7:45 AM                         | 0    | 0    | 0     | 2                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 2                        | 0    | 0    | 0     | 1   |
| 8:00 AM                         | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 1                        | 0    | 0    | 0     | 0   |
| 08:15 AM                        | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 0                        | 0    | 0    | 0     | 0   |
| 08:30 AM                        | 0    | 0    | 0     | 4                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 4                        | 0    | 0    | 0     | 0   |
| 08:45 AM                        | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 0                        | 0    | 0    | 0     | 0   |

| North Main Street<br>Northbound |      |      |       | North Main Street<br>Southbound |      |      |       | Scanlon Drive<br>Eastbound |      |      |       | Russ Street<br>Westbound |      |      |       |     |
|---------------------------------|------|------|-------|---------------------------------|------|------|-------|----------------------------|------|------|-------|--------------------------|------|------|-------|-----|
| Start Time                      | Left | Thru | Right | PED                             | Left | Thru | Right | PED                        | Left | Thru | Right | PED                      | Left | Thru | Right | PED |
| 4:00 PM                         | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 0                        | 0    | 0    | 0     | 1   |
| 4:15 PM                         | 0    | 0    | 0     | 1                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 0                        | 0    | 0    | 0     | 0   |
| 4:30 PM                         | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 0                        | 0    | 0    | 0     | 0   |
| 4:45 PM                         | 0    | 0    | 0     | 2                               | 0    | 0    | 1     | 0                          | 0    | 0    | 0     | 3                        | 0    | 0    | 0     | 2   |
| 5:00 PM                         | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 0                        | 0    | 0    | 0     | 2   |
| 5:15 PM                         | 0    | 0    | 0     | 0                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 0                        | 0    | 0    | 0     | 2   |
| 5:30 PM                         | 0    | 0    | 0     | 1                               | 0    | 0    | 0     | 0                          | 2    | 0    | 0     | 1                        | 0    | 0    | 0     | 0   |
| 5:45 PM                         | 0    | 0    | 0     | 1                               | 0    | 0    | 0     | 0                          | 0    | 0    | 0     | 1                        | 0    | 0    | 0     | 0   |

| AM PEAK HOUR <sup>1</sup><br>8:00 AM<br>to<br>9:00 AM | North Main Street<br>Northbound |      |       |     | North Main Street<br>Southbound |      |       |     | Scanlon Drive<br>Eastbound |      |       |     | Russ Street<br>Westbound |      |       |     |
|---|---------------------------------|------|-------|-----|---------------------------------|------|-------|-----|----------------------------|------|-------|-----|--------------------------|------|-------|-----|
|   | Left                            | Thru | Right | PED | Left                            | Thru | Right | PED | Left                       | Thru | Right | PED | Left                     | Thru | Right | PED |
|   | 0                               | 0    | 0     | 4   | 0                               | 0    | 0     | 0   | 0                          | 0    | 0     | 5   | 0                        | 0    | 0     | 0   |

| PM PEAK HOUR <sup>1</sup><br>4:15 PM<br>to<br>5:15 PM | North Main Street<br>Northbound |      |       |     | North Main Street<br>Southbound |      |       |     | Scanlon Drive<br>Eastbound |      |       |     | Russ Street<br>Westbound |      |       |     |
|---|---------------------------------|------|-------|-----|---------------------------------|------|-------|-----|----------------------------|------|-------|-----|--------------------------|------|-------|-----|
|   | Left                            | Thru | Right | PED | Left                            | Thru | Right | PED | Left                       | Thru | Right | PED | Left                     | Thru | Right | PED |
|   | 0                               | 0    | 0     | 3   | 0                               | 0    | 1     | 0   | 0                          | 0    | 0     | 3   | 0                        | 0    | 0     | 4   |

<sup>1</sup>NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.



HOWARD STEIN HUDSON

Engineers + Planners

## Appendix B

### MassDOT Seasonal Factors

Massachusetts Highway Department  
 Statewide Traffic Data Collection  
 2019 Weekday Seasonal Factors

Section E, Item1.

| Factor Group | JAN  | FEB  | MAR  | APR  | MAY  | JUN  | JUL  | AUG  | SEP  | OCT  | NOV  | DEC  | Axle Factor |
|--------------|------|------|------|------|------|------|------|------|------|------|------|------|-------------|
| R1           | 1.22 | 1.14 | 1.12 | 1.06 | 1.00 | 0.96 | 0.87 | 0.85 | 0.96 | 0.99 | 1.04 | 1.12 | 0.85        |
| R2           | 0.95 | 0.96 | 0.98 | 0.97 | 0.97 | 0.93 | 0.97 | 0.94 | 0.96 | 0.90 | 0.92 | 0.93 | 0.96        |
| R3           | 1.15 | 1.06 | 1.07 | 1.00 | 0.89 | 0.88 | 0.89 | 0.89 | 0.95 | 0.92 | 1.02 | 1.01 | 0.97        |
| R4-R7        | 1.09 | 1.09 | 1.11 | 1.02 | 0.96 | 0.92 | 0.89 | 0.89 | 0.99 | 0.98 | 1.09 | 1.13 | 0.98        |
| U1-Boston    | 1.03 | 1.01 | 0.98 | 0.94 | 0.94 | 0.92 | 0.95 | 0.93 | 0.94 | 0.94 | 0.97 | 1.04 | 0.96        |
| U1-Essex     | 1.09 | 1.06 | 1.03 | 0.99 | 0.94 | 0.90 | 0.88 | 0.86 | 0.93 | 0.94 | 0.99 | 1.06 | 0.93        |
| U1-Southeast | 1.06 | 1.05 | 1.01 | 0.97 | 0.95 | 0.93 | 0.93 | 0.90 | 0.94 | 0.94 | 0.98 | 1.04 | 0.98        |
| U1-West      | 1.19 | 1.14 | 1.09 | 0.95 | 0.92 | 0.89 | 0.89 | 0.86 | 0.91 | 0.95 | 0.97 | 1.07 | 0.84        |
| U1-Worcester | 1.02 | 1.04 | 0.97 | 0.94 | 0.93 | 0.91 | 0.95 | 0.91 | 0.93 | 0.92 | 0.95 | 1.10 | 0.88        |
| U2           | 1.01 | 1.00 | 0.94 | 0.93 | 0.91 | 0.89 | 0.93 | 0.90 | 0.90 | 0.91 | 0.94 | 1.02 | 0.99        |
| U3           | 1.06 | 1.03 | 0.98 | 0.94 | 0.93 | 0.91 | 0.95 | 0.91 | 0.92 | 0.93 | 0.97 | 1.00 | 0.98        |
| U4-U7        | 1.01 | 1.00 | 0.95 | 0.92 | 0.88 | 0.86 | 0.92 | 0.91 | 0.92 | 0.94 | 0.99 | 1.04 | 0.99        |
| Rec - East   | 1.04 | 1.16 | 1.12 | 0.98 | 0.92 | 0.88 | 0.77 | 0.81 | 0.94 | 1.02 | 1.08 | 1.12 | 0.99        |
| Rec - West   | 1.30 | 1.23 | 1.32 | 1.18 | 0.95 | 0.82 | 0.70 | 0.69 | 0.97 | 0.96 | 1.16 | 1.15 | 0.98        |

Round off:

0-999 = 10

>1000 = 100

U = Urban

R = Rural

1 - Interstate

2 - Freeway and Expressway

3 - Other Principal Arterial

4 - Minor Arterial

5 - Major Collector

6 - Minor Collector

7 - Local Road and Street

**Recreational - East Group** - Cape Cod (all towns) including the town of Plymouth south of Route 3A (stations

7014,7079,7080,7090,7091,7092,7093,7094,7095,7096,7097,7108 and 7178), Martha's Vineyard and Nantucket.

**Recreational - West Group** - Continuous Stations 2 and 189 including stations

1066,1067,1083,1084,1085,1086,1087,1088,1089,1090,1091,1092,1093,1094,1095,1096,1097,1098,1099,1100,1101,1102,1103,1104,1105,1106,1107,1108,1113,1114,1116,2196,2197 and 2198.



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## Appendix C

### Crash Data and Worksheets

*Section E, Item 1.*



## INTERSECTION CRASH RATE WORKSHEET

CITY/TOWN : Randolph COUNT DATE : 9/13/2023

DISTRICT : 6 UNSIGNALIZED :  SIGNALIZED :

**~ INTERSECTION DATA ~**

MAJOR STREET : North Main Street

MINOR STREET(S) : Scanlon Drive

Russ Street

Sc

**INTERSECTION  
DIAGRAM  
(Label Approaches)**



**Peak Hour Volumes**

| APPROACH :                    | 1   | 2   | 3   | 4     | 5 | <b>Total Peak Hourly Approach Volume</b> |
|-------------------------------|-----|-----|-----|-------|---|--|
| DIRECTION :                   | EB  | WB  | NB  | SB    |   |  |
| PEAK HOURLY VOLUMES (AM/PM) : | 335 | 337 | 598 | 1,631 |   | <b>2,901</b>                             |

"K" FACTOR :

**0.090**

INTERSECTION ADT (V) = TOTAL DAILY APPROACH VOLUME :

**32,233**

TOTAL # OF CRASHES :

**59**

# OF YEARS :

**5**

AVERAGE # OF CRASHES PER YEAR (A) :

**11.80**

CRASH RATE CALCULATION :

**1.00**

RATE = 
$$\frac{(A * 1,000,000)}{(ADT * 365)}$$

Comments : \_\_\_\_\_

Project Title & Date: Randolph North Redevelopment



## INTERSECTION CRASH RATE WORKSHEET

CITY/TOWN : Randolph COUNT DATE : 9/13/2023

DISTRICT : 6 UNSIGNALIZED :  SIGNALIZED :

**~ INTERSECTION DATA ~**

MAJOR STREET : Scanlon Drive

MINOR STREET(S) : High Street



**INTERSECTION**

**DIAGRAM**

(Label Approaches)

**Peak Hour Volumes**

| APPROACH :                    | 1  | 2   | 3   | 4  | 5 | <b>Total Peak Hourly Approach Volume</b> |
|-------------------------------|----|-----|-----|----|---|--|
| DIRECTION :                   | EB | WB  | NB  | SB |   |  |
| PEAK HOURLY VOLUMES (AM/PM) : |    | 471 | 274 | 3  |   | <b>748</b>                               |

"K" FACTOR :

**0.090**

INTERSECTION ADT (V) = TOTAL DAILY APPROACH VOLUME :

**8,311**

TOTAL # OF CRASHES :

**1**

# OF YEARS :

**5**

AVERAGE # OF CRASHES PER YEAR (A) :

**0.20**

CRASH RATE CALCULATION :

**0.07**

RATE = 
$$\frac{(A * 1,000,000)}{(ADT * 365)}$$

Comments : \_\_\_\_\_

Project Title & Date: Randolph North Redevelopment



## INTERSECTION CRASH RATE WORKSHEET

CITY/TOWN : Randolph COUNT DATE : 9/13/2023

DISTRICT : 6 UNSIGNALIZED :  SIGNALIZED :

### ~ INTERSECTION DATA ~

MAJOR STREET : Reed Street

MINOR STREET(S) : High Street



### INTERSECTION

### DIAGRAM

(Label Approaches)

### Peak Hour Volumes

| APPROACH :                    | 1   | 2   | 3   | 4   | 5 | Total Peak Hourly Approach Volume |
|-------------------------------|-----|-----|-----|-----|---|-----------------------------------|
| DIRECTION :                   | EB  | WB  | NB  | SB  |   |                                   |
| PEAK HOURLY VOLUMES (AM/PM) : | 276 | 320 | 321 | 452 |   | 1,369                             |

"K" FACTOR :

**0.090**

INTERSECTION ADT (V) = TOTAL DAILY APPROACH VOLUME :

**15,211**

TOTAL # OF CRASHES :

**25**

# OF YEARS :

**5**

AVERAGE # OF CRASHES PER YEAR (A) :

**5.00**

CRASH RATE CALCULATION :

**0.90**

RATE =  $\frac{(A * 1,000,000)}{(ADT * 365)}$

Comments :

Project Title & Date: Randolph North Redevelopment



HOWARD STEIN HUDSON

Engineers + Planners

## Appendix D

### Trip Generation

**Randolph North**  
Trip Generation Assessment

HOWARD STEIN HUDSON  
14-Dec-2023

Section E, Item1.

XXX Means Columns U, X, and AA do not sum to Column R; hard code adjustments are needed  
XX HARD CODED TO BALANCE (Manually change formatting)

| Land Use            | Size    | Category | Directional Split | Average Trip Rate | Unadjusted Vehicle Trips | Assumed National Vehicle Occupancy Rate <sup>1</sup> | Unadjusted Person-Trips | Primary Person Trips | Transit Person-Shares <sup>2</sup> | Walk/Bike/Other Share <sup>2</sup> | Walk/ Bike/ Other Trips | Auto Share <sup>2</sup> | Auto Person-Trips | % Taxi/ TNC Person-Trips | Assumed Local Auto Occupancy Rate for Taxis <sup>5</sup> | Assumed Local Auto Occupancy Rate <sup>4</sup> | Assumed Primary Non-Taxi Auto Trips | Taxi/TNC Auto Trips | Primary AutoTrips |            |     |
|---------------------|---------|----------|-------------------|-------------------|--------------------------|--|-------------------------|----------------------|------------------------------------|------------------------------------|-------------------------|-------------------------|-------------------|--------------------------|--|--|-------------------------------------|---------------------|-------------------|------------|-----|
|                     |         |          |                   |                   |                          |  |                         |                      |                                    |                                    |                         |                         |                   |                          |  |  |                                     |                     |                   |            |     |
| <b>Daily</b>        |         |          |                   |                   |                          |  |                         |                      |                                    |                                    |                         |                         |                   |                          |  |  |                                     |                     |                   |            |     |
| Hotel <sup>b</sup>  | 130.468 | Total    |                   | 7.990             | 1,042                    | 2.10   | 2,188                   | 2,188                | 7%                                 | 154                                | 2%                      | 44                      | 91%               | 1,990                    | 0  | 2.10   | 2.10                                | 0                   | 948               | 948        |     |
|                     | KSF     | In       | 50%               | 3.995             | 521                      | 2.10   | 1,094                   | 1,094                | 7%                                 | 77                                 | 2%                      | 22                      | 91%               | 995                      | 0%   | 0  | 2.10                                | 2.10                | 0                 | 474        | 474 |
|                     |         | Out      | 50%               | 3.995             | 521                      | 2.10   | 1,094                   | 1,094                | 7%                                 | 77                                 | 2%                      | 22                      | 91%               | 995                      | 0%   | 0  | 2.10                                | 2.10                | 0                 | 474        | 474 |
| <b>Total</b>        |         | Total    |                   |                   | <b>1,042</b>             |  | <b>2,188</b>            | <b>2,188</b>         |                                    | <b>154</b>                         |                         | <b>44</b>               |                   | <b>1,990</b>             |  |  |                                     |                     | <b>0</b>          | <b>948</b> |     |
|                     |         | In       |                   |                   | <b>521</b>               |  | <b>1,094</b>            | <b>1,094</b>         |                                    | <b>77</b>                          |                         | <b>22</b>               |                   | <b>995</b>               |  |  |                                     |                     | <b>0</b>          | <b>474</b> |     |
|                     |         | Out      |                   |                   | <b>521</b>               |  | <b>1,094</b>            | <b>1,094</b>         |                                    | <b>77</b>                          |                         | <b>22</b>               |                   | <b>995</b>               |  |  |                                     |                     | <b>0</b>          | <b>474</b> |     |
| <b>AM Peak Hour</b> |         |          |                   |                   |                          |  |                         |                      |                                    |                                    |                         |                         |                   |                          |  |  |                                     |                     |                   |            |     |
| Hotel <sup>b</sup>  | 130.468 | Total    |                   | 0.46              | 60                       | 2.10   | 126                     | 126                  |                                    | 9                                  |                         | 2                       |                   | 115                      | 0  | 2.10   | 2.10                                | 0                   | 55                | 55         |     |
|                     | KSF     | In       | 56%               | 0.258             | 34                       | 2.10   | 71                      | 71                   | 7%                                 | 5                                  | 2%                      | 1                       | 91%               | 65                       | 0%   | 0  | 2.10                                | 2.10                | 0                 | 31         | 31  |
|                     |         | Out      | 44%               | 0.202             | 26                       | 2.10   | 55                      | 55                   | 7%                                 | 4                                  | 2%                      | 1                       | 91%               | 50                       | 0%   | 0  | 2.10                                | 2.10                | 0                 | 24         | 24  |
| <b>Total</b>        |         | Total    |                   |                   | <b>60</b>                |  | <b>126</b>              | <b>126</b>           |                                    | <b>9</b>                           |                         | <b>2</b>                |                   | <b>115</b>               |  |  |                                     |                     | <b>0</b>          | <b>58</b>  |     |
|                     |         | In       |                   |                   | <b>34</b>                |  | <b>71</b>               | <b>71</b>            |                                    | <b>5</b>                           |                         | <b>1</b>                |                   | <b>67</b>                |  |  |                                     |                     | <b>0</b>          | <b>33</b>  |     |
|                     |         | Out      |                   |                   | <b>26</b>                |  | <b>55</b>               | <b>55</b>            |                                    | <b>4</b>                           |                         | <b>1</b>                |                   | <b>51</b>                |  |  |                                     |                     | <b>0</b>          | <b>25</b>  |     |
| <b>PM Peak Hour</b> |         |          |                   |                   |                          |  |                         |                      |                                    |                                    |                         |                         |                   |                          |  |  |                                     |                     |                   |            |     |
| Hotel <sup>b</sup>  | 130.468 | Total    |                   | 0.59              | 77                       | 2.10   | 162                     | 162                  |                                    | 12                                 |                         | 4                       |                   | 146                      | 0  | 2.10   | 2.10                                | 0                   | 69                | 69         |     |
|                     | KSF     | In       | 51%               | 0.301             | 39                       | 2.10   | 82                      | 82                   | 7%                                 | 6                                  | 2%                      | 2                       | 91%               | 74                       | 0%   | 0  | 2.10                                | 2.10                | 0                 | 35         | 35  |
|                     |         | Out      | 49%               | 0.289             | 38                       | 2.10   | 80                      | 80                   | 7%                                 | 6                                  | 2%                      | 2                       | 91%               | 72                       | 0%   | 0  | 2.10                                | 2.10                | 0                 | 34         | 34  |
| <b>Total</b>        |         | Total    |                   |                   | <b>77</b>                |  | <b>162</b>              | <b>162</b>           |                                    | <b>12</b>                          |                         | <b>4</b>                |                   | <b>147</b>               |  |  |                                     |                     | <b>0</b>          | <b>70</b>  |     |
|                     |         | In       |                   |                   | <b>39</b>                |  | <b>82</b>               | <b>82</b>            |                                    | <b>6</b>                           |                         | <b>2</b>                |                   | <b>74</b>                |  |  |                                     |                     | <b>0</b>          | <b>35</b>  |     |
|                     |         | Out      |                   |                   | <b>38</b>                |  | <b>80</b>               | <b>80</b>            |                                    | <b>6</b>                           |                         | <b>2</b>                |                   | <b>73</b>                |  |  |                                     |                     | <b>0</b>          | <b>35</b>  |     |

1. 2017 National vehicle occupancy rates - 1.18:home to work; 1.82: family/personal business; 1.82: shopping; 2.1 social/recreational

2. Mode shares based on Census Data for Tract 4202.02 (2021 ACS 5 Year Tables)

3. Taxi/TNC Percentage based on Census Data for Tract 4202.02

4. Local vehicle occupancy rates based on 2017 National vehicle occupancy rates

5. For taxi cabs, 1.2 passengers per cab. (2.2 minus 1 driver equals 1.2)

6. ITE Trip Generation Manual, 11th Edition, LUC 310 (Hotel), average rate

**Randolph North**  
Trip Generation Assessment

Section E, Item1.

HOWARD STEIN HUDSON  
25-Oct-2023

XXX Means Columns U, X, and AA do not sum to Column R; hard code adjustments are needed  
XX HARD CODED TO BALANCE (Manually change formatting)

| Land Use                                   | Size | Category | Directional Split | Average Trip Rate | Unadjusted Vehicle Trips | Assumed National Vehicle Occupancy Rate <sup>1</sup> | Unadjusted Person-Trips | Primary Person Trips | Transit Person-Shares <sup>2</sup> | Walk/Bike/Other Share <sup>2</sup> | Walk/ Bike/ Other Trips | Auto Person-Trips | % Taxi/ TNC Person-Trips | Assumed Local Auto Occupancy Rate for Taxis <sup>5</sup> | Assumed Primary Non-Taxi Auto Trips |                             |                   |      |    |       |     |
|--|------|----------|-------------------|-------------------|--------------------------|--|-------------------------|----------------------|------------------------------------|------------------------------------|-------------------------|-------------------|--------------------------|--|-------------------------------------|-----------------------------|-------------------|------|----|-------|-----|
|  |      |          |                   |                   |                          |  |                         |                      |                                    |                                    |                         |                   |                          |  | Taxi/TNC Auto Trips                 | Primary Non-Taxi Auto Trips | Primary AutoTrips |      |    |       |     |
| <b>Daily</b>                               |      |          |                   |                   |                          |  |                         |                      |                                    |                                    |                         |                   |                          |  |                                     |                             |                   |      |    |       |     |
| Manufacturing <sup>6</sup>                 | 110  | Total    |                   | 4.750             | 522                      | 1.82   | 950                     | 950                  | 7%                                 | 66                                 | 2%                      | 20                | 91%                      | 864  | 1%                                  | 8                           | 1.82              | 1.82 | 8  | 470   | 478 |
|  | KSF  | In       | 50%               | 2.375             | 261                      | 1.82   | 475                     | 475                  | 7%                                 | 33                                 | 2%                      | 10                | 91%                      | 432  | 1%                                  | 4                           | 1.82              | 1.82 | 4  | 235   | 239 |
|  |      | Out      | 50%               | 2.375             | 261                      | 1.82   | 475                     | 475                  | 7%                                 | 33                                 | 2%                      | 10                | 91%                      | 432  | 1%                                  | 4                           | 1.82              | 1.82 | 4  | 235   | 239 |
| General Office <sup>7</sup>                | 68   | Total    |                   | 10.840            | 738                      | 1.18   | 870                     | 870                  | 7%                                 | 60                                 | 2%                      | 18                | 91%                      | 792  | 1%                                  | 8                           | 1.18              | 1.18 | 12 | 664   | 676 |
|  | KSF  | In       | 50%               | 5.420             | 369                      | 1.18   | 435                     | 435                  | 7%                                 | 30                                 | 2%                      | 9                 | 91%                      | 396  | 1%                                  | 4                           | 1.18              | 1.18 | 6  | 332   | 338 |
|  |      | Out      | 50%               | 5.420             | 369                      | 1.18   | 435                     | 435                  | 7%                                 | 30                                 | 2%                      | 9                 | 91%                      | 396  | 1%                                  | 4                           | 1.18              | 1.18 | 6  | 332   | 338 |
| Research & Development Center <sup>8</sup> | 75   | Total    |                   | 11.080            | 832                      | 1.18   | 982                     | 982                  | 7%                                 | 68                                 | 2%                      | 20                | 91%                      | 894  | 1%                                  | 8                           | 1.18              | 1.18 | 12 | 750   | 762 |
|  | KSF  | In       | 50%               | 5.540             | 416                      | 1.18   | 491                     | 491                  | 7%                                 | 34                                 | 2%                      | 10                | 91%                      | 447  | 1%                                  | 4                           | 1.18              | 1.18 | 6  | 375   | 381 |
|  |      | Out      | 50%               | 5.540             | 416                      | 1.18   | 491                     | 491                  | 7%                                 | 34                                 | 2%                      | 10                | 91%                      | 447  | 1%                                  | 4                           | 1.18              | 1.18 | 6  | 375   | 381 |
| Warehousing <sup>9</sup>                   | 22   | Total    |                   | 1.710             | 38                       | 1.82   | 70                      | 70                   | 7%                                 | 4                                  | 2%                      | 2                 | 91%                      | 64   | 0%                                  | 0                           | 1.82              | 1.82 | 0  | 36    | 36  |
|  | KSF  | In       | 50%               | 0.855             | 19                       | 1.82   | 35                      | 35                   | 7%                                 | 2                                  | 2%                      | 1                 | 91%                      | 32   | 0%                                  | 0                           | 1.82              | 1.82 | 0  | 18    | 18  |
|  |      | Out      | 50%               | 0.855             | 19                       | 1.82   | 35                      | 35                   | 7%                                 | 2                                  | 2%                      | 1                 | 91%                      | 32   | 0%                                  | 0                           | 1.82              | 1.82 | 0  | 18    | 18  |
| <b>Total</b>                               |      | Total    |                   |                   | 2,130                    |  | 2,872                   | 2,872                |                                    | 198                                |                         | 60                |                          | 2,614  |                                     |                             |                   |      | 32 | 1,952 |     |
|  |      | In       |                   |                   | 1,065                    |  | 1,436                   | 1,436                |                                    | 99                                 |                         | 30                |                          | 1,307  |                                     |                             |                   |      | 16 | 976   |     |
|  |      | Out      |                   |                   | 1,065                    |  | 1,436                   | 1,436                |                                    | 99                                 |                         | 30                |                          | 1,307  |                                     |                             |                   |      | 16 | 976   |     |
| <b>AM Peak Hour</b>                        |      |          |                   |                   |                          |  |                         |                      |                                    |                                    |                         |                   |                          |  |                                     |                             |                   |      |    |       |     |
| Manufacturing <sup>6</sup>                 | 110  | Total    |                   | 0.68              | 75                       | 1.82   | 137                     | 137                  |                                    | 9                                  |                         | 3                 |                          | 125  | 1%                                  | 1                           | 1.82              | 1.82 | 2  | 68    | 70  |
|  | KSF  | In       | 76%               | 0.517             | 57                       | 1.82   | 104                     | 104                  | 7%                                 | 7                                  | 2%                      | 2                 | 91%                      | 95   | 1%                                  | 1                           | 1.82              | 1.82 | 1  | 52    | 53  |
|  |      | Out      | 24%               | 0.163             | 18                       | 1.82   | 33                      | 33                   | 7%                                 | 2                                  | 2%                      | 1                 | 91%                      | 30   | 1%                                  | 0                           | 1.82              | 1.82 | 1  | 16    | 17  |
| General Office <sup>7</sup>                | 68   | Total    |                   | 1.52              | 103                      | 1.18   | 121                     | 121                  |                                    | 8                                  |                         | 2                 |                          | 111  | 1%                                  | 1                           | 1.18              | 1.18 | 2  | 93    | 95  |
|  | KSF  | In       | 88%               | 1.338             | 91                       | 1.18   | 107                     | 107                  | 7%                                 | 7                                  | 2%                      | 2                 | 91%                      | 98   | 1%                                  | 1                           | 1.18              | 1.18 | 1  | 82    | 83  |
|  |      | Out      | 12%               | 0.182             | 12                       | 1.18   | 14                      | 14                   | 7%                                 | 1                                  | 2%                      | 0                 | 91%                      | 13   | 1%                                  | 0                           | 1.18              | 1.18 | 1  | 11    | 12  |
| Research & Development Center <sup>9</sup> | 75   | Total    |                   | 1.030             | 77                       | 1.18   | 91                      | 91                   |                                    | 6                                  |                         | 1                 |                          | 84   | 1%                                  | 1                           | 1.18              | 1.18 | 2  | 71    | 73  |
|  | KSF  | In       | 82%               | 0.845             | 63                       | 1.18   | 74                      | 74                   | 7%                                 | 5                                  | 2%                      | 1                 | 91%                      | 68   | 1%                                  | 1                           | 1.18              | 1.18 | 1  | 57    | 58  |
|  |      | Out      | 18%               | 0.185             | 14                       | 1.18   | 17                      | 17                   | 7%                                 | 1                                  | 2%                      | 0                 | 91%                      | 16   | 1%                                  | 0                           | 1.18              | 1.18 | 1  | 14    | 15  |
| Warehousing <sup>9</sup>                   | 22   | Total    |                   | 0.17              | 4                        | 1.82   | 7                       | 7                    |                                    | 0                                  |                         | 0                 |                          | 7  | 0%                                  | 0                           | 1.82              | 1.82 | 0  | 4     | 4   |
|  | KSF  | In       | 77%               | 0.131             | 3                        | 1.82   | 5                       | 5                    | 7%                                 | 0                                  | 2%                      | 0                 | 91%                      | 5  | 0%                                  | 0                           | 1.82              | 1.82 | 0  | 3     | 3   |
|  |      | Out      | 23%               | 0.039             | 1                        | 1.82   | 2                       | 2                    | 7%                                 | 0                                  | 2%                      | 0                 | 91%                      | 2  | 0%                                  | 0                           | 1.82              | 1.82 | 0  | 1     | 1   |
| <b>Total</b>                               |      | Total    |                   |                   | 259                      |  | 356                     | 356                  |                                    | 23                                 |                         | 6                 |                          | 327  |                                     |                             |                   |      | 6  | 242   |     |
|  |      | In       |                   |                   | 214                      |  | 290                     | 290                  |                                    | 19                                 |                         | 5                 |                          | 266  |                                     |                             |                   |      | 3  | 197   |     |
|  |      | Out      |                   |                   | 45                       |  | 66                      | 66                   |                                    | 4                                  |                         | 1                 |                          | 61   |                                     |                             |                   |      | 3  | 45    |     |
| <b>PM Peak Hour</b>                        |      |          |                   |                   |                          |  |                         |                      |                                    |                                    |                         |                   |                          |  |                                     |                             |                   |      |    |       |     |
| Manufacturing <sup>6</sup>                 | 110  | Total    |                   | 0.74              | 81                       | 1.82   | 148                     | 148                  |                                    | 10                                 |                         | 3                 |                          | 135  | 1%                                  | 1                           | 1.82              | 1.82 | 2  | 74    | 76  |
|  | KSF  | In       | 31%               | 0.229             | 25                       | 1.82   | 46                      | 46                   | 7%                                 | 3                                  | 2%                      | 1                 | 91%                      | 42   | 1%                                  | 0                           | 1.82              | 1.82 | 1  | 23    | 24  |
|  |      | Out      | 69%               | 0.511             | 56                       | 1.82   | 102                     | 102                  | 7%                                 | 7                                  | 2%                      | 2                 | 91%                      | 93   | 1%                                  | 1                           | 1.82              | 1.82 | 1  | 51    | 52  |
| General Office <sup>7</sup>                | 68   | Total    |                   | 1.44              | 98                       | 1.18   | 116                     | 116                  |                                    | 8                                  |                         | 2                 |                          | 106  | 1%                                  | 1                           | 1.18              | 1.18 | 2  | 89    | 91  |
|  | KSF  | In       | 17%               | 0.245             | 17                       | 1.18   | 20                      | 20                   | 7%                                 | 1                                  | 2%                      | 0                 | 91%                      | 19   | 1%                                  | 0                           | 1.18              | 1.18 | 1  | 16    | 17  |
|  |      | Out      | 83%               | 1.195             | 81                       | 1.18   | 96                      | 96                   | 7%                                 | 7                                  | 2%                      | 2                 | 91%                      | 87   | 1%                                  | 1                           | 1.18              | 1.18 | 1  | 73    | 74  |
| Research & Development Center <sup>9</sup> | 75   | Total    |                   | 0.980             | 74                       | 1.18   | 87                      | 87                   |                                    | 6                                  |                         | 1                 |                          | 80   | 1%                                  | 1                           | 1.18              | 1.18 | 2  | 67    | 69  |
|  | KSF  | In       | 16%               | 0.157             | 12                       | 1.18   | 14                      | 14                   | 7%                                 | 1                                  | 2%                      | 0                 | 91%                      | 13   | 1%                                  | 0                           | 1.18              | 1.18 | 1  | 11    | 12  |
|  |      | Out      | 84%               | 0.823             | 62                       | 1.18   | 73                      | 73                   | 7%                                 | 5                                  | 2%                      | 1                 | 91%                      | 67   | 1%                                  | 1                           | 1.18              | 1.18 | 1  | 56    | 57  |
| Warehousing <sup>9</sup>                   | 22   | Total    |                   | 0.18              | 4                        | 1.82   | 7                       | 7                    |                                    | 0                                  |                         | 0                 |                          | 7  | 0%                                  | 0                           | 1.82              | 1.82 | 0  | 4     | 4   |
|  | KSF  | In       | 28%               | 0.050             | 1                        | 1.82   | 2                       | 2                    | 7%                                 | 0                                  | 2%                      | 0                 | 91%                      | 2  | 0%                                  | 0                           | 1.82              | 1.82 | 0  | 1     | 1   |
|  |      | Out      | 72%               | 0.130             | 3                        | 1.82   | 5                       | 5                    | 7%                                 | 0                                  | 2%                      | 0                 | 91%                      | 5  | 0%                                  | 0                           | 1.82              | 1.82 | 0  | 3     | 3   |
| <b>Total</b>                               |      | Total    |                   |                   | 257                      |  | 358                     | 358                  |                                    | 24                                 |                         | 6                 |                          | 328  |                                     |                             |                   |      | 6  | 240   |     |
|  |      | In       |                   |                   | 55                       |  | 82                      | 82                   |                                    | 5                                  |                         | 1                 |                          | 76   |                                     |                             |                   |      | 3  | 54    |     |
|  |      | Out      |                   |                   | 202                      |  | 276                     | 276                  |                                    | 19                                 |                         | 5                 |                          | 252  |                                     |                             |                   |      | 3  | 186   |     |

1. 2017 National vehicle occupancy rates - 1.18:home to work; 1.82: family/personal business; 1.82: shopping; 2.1 social/recreational

2. Mode shares based on Census Data for Tract 4202.02 (2021 ACS 5 Year Tables)

3. Taxi/TNC Percentage based on Census Data for Tract 4202.02

4. Local vehicle occupancy rates based on 2017 National vehicle occupancy rates

5. For taxi cabs, 1.2 passengers per cab. (2.2 minus 1 driver equals 1.2)

6. ITE Trip Generation Manual, 11th Edition, LUC 140 (Manufacturing), average rate

7. ITE Trip Generation Manual, 11th Edition, LUC 710 (General Office), average rate

8. ITE Trip Generation Manual, 11th Edition, LUC 150 (Warehousing), average rate

9. ITE Trip Generation Manual, 11th Edition, LUC 760 (Research & Development Center), average rate



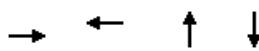
HOWARD STEIN HUDSON

Engineers + Planners

## Appendix E

### Synchro Reports

| Intersection               |       |       |       |      |      |      |
|----------------------------|-------|-------|-------|------|------|------|
| Intersection Delay, s/veh  | 15.8  |       |       |      |      |      |
| Intersection LOS           | C     |       |       |      |      |      |
| Movement                   | WBL   | WBR   | NBT   | NBR  | SBL  | SBT  |
| Lane Configurations        |       |       |       |      |      |      |
| Traffic Vol, veh/h         | 272   | 4     | 3     | 451  | 1    | 0    |
| Future Vol, veh/h          | 272   | 4     | 3     | 451  | 1    | 0    |
| Peak Hour Factor           | 0.85  | 0.85  | 0.76  | 0.76 | 0.25 | 0.25 |
| Heavy Vehicles, %          | 5     | 0     | 0     | 4    | 0    | 0    |
| Mvmt Flow                  | 320   | 5     | 4     | 593  | 4    | 0    |
| Number of Lanes            | 1     | 0     | 1     | 0    | 0    | 1    |
| Approach                   | WB    | NB    |       | SB   |      |      |
| Opposing Approach          |       | SB    |       | NB   |      |      |
| Opposing Lanes             | 0     | 1     |       | 1    |      |      |
| Conflicting Approach Left  | NB    |       |       | WB   |      |      |
| Conflicting Lanes Left     | 1     | 0     |       | 1    |      |      |
| Conflicting Approach Right | SB    | WB    |       |      |      |      |
| Conflicting Lanes Right    | 1     | 1     |       | 0    |      |      |
| HCM Control Delay          | 14    | 16.8  |       | 8.9  |      |      |
| HCM LOS                    | B     | C     |       | A    |      |      |
| Lane                       | NBLn1 | WBLn1 | SBLn1 |      |      |      |
| Vol Left, %                | 0%    | 99%   | 100%  |      |      |      |
| Vol Thru, %                | 1%    | 0%    | 0%    |      |      |      |
| Vol Right, %               | 99%   | 1%    | 0%    |      |      |      |
| Sign Control               | Stop  | Stop  | Stop  |      |      |      |
| Traffic Vol by Lane        | 454   | 276   | 1     |      |      |      |
| LT Vol                     | 0     | 272   | 1     |      |      |      |
| Through Vol                | 3     | 0     | 0     |      |      |      |
| RT Vol                     | 451   | 4     | 0     |      |      |      |
| Lane Flow Rate             | 597   | 325   | 4     |      |      |      |
| Geometry Grp               | 1     | 1     | 1     |      |      |      |
| Degree of Util (X)         | 0.703 | 0.501 | 0.006 |      |      |      |
| Departure Headway (Hd)     | 4.234 | 5.558 | 5.804 |      |      |      |
| Convergence, Y/N           | Yes   | Yes   | Yes   |      |      |      |
| Cap                        | 848   | 653   | 618   |      |      |      |
| Service Time               | 2.293 | 3.558 | 3.827 |      |      |      |
| HCM Lane V/C Ratio         | 0.704 | 0.498 | 0.006 |      |      |      |
| HCM Control Delay          | 16.8  | 14    | 8.9   |      |      |      |
| HCM Lane LOS               | C     | B     | A     |      |      |      |
| HCM 95th-tile Q            | 6     | 2.8   | 0     |      |      |      |



| Lane Group              | EBT  | WBT  | NBT  | SBT  |
|-------------------------|------|------|------|------|
| Lane Group Flow (vph)   | 538  | 305  | 680  | 313  |
| v/c Ratio               | 0.81 | 0.50 | 1.01 | 0.45 |
| Control Delay           | 26.6 | 15.1 | 58.2 | 14.4 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay             | 26.6 | 15.1 | 58.2 | 14.4 |
| Queue Length 50th (ft)  | 146  | 69   | ~218 | 71   |
| Queue Length 95th (ft)  | #264 | 100  | #358 | 124  |
| Internal Link Dist (ft) | 410  | 2031 | 474  | 3954 |
| Turn Bay Length (ft)    |      |      |      |      |
| Base Capacity (vph)     | 662  | 609  | 672  | 693  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.81 | 0.50 | 1.01 | 0.45 |

## Intersection Summary

~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis  
3: Reed Street & High Street

Section E, Item1.



| Movement                          | EBL  | EBT   | EBR  | WBL  | WBT                       | WBR  | NBL  | NBT   | NBR  | SBL  | SBT  | SBR  |
|-----------------------------------|------|-------|------|------|---------------------------|------|------|-------|------|------|------|------|
| Lane Configurations               |      |       |      |      |                           |      |      |       |      |      |      |      |
| Traffic Volume (vph)              | 155  | 278   | 13   | 55   | 167                       | 7    | 56   | 370   | 132  | 5    | 188  | 82   |
| Future Volume (vph)               | 155  | 278   | 13   | 55   | 167                       | 7    | 56   | 370   | 132  | 5    | 188  | 82   |
| Ideal Flow (vphpl)                | 1900 | 1900  | 1900 | 1900 | 1900                      | 1900 | 1900 | 1900  | 1900 | 1900 | 1900 | 1900 |
| Lane Width                        | 12   | 15    | 12   | 12   | 11                        | 12   | 12   | 12    | 12   | 12   | 12   | 12   |
| Total Lost time (s)               |      | 4.5   |      |      | 4.5                       |      |      | 4.5   |      |      | 4.5  |      |
| Lane Util. Factor                 |      | 1.00  |      |      | 1.00                      |      |      | 1.00  |      |      | 1.00 |      |
| Frpb, ped/bikes                   |      | 1.00  |      |      | 1.00                      |      |      | 0.99  |      |      | 0.99 |      |
| Fpb, ped/bikes                    |      | 0.99  |      |      | 1.00                      |      |      | 1.00  |      |      | 1.00 |      |
| Frt                               |      | 1.00  |      |      | 1.00                      |      |      | 0.97  |      |      | 0.96 |      |
| Flt Protected                     |      | 0.98  |      |      | 0.99                      |      |      | 1.00  |      |      | 1.00 |      |
| Satd. Flow (prot)                 |      | 1995  |      |      | 1716                      |      |      | 1751  |      |      | 1714 |      |
| Flt Permitted                     |      | 0.76  |      |      | 0.82                      |      |      | 0.93  |      |      | 0.99 |      |
| Satd. Flow (perm)                 |      | 1551  |      |      | 1425                      |      |      | 1645  |      |      | 1695 |      |
| Peak-hour factor, PHF             | 0.83 | 0.83  | 0.83 | 0.75 | 0.75                      | 0.75 | 0.82 | 0.82  | 0.82 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph)                   | 187  | 335   | 16   | 73   | 223                       | 9    | 68   | 451   | 161  | 6    | 214  | 93   |
| RTOR Reduction (vph)              | 0    | 0     | 0    | 0    | 0                         | 0    | 0    | 0     | 0    | 0    | 0    | 0    |
| Lane Group Flow (vph)             | 0    | 538   | 0    | 0    | 305                       | 0    | 0    | 680   | 0    | 0    | 313  | 0    |
| Confl. Peds. (#/hr)               | 46   |       | 17   | 17   |                           | 46   | 12   |       | 4    | 4    |      | 12   |
| Heavy Vehicles (%)                | 1%   | 1%    | 0%   | 11%  | 3%                        | 0%   | 0%   | 5%    | 2%   | 0%   | 7%   | 1%   |
| Turn Type                         | Perm | NA    |      | Perm | NA                        |      | Perm | NA    |      | Perm | NA   |      |
| Protected Phases                  |      | 4     |      |      | 8                         |      |      | 2     |      |      | 6    |      |
| Permitted Phases                  |      | 4     |      |      | 8                         |      |      | 2     |      |      | 6    |      |
| Actuated Green, G (s)             |      | 23.5  |      |      | 23.5                      |      |      | 22.5  |      |      | 22.5 |      |
| Effective Green, g (s)            |      | 23.5  |      |      | 23.5                      |      |      | 22.5  |      |      | 22.5 |      |
| Actuated g/C Ratio                |      | 0.43  |      |      | 0.43                      |      |      | 0.41  |      |      | 0.41 |      |
| Clearance Time (s)                |      | 4.5   |      |      | 4.5                       |      |      | 4.5   |      |      | 4.5  |      |
| Lane Grp Cap (vph)                |      | 662   |      |      | 608                       |      |      | 672   |      |      | 693  |      |
| v/s Ratio Prot                    |      |       |      |      |                           |      |      |       |      |      |      |      |
| v/s Ratio Perm                    |      | c0.35 |      |      | 0.21                      |      |      | c0.41 |      |      | 0.18 |      |
| v/c Ratio                         |      | 0.81  |      |      | 0.50                      |      |      | 1.01  |      |      | 0.45 |      |
| Uniform Delay, d1                 |      | 13.8  |      |      | 11.5                      |      |      | 16.2  |      |      | 11.8 |      |
| Progression Factor                |      | 1.00  |      |      | 1.00                      |      |      | 1.00  |      |      | 1.00 |      |
| Incremental Delay, d2             |      | 10.5  |      |      | 2.9                       |      |      | 37.7  |      |      | 2.1  |      |
| Delay (s)                         |      | 24.3  |      |      | 14.4                      |      |      | 54.0  |      |      | 13.9 |      |
| Level of Service                  |      | C     |      |      | B                         |      |      | D     |      |      | B    |      |
| Approach Delay (s)                |      | 24.3  |      |      | 14.4                      |      |      | 54.0  |      |      | 13.9 |      |
| Approach LOS                      |      | C     |      |      | B                         |      |      | D     |      |      | B    |      |
| Intersection Summary              |      |       |      |      |                           |      |      |       |      |      |      |      |
| HCM 2000 Control Delay            |      | 31.9  |      |      | HCM 2000 Level of Service |      |      | C     |      |      |      |      |
| HCM 2000 Volume to Capacity ratio |      | 0.91  |      |      |                           |      |      |       |      |      |      |      |
| Actuated Cycle Length (s)         |      | 55.0  |      |      | Sum of lost time (s)      |      |      | 9.0   |      |      |      |      |
| Intersection Capacity Utilization |      | 94.9% |      |      | ICU Level of Service      |      |      | F     |      |      |      |      |
| Analysis Period (min)             |      | 15    |      |      |                           |      |      |       |      |      |      |      |
| c Critical Lane Group             |      |       |      |      |                           |      |      |       |      |      |      |      |

## Queues

9: N Main Street &amp; Scanlon Drive/Russ Street

Section E, Item1.



| Lane Group              | EBL  | EBT  | WBL  | WBT  | NBL  | NBT  | SBL  | SBT  | SBR  |
|-------------------------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 292  | 291  | 61   | 166  | 17   | 1069 | 305  | 714  | 256  |
| v/c Ratio               | 0.87 | 0.83 | 0.66 | 0.97 | 0.05 | 0.86 | 0.99 | 0.44 | 0.21 |
| Control Delay           | 66.8 | 61.3 | 83.1 | 88.6 | 11.2 | 38.0 | 77.0 | 16.7 | 0.9  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay             | 66.8 | 61.3 | 83.1 | 88.6 | 11.2 | 38.0 | 77.0 | 16.7 | 0.9  |
| Queue Length 50th (ft)  | 202  | 197  | 42   | 58   | 5    | 345  | 155  | 130  | 0    |
| Queue Length 95th (ft)  | #357 | #345 | #91  | #149 | 14   | 431  | #353 | 230  | 19   |
| Internal Link Dist (ft) |      |      | 42   |      | 451  |      | 3510 |      | 583  |
| Turn Bay Length (ft)    | 50   |      | 60   |      | 200  |      | 180  |      |      |
| Base Capacity (vph)     | 351  | 366  | 93   | 172  | 328  | 1521 | 309  | 1664 | 1231 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.83 | 0.80 | 0.66 | 0.97 | 0.05 | 0.70 | 0.99 | 0.43 | 0.21 |

## Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

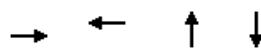
HCM Signalized Intersection Capacity Analysis  
9: N Main Street & Scanlon Drive/Russ Street

Section E, Item1.

| Movement                          | EBL   | EBT   | EBR  | WBL   | WBT   | WBR                       | NBL   | NBT  | NBR  | SBU    | SBL   | SBT   | SBR   |
|-----------------------------------|-------|-------|------|-------|-------|---------------------------|-------|------|------|--------|-------|-------|-------|
| Lane Configurations               | ↑     | ↔     |      | ↑     | ↔     |                           | ↑     | ↔    |      |        | ↑     | ↔     | ↑     |
| Traffic Volume (vph)              | 421   | 64    | 11   | 47    | 37    | 91                        | 15    | 919  | 43   | 2      | 276   | 650   | 233   |
| Future Volume (vph)               | 421   | 64    | 11   | 47    | 37    | 91                        | 15    | 919  | 43   | 2      | 276   | 650   | 233   |
| Ideal Flow (vphpl)                | 1900  | 1900  | 1900 | 1900  | 1900  | 1900                      | 1900  | 1900 | 1900 | 1900   | 1900  | 1900  | 1900  |
| Lane Width                        | 11    | 12    | 12   | 10    | 12    | 12                        | 10    | 11   | 11   | 12     | 10    | 10    | 11    |
| Total Lost time (s)               | 5.0   | 5.0   |      | 5.0   | 5.0   |                           | 7.0   | 5.0  |      |        | 7.0   | 5.0   | 5.0   |
| Lane Util. Factor                 | 0.95  | 0.95  |      | 1.00  | 1.00  |                           | 1.00  | 0.95 |      |        | 1.00  | 0.95  | 1.00  |
| Frpb, ped/bikes                   | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Frbp, ped/bikes                   | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Frt                               | 1.00  | 0.99  |      | 1.00  | 0.89  |                           | 1.00  | 0.99 |      |        | 1.00  | 1.00  | 0.85  |
| Flt Protected                     | 0.95  | 0.97  |      | 0.95  | 1.00  |                           | 0.95  | 1.00 |      |        | 0.95  | 1.00  | 1.00  |
| Satd. Flow (prot)                 | 1594  | 1653  |      | 1620  | 1650  |                           | 1572  | 3298 |      |        | 1636  | 3008  | 1473  |
| Flt Permitted                     | 0.95  | 0.97  |      | 0.95  | 1.00  |                           | 0.38  | 1.00 |      |        | 0.10  | 1.00  | 1.00  |
| Satd. Flow (perm)                 | 1594  | 1653  |      | 1620  | 1650  |                           | 629   | 3298 |      |        | 174   | 3008  | 1473  |
| Peak-hour factor, PHF             | 0.85  | 0.85  | 0.85 | 0.77  | 0.77  | 0.77                      | 0.90  | 0.90 | 0.90 | 0.91   | 0.91  | 0.91  | 0.91  |
| Adj. Flow (vph)                   | 495   | 75    | 13   | 61    | 48    | 118                       | 17    | 1021 | 48   | 2      | 303   | 714   | 256   |
| RTOR Reduction (vph)              | 0     | 2     | 0    | 0     | 77    | 0                         | 0     | 3    | 0    | 0      | 0     | 0     | 60    |
| Lane Group Flow (vph)             | 292   | 289   | 0    | 61    | 89    | 0                         | 17    | 1066 | 0    | 0      | 305   | 714   | 196   |
| Confl. Peds. (#/hr)               |       |       |      | 4     | 4     |                           |       | 5    |      |        |       |       | 5     |
| Heavy Vehicles (%)                | 4%    | 6%    | 9%   | 4%    | 0%    | 4%                        | 7%    | 5%   | 7%   | 2%     | 3%    | 12%   | 6%    |
| Turn Type                         | Split | NA    |      | Split | NA    |                           | pm+pt | NA   |      | custom | pm+pt | NA    | pt+ov |
| Protected Phases                  | 3     | 3     |      | 4     | 4     |                           | 5     | 2    |      |        | 1     | 6     | 6.3   |
| Permitted Phases                  |       |       |      |       |       |                           | 2     |      |      |        | 1     | 6     |       |
| Actuated Green, G (s)             | 22.2  | 22.2  |      | 6.0   | 6.0   |                           | 46.4  | 43.9 |      |        | 66.0  | 56.5  | 83.7  |
| Effective Green, g (s)            | 22.2  | 22.2  |      | 6.0   | 6.0   |                           | 46.4  | 43.9 |      |        | 66.0  | 56.5  | 83.7  |
| Actuated g/C Ratio                | 0.20  | 0.20  |      | 0.05  | 0.05  |                           | 0.42  | 0.40 |      |        | 0.60  | 0.52  | 0.77  |
| Clearance Time (s)                | 5.0   | 5.0   |      | 5.0   | 5.0   |                           | 7.0   | 5.0  |      |        | 7.0   | 5.0   |       |
| Vehicle Extension (s)             | 3.0   | 3.0   |      | 3.0   | 3.0   |                           | 3.0   | 2.0  |      |        | 3.0   | 2.0   |       |
| Lane Grp Cap (vph)                | 324   | 336   |      | 89    | 90    |                           | 288   | 1325 |      |        | 307   | 1556  | 1129  |
| v/s Ratio Prot                    | c0.18 | 0.18  |      | 0.04  | c0.05 |                           | 0.00  | 0.32 |      |        | c0.14 | 0.24  | 0.13  |
| v/s Ratio Perm                    |       |       |      |       |       |                           | 0.02  |      |      |        |       | c0.46 |       |
| v/c Ratio                         | 0.90  | 0.86  |      | 0.69  | 0.98  |                           | 0.06  | 0.80 |      |        | 0.99  | 0.46  | 0.17  |
| Uniform Delay, d1                 | 42.4  | 42.0  |      | 50.7  | 51.6  |                           | 18.3  | 28.9 |      |        | 31.0  | 16.7  | 3.4   |
| Progression Factor                | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Incremental Delay, d2             | 26.6  | 19.6  |      | 19.7  | 88.9  |                           | 0.1   | 3.4  |      |        | 49.3  | 0.1   | 0.0   |
| Delay (s)                         | 69.1  | 61.7  |      | 70.3  | 140.4 |                           | 18.3  | 32.3 |      |        | 80.3  | 16.8  | 3.5   |
| Level of Service                  | E     | E     |      | E     | F     |                           | B     | C    |      |        | F     | B     | A     |
| Approach Delay (s)                |       | 65.4  |      |       | 121.6 |                           |       | 32.1 |      |        |       | 29.3  |       |
| Approach LOS                      |       | E     |      |       | F     |                           |       | C    |      |        |       | C     |       |
| Intersection Summary              |       |       |      |       |       |                           |       |      |      |        |       |       |       |
| HCM 2000 Control Delay            |       | 43.5  |      |       |       | HCM 2000 Level of Service |       |      | D    |        |       |       |       |
| HCM 2000 Volume to Capacity ratio |       | 1.00  |      |       |       |                           |       |      |      |        |       |       |       |
| Actuated Cycle Length (s)         |       | 109.2 |      |       |       | Sum of lost time (s)      |       |      | 22.0 |        |       |       |       |
| Intersection Capacity Utilization |       | 82.1% |      |       |       | ICU Level of Service      |       |      | E    |        |       |       |       |
| Analysis Period (min)             |       | 15    |      |       |       |                           |       |      |      |        |       |       |       |
| c Critical Lane Group             |       |       |      |       |       |                           |       |      |      |        |       |       |       |



| Intersection               |       |       |       |      |      |      |  |
|----------------------------|-------|-------|-------|------|------|------|--|
| Intersection Delay, s/veh  | 15.3  |       |       |      |      |      |  |
| Intersection LOS           | C     |       |       |      |      |      |  |
| Movement                   | WBL   | WBR   | NBT   | NBR  | SBL  | SBT  |  |
| Lane Configurations        |       |       |       |      |      |      |  |
| Traffic Vol, veh/h         | 471   | 0     | 2     | 272  | 1    | 2    |  |
| Future Vol, veh/h          | 471   | 0     | 2     | 272  | 1    | 2    |  |
| Peak Hour Factor           | 0.93  | 0.93  | 0.84  | 0.84 | 0.25 | 0.25 |  |
| Heavy Vehicles, %          | 2     | 0     | 0     | 2    | 0    | 0    |  |
| Mvmt Flow                  | 506   | 0     | 2     | 324  | 4    | 8    |  |
| Number of Lanes            | 1     | 0     | 1     | 0    | 0    | 1    |  |
| Approach                   | WB    | NB    |       | SB   |      |      |  |
| Opposing Approach          |       | SB    |       | NB   |      |      |  |
| Opposing Lanes             | 0     | 1     |       | 1    |      |      |  |
| Conflicting Approach Left  | NB    |       |       | WB   |      |      |  |
| Conflicting Lanes Left     | 1     | 0     |       | 1    |      |      |  |
| Conflicting Approach Right | SB    | WB    |       |      |      |      |  |
| Conflicting Lanes Right    | 1     | 1     |       | 0    |      |      |  |
| HCM Control Delay          | 18.3  | 11    |       | 8.9  |      |      |  |
| HCM LOS                    | C     | B     |       | A    |      |      |  |
| Lane                       | NBLn1 | WBLn1 | SBLn1 |      |      |      |  |
| Vol Left, %                | 0%    | 100%  | 33%   |      |      |      |  |
| Vol Thru, %                | 1%    | 0%    | 67%   |      |      |      |  |
| Vol Right, %               | 99%   | 0%    | 0%    |      |      |      |  |
| Sign Control               | Stop  | Stop  | Stop  |      |      |      |  |
| Traffic Vol by Lane        | 274   | 471   | 3     |      |      |      |  |
| LT Vol                     | 0     | 471   | 1     |      |      |      |  |
| Through Vol                | 2     | 0     | 2     |      |      |      |  |
| RT Vol                     | 272   | 0     | 0     |      |      |      |  |
| Lane Flow Rate             | 326   | 506   | 12    |      |      |      |  |
| Geometry Grp               | 1     | 1     | 1     |      |      |      |  |
| Degree of Util (X)         | 0.419 | 0.69  | 0.019 |      |      |      |  |
| Departure Headway (Hd)     | 4.625 | 4.906 | 5.801 |      |      |      |  |
| Convergence, Y/N           | Yes   | Yes   | Yes   |      |      |      |  |
| Cap                        | 773   | 729   | 621   |      |      |      |  |
| Service Time               | 2.679 | 2.986 | 3.801 |      |      |      |  |
| HCM Lane V/C Ratio         | 0.422 | 0.694 | 0.019 |      |      |      |  |
| HCM Control Delay          | 11    | 18.3  | 8.9   |      |      |      |  |
| HCM Lane LOS               | B     | C     | A     |      |      |      |  |
| HCM 95th-tile Q            | 2.1   | 5.6   | 0.1   |      |      |      |  |



| Lane Group              | EBT  | WBT  | NBT  | SBT  |
|-------------------------|------|------|------|------|
| Lane Group Flow (vph)   | 307  | 351  | 369  | 486  |
| v/c Ratio               | 0.44 | 0.61 | 0.52 | 0.69 |
| Control Delay           | 12.4 | 16.2 | 13.4 | 18.1 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay             | 12.4 | 16.2 | 13.4 | 18.1 |
| Queue Length 50th (ft)  | 55   | 68   | 68   | 98   |
| Queue Length 95th (ft)  | 106  | 135  | 121  | #194 |
| Internal Link Dist (ft) | 410  | 2031 | 474  | 3954 |
| Turn Bay Length (ft)    |      |      |      |      |
| Base Capacity (vph)     | 691  | 578  | 715  | 702  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.44 | 0.61 | 0.52 | 0.69 |

## Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis  
3: Reed Street & High Street

Section E, Item1.



| Movement                          | EBL   | EBT  | EBR  | WBL  | WBT                       | WBR  | NBL  | NBT  | NBR  | SBL  | SBT   | SBR  |
|-----------------------------------|-------|------|------|------|---------------------------|------|------|------|------|------|-------|------|
| Lane Configurations               |       |      |      |      |                           |      |      |      |      |      |       |      |
| Traffic Volume (vph)              | 79    | 187  | 10   | 109  | 206                       | 5    | 5    | 233  | 83   | 6    | 316   | 130  |
| Future Volume (vph)               | 79    | 187  | 10   | 109  | 206                       | 5    | 5    | 233  | 83   | 6    | 316   | 130  |
| Ideal Flow (vphpl)                | 1900  | 1900 | 1900 | 1900 | 1900                      | 1900 | 1900 | 1900 | 1900 | 1900 | 1900  | 1900 |
| Lane Width                        | 12    | 15   | 12   | 12   | 11                        | 12   | 12   | 12   | 12   | 12   | 12    | 12   |
| Total Lost time (s)               | 4.5   |      |      |      | 4.5                       |      |      | 4.5  |      |      | 4.5   |      |
| Lane Util. Factor                 | 1.00  |      |      |      | 1.00                      |      |      | 1.00 |      |      | 1.00  |      |
| Frpb, ped/bikes                   | 1.00  |      |      |      | 1.00                      |      |      | 1.00 |      |      | 0.99  |      |
| Flpb, ped/bikes                   | 1.00  |      |      |      | 1.00                      |      |      | 1.00 |      |      | 1.00  |      |
| Frt                               | 1.00  |      |      |      | 1.00                      |      |      | 0.97 |      |      | 0.96  |      |
| Flt Protected                     | 0.99  |      |      |      | 0.98                      |      |      | 1.00 |      |      | 1.00  |      |
| Satd. Flow (prot)                 | 2034  |      |      |      | 1754                      |      |      | 1802 |      |      | 1765  |      |
| Flt Permitted                     | 0.84  |      |      |      | 0.81                      |      |      | 0.99 |      |      | 0.99  |      |
| Satd. Flow (perm)                 | 1728  |      |      |      | 1445                      |      |      | 1788 |      |      | 1757  |      |
| Peak-hour factor, PHF             | 0.90  | 0.90 | 0.90 | 0.91 | 0.91                      | 0.91 | 0.87 | 0.87 | 0.87 | 0.93 | 0.93  | 0.93 |
| Adj. Flow (vph)                   | 88    | 208  | 11   | 120  | 226                       | 5    | 6    | 268  | 95   | 6    | 340   | 140  |
| RTOR Reduction (vph)              | 0     | 0    | 0    | 0    | 0                         | 0    | 0    | 0    | 0    | 0    | 0     | 0    |
| Lane Group Flow (vph)             | 0     | 307  | 0    | 0    | 351                       | 0    | 0    | 369  | 0    | 0    | 486   | 0    |
| Confl. Peds. (#/hr)               | 3     |      | 6    | 6    |                           | 3    | 4    |      |      |      | 4     |      |
| Heavy Vehicles (%)                | 0%    | 1%   | 0%   | 0%   | 4%                        | 0%   | 0%   | 2%   | 1%   | 0%   | 3%    | 2%   |
| Turn Type                         | Perm  | NA   |      | Perm | NA                        |      | Perm | NA   |      | Perm | NA    |      |
| Protected Phases                  |       | 4    |      |      |                           | 8    |      |      | 2    |      |       | 6    |
| Permitted Phases                  |       | 4    |      |      |                           | 8    |      |      | 2    |      |       | 6    |
| Actuated Green, G (s)             | 18.0  |      |      |      | 18.0                      |      |      | 18.0 |      |      | 18.0  |      |
| Effective Green, g (s)            | 18.0  |      |      |      | 18.0                      |      |      | 18.0 |      |      | 18.0  |      |
| Actuated g/C Ratio                | 0.40  |      |      |      | 0.40                      |      |      | 0.40 |      |      | 0.40  |      |
| Clearance Time (s)                | 4.5   |      |      |      | 4.5                       |      |      | 4.5  |      |      | 4.5   |      |
| Lane Grp Cap (vph)                | 691   |      |      |      | 578                       |      |      | 715  |      |      | 702   |      |
| v/s Ratio Prot                    |       |      |      |      |                           |      |      |      |      |      |       |      |
| v/s Ratio Perm                    | 0.18  |      |      |      | c0.24                     |      |      | 0.21 |      |      | c0.28 |      |
| v/c Ratio                         | 0.44  |      |      |      | 0.61                      |      |      | 0.52 |      |      | 0.69  |      |
| Uniform Delay, d1                 | 9.9   |      |      |      | 10.7                      |      |      | 10.2 |      |      | 11.2  |      |
| Progression Factor                | 1.00  |      |      |      | 1.00                      |      |      | 1.00 |      |      | 1.00  |      |
| Incremental Delay, d2             | 2.1   |      |      |      | 4.7                       |      |      | 2.7  |      |      | 5.5   |      |
| Delay (s)                         | 11.9  |      |      |      | 15.4                      |      |      | 12.9 |      |      | 16.7  |      |
| Level of Service                  | B     |      |      |      | B                         |      |      | B    |      |      | B     |      |
| Approach Delay (s)                | 11.9  |      |      |      | 15.4                      |      |      | 12.9 |      |      | 16.7  |      |
| Approach LOS                      | B     |      |      |      | B                         |      |      | B    |      |      | B     |      |
| Intersection Summary              |       |      |      |      |                           |      |      |      |      |      |       |      |
| HCM 2000 Control Delay            | 14.5  |      |      |      | HCM 2000 Level of Service |      |      | B    |      |      |       |      |
| HCM 2000 Volume to Capacity ratio | 0.65  |      |      |      |                           |      |      |      |      |      |       |      |
| Actuated Cycle Length (s)         | 45.0  |      |      |      | Sum of lost time (s)      |      |      | 9.0  |      |      |       |      |
| Intersection Capacity Utilization | 60.0% |      |      |      | ICU Level of Service      |      |      | B    |      |      |       |      |
| Analysis Period (min)             | 15    |      |      |      |                           |      |      |      |      |      |       |      |
| c Critical Lane Group             |       |      |      |      |                           |      |      |      |      |      |       |      |

## Queues

9: N Main Street &amp; Scanlon Drive/Russ Street

Section E, Item1.



| Lane Group              | EBL  | EBT  | WBL  | WBT  | NBL  | NBT  | SBL  | SBT  | SBR  |
|-------------------------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 208  | 206  | 52   | 327  | 15   | 635  | 149  | 1168 | 437  |
| v/c Ratio               | 0.64 | 0.60 | 0.24 | 0.82 | 0.08 | 0.66 | 0.44 | 0.83 | 0.37 |
| Control Delay           | 43.0 | 39.6 | 39.8 | 31.9 | 17.0 | 32.7 | 19.5 | 31.3 | 1.7  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay             | 43.0 | 39.6 | 39.8 | 31.9 | 17.0 | 32.7 | 19.5 | 31.3 | 1.7  |
| Queue Length 50th (ft)  | 107  | 101  | 25   | 57   | 5    | 167  | 50   | 277  | 0    |
| Queue Length 95th (ft)  | 185  | 176  | 67   | #197 | 17   | 258  | 96   | #556 | 34   |
| Internal Link Dist (ft) |      |      | 42   | 451  |      | 3510 | 583  |      |      |
| Turn Bay Length (ft)    | 50   |      | 60   |      | 200  |      | 180  |      |      |
| Base Capacity (vph)     | 433  | 455  | 292  | 463  | 182  | 1134 | 415  | 1433 | 1255 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.48 | 0.45 | 0.18 | 0.71 | 0.08 | 0.56 | 0.36 | 0.82 | 0.35 |

## Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis  
9: N Main Street & Scanlon Drive/Russ Street

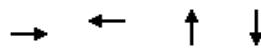
Section E, Item1.

| Movement                          | EBL   | EBT   | EBR  | WBL   | WBT   | WBR  | NBU                       | NBL   | NBT  | NBR  | SBU    | SBL   | SBT   | SBR   |     |
|-----------------------------------|-------|-------|------|-------|-------|------|---------------------------|-------|------|------|--------|-------|-------|-------|-----|
| Lane Configurations               | ↑     | ↔     | ↑    | ↑     | ↔     | ↑    | ↑                         | ↑     | ↑↔   | ↑    | ↑      | ↑     | ↑↔    | ↑     |     |
| Traffic Volume (vph)              | 285   | 25    | 25   | 46    | 38    | 253  | 1                         | 13    | 550  | 34   | 1      | 138   | 1086  | 406   |     |
| Future Volume (vph)               | 285   | 25    | 25   | 46    | 38    | 253  | 1                         | 13    | 550  | 34   | 1      | 138   | 1086  | 406   |     |
| Ideal Flow (vphpl)                | 1900  | 1900  | 1900 | 1900  | 1900  | 1900 | 1900                      | 1900  | 1900 | 1900 | 1900   | 1900  | 1900  | 1900  |     |
| Lane Width                        | 11    | 12    | 12   | 10    | 12    | 12   | 12                        | 10    | 11   | 11   | 12     | 10    | 10    | 11    |     |
| Total Lost time (s)               | 5.0   | 5.0   |      | 5.0   | 5.0   |      |                           |       | 7.0  | 5.0  |        | 7.0   | 5.0   | 5.0   |     |
| Lane Util. Factor                 | 0.95  | 0.95  |      | 1.00  | 1.00  |      |                           |       | 1.00 | 0.95 |        | 1.00  | 0.95  | 1.00  |     |
| Frpb, ped/bikes                   | 1.00  | 1.00  |      | 1.00  | 0.99  |      |                           |       | 1.00 | 1.00 |        | 1.00  | 1.00  | 1.00  |     |
| Flpb, ped/bikes                   | 1.00  | 1.00  |      | 1.00  | 1.00  |      |                           |       | 1.00 | 1.00 |        | 1.00  | 1.00  | 1.00  |     |
| Frt                               | 1.00  | 0.98  |      | 1.00  | 0.87  |      |                           |       | 1.00 | 0.99 |        | 1.00  | 1.00  | 0.85  |     |
| Flt Protected                     | 0.95  | 0.97  |      | 0.95  | 1.00  |      |                           |       | 0.95 | 1.00 |        | 0.95  | 1.00  | 1.00  |     |
| Satd. Flow (prot)                 | 1594  | 1655  |      | 1652  | 1619  |      |                           |       | 1685 | 3357 |        | 1685  | 3240  | 1516  |     |
| Flt Permitted                     | 0.95  | 0.97  |      | 0.95  | 1.00  |      |                           |       | 0.14 | 1.00 |        | 0.23  | 1.00  | 1.00  |     |
| Satd. Flow (perm)                 | 1594  | 1655  |      | 1652  | 1619  |      |                           |       | 240  | 3357 |        | 408   | 3240  | 1516  |     |
| Peak-hour factor, PHF             | 0.81  | 0.81  | 0.81 | 0.89  | 0.89  | 0.89 | 0.92                      | 0.92  | 0.92 | 0.92 | 0.93   | 0.93  | 0.93  | 0.93  |     |
| Adj. Flow (vph)                   | 352   | 31    | 31   | 52    | 43    | 284  | 1                         | 14    | 598  | 37   | 1      | 148   | 1168  | 437   |     |
| RTOR Reduction (vph)              | 0     | 6     | 0    | 0     | 188   | 0    | 0                         | 0     | 4    | 0    | 0      | 0     | 0     | 146   |     |
| Lane Group Flow (vph)             | 208   | 200   | 0    | 52    | 139   | 0    | 0                         | 15    | 631  | 0    | 0      | 149   | 1168  | 291   |     |
| Confl. Peds. (#/hr)               |       |       | 2    | 2     |       |      |                           |       | 3    |      | 6      |       | 6     | 3     |     |
| Confl. Bikes (#/hr)               |       |       |      |       |       |      | 1                         |       |      |      |        |       |       |       |     |
| Heavy Vehicles (%)                | 4%    | 0%    | 0%   | 2%    | 0%    | 1%   | 0%                        | 0%    | 3%   | 0%   | 0%     | 0%    | 4%    | 3%    |     |
| Turn Type                         | Split | NA    |      | Split | NA    |      | custom                    | pm+pt | NA   |      | custom | pm+pt | NA    | pt+ov |     |
| Protected Phases                  | 3     | 3     |      | 4     | 4     |      |                           |       | 5    | 2    |        |       | 1     | 6     | 6.3 |
| Permitted Phases                  |       |       |      |       |       |      | 5                         | 2     |      |      | 1      | 6     |       |       |     |
| Actuated Green, G (s)             | 17.8  | 17.8  |      | 11.5  | 11.5  |      |                           |       | 31.5 | 29.5 |        | 46.9  | 37.9  | 60.7  |     |
| Effective Green, g (s)            | 17.8  | 17.8  |      | 11.5  | 11.5  |      |                           |       | 31.5 | 29.5 |        | 46.9  | 37.9  | 60.7  |     |
| Actuated g/C Ratio                | 0.20  | 0.20  |      | 0.13  | 0.13  |      |                           |       | 0.35 | 0.32 |        | 0.51  | 0.42  | 0.67  |     |
| Clearance Time (s)                | 5.0   | 5.0   |      | 5.0   | 5.0   |      |                           |       | 7.0  | 5.0  |        | 7.0   | 5.0   |       |     |
| Vehicle Extension (s)             | 3.0   | 3.0   |      | 3.0   | 3.0   |      |                           |       | 3.0  | 2.0  |        | 3.0   | 2.0   |       |     |
| Lane Grp Cap (vph)                | 311   | 323   |      | 208   | 204   |      |                           |       | 114  | 1085 |        | 355   | 1346  | 1009  |     |
| v/s Ratio Prot                    | c0.13 | 0.12  |      | 0.03  | c0.09 |      |                           |       | 0.00 | 0.19 |        | c0.05 | c0.36 | 0.19  |     |
| v/s Ratio Perm                    |       |       |      |       |       |      |                           |       | 0.04 |      |        | 0.17  |       |       |     |
| v/c Ratio                         | 0.67  | 0.62  |      | 0.25  | 0.68  |      |                           |       | 0.13 | 0.58 |        | 0.42  | 0.87  | 0.29  |     |
| Uniform Delay, d1                 | 34.0  | 33.6  |      | 36.0  | 38.1  |      |                           |       | 20.9 | 25.7 |        | 13.6  | 24.4  | 6.3   |     |
| Progression Factor                | 1.00  | 1.00  |      | 1.00  | 1.00  |      |                           |       | 1.00 | 1.00 |        | 1.00  | 1.00  | 1.00  |     |
| Incremental Delay, d2             | 5.4   | 3.5   |      | 0.6   | 9.0   |      |                           |       | 0.5  | 0.5  |        | 0.8   | 6.0   | 0.1   |     |
| Delay (s)                         | 39.3  | 37.1  |      | 36.6  | 47.1  |      |                           |       | 21.4 | 26.2 |        | 14.4  | 30.3  | 6.4   |     |
| Level of Service                  | D     | D     |      | D     | D     |      |                           |       | C    | C    |        | B     | C     | A     |     |
| Approach Delay (s)                |       | 38.2  |      |       | 45.7  |      |                           |       | 26.1 |      |        |       | 23.0  |       |     |
| Approach LOS                      |       | D     |      |       | D     |      |                           |       | C    |      |        | C     |       |       |     |
| <b>Intersection Summary</b>       |       |       |      |       |       |      |                           |       |      |      |        |       |       |       |     |
| HCM 2000 Control Delay            |       | 28.3  |      |       |       |      | HCM 2000 Level of Service |       |      | C    |        |       |       |       |     |
| HCM 2000 Volume to Capacity ratio |       | 0.80  |      |       |       |      |                           |       |      |      |        |       |       |       |     |
| Actuated Cycle Length (s)         |       | 91.2  |      |       |       |      | Sum of lost time (s)      |       |      | 22.0 |        |       |       |       |     |
| Intersection Capacity Utilization |       | 79.9% |      |       |       |      | ICU Level of Service      |       |      | D    |        |       |       |       |     |
| Analysis Period (min)             |       | 15    |      |       |       |      |                           |       |      |      |        |       |       |       |     |
| c Critical Lane Group             |       |       |      |       |       |      |                           |       |      |      |        |       |       |       |     |



| Intersection               |       |       |       |      |      |      |
|----------------------------|-------|-------|-------|------|------|------|
| Movement                   | WBL   | WBR   | NBT   | NBR  | SBL  | SBT  |
| Lane Configurations        |       |       |       |      |      |      |
| Traffic Vol, veh/h         | 292   | 4     | 3     | 470  | 1    | 0    |
| Future Vol, veh/h          | 292   | 4     | 3     | 470  | 1    | 0    |
| Peak Hour Factor           | 0.92  | 0.92  | 0.92  | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, %          | 5     | 0     | 0     | 4    | 0    | 0    |
| Mvmt Flow                  | 317   | 4     | 3     | 511  | 1    | 0    |
| Number of Lanes            | 1     | 0     | 1     | 0    | 0    | 1    |
| Approach                   |       |       |       |      |      |      |
| Opposing Approach          |       |       | SB    |      | NB   |      |
| Opposing Lanes             | 0     |       | 1     |      | 1    |      |
| Conflicting Approach Left  | NB    |       |       | WB   |      |      |
| Conflicting Lanes Left     | 1     |       | 0     |      | 1    |      |
| Conflicting Approach Right | SB    |       | WB    |      |      |      |
| Conflicting Lanes Right    | 1     |       | 1     |      | 0    |      |
| HCM Control Delay          | 13    |       | 13.3  |      | 8.7  |      |
| HCM LOS                    | B     |       | B     |      | A    |      |
| Lane                       |       |       |       |      |      |      |
|                            | NBLn1 | WBLn1 | SBLn1 |      |      |      |
| Vol Left, %                | 0%    | 99%   | 100%  |      |      |      |
| Vol Thru, %                | 1%    | 0%    | 0%    |      |      |      |
| Vol Right, %               | 99%   | 1%    | 0%    |      |      |      |
| Sign Control               | Stop  | Stop  | Stop  |      |      |      |
| Traffic Vol by Lane        | 473   | 296   | 1     |      |      |      |
| LT Vol                     | 0     | 292   | 1     |      |      |      |
| Through Vol                | 3     | 0     | 0     |      |      |      |
| RT Vol                     | 470   | 4     | 0     |      |      |      |
| Lane Flow Rate             | 514   | 322   | 1     |      |      |      |
| Geometry Grp               | 1     | 1     | 1     |      |      |      |
| Degree of Util (X)         | 0.599 | 0.47  | 0.002 |      |      |      |
| Departure Headway (Hd)     | 4.194 | 5.258 | 5.563 |      |      |      |
| Convergence, Y/N           | Yes   | Yes   | Yes   |      |      |      |
| Cap                        | 859   | 679   | 637   |      |      |      |
| Service Time               | 2.227 | 3.35  | 3.649 |      |      |      |
| HCM Lane V/C Ratio         | 0.598 | 0.474 | 0.002 |      |      |      |
| HCM Control Delay          | 13.3  | 13    | 8.7   |      |      |      |
| HCM Lane LOS               | B     | B     | A     |      |      |      |
| HCM 95th-tile Q            | 4.1   | 2.5   | 0     |      |      |      |

## 3: Reed Street &amp; High Street



| Lane Group              | EBT  | WBT  | NBT  | SBT  |
|-------------------------|------|------|------|------|
| Lane Group Flow (vph)   | 529  | 268  | 668  | 326  |
| v/c Ratio               | 0.78 | 0.43 | 0.99 | 0.47 |
| Control Delay           | 24.5 | 13.9 | 52.9 | 14.7 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay             | 24.5 | 13.9 | 52.9 | 14.7 |
| Queue Length 50th (ft)  | 141  | 58   | 207  | 74   |
| Queue Length 95th (ft)  | #294 | 111  | #407 | 134  |
| Internal Link Dist (ft) | 410  | 2031 | 474  | 3954 |
| Turn Bay Length (ft)    |      |      |      |      |
| Base Capacity (vph)     | 675  | 617  | 674  | 695  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.78 | 0.43 | 0.99 | 0.47 |

## Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis  
3: Reed Street & High Street

Section E, Item1.



| Movement                          | EBL    | EBT  | EBR  | WBL                       | WBT  | WBR  | NBL   | NBT  | NBR  | SBL  | SBT  | SBR  |
|-----------------------------------|--------|------|------|---------------------------|------|------|-------|------|------|------|------|------|
| Lane Configurations               |        |      |      |                           |      |      |       |      |      |      |      |      |
| Traffic Volume (vph)              | 175    | 298  | 14   | 59                        | 179  | 8    | 60    | 413  | 142  | 5    | 206  | 89   |
| Future Volume (vph)               | 175    | 298  | 14   | 59                        | 179  | 8    | 60    | 413  | 142  | 5    | 206  | 89   |
| Ideal Flow (vphpl)                | 1900   | 1900 | 1900 | 1900                      | 1900 | 1900 | 1900  | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width                        | 12     | 15   | 12   | 12                        | 11   | 12   | 12    | 12   | 12   | 12   | 12   | 12   |
| Total Lost time (s)               |        | 4.5  |      |                           | 4.5  |      |       | 4.5  |      |      | 4.5  |      |
| Lane Util. Factor                 |        | 1.00 |      |                           | 1.00 |      |       | 1.00 |      |      | 1.00 |      |
| Frpb, ped/bikes                   |        | 1.00 |      |                           | 1.00 |      |       | 0.99 |      |      | 0.99 |      |
| Flpb, ped/bikes                   |        | 0.98 |      |                           | 1.00 |      |       | 1.00 |      |      | 1.00 |      |
| Frt                               |        | 1.00 |      |                           | 1.00 |      |       | 0.97 |      |      | 0.96 |      |
| Flt Protected                     |        | 0.98 |      |                           | 0.99 |      |       | 1.00 |      |      | 1.00 |      |
| Satd. Flow (prot)                 |        | 1991 |      |                           | 1715 |      |       | 1752 |      |      | 1714 |      |
| Flt Permitted                     |        | 0.78 |      |                           | 0.83 |      |       | 0.94 |      |      | 0.99 |      |
| Satd. Flow (perm)                 |        | 1581 |      |                           | 1446 |      |       | 1648 |      |      | 1700 |      |
| Peak-hour factor, PHF             | 0.92   | 0.92 | 0.92 | 0.92                      | 0.92 | 0.92 | 0.92  | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph)                   | 190    | 324  | 15   | 64                        | 195  | 9    | 65    | 449  | 154  | 5    | 224  | 97   |
| RTOR Reduction (vph)              | 0      | 0    | 0    | 0                         | 0    | 0    | 0     | 0    | 0    | 0    | 0    | 0    |
| Lane Group Flow (vph)             | 0      | 529  | 0    | 0                         | 268  | 0    | 0     | 668  | 0    | 0    | 326  | 0    |
| Confl. Peds. (#/hr)               | 46     |      | 17   | 17                        |      | 46   | 12    |      | 4    | 4    |      | 12   |
| Heavy Vehicles (%)                | 1%     | 1%   | 0%   | 11%                       | 3%   | 0%   | 0%    | 5%   | 2%   | 0%   | 7%   | 1%   |
| Turn Type                         | Perm   | NA   |      | Perm                      | NA   |      | Perm  | NA   |      | Perm | NA   |      |
| Protected Phases                  |        | 4    |      |                           | 8    |      |       | 2    |      |      | 6    |      |
| Permitted Phases                  | 4      |      |      | 8                         |      |      | 2     |      |      | 6    |      |      |
| Actuated Green, G (s)             | 23.5   |      |      | 23.5                      |      |      | 22.5  |      |      | 22.5 |      |      |
| Effective Green, g (s)            | 23.5   |      |      | 23.5                      |      |      | 22.5  |      |      | 22.5 |      |      |
| Actuated g/C Ratio                | 0.43   |      |      | 0.43                      |      |      | 0.41  |      |      | 0.41 |      |      |
| Clearance Time (s)                | 4.5    |      |      | 4.5                       |      |      | 4.5   |      |      | 4.5  |      |      |
| Lane Grp Cap (vph)                | 675    |      |      | 617                       |      |      | 674   |      |      | 695  |      |      |
| v/s Ratio Prot                    |        |      |      |                           |      |      |       |      |      |      |      |      |
| v/s Ratio Perm                    | c0.33  |      |      | 0.19                      |      |      | c0.41 |      |      | 0.19 |      |      |
| v/c Ratio                         | 0.78   |      |      | 0.43                      |      |      | 0.99  |      |      | 0.47 |      |      |
| Uniform Delay, d1                 | 13.6   |      |      | 11.1                      |      |      | 16.2  |      |      | 11.9 |      |      |
| Progression Factor                | 1.00   |      |      | 1.00                      |      |      | 1.00  |      |      | 1.00 |      |      |
| Incremental Delay, d2             | 8.9    |      |      | 2.2                       |      |      | 32.6  |      |      | 2.3  |      |      |
| Delay (s)                         | 22.4   |      |      | 13.3                      |      |      | 48.7  |      |      | 14.1 |      |      |
| Level of Service                  | C      |      |      | B                         |      |      | D     |      |      | B    |      |      |
| Approach Delay (s)                | 22.4   |      |      | 13.3                      |      |      | 48.7  |      |      | 14.1 |      |      |
| Approach LOS                      | C      |      |      | B                         |      |      | D     |      |      | B    |      |      |
| Intersection Summary              |        |      |      |                           |      |      |       |      |      |      |      |      |
| HCM 2000 Control Delay            | 29.4   |      |      | HCM 2000 Level of Service |      |      | C     |      |      |      |      |      |
| HCM 2000 Volume to Capacity ratio | 0.88   |      |      |                           |      |      |       |      |      |      |      |      |
| Actuated Cycle Length (s)         | 55.0   |      |      | Sum of lost time (s)      |      |      | 9.0   |      |      |      |      |      |
| Intersection Capacity Utilization | 103.5% |      |      | ICU Level of Service      |      |      | G     |      |      |      |      |      |
| Analysis Period (min)             | 15     |      |      |                           |      |      |       |      |      |      |      |      |
| c Critical Lane Group             |        |      |      |                           |      |      |       |      |      |      |      |      |

## Queues

9: N Main Street &amp; Scanlon Drive/Russ Street

Section E, Item1.



| Lane Group              | EBL  | EBT  | WBL  | WBT  | NBL  | NBT  | SBL   | SBT  | SBR  |
|-------------------------|------|------|------|------|------|------|-------|------|------|
| Lane Group Flow (vph)   | 316  | 318  | 54   | 152  | 49   | 1121 | 324   | 777  | 297  |
| v/c Ratio               | 0.92 | 0.89 | 0.60 | 0.92 | 0.16 | 0.88 | 1.12  | 0.53 | 0.25 |
| Control Delay           | 76.4 | 70.1 | 78.7 | 77.5 | 12.2 | 39.8 | 122.1 | 21.1 | 1.0  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0   | 0.0  | 0.0  |
| Total Delay             | 76.4 | 70.1 | 78.7 | 77.5 | 12.2 | 39.8 | 122.1 | 21.1 | 1.0  |
| Queue Length 50th (ft)  | 229  | 227  | 37   | 51   | 14   | 371  | ~218  | 198  | 0    |
| Queue Length 95th (ft)  | #436 | #431 | #103 | #185 | 31   | 461  | #414  | 256  | 20   |
| Internal Link Dist (ft) |      |      | 42   |      | 451  |      | 3510  |      | 583  |
| Turn Bay Length (ft)    | 50   |      | 60   |      | 200  |      | 180   |      |      |
| Base Capacity (vph)     | 342  | 356  | 90   | 166  | 309  | 1479 | 288   | 1571 | 1174 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    |
| Reduced v/c Ratio       | 0.92 | 0.89 | 0.60 | 0.92 | 0.16 | 0.76 | 1.13  | 0.49 | 0.25 |

## Intersection Summary

~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

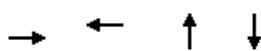
HCM Signalized Intersection Capacity Analysis  
9: N Main Street & Scanlon Drive/Russ Street

Section E, Item1.

| Movement                          | EBL   | EBT   | EBR  | WBL   | WBT   | WBR                       | NBL   | NBT  | NBR  | SBU    | SBL   | SBT   | SBR   |
|-----------------------------------|-------|-------|------|-------|-------|---------------------------|-------|------|------|--------|-------|-------|-------|
| Lane Configurations               | ↑     | ↔     |      | ↑     | ↔     |                           | ↑     | ↔    |      |        | ↑     | ↔     | ↑     |
| Traffic Volume (vph)              | 501   | 70    | 12   | 50    | 41    | 98                        | 45    | 985  | 46   | 2      | 296   | 715   | 273   |
| Future Volume (vph)               | 501   | 70    | 12   | 50    | 41    | 98                        | 45    | 985  | 46   | 2      | 296   | 715   | 273   |
| Ideal Flow (vphpl)                | 1900  | 1900  | 1900 | 1900  | 1900  | 1900                      | 1900  | 1900 | 1900 | 1900   | 1900  | 1900  | 1900  |
| Lane Width                        | 11    | 12    | 12   | 10    | 12    | 12                        | 10    | 11   | 11   | 12     | 10    | 10    | 11    |
| Total Lost time (s)               | 5.0   | 5.0   |      | 5.0   | 5.0   |                           | 7.0   | 5.0  |      |        | 7.0   | 5.0   | 5.0   |
| Lane Util. Factor                 | 0.95  | 0.95  |      | 1.00  | 1.00  |                           | 1.00  | 0.95 |      |        | 1.00  | 0.95  | 1.00  |
| Frpb, ped/bikes                   | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Frbp, ped/bikes                   | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Frt                               | 1.00  | 0.99  |      | 1.00  | 0.89  |                           | 1.00  | 0.99 |      |        | 1.00  | 1.00  | 0.85  |
| Flt Protected                     | 0.95  | 0.97  |      | 0.95  | 1.00  |                           | 0.95  | 1.00 |      |        | 0.95  | 1.00  | 1.00  |
| Satd. Flow (prot)                 | 1594  | 1653  |      | 1620  | 1653  |                           | 1572  | 3298 |      |        | 1636  | 3008  | 1473  |
| Flt Permitted                     | 0.95  | 0.97  |      | 0.95  | 1.00  |                           | 0.34  | 1.00 |      |        | 0.08  | 1.00  | 1.00  |
| Satd. Flow (perm)                 | 1594  | 1653  |      | 1620  | 1653  |                           | 567   | 3298 |      |        | 138   | 3008  | 1473  |
| Peak-hour factor, PHF             | 0.92  | 0.92  | 0.92 | 0.92  | 0.92  | 0.92                      | 0.92  | 0.92 | 0.92 | 0.92   | 0.92  | 0.92  | 0.92  |
| Adj. Flow (vph)                   | 545   | 76    | 13   | 54    | 45    | 107                       | 49    | 1071 | 50   | 2      | 322   | 777   | 297   |
| RTOR Reduction (vph)              | 0     | 2     | 0    | 0     | 75    | 0                         | 0     | 3    | 0    | 0      | 0     | 0     | 77    |
| Lane Group Flow (vph)             | 316   | 316   | 0    | 54    | 77    | 0                         | 49    | 1118 | 0    | 0      | 324   | 777   | 220   |
| Confl. Peds. (#/hr)               |       |       |      | 4     | 4     |                           |       | 5    |      |        |       |       | 5     |
| Heavy Vehicles (%)                | 4%    | 6%    | 9%   | 4%    | 0%    | 4%                        | 7%    | 5%   | 7%   | 2%     | 3%    | 12%   | 6%    |
| Turn Type                         | Split | NA    |      | Split | NA    |                           | pm+pt | NA   |      | custom | pm+pt | NA    | pt+ov |
| Protected Phases                  | 3     | 3     |      | 4     | 4     |                           | 5     | 2    |      |        | 1     | 6     | 6.3   |
| Permitted Phases                  |       |       |      |       |       |                           | 2     |      |      |        | 1     | 6     |       |
| Actuated Green, G (s)             | 23.1  | 23.1  |      | 6.0   | 6.0   |                           | 48.1  | 42.8 |      |        | 64.9  | 52.6  | 80.7  |
| Effective Green, g (s)            | 23.1  | 23.1  |      | 6.0   | 6.0   |                           | 48.1  | 42.8 |      |        | 64.9  | 52.6  | 80.7  |
| Actuated g/C Ratio                | 0.21  | 0.21  |      | 0.06  | 0.06  |                           | 0.44  | 0.39 |      |        | 0.60  | 0.48  | 0.74  |
| Clearance Time (s)                | 5.0   | 5.0   |      | 5.0   | 5.0   |                           | 7.0   | 5.0  |      |        | 7.0   | 5.0   |       |
| Vehicle Extension (s)             | 3.0   | 3.0   |      | 3.0   | 3.0   |                           | 3.0   | 2.0  |      |        | 3.0   | 2.0   |       |
| Lane Grp Cap (vph)                | 337   | 350   |      | 89    | 90    |                           | 299   | 1294 |      |        | 289   | 1451  | 1090  |
| v/s Ratio Prot                    | c0.20 | 0.19  |      | 0.03  | c0.05 |                           | 0.01  | 0.34 |      |        | c0.15 | 0.26  | 0.15  |
| v/s Ratio Perm                    |       |       |      |       |       |                           | 0.06  |      |      |        |       | c0.51 |       |
| v/c Ratio                         | 0.94  | 0.90  |      | 0.61  | 0.86  |                           | 0.16  | 0.86 |      |        | 1.12  | 0.54  | 0.20  |
| Uniform Delay, d1                 | 42.2  | 41.9  |      | 50.3  | 51.1  |                           | 17.6  | 30.4 |      |        | 33.9  | 19.7  | 4.3   |
| Progression Factor                | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Incremental Delay, d2             | 32.9  | 25.6  |      | 11.2  | 51.3  |                           | 0.3   | 6.0  |      |        | 89.6  | 0.2   | 0.0   |
| Delay (s)                         | 75.1  | 67.4  |      | 61.5  | 102.4 |                           | 17.8  | 36.4 |      |        | 123.5 | 19.9  | 4.4   |
| Level of Service                  | E     | E     |      | E     | F     |                           | B     | D    |      |        | F     | B     | A     |
| Approach Delay (s)                |       | 71.3  |      |       | 91.7  |                           |       | 35.7 |      |        |       | 40.6  |       |
| Approach LOS                      |       | E     |      |       | F     |                           |       | D    |      |        |       | D     |       |
| Intersection Summary              |       |       |      |       |       |                           |       |      |      |        |       |       |       |
| HCM 2000 Control Delay            |       | 47.7  |      |       |       | HCM 2000 Level of Service |       |      | D    |        |       |       |       |
| HCM 2000 Volume to Capacity ratio |       | 1.09  |      |       |       |                           |       |      |      |        |       |       |       |
| Actuated Cycle Length (s)         |       | 109.0 |      |       |       | Sum of lost time (s)      |       |      | 22.0 |        |       |       |       |
| Intersection Capacity Utilization |       | 87.9% |      |       |       | ICU Level of Service      |       |      | E    |        |       |       |       |
| Analysis Period (min)             |       | 15    |      |       |       |                           |       |      |      |        |       |       |       |
| c Critical Lane Group             |       |       |      |       |       |                           |       |      |      |        |       |       |       |



| Intersection               |   |       |       |      |      |      |  |
|----------------------------|---|-------|-------|------|------|------|--|
| Intersection Delay, s/veh  | 17.4  |       |       |      |      |      |  |
| Intersection LOS           | C   |       |       |      |      |      |  |
| Movement                   | WBL   | WBR   | NBT   | NBR  | SBL  | SBT  |  |
| Lane Configurations        |  |       |       |      |      |      |  |
| Traffic Vol, veh/h         | 505   | 0     | 2     | 292  | 1    | 2    |  |
| Future Vol, veh/h          | 505   | 0     | 2     | 292  | 1    | 2    |  |
| Peak Hour Factor           | 0.92  | 0.92  | 0.92  | 0.92 | 0.92 | 0.92 |  |
| Heavy Vehicles, %          | 2   | 0     | 0     | 2    | 0    | 0    |  |
| Mvmt Flow                  | 549   | 0     | 2     | 317  | 1    | 2    |  |
| Number of Lanes            | 1   | 0     | 1     | 0    | 0    | 1    |  |
| Approach                   | WB  | NB    |       | SB   |      |      |  |
| Opposing Approach          |   | SB    |       | NB   |      |      |  |
| Opposing Lanes             | 0   | 1     |       | 1    |      |      |  |
| Conflicting Approach Left  | NB  |       |       | WB   |      |      |  |
| Conflicting Lanes Left     | 1   | 0     |       | 1    |      |      |  |
| Conflicting Approach Right | SB  | WB    |       |      |      |      |  |
| Conflicting Lanes Right    | 1   | 1     |       | 0    |      |      |  |
| HCM Control Delay          | 21  | 11.2  |       | 8.9  |      |      |  |
| HCM LOS                    | C   | B     |       | A    |      |      |  |
| Lane                       | NBLn1   | WBLn1 | SBLn1 |      |      |      |  |
| Vol Left, %                | 0%  | 100%  | 33%   |      |      |      |  |
| Vol Thru, %                | 1%  | 0%    | 67%   |      |      |      |  |
| Vol Right, %               | 99%   | 0%    | 0%    |      |      |      |  |
| Sign Control               | Stop  | Stop  | Stop  |      |      |      |  |
| Traffic Vol by Lane        | 294   | 505   | 3     |      |      |      |  |
| LT Vol                     | 0   | 505   | 1     |      |      |      |  |
| Through Vol                | 2   | 0     | 2     |      |      |      |  |
| RT Vol                     | 292   | 0     | 0     |      |      |      |  |
| Lane Flow Rate             | 320   | 549   | 3     |      |      |      |  |
| Geometry Grp               | 1   | 1     | 1     |      |      |      |  |
| Degree of Util (X)         | 0.418   | 0.745 | 0.005 |      |      |      |  |
| Departure Headway (Hd)     | 4.714   | 4.884 | 5.918 |      |      |      |  |
| Convergence, Y/N           | Yes   | Yes   | Yes   |      |      |      |  |
| Cap                        | 761   | 736   | 608   |      |      |      |  |
| Service Time               | 2.771   | 2.96  | 3.918 |      |      |      |  |
| HCM Lane V/C Ratio         | 0.42  | 0.746 | 0.005 |      |      |      |  |
| HCM Control Delay          | 11.2  | 21    | 8.9   |      |      |      |  |
| HCM Lane LOS               | B   | C     | A     |      |      |      |  |
| HCM 95th-tile Q            | 2.1   | 6.8   | 0     |      |      |      |  |



| Lane Group              | EBT  | WBT  | NBT  | SBT  |
|-------------------------|------|------|------|------|
| Lane Group Flow (vph)   | 324  | 372  | 377  | 550  |
| v/c Ratio               | 0.48 | 0.65 | 0.53 | 0.78 |
| Control Delay           | 12.9 | 18.0 | 13.6 | 22.7 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay             | 12.9 | 18.0 | 13.6 | 22.7 |
| Queue Length 50th (ft)  | 58   | 74   | 70   | 117  |
| Queue Length 95th (ft)  | 112  | #156 | 131  | #259 |
| Internal Link Dist (ft) | 410  | 2031 | 474  | 3954 |
| Turn Bay Length (ft)    |      |      |      |      |
| Base Capacity (vph)     | 680  | 570  | 716  | 702  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.48 | 0.65 | 0.53 | 0.78 |

Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis  
3: Reed Street & High Street

Section E, Item1.



| Movement                          | EBL   | EBT  | EBR  | WBL                       | WBT  | WBR  | NBL  | NBT  | NBR  | SBL   | SBT  | SBR  |
|-----------------------------------|-------|------|------|---------------------------|------|------|------|------|------|-------|------|------|
| Lane Configurations               |       |      |      |                           |      |      |      |      |      |       |      |      |
| Traffic Volume (vph)              | 87    | 200  | 11   | 117                       | 221  | 5    | 5    | 253  | 89   | 7     | 354  | 144  |
| Future Volume (vph)               | 87    | 200  | 11   | 117                       | 221  | 5    | 5    | 253  | 89   | 7     | 354  | 144  |
| Ideal Flow (vphpl)                | 1900  | 1900 | 1900 | 1900                      | 1900 | 1900 | 1900 | 1900 | 1900 | 1900  | 1900 | 1900 |
| Lane Width                        | 12    | 15   | 12   | 12                        | 11   | 12   | 12   | 12   | 12   | 12    | 12   | 12   |
| Total Lost time (s)               |       | 4.5  |      |                           | 4.5  |      |      | 4.5  |      |       | 4.5  |      |
| Lane Util. Factor                 |       | 1.00 |      |                           | 1.00 |      |      | 1.00 |      |       | 1.00 |      |
| Frpb, ped/bikes                   |       | 1.00 |      |                           | 1.00 |      |      | 1.00 |      |       | 0.99 |      |
| Fpb, ped/bikes                    |       | 1.00 |      |                           | 1.00 |      |      | 1.00 |      |       | 1.00 |      |
| Frt                               |       | 0.99 |      |                           | 1.00 |      |      | 0.97 |      |       | 0.96 |      |
| Flt Protected                     |       | 0.99 |      |                           | 0.98 |      |      | 1.00 |      |       | 1.00 |      |
| Satd. Flow (prot)                 |       | 2033 |      |                           | 1754 |      |      | 1802 |      |       | 1765 |      |
| Flt Permitted                     |       | 0.83 |      |                           | 0.80 |      |      | 0.99 |      |       | 0.99 |      |
| Satd. Flow (perm)                 |       | 1702 |      |                           | 1425 |      |      | 1790 |      |       | 1755 |      |
| Peak-hour factor, PHF             | 0.92  | 0.92 | 0.92 | 0.92                      | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92  | 0.92 | 0.92 |
| Adj. Flow (vph)                   | 95    | 217  | 12   | 127                       | 240  | 5    | 5    | 275  | 97   | 8     | 385  | 157  |
| RTOR Reduction (vph)              | 0     | 0    | 0    | 0                         | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    |
| Lane Group Flow (vph)             | 0     | 324  | 0    | 0                         | 372  | 0    | 0    | 377  | 0    | 0     | 550  | 0    |
| Confl. Peds. (#/hr)               | 3     |      | 6    | 6                         |      | 3    | 4    |      |      |       | 4    |      |
| Heavy Vehicles (%)                | 0%    | 1%   | 0%   | 0%                        | 4%   | 0%   | 0%   | 2%   | 1%   | 0%    | 3%   | 2%   |
| Turn Type                         | Perm  | NA   |      | Perm                      | NA   |      | Perm | NA   |      | Perm  | NA   |      |
| Protected Phases                  |       | 4    |      |                           | 8    |      |      | 2    |      |       | 6    |      |
| Permitted Phases                  | 4     |      |      | 8                         |      |      | 2    |      |      | 6     |      |      |
| Actuated Green, G (s)             | 18.0  |      |      | 18.0                      |      |      | 18.0 |      |      | 18.0  |      |      |
| Effective Green, g (s)            | 18.0  |      |      | 18.0                      |      |      | 18.0 |      |      | 18.0  |      |      |
| Actuated g/C Ratio                | 0.40  |      |      | 0.40                      |      |      | 0.40 |      |      | 0.40  |      |      |
| Clearance Time (s)                | 4.5   |      |      | 4.5                       |      |      | 4.5  |      |      | 4.5   |      |      |
| Lane Grp Cap (vph)                | 680   |      |      | 570                       |      |      | 716  |      |      | 702   |      |      |
| v/s Ratio Prot                    |       |      |      |                           |      |      |      |      |      |       |      |      |
| v/s Ratio Perm                    | 0.19  |      |      | c0.26                     |      |      | 0.21 |      |      | c0.31 |      |      |
| v/c Ratio                         | 0.48  |      |      | 0.65                      |      |      | 0.53 |      |      | 0.78  |      |      |
| Uniform Delay, d1                 | 10.0  |      |      | 11.0                      |      |      | 10.3 |      |      | 11.8  |      |      |
| Progression Factor                | 1.00  |      |      | 1.00                      |      |      | 1.00 |      |      | 1.00  |      |      |
| Incremental Delay, d2             | 2.4   |      |      | 5.7                       |      |      | 2.8  |      |      | 8.5   |      |      |
| Delay (s)                         | 12.4  |      |      | 16.7                      |      |      | 13.0 |      |      | 20.3  |      |      |
| Level of Service                  | B     |      |      | B                         |      |      | B    |      |      | C     |      |      |
| Approach Delay (s)                | 12.4  |      |      | 16.7                      |      |      | 13.0 |      |      | 20.3  |      |      |
| Approach LOS                      | B     |      |      | B                         |      |      | B    |      |      | C     |      |      |
| Intersection Summary              |       |      |      |                           |      |      |      |      |      |       |      |      |
| HCM 2000 Control Delay            | 16.2  |      |      | HCM 2000 Level of Service |      |      | B    |      |      |       |      |      |
| HCM 2000 Volume to Capacity ratio | 0.72  |      |      |                           |      |      |      |      |      |       |      |      |
| Actuated Cycle Length (s)         | 45.0  |      |      | Sum of lost time (s)      |      |      | 9.0  |      |      |       |      |      |
| Intersection Capacity Utilization | 65.0% |      |      | ICU Level of Service      |      |      | C    |      |      |       |      |      |
| Analysis Period (min)             | 15    |      |      |                           |      |      |      |      |      |       |      |      |
| c Critical Lane Group             |       |      |      |                           |      |      |      |      |      |       |      |      |

## Queues

9: N Main Street &amp; Scanlon Drive/Russ Street

Section E, Item1.



| Lane Group              | EBL  | EBT  | WBL  | WBT  | NBL  | NBT  | SBL  | SBT  | SBR  |
|-------------------------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 221  | 215  | 53   | 341  | 33   | 680  | 162  | 1290 | 499  |
| v/c Ratio               | 0.67 | 0.62 | 0.24 | 0.86 | 0.19 | 0.69 | 0.50 | 0.96 | 0.42 |
| Control Delay           | 45.8 | 41.7 | 41.1 | 39.2 | 18.8 | 34.3 | 21.3 | 47.3 | 1.9  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay             | 45.8 | 41.7 | 41.1 | 39.2 | 18.8 | 34.3 | 21.3 | 47.3 | 1.9  |
| Queue Length 50th (ft)  | 138  | 129  | 31   | 88   | 11   | 200  | 61   | ~510 | 0    |
| Queue Length 95th (ft)  | 224  | 211  | 68   | #241 | 29   | 281  | 103  | #646 | 36   |
| Internal Link Dist (ft) |      |      | 42   | 451  |      | 3510 |      | 583  |      |
| Turn Bay Length (ft)    | 50   |      | 60   |      | 200  |      | 180  |      |      |
| Base Capacity (vph)     | 409  | 431  | 277  | 440  | 176  | 1092 | 390  | 1340 | 1238 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.54 | 0.50 | 0.19 | 0.78 | 0.19 | 0.62 | 0.42 | 0.96 | 0.40 |

## Intersection Summary

~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

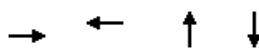
HCM Signalized Intersection Capacity Analysis  
9: N Main Street & Scanlon Drive/Russ Street

Section E, Item1.

| Movement                          | EBL   | EBT   | EBR  | WBL                       | WBT   | WBR  | NBU    | NBL   | NBT  | NBR  | SBU    | SBL   | SBT   | SBR   |
|-----------------------------------|-------|-------|------|---------------------------|-------|------|--------|-------|------|------|--------|-------|-------|-------|
| Lane Configurations               |       |       |      |                           |       |      |        |       |      |      |        |       |       |       |
| Traffic Volume (vph)              | 344   | 29    | 28   | 49                        | 42    | 271  | 1      | 29    | 590  | 36   | 1      | 148   | 1187  | 459   |
| Future Volume (vph)               | 344   | 29    | 28   | 49                        | 42    | 271  | 1      | 29    | 590  | 36   | 1      | 148   | 1187  | 459   |
| Ideal Flow (vphpl)                | 1900  | 1900  | 1900 | 1900                      | 1900  | 1900 | 1900   | 1900  | 1900 | 1900 | 1900   | 1900  | 1900  | 1900  |
| Lane Width                        | 11    | 12    | 12   | 10                        | 12    | 12   | 12     | 10    | 11   | 11   | 12     | 10    | 10    | 11    |
| Total Lost time (s)               | 5.0   | 5.0   |      | 5.0                       | 5.0   |      |        | 7.0   | 5.0  |      |        | 7.0   | 5.0   | 5.0   |
| Lane Util. Factor                 | 0.95  | 0.95  |      | 1.00                      | 1.00  |      |        | 1.00  | 0.95 |      |        | 1.00  | 0.95  | 1.00  |
| Frpb, ped/bikes                   | 1.00  | 1.00  |      | 1.00                      | 0.99  |      |        | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Flpb, ped/bikes                   | 1.00  | 1.00  |      | 1.00                      | 1.00  |      |        | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Frt                               | 1.00  | 0.98  |      | 1.00                      | 0.87  |      |        | 1.00  | 0.99 |      |        | 1.00  | 1.00  | 0.85  |
| Flt Protected                     | 0.95  | 0.97  |      | 0.95                      | 1.00  |      |        | 0.95  | 1.00 |      |        | 0.95  | 1.00  | 1.00  |
| Satd. Flow (prot)                 | 1594  | 1656  |      | 1652                      | 1620  |      |        | 1685  | 3357 |      |        | 1685  | 3240  | 1516  |
| Flt Permitted                     | 0.95  | 0.97  |      | 0.95                      | 1.00  |      |        | 0.13  | 1.00 |      |        | 0.20  | 1.00  | 1.00  |
| Satd. Flow (perm)                 | 1594  | 1656  |      | 1652                      | 1620  |      |        | 234   | 3357 |      |        | 361   | 3240  | 1516  |
| Peak-hour factor, PHF             | 0.92  | 0.92  | 0.92 | 0.92                      | 0.92  | 0.92 | 0.92   | 0.92  | 0.92 | 0.92 | 0.92   | 0.92  | 0.92  | 0.92  |
| Adj. Flow (vph)                   | 374   | 32    | 30   | 53                        | 46    | 295  | 1      | 32    | 641  | 39   | 1      | 161   | 1290  | 499   |
| RTOR Reduction (vph)              | 0     | 6     | 0    | 0                         | 176   | 0    | 0      | 0     | 4    | 0    | 0      | 0     | 0     | 172   |
| Lane Group Flow (vph)             | 221   | 209   | 0    | 53                        | 165   | 0    | 0      | 33    | 676  | 0    | 0      | 162   | 1290  | 327   |
| Confl. Peds. (#/hr)               |       |       |      | 2                         | 2     |      |        | 3     |      | 6    |        | 6     |       | 3     |
| Confl. Bikes (#/hr)               |       |       |      |                           |       |      | 1      |       |      |      |        |       |       |       |
| Heavy Vehicles (%)                | 4%    | 0%    | 0%   | 2%                        | 0%    | 1%   | 0%     | 0%    | 3%   | 0%   | 0%     | 0%    | 4%    | 3%    |
| Turn Type                         | Split | NA    |      | Split                     | NA    |      | custom | pm+pt | NA   |      | custom | pm+pt | NA    | pt+ov |
| Protected Phases                  | 3     | 3     |      | 4                         | 4     |      |        | 5     | 2    |      |        | 1     | 6     | 6.3   |
| Permitted Phases                  |       |       |      |                           |       | 5    | 2      |       |      | 1    | 6      |       |       |       |
| Actuated Green, G (s)             | 19.0  | 19.0  |      | 12.5                      | 12.5  |      |        | 33.5  | 30.3 |      |        | 48.2  | 38.0  | 62.0  |
| Effective Green, g (s)            | 19.0  | 19.0  |      | 12.5                      | 12.5  |      |        | 33.5  | 30.3 |      |        | 48.2  | 38.0  | 62.0  |
| Actuated g/C Ratio                | 0.20  | 0.20  |      | 0.13                      | 0.13  |      |        | 0.35  | 0.32 |      |        | 0.51  | 0.40  | 0.65  |
| Clearance Time (s)                | 5.0   | 5.0   |      | 5.0                       | 5.0   |      |        | 7.0   | 5.0  |      |        | 7.0   | 5.0   |       |
| Vehicle Extension (s)             | 3.0   | 3.0   |      | 3.0                       | 3.0   |      |        | 3.0   | 2.0  |      |        | 3.0   | 2.0   |       |
| Lane Grp Cap (vph)                | 319   | 332   |      | 218                       | 213   |      |        | 131   | 1074 |      |        | 336   | 1300  | 992   |
| v/s Ratio Prot                    | c0.14 | 0.13  |      | 0.03                      | c0.10 |      |        | 0.01  | 0.20 |      |        | c0.06 | c0.40 | 0.22  |
| v/s Ratio Perm                    |       |       |      |                           |       |      | 0.08   |       |      |      |        | 0.19  |       |       |
| v/c Ratio                         | 0.69  | 0.63  |      | 0.24                      | 0.77  |      |        | 0.25  | 0.63 |      |        | 0.48  | 0.99  | 0.33  |
| Uniform Delay, d1                 | 35.1  | 34.6  |      | 36.9                      | 39.7  |      |        | 22.7  | 27.4 |      |        | 14.9  | 28.2  | 7.2   |
| Progression Factor                | 1.00  | 1.00  |      | 1.00                      | 1.00  |      |        | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Incremental Delay, d2             | 6.4   | 3.9   |      | 0.6                       | 15.9  |      |        | 1.0   | 0.8  |      |        | 1.1   | 23.0  | 0.1   |
| Delay (s)                         | 41.5  | 38.5  |      | 37.4                      | 55.7  |      |        | 23.8  | 28.3 |      |        | 15.9  | 51.2  | 7.3   |
| Level of Service                  | D     | D     |      | D                         | E     |      |        | C     | C    |      |        | B     | D     | A     |
| Approach Delay (s)                | 40.0  |       |      |                           | 53.2  |      |        |       | 28.0 |      |        |       | 37.0  |       |
| Approach LOS                      | D     |       |      | D                         |       |      |        | C     |      |      |        | D     |       |       |
| <b>Intersection Summary</b>       |       |       |      |                           |       |      |        |       |      |      |        |       |       |       |
| HCM 2000 Control Delay            |       | 37.4  |      | HCM 2000 Level of Service |       |      |        |       | D    |      |        |       |       |       |
| HCM 2000 Volume to Capacity ratio |       | 0.88  |      |                           |       |      |        |       |      |      |        |       |       |       |
| Actuated Cycle Length (s)         |       | 94.7  |      | Sum of lost time (s)      |       |      |        |       | 22.0 |      |        |       |       |       |
| Intersection Capacity Utilization |       | 85.8% |      | ICU Level of Service      |       |      |        |       | E    |      |        |       |       |       |
| Analysis Period (min)             |       | 15    |      |                           |       |      |        |       |      |      |        |       |       |       |
| c Critical Lane Group             |       |       |      |                           |       |      |        |       |      |      |        |       |       |       |



| Intersection               |       |       |       |      |      |      |
|----------------------------|-------|-------|-------|------|------|------|
| Intersection Delay, s/veh  | 14.3  |       |       |      |      |      |
| Intersection LOS           | B     |       |       |      |      |      |
| Movement                   | WBL   | WBR   | NBT   | NBR  | SBL  | SBT  |
| Lane Configurations        |       |       |       |      |      |      |
| Traffic Vol, veh/h         | 297   | 4     | 3     | 504  | 1    | 0    |
| Future Vol, veh/h          | 297   | 4     | 3     | 504  | 1    | 0    |
| Peak Hour Factor           | 0.92  | 0.92  | 0.92  | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, %          | 5     | 0     | 0     | 4    | 0    | 0    |
| Mvmt Flow                  | 323   | 4     | 3     | 548  | 1    | 0    |
| Number of Lanes            | 1     | 0     | 1     | 0    | 0    | 1    |
| Approach                   | WB    | NB    |       | SB   |      |      |
| Opposing Approach          |       | SB    |       | NB   |      |      |
| Opposing Lanes             | 0     | 1     |       | 1    |      |      |
| Conflicting Approach Left  | NB    |       |       | WB   |      |      |
| Conflicting Lanes Left     | 1     | 0     |       | 1    |      |      |
| Conflicting Approach Right | SB    |       |       | WB   |      |      |
| Conflicting Lanes Right    | 1     | 1     |       | 0    |      |      |
| HCM Control Delay          | 13.7  | 14.7  |       | 8.8  |      |      |
| HCM LOS                    | B     | B     |       | A    |      |      |
| Lane                       | NBLn1 | WBLn1 | SBLn1 |      |      |      |
| Vol Left, %                | 0%    | 99%   | 100%  |      |      |      |
| Vol Thru, %                | 1%    | 0%    | 0%    |      |      |      |
| Vol Right, %               | 99%   | 1%    | 0%    |      |      |      |
| Sign Control               | Stop  | Stop  | Stop  |      |      |      |
| Traffic Vol by Lane        | 507   | 301   | 1     |      |      |      |
| LT Vol                     | 0     | 297   | 1     |      |      |      |
| Through Vol                | 3     | 0     | 0     |      |      |      |
| RT Vol                     | 504   | 4     | 0     |      |      |      |
| Lane Flow Rate             | 551   | 327   | 1     |      |      |      |
| Geometry Grp               | 1     | 1     | 1     |      |      |      |
| Degree of Util (X)         | 0.646 | 0.495 | 0.002 |      |      |      |
| Departure Headway (Hd)     | 4.221 | 5.442 | 5.754 |      |      |      |
| Convergence, Y/N           | Yes   | Yes   | Yes   |      |      |      |
| Cap                        | 849   | 667   | 626   |      |      |      |
| Service Time               | 2.276 | 3.442 | 3.754 |      |      |      |
| HCM Lane V/C Ratio         | 0.649 | 0.49  | 0.002 |      |      |      |
| HCM Control Delay          | 14.7  | 13.7  | 8.8   |      |      |      |
| HCM Lane LOS               | B     | B     | A     |      |      |      |
| HCM 95th-tile Q            | 4.8   | 2.8   | 0     |      |      |      |



| Lane Group              | EBT  | WBT  | NBT  | SBT  |
|-------------------------|------|------|------|------|
| Lane Group Flow (vph)   | 531  | 268  | 687  | 331  |
| v/c Ratio               | 0.79 | 0.43 | 1.02 | 0.48 |
| Control Delay           | 24.7 | 13.9 | 59.3 | 14.8 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay             | 24.7 | 13.9 | 59.3 | 14.8 |
| Queue Length 50th (ft)  | 142  | 58   | ~223 | 76   |
| Queue Length 95th (ft)  | #295 | 111  | #421 | 136  |
| Internal Link Dist (ft) | 410  | 2031 | 474  | 3954 |
| Turn Bay Length (ft)    |      |      |      |      |
| Base Capacity (vph)     | 674  | 617  | 676  | 695  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.79 | 0.43 | 1.02 | 0.48 |

## Intersection Summary

~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis  
3: Reed Street & High Street

Section E, Item1.



| Movement                          | EBL    | EBT  | EBR  | WBL                       | WBT  | WBR  | NBL   | NBT  | NBR  | SBL  | SBT  | SBR  |
|-----------------------------------|--------|------|------|---------------------------|------|------|-------|------|------|------|------|------|
| Lane Configurations               |        |      |      |                           |      |      |       |      |      |      |      |      |
| Traffic Volume (vph)              | 177    | 298  | 14   | 59                        | 179  | 8    | 60    | 431  | 142  | 5    | 211  | 89   |
| Future Volume (vph)               | 177    | 298  | 14   | 59                        | 179  | 8    | 60    | 431  | 142  | 5    | 211  | 89   |
| Ideal Flow (vphpl)                | 1900   | 1900 | 1900 | 1900                      | 1900 | 1900 | 1900  | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width                        | 12     | 15   | 12   | 12                        | 11   | 12   | 12    | 12   | 12   | 12   | 12   | 12   |
| Total Lost time (s)               |        | 4.5  |      |                           | 4.5  |      |       | 4.5  |      |      | 4.5  |      |
| Lane Util. Factor                 |        | 1.00 |      |                           | 1.00 |      |       | 1.00 |      |      | 1.00 |      |
| Frpb, ped/bikes                   |        | 1.00 |      |                           | 1.00 |      |       | 0.99 |      |      | 0.99 |      |
| Flpb, ped/bikes                   |        | 0.98 |      |                           | 1.00 |      |       | 1.00 |      |      | 1.00 |      |
| Frt                               |        | 1.00 |      |                           | 1.00 |      |       | 0.97 |      |      | 0.96 |      |
| Flt Protected                     |        | 0.98 |      |                           | 0.99 |      |       | 1.00 |      |      | 1.00 |      |
| Satd. Flow (prot)                 |        | 1991 |      |                           | 1715 |      |       | 1754 |      |      | 1715 |      |
| Flt Permitted                     |        | 0.78 |      |                           | 0.83 |      |       | 0.94 |      |      | 0.99 |      |
| Satd. Flow (perm)                 |        | 1579 |      |                           | 1445 |      |       | 1653 |      |      | 1700 |      |
| Peak-hour factor, PHF             | 0.92   | 0.92 | 0.92 | 0.92                      | 0.92 | 0.92 | 0.92  | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph)                   | 192    | 324  | 15   | 64                        | 195  | 9    | 65    | 468  | 154  | 5    | 229  | 97   |
| RTOR Reduction (vph)              | 0      | 0    | 0    | 0                         | 0    | 0    | 0     | 0    | 0    | 0    | 0    | 0    |
| Lane Group Flow (vph)             | 0      | 531  | 0    | 0                         | 268  | 0    | 0     | 687  | 0    | 0    | 331  | 0    |
| Confl. Peds. (#/hr)               | 46     |      | 17   | 17                        |      | 46   | 12    |      | 4    | 4    |      | 12   |
| Heavy Vehicles (%)                | 1%     | 1%   | 0%   | 11%                       | 3%   | 0%   | 0%    | 5%   | 2%   | 0%   | 7%   | 1%   |
| Turn Type                         | Perm   | NA   |      | Perm                      | NA   |      | Perm  | NA   |      | Perm | NA   |      |
| Protected Phases                  |        | 4    |      |                           | 8    |      |       | 2    |      |      | 6    |      |
| Permitted Phases                  | 4      |      |      | 8                         |      |      | 2     |      |      | 6    |      |      |
| Actuated Green, G (s)             | 23.5   |      |      | 23.5                      |      |      | 22.5  |      |      | 22.5 |      |      |
| Effective Green, g (s)            | 23.5   |      |      | 23.5                      |      |      | 22.5  |      |      | 22.5 |      |      |
| Actuated g/C Ratio                | 0.43   |      |      | 0.43                      |      |      | 0.41  |      |      | 0.41 |      |      |
| Clearance Time (s)                | 4.5    |      |      | 4.5                       |      |      | 4.5   |      |      | 4.5  |      |      |
| Lane Grp Cap (vph)                | 674    |      |      | 617                       |      |      | 676   |      |      | 695  |      |      |
| v/s Ratio Prot                    |        |      |      |                           |      |      |       |      |      |      |      |      |
| v/s Ratio Perm                    | c0.34  |      |      | 0.19                      |      |      | c0.42 |      |      | 0.19 |      |      |
| v/c Ratio                         | 0.79   |      |      | 0.43                      |      |      | 1.02  |      |      | 0.48 |      |      |
| Uniform Delay, d1                 | 13.6   |      |      | 11.1                      |      |      | 16.2  |      |      | 11.9 |      |      |
| Progression Factor                | 1.00   |      |      | 1.00                      |      |      | 1.00  |      |      | 1.00 |      |      |
| Incremental Delay, d2             | 9.1    |      |      | 2.2                       |      |      | 38.7  |      |      | 2.3  |      |      |
| Delay (s)                         | 22.7   |      |      | 13.3                      |      |      | 55.0  |      |      | 14.3 |      |      |
| Level of Service                  | C      |      |      | B                         |      |      | D     |      |      | B    |      |      |
| Approach Delay (s)                | 22.7   |      |      | 13.3                      |      |      | 55.0  |      |      | 14.3 |      |      |
| Approach LOS                      | C      |      |      | B                         |      |      | D     |      |      | B    |      |      |
| Intersection Summary              |        |      |      |                           |      |      |       |      |      |      |      |      |
| HCM 2000 Control Delay            | 32.0   |      |      | HCM 2000 Level of Service |      |      | C     |      |      |      |      |      |
| HCM 2000 Volume to Capacity ratio | 0.90   |      |      |                           |      |      |       |      |      |      |      |      |
| Actuated Cycle Length (s)         | 55.0   |      |      | Sum of lost time (s)      |      |      | 9.0   |      |      |      |      |      |
| Intersection Capacity Utilization | 105.1% |      |      | ICU Level of Service      |      |      | G     |      |      |      |      |      |
| Analysis Period (min)             | 15     |      |      |                           |      |      |       |      |      |      |      |      |
| c Critical Lane Group             |        |      |      |                           |      |      |       |      |      |      |      |      |

## Queues

9: N Main Street &amp; Scanlon Drive/Russ Street

Section E, Item1.



| Lane Group              | EBL  | EBT  | WBL  | WBT   | NBL  | NBT  | SBL   | SBT  | SBR  |
|-------------------------|------|------|------|-------|------|------|-------|------|------|
| Lane Group Flow (vph)   | 336  | 342  | 54   | 158   | 85   | 1121 | 324   | 777  | 447  |
| v/c Ratio               | 0.98 | 0.96 | 0.60 | 1.00  | 0.28 | 0.88 | 1.12  | 0.53 | 0.37 |
| Control Delay           | 88.8 | 82.8 | 78.7 | 101.7 | 13.8 | 39.8 | 122.1 | 21.2 | 1.3  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0   | 0.0  | 0.0  | 0.0   | 0.0  | 0.0  |
| Total Delay             | 88.8 | 82.8 | 78.7 | 101.7 | 13.8 | 39.8 | 122.1 | 21.2 | 1.3  |
| Queue Length 50th (ft)  | 247  | 249  | 37   | ~62   | 25   | 371  | ~218  | 198  | 0    |
| Queue Length 95th (ft)  | #473 | #475 | #103 | #210  | 47   | 461  | #414  | 256  | 24   |
| Internal Link Dist (ft) |      |      | 42   |       | 451  |      | 3510  |      | 583  |
| Turn Bay Length (ft)    | 50   |      | 60   |       | 200  |      | 180   |      |      |
| Base Capacity (vph)     | 342  | 355  | 90   | 158   | 308  | 1479 | 288   | 1571 | 1210 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0     | 0    | 0    | 0     | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0     | 0    | 0    | 0     | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0     | 0    | 0    | 0     | 0    | 0    |
| Reduced v/c Ratio       | 0.98 | 0.96 | 0.60 | 1.00  | 0.28 | 0.76 | 1.13  | 0.49 | 0.37 |

## Intersection Summary

~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

# 95th percentile volume exceeds capacity, queue may be longer.

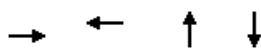
Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis  
9: N Main Street & Scanlon Drive/Russ Street

Section E, Item1.

| Movement                          | EBL   | EBT   | EBR  | WBL   | WBT   | WBR                       | NBL   | NBT  | NBR  | SBU    | SBL   | SBT   | SBR   |
|-----------------------------------|-------|-------|------|-------|-------|---------------------------|-------|------|------|--------|-------|-------|-------|
| Lane Configurations               | ↑     | ↔     |      | ↑     | ↔     |                           | ↑     | ↔    |      |        | ↑     | ↔     | ↑     |
| Traffic Volume (vph)              | 533   | 71    | 20   | 50    | 47    | 98                        | 78    | 985  | 46   | 2      | 296   | 715   | 411   |
| Future Volume (vph)               | 533   | 71    | 20   | 50    | 47    | 98                        | 78    | 985  | 46   | 2      | 296   | 715   | 411   |
| Ideal Flow (vphpl)                | 1900  | 1900  | 1900 | 1900  | 1900  | 1900                      | 1900  | 1900 | 1900 | 1900   | 1900  | 1900  | 1900  |
| Lane Width                        | 11    | 12    | 12   | 10    | 12    | 12                        | 10    | 11   | 11   | 12     | 10    | 10    | 11    |
| Total Lost time (s)               | 5.0   | 5.0   |      | 5.0   | 5.0   |                           | 7.0   | 5.0  |      |        | 7.0   | 5.0   | 5.0   |
| Lane Util. Factor                 | 0.95  | 0.95  |      | 1.00  | 1.00  |                           | 1.00  | 0.95 |      |        | 1.00  | 0.95  | 1.00  |
| Frpb, ped/bikes                   | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Frbp, ped/bikes                   | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Frt                               | 1.00  | 0.99  |      | 1.00  | 0.90  |                           | 1.00  | 0.99 |      |        | 1.00  | 1.00  | 0.85  |
| Flt Protected                     | 0.95  | 0.97  |      | 0.95  | 1.00  |                           | 0.95  | 1.00 |      |        | 0.95  | 1.00  | 1.00  |
| Satd. Flow (prot)                 | 1594  | 1646  |      | 1620  | 1662  |                           | 1572  | 3298 |      |        | 1636  | 3008  | 1473  |
| Flt Permitted                     | 0.95  | 0.97  |      | 0.95  | 1.00  |                           | 0.34  | 1.00 |      |        | 0.08  | 1.00  | 1.00  |
| Satd. Flow (perm)                 | 1594  | 1646  |      | 1620  | 1662  |                           | 563   | 3298 |      |        | 138   | 3008  | 1473  |
| Peak-hour factor, PHF             | 0.92  | 0.92  | 0.92 | 0.92  | 0.92  | 0.92                      | 0.92  | 0.92 | 0.92 | 0.92   | 0.92  | 0.92  | 0.92  |
| Adj. Flow (vph)                   | 579   | 77    | 22   | 54    | 51    | 107                       | 85    | 1071 | 50   | 2      | 322   | 777   | 447   |
| RTOR Reduction (vph)              | 0     | 2     | 0    | 0     | 66    | 0                         | 0     | 3    | 0    | 0      | 0     | 0     | 117   |
| Lane Group Flow (vph)             | 336   | 340   | 0    | 54    | 92    | 0                         | 85    | 1118 | 0    | 0      | 324   | 777   | 330   |
| Confl. Peds. (#/hr)               |       |       |      | 4     | 4     |                           |       | 5    |      |        |       |       | 5     |
| Heavy Vehicles (%)                | 4%    | 6%    | 9%   | 4%    | 0%    | 4%                        | 7%    | 5%   | 7%   | 2%     | 3%    | 12%   | 6%    |
| Turn Type                         | Split | NA    |      | Split | NA    |                           | pm+pt | NA   |      | custom | pm+pt | NA    | pt+ov |
| Protected Phases                  | 3     | 3     |      | 4     | 4     |                           | 5     | 2    |      |        | 1     | 6     | 6.3   |
| Permitted Phases                  |       |       |      |       |       |                           | 2     |      |      |        | 1     | 6     |       |
| Actuated Green, G (s)             | 23.1  | 23.1  |      | 6.0   | 6.0   |                           | 48.4  | 42.9 |      |        | 65.0  | 52.5  | 80.6  |
| Effective Green, g (s)            | 23.1  | 23.1  |      | 6.0   | 6.0   |                           | 48.4  | 42.9 |      |        | 65.0  | 52.5  | 80.6  |
| Actuated g/C Ratio                | 0.21  | 0.21  |      | 0.05  | 0.05  |                           | 0.44  | 0.39 |      |        | 0.60  | 0.48  | 0.74  |
| Clearance Time (s)                | 5.0   | 5.0   |      | 5.0   | 5.0   |                           | 7.0   | 5.0  |      |        | 7.0   | 5.0   |       |
| Vehicle Extension (s)             | 3.0   | 3.0   |      | 3.0   | 3.0   |                           | 3.0   | 2.0  |      |        | 3.0   | 2.0   |       |
| Lane Grp Cap (vph)                | 337   | 348   |      | 89    | 91    |                           | 300   | 1296 |      |        | 289   | 1447  | 1088  |
| v/s Ratio Prot                    | c0.21 | 0.21  |      | 0.03  | c0.06 |                           | 0.01  | 0.34 |      |        | c0.15 | 0.26  | 0.22  |
| v/s Ratio Perm                    |       |       |      |       |       |                           | 0.11  |      |      |        |       | c0.51 |       |
| v/c Ratio                         | 1.00  | 0.98  |      | 0.61  | 1.01  |                           | 0.28  | 0.86 |      |        | 1.12  | 0.54  | 0.30  |
| Uniform Delay, d1                 | 43.0  | 42.7  |      | 50.4  | 51.5  |                           | 17.9  | 30.4 |      |        | 34.0  | 19.8  | 4.8   |
| Progression Factor                | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Incremental Delay, d2             | 47.9  | 41.4  |      | 11.2  | 96.9  |                           | 0.5   | 6.0  |      |        | 89.6  | 0.2   | 0.1   |
| Delay (s)                         | 90.9  | 84.1  |      | 61.6  | 148.5 |                           | 18.4  | 36.3 |      |        | 123.6 | 20.0  | 4.9   |
| Level of Service                  | F     | F     |      | E     | F     |                           | B     | D    |      |        | F     | B     | A     |
| Approach Delay (s)                |       | 87.5  |      |       | 126.3 |                           |       | 35.1 |      |        |       | 37.3  |       |
| Approach LOS                      |       | F     |      |       | F     |                           |       | D    |      |        |       | D     |       |
| Intersection Summary              |       |       |      |       |       |                           |       |      |      |        |       |       |       |
| HCM 2000 Control Delay            |       | 51.1  |      |       |       | HCM 2000 Level of Service |       |      | D    |        |       |       |       |
| HCM 2000 Volume to Capacity ratio |       | 1.12  |      |       |       |                           |       |      |      |        |       |       |       |
| Actuated Cycle Length (s)         |       | 109.1 |      |       |       | Sum of lost time (s)      |       |      | 22.0 |        |       |       |       |
| Intersection Capacity Utilization |       | 89.3% |      |       |       | ICU Level of Service      |       |      | E    |        |       |       |       |
| Analysis Period (min)             |       | 15    |      |       |       |                           |       |      |      |        |       |       |       |
| c Critical Lane Group             |       |       |      |       |       |                           |       |      |      |        |       |       |       |

| Intersection               |   |       |       |      |      |      |
|----------------------------|---|-------|-------|------|------|------|
| Intersection Delay, s/veh  | 18.8  |       |       |      |      |      |
| Intersection LOS           | C   |       |       |      |      |      |
| Movement                   | WBL   | WBR   | NBT   | NBR  | SBL  | SBT  |
| Lane Configurations        |  |       |       |      |      |      |
| Traffic Vol, veh/h         | 524   | 0     | 2     | 297  | 1    | 2    |
| Future Vol, veh/h          | 524   | 0     | 2     | 297  | 1    | 2    |
| Peak Hour Factor           | 0.92  | 0.92  | 0.92  | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, %          | 2   | 0     | 0     | 2    | 0    | 0    |
| Mvmt Flow                  | 570   | 0     | 2     | 323  | 1    | 2    |
| Number of Lanes            | 1   | 0     | 1     | 0    | 0    | 1    |
| Approach                   | WB  | NB    |       | SB   |      |      |
| Opposing Approach          |   | SB    |       | NB   |      |      |
| Opposing Lanes             | 0   | 1     |       | 1    |      |      |
| Conflicting Approach Left  | NB  |       |       | WB   |      |      |
| Conflicting Lanes Left     | 1   | 0     |       | 1    |      |      |
| Conflicting Approach Right | SB  | WB    |       |      |      |      |
| Conflicting Lanes Right    | 1   | 1     |       | 0    |      |      |
| HCM Control Delay          | 23  | 11.4  |       | 9    |      |      |
| HCM LOS                    | C   | B     |       | A    |      |      |
| Lane                       | NBLn1   | WBLn1 | SBLn1 |      |      |      |
| Vol Left, %                | 0%  | 100%  | 33%   |      |      |      |
| Vol Thru, %                | 1%  | 0%    | 67%   |      |      |      |
| Vol Right, %               | 99%   | 0%    | 0%    |      |      |      |
| Sign Control               | Stop  | Stop  | Stop  |      |      |      |
| Traffic Vol by Lane        | 299   | 524   | 3     |      |      |      |
| LT Vol                     | 0   | 524   | 1     |      |      |      |
| Through Vol                | 2   | 0     | 2     |      |      |      |
| RT Vol                     | 297   | 0     | 0     |      |      |      |
| Lane Flow Rate             | 325   | 570   | 3     |      |      |      |
| Geometry Grp               | 1   | 1     | 1     |      |      |      |
| Degree of Util (X)         | 0.431   | 0.776 | 0.005 |      |      |      |
| Departure Headway (Hd)     | 4.769   | 4.902 | 6     |      |      |      |
| Convergence, Y/N           | Yes   | Yes   | Yes   |      |      |      |
| Cap                        | 751   | 729   | 600   |      |      |      |
| Service Time               | 2.831   | 2.986 | 4     |      |      |      |
| HCM Lane V/C Ratio         | 0.433   | 0.782 | 0.005 |      |      |      |
| HCM Control Delay          | 11.4  | 23    | 9     |      |      |      |
| HCM Lane LOS               | B   | C     | A     |      |      |      |
| HCM 95th-tile Q            | 2.2   | 7.6   | 0     |      |      |      |



| Lane Group              | EBT  | WBT  | NBT  | SBT  |
|-------------------------|------|------|------|------|
| Lane Group Flow (vph)   | 324  | 372  | 382  | 570  |
| v/c Ratio               | 0.48 | 0.65 | 0.53 | 0.81 |
| Control Delay           | 12.9 | 18.0 | 13.7 | 24.5 |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay             | 12.9 | 18.0 | 13.7 | 24.5 |
| Queue Length 50th (ft)  | 58   | 74   | 71   | 123  |
| Queue Length 95th (ft)  | 112  | #156 | 133  | #272 |
| Internal Link Dist (ft) | 410  | 2031 | 474  | 3954 |
| Turn Bay Length (ft)    |      |      |      |      |
| Base Capacity (vph)     | 680  | 570  | 716  | 702  |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.48 | 0.65 | 0.53 | 0.81 |

## Intersection Summary

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis  
3: Reed Street & High Street

Section E, Item1.



| Movement                          | EBL   | EBT  | EBR  | WBL                       | WBT  | WBR  | NBL  | NBT  | NBR  | SBL   | SBT  | SBR  |
|-----------------------------------|-------|------|------|---------------------------|------|------|------|------|------|-------|------|------|
| Lane Configurations               |       |      |      |                           |      |      |      |      |      |       |      |      |
| Traffic Volume (vph)              | 87    | 200  | 11   | 117                       | 221  | 5    | 5    | 258  | 89   | 7     | 371  | 146  |
| Future Volume (vph)               | 87    | 200  | 11   | 117                       | 221  | 5    | 5    | 258  | 89   | 7     | 371  | 146  |
| Ideal Flow (vphpl)                | 1900  | 1900 | 1900 | 1900                      | 1900 | 1900 | 1900 | 1900 | 1900 | 1900  | 1900 | 1900 |
| Lane Width                        | 12    | 15   | 12   | 12                        | 11   | 12   | 12   | 12   | 12   | 12    | 12   | 12   |
| Total Lost time (s)               |       | 4.5  |      |                           | 4.5  |      |      | 4.5  |      |       | 4.5  |      |
| Lane Util. Factor                 |       | 1.00 |      |                           | 1.00 |      |      | 1.00 |      |       | 1.00 |      |
| Frpb, ped/bikes                   |       | 1.00 |      |                           | 1.00 |      |      | 1.00 |      |       | 0.99 |      |
| Fpb, ped/bikes                    |       | 1.00 |      |                           | 1.00 |      |      | 1.00 |      |       | 1.00 |      |
| Frt                               |       | 0.99 |      |                           | 1.00 |      |      | 0.97 |      |       | 0.96 |      |
| Flt Protected                     |       | 0.99 |      |                           | 0.98 |      |      | 1.00 |      |       | 1.00 |      |
| Satd. Flow (prot)                 |       | 2033 |      |                           | 1754 |      |      | 1803 |      |       | 1767 |      |
| Flt Permitted                     |       | 0.83 |      |                           | 0.80 |      |      | 0.99 |      |       | 0.99 |      |
| Satd. Flow (perm)                 |       | 1702 |      |                           | 1425 |      |      | 1791 |      |       | 1757 |      |
| Peak-hour factor, PHF             | 0.92  | 0.92 | 0.92 | 0.92                      | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92  | 0.92 | 0.92 |
| Adj. Flow (vph)                   | 95    | 217  | 12   | 127                       | 240  | 5    | 5    | 280  | 97   | 8     | 403  | 159  |
| RTOR Reduction (vph)              | 0     | 0    | 0    | 0                         | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    |
| Lane Group Flow (vph)             | 0     | 324  | 0    | 0                         | 372  | 0    | 0    | 382  | 0    | 0     | 570  | 0    |
| Confl. Peds. (#/hr)               | 3     |      | 6    | 6                         |      | 3    | 4    |      |      |       | 4    |      |
| Heavy Vehicles (%)                | 0%    | 1%   | 0%   | 0%                        | 4%   | 0%   | 0%   | 2%   | 1%   | 0%    | 3%   | 2%   |
| Turn Type                         | Perm  | NA   |      | Perm                      | NA   |      | Perm | NA   |      | Perm  | NA   |      |
| Protected Phases                  |       | 4    |      |                           | 8    |      |      | 2    |      |       | 6    |      |
| Permitted Phases                  | 4     |      |      | 8                         |      |      | 2    |      |      | 6     |      |      |
| Actuated Green, G (s)             | 18.0  |      |      | 18.0                      |      |      | 18.0 |      |      | 18.0  |      |      |
| Effective Green, g (s)            | 18.0  |      |      | 18.0                      |      |      | 18.0 |      |      | 18.0  |      |      |
| Actuated g/C Ratio                | 0.40  |      |      | 0.40                      |      |      | 0.40 |      |      | 0.40  |      |      |
| Clearance Time (s)                | 4.5   |      |      | 4.5                       |      |      | 4.5  |      |      | 4.5   |      |      |
| Lane Grp Cap (vph)                | 680   |      |      | 570                       |      |      | 716  |      |      | 702   |      |      |
| v/s Ratio Prot                    |       |      |      |                           |      |      |      |      |      |       |      |      |
| v/s Ratio Perm                    | 0.19  |      |      | c0.26                     |      |      | 0.21 |      |      | c0.32 |      |      |
| v/c Ratio                         | 0.48  |      |      | 0.65                      |      |      | 0.53 |      |      | 0.81  |      |      |
| Uniform Delay, d1                 | 10.0  |      |      | 11.0                      |      |      | 10.3 |      |      | 12.0  |      |      |
| Progression Factor                | 1.00  |      |      | 1.00                      |      |      | 1.00 |      |      | 1.00  |      |      |
| Incremental Delay, d2             | 2.4   |      |      | 5.7                       |      |      | 2.8  |      |      | 9.9   |      |      |
| Delay (s)                         | 12.4  |      |      | 16.7                      |      |      | 13.1 |      |      | 21.9  |      |      |
| Level of Service                  | B     |      |      | B                         |      |      | B    |      |      | C     |      |      |
| Approach Delay (s)                | 12.4  |      |      | 16.7                      |      |      | 13.1 |      |      | 21.9  |      |      |
| Approach LOS                      | B     |      |      | B                         |      |      | B    |      |      | C     |      |      |
| Intersection Summary              |       |      |      |                           |      |      |      |      |      |       |      |      |
| HCM 2000 Control Delay            | 16.8  |      |      | HCM 2000 Level of Service |      |      | B    |      |      |       |      |      |
| HCM 2000 Volume to Capacity ratio | 0.73  |      |      |                           |      |      |      |      |      |       |      |      |
| Actuated Cycle Length (s)         | 45.0  |      |      | Sum of lost time (s)      |      |      | 9.0  |      |      |       |      |      |
| Intersection Capacity Utilization | 66.0% |      |      | ICU Level of Service      |      |      | C    |      |      |       |      |      |
| Analysis Period (min)             | 15    |      |      |                           |      |      |      |      |      |       |      |      |
| c Critical Lane Group             |       |      |      |                           |      |      |      |      |      |       |      |      |

## Queues

9: N Main Street &amp; Scanlon Drive/Russ Street

Section E, Item1.



| Lane Group              | EBL  | EBT  | WBL  | WBT  | NBL  | NBT  | SBL  | SBT  | SBR  |
|-------------------------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph)   | 314  | 303  | 53   | 343  | 42   | 680  | 162  | 1290 | 540  |
| v/c Ratio               | 0.86 | 0.78 | 0.22 | 0.89 | 0.25 | 0.73 | 0.53 | 1.02 | 0.45 |
| Control Delay           | 59.9 | 50.1 | 41.0 | 47.0 | 20.6 | 37.0 | 23.3 | 61.2 | 2.0  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay             | 59.9 | 50.1 | 41.0 | 47.0 | 20.6 | 37.0 | 23.3 | 61.2 | 2.0  |
| Queue Length 50th (ft)  | 211  | 192  | 31   | 111  | 15   | 201  | 61   | ~512 | 0    |
| Queue Length 95th (ft)  | #374 | #337 | 68   | #277 | 34   | 281  | 103  | #646 | 37   |
| Internal Link Dist (ft) |      |      | 42   |      | 451  |      | 3510 |      | 583  |
| Turn Bay Length (ft)    | 50   |      | 60   |      | 200  |      | 180  |      |      |
| Base Capacity (vph)     | 386  | 407  | 261  | 404  | 167  | 1032 | 362  | 1268 | 1209 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.81 | 0.74 | 0.20 | 0.85 | 0.25 | 0.66 | 0.45 | 1.02 | 0.45 |

## Intersection Summary

~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis  
9: N Main Street & Scanlon Drive/Russ Street

Section E, Item1.

| Movement                          | EBL   | EBT   | EBR  | WBL                       | WBT   | WBR  | NBU    | NBL   | NBT  | NBR  | SBU    | SBL   | SBT   | SBR   |
|-----------------------------------|-------|-------|------|---------------------------|-------|------|--------|-------|------|------|--------|-------|-------|-------|
| Lane Configurations               | ↑     | ↔     |      | ↑                         | ↔     |      |        | ↑     | ↔    |      |        | ↑     | ↔     |       |
| Traffic Volume (vph)              | 473   | 35    | 60   | 49                        | 44    | 271  | 1      | 38    | 590  | 36   | 1      | 148   | 1187  | 497   |
| Future Volume (vph)               | 473   | 35    | 60   | 49                        | 44    | 271  | 1      | 38    | 590  | 36   | 1      | 148   | 1187  | 497   |
| Ideal Flow (vphpl)                | 1900  | 1900  | 1900 | 1900                      | 1900  | 1900 | 1900   | 1900  | 1900 | 1900 | 1900   | 1900  | 1900  | 1900  |
| Lane Width                        | 11    | 12    | 12   | 10                        | 12    | 12   | 12     | 10    | 11   | 11   | 12     | 10    | 10    | 11    |
| Total Lost time (s)               | 5.0   | 5.0   |      | 5.0                       | 5.0   |      |        | 7.0   | 5.0  |      |        | 7.0   | 5.0   | 5.0   |
| Lane Util. Factor                 | 0.95  | 0.95  |      | 1.00                      | 1.00  |      |        | 1.00  | 0.95 |      |        | 1.00  | 0.95  | 1.00  |
| Frpb, ped/bikes                   | 1.00  | 1.00  |      | 1.00                      | 0.99  |      |        | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Flpb, ped/bikes                   | 1.00  | 1.00  |      | 1.00                      | 1.00  |      |        | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Frt                               | 1.00  | 0.97  |      | 1.00                      | 0.87  |      |        | 1.00  | 0.99 |      |        | 1.00  | 1.00  | 0.85  |
| Flt Protected                     | 0.95  | 0.97  |      | 0.95                      | 1.00  |      |        | 0.95  | 1.00 |      |        | 0.95  | 1.00  | 1.00  |
| Satd. Flow (prot)                 | 1594  | 1642  |      | 1652                      | 1622  |      |        | 1685  | 3357 |      |        | 1685  | 3240  | 1516  |
| Flt Permitted                     | 0.95  | 0.97  |      | 0.95                      | 1.00  |      |        | 0.13  | 1.00 |      |        | 0.19  | 1.00  | 1.00  |
| Satd. Flow (perm)                 | 1594  | 1642  |      | 1652                      | 1622  |      |        | 238   | 3357 |      |        | 335   | 3240  | 1516  |
| Peak-hour factor, PHF             | 0.92  | 0.92  | 0.92 | 0.92                      | 0.92  | 0.92 | 0.92   | 0.92  | 0.92 | 0.92 | 0.92   | 0.92  | 0.92  | 0.92  |
| Adj. Flow (vph)                   | 514   | 38    | 65   | 53                        | 48    | 295  | 1      | 41    | 641  | 39   | 1      | 161   | 1290  | 540   |
| RTOR Reduction (vph)              | 0     | 9     | 0    | 0                         | 151   | 0    | 0      | 0     | 4    | 0    | 0      | 0     | 0     | 187   |
| Lane Group Flow (vph)             | 314   | 294   | 0    | 53                        | 192   | 0    | 0      | 42    | 676  | 0    | 0      | 162   | 1290  | 353   |
| Confl. Peds. (#/hr)               |       |       |      | 2                         | 2     |      |        | 3     |      | 6    |        | 6     |       | 3     |
| Confl. Bikes (#/hr)               |       |       |      |                           |       |      | 1      |       |      |      |        |       |       |       |
| Heavy Vehicles (%)                | 4%    | 0%    | 0%   | 2%                        | 0%    | 1%   | 0%     | 0%    | 3%   | 0%   | 0%     | 0%    | 4%    | 3%    |
| Turn Type                         | Split | NA    |      | Split                     | NA    |      | custom | pm+pt | NA   |      | custom | pm+pt | NA    | pt+ov |
| Protected Phases                  | 3     | 3     |      | 4                         | 4     |      |        | 5     | 2    |      |        | 1     | 6     | 6.3   |
| Permitted Phases                  |       |       |      |                           |       | 5    | 2      |       |      | 1    | 6      |       |       |       |
| Actuated Green, G (s)             | 22.1  | 22.1  |      | 13.8                      | 13.8  |      |        | 33.2  | 29.8 |      |        | 47.9  | 37.5  | 64.6  |
| Effective Green, g (s)            | 22.1  | 22.1  |      | 13.8                      | 13.8  |      |        | 33.2  | 29.8 |      |        | 47.9  | 37.5  | 64.6  |
| Actuated g/C Ratio                | 0.22  | 0.22  |      | 0.14                      | 0.14  |      |        | 0.34  | 0.30 |      |        | 0.48  | 0.38  | 0.65  |
| Clearance Time (s)                | 5.0   | 5.0   |      | 5.0                       | 5.0   |      |        | 7.0   | 5.0  |      |        | 7.0   | 5.0   |       |
| Vehicle Extension (s)             | 3.0   | 3.0   |      | 3.0                       | 3.0   |      |        | 3.0   | 2.0  |      |        | 3.0   | 2.0   |       |
| Lane Grp Cap (vph)                | 356   | 367   |      | 230                       | 226   |      |        | 129   | 1012 |      |        | 314   | 1229  | 991   |
| v/s Ratio Prot                    | c0.20 | 0.18  |      | 0.03                      | c0.12 |      |        | 0.01  | 0.20 |      |        | c0.06 | c0.40 | 0.23  |
| v/s Ratio Perm                    |       |       |      |                           |       |      | 0.10   |       |      |      |        | 0.19  |       |       |
| v/c Ratio                         | 0.88  | 0.80  |      | 0.23                      | 0.85  |      |        | 0.33  | 0.67 |      |        | 0.52  | 1.05  | 0.36  |
| Uniform Delay, d1                 | 37.1  | 36.3  |      | 37.8                      | 41.5  |      |        | 25.5  | 30.2 |      |        | 16.9  | 30.6  | 7.7   |
| Progression Factor                | 1.00  | 1.00  |      | 1.00                      | 1.00  |      |        | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Incremental Delay, d2             | 21.7  | 11.8  |      | 0.5                       | 24.3  |      |        | 1.5   | 1.3  |      |        | 1.4   | 39.7  | 0.1   |
| Delay (s)                         | 58.8  | 48.1  |      | 38.3                      | 65.8  |      |        | 26.9  | 31.5 |      |        | 18.3  | 70.4  | 7.8   |
| Level of Service                  | E     | D     |      | D                         | E     |      |        | C     | C    |      |        | B     | E     | A     |
| Approach Delay (s)                |       | 53.5  |      |                           | 62.1  |      |        |       | 31.2 |      |        |       | 49.2  |       |
| Approach LOS                      |       | D     |      |                           | E     |      |        |       | C    |      |        |       | D     |       |
| <b>Intersection Summary</b>       |       |       |      |                           |       |      |        |       |      |      |        |       |       |       |
| HCM 2000 Control Delay            |       | 47.8  |      | HCM 2000 Level of Service |       |      |        |       | D    |      |        |       |       |       |
| HCM 2000 Volume to Capacity ratio |       | 0.97  |      |                           |       |      |        |       |      |      |        |       |       |       |
| Actuated Cycle Length (s)         |       | 98.8  |      | Sum of lost time (s)      |       |      |        |       | 22.0 |      |        |       |       |       |
| Intersection Capacity Utilization |       | 90.3% |      | ICU Level of Service      |       |      |        |       | E    |      |        |       |       |       |
| Analysis Period (min)             |       | 15    |      |                           |       |      |        |       |      |      |        |       |       |       |

c Critical Lane Group



## Queues

9: N Main Street &amp; Scanlon Drive/Russ Street

Section E, Item1.



| Lane Group              | EBL  | EBT  | WBL  | WBT  | NBL  | NBT  | SBL   | SBT  | SBR  |
|-------------------------|------|------|------|------|------|------|-------|------|------|
| Lane Group Flow (vph)   | 336  | 342  | 54   | 158  | 85   | 1121 | 324   | 777  | 447  |
| v/c Ratio               | 0.93 | 0.91 | 0.53 | 0.92 | 0.29 | 0.90 | 1.16  | 0.54 | 0.37 |
| Control Delay           | 76.7 | 72.0 | 70.7 | 81.2 | 15.2 | 43.7 | 134.7 | 23.0 | 1.3  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0   | 0.0  | 0.0  |
| Total Delay             | 76.7 | 72.0 | 70.7 | 81.2 | 15.2 | 43.7 | 134.7 | 23.0 | 1.3  |
| Queue Length 50th (ft)  | 257  | 260  | 39   | 64   | 27   | 389  | ~238  | 210  | 0    |
| Queue Length 95th (ft)  | #450 | #451 | #92  | #198 | 51   | 484  | #420  | 271  | 25   |
| Internal Link Dist (ft) |      |      | 42   |      | 451  |      | 3510  |      | 583  |
| Turn Bay Length (ft)    | 50   |      | 60   |      | 200  |      | 180   |      |      |
| Base Capacity (vph)     | 360  | 375  | 102  | 171  | 295  | 1346 | 280   | 1455 | 1204 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    |
| Reduced v/c Ratio       | 0.93 | 0.91 | 0.53 | 0.92 | 0.29 | 0.83 | 1.16  | 0.53 | 0.37 |

## Intersection Summary

~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

# 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis  
9: N Main Street & Scanlon Drive/Russ Street

Section E, Item1.

| Movement                          | EBL   | EBT   | EBR  | WBL   | WBT   | WBR                       | NBL   | NBT  | NBR  | SBU    | SBL   | SBT   | SBR   |
|-----------------------------------|-------|-------|------|-------|-------|---------------------------|-------|------|------|--------|-------|-------|-------|
| Lane Configurations               | ↑     | ↔     |      | ↑     | ↔     |                           | ↑     | ↔    |      |        | ↑     | ↔     | ↑     |
| Traffic Volume (vph)              | 533   | 71    | 20   | 50    | 47    | 98                        | 78    | 985  | 46   | 2      | 296   | 715   | 411   |
| Future Volume (vph)               | 533   | 71    | 20   | 50    | 47    | 98                        | 78    | 985  | 46   | 2      | 296   | 715   | 411   |
| Ideal Flow (vphpl)                | 1900  | 1900  | 1900 | 1900  | 1900  | 1900                      | 1900  | 1900 | 1900 | 1900   | 1900  | 1900  | 1900  |
| Lane Width                        | 11    | 12    | 12   | 10    | 12    | 12                        | 10    | 11   | 11   | 12     | 10    | 10    | 11    |
| Total Lost time (s)               | 5.0   | 5.0   |      | 5.0   | 5.0   |                           | 7.0   | 5.0  |      |        | 7.0   | 5.0   | 5.0   |
| Lane Util. Factor                 | 0.95  | 0.95  |      | 1.00  | 1.00  |                           | 1.00  | 0.95 |      |        | 1.00  | 0.95  | 1.00  |
| Frpb, ped/bikes                   | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Frbp, ped/bikes                   | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Frt                               | 1.00  | 0.99  |      | 1.00  | 0.90  |                           | 1.00  | 0.99 |      |        | 1.00  | 1.00  | 0.85  |
| Flt Protected                     | 0.95  | 0.97  |      | 0.95  | 1.00  |                           | 0.95  | 1.00 |      |        | 0.95  | 1.00  | 1.00  |
| Satd. Flow (prot)                 | 1594  | 1646  |      | 1620  | 1662  |                           | 1572  | 3298 |      |        | 1636  | 3008  | 1473  |
| Flt Permitted                     | 0.95  | 0.97  |      | 0.95  | 1.00  |                           | 0.33  | 1.00 |      |        | 0.08  | 1.00  | 1.00  |
| Satd. Flow (perm)                 | 1594  | 1646  |      | 1620  | 1662  |                           | 550   | 3298 |      |        | 138   | 3008  | 1473  |
| Peak-hour factor, PHF             | 0.92  | 0.92  | 0.92 | 0.92  | 0.92  | 0.92                      | 0.92  | 0.92 | 0.92 | 0.92   | 0.92  | 0.92  | 0.92  |
| Adj. Flow (vph)                   | 579   | 77    | 22   | 54    | 51    | 107                       | 85    | 1071 | 50   | 2      | 322   | 777   | 447   |
| RTOR Reduction (vph)              | 0     | 2     | 0    | 0     | 67    | 0                         | 0     | 3    | 0    | 0      | 0     | 0     | 118   |
| Lane Group Flow (vph)             | 336   | 340   | 0    | 54    | 91    | 0                         | 85    | 1118 | 0    | 0      | 324   | 777   | 329   |
| Confl. Peds. (#/hr)               |       |       |      | 4     | 4     |                           |       | 5    |      |        |       |       | 5     |
| Heavy Vehicles (%)                | 4%    | 6%    | 9%   | 4%    | 0%    | 4%                        | 7%    | 5%   | 7%   | 2%     | 3%    | 12%   | 6%    |
| Turn Type                         | Split | NA    |      | Split | NA    |                           | pm+pt | NA   |      | custom | pm+pt | NA    | pt+ov |
| Protected Phases                  | 3     | 3     |      | 4     | 4     |                           | 5     | 2    |      |        | 1     | 6     | 6.3   |
| Permitted Phases                  |       |       |      |       |       |                           | 2     |      |      |        | 1     | 6     |       |
| Actuated Green, G (s)             | 25.0  | 25.0  |      | 7.0   | 7.0   |                           | 48.5  | 43.0 |      |        | 65.0  | 52.5  | 82.5  |
| Effective Green, g (s)            | 25.0  | 25.0  |      | 7.0   | 7.0   |                           | 48.5  | 43.0 |      |        | 65.0  | 52.5  | 82.5  |
| Actuated g/C Ratio                | 0.22  | 0.22  |      | 0.06  | 0.06  |                           | 0.43  | 0.38 |      |        | 0.58  | 0.47  | 0.74  |
| Clearance Time (s)                | 5.0   | 5.0   |      | 5.0   | 5.0   |                           | 7.0   | 5.0  |      |        | 7.0   | 5.0   |       |
| Vehicle Extension (s)             | 3.0   | 3.0   |      | 3.0   | 3.0   |                           | 3.0   | 2.0  |      |        | 3.0   | 2.0   |       |
| Lane Grp Cap (vph)                | 355   | 367   |      | 101   | 103   |                           | 288   | 1266 |      |        | 280   | 1410  | 1085  |
| v/s Ratio Prot                    | c0.21 | 0.21  |      | 0.03  | c0.06 |                           | 0.01  | 0.34 |      |        | c0.15 | 0.26  | 0.22  |
| v/s Ratio Perm                    |       |       |      |       |       |                           | 0.11  |      |      |        |       | c0.52 |       |
| v/c Ratio                         | 0.95  | 0.93  |      | 0.53  | 0.89  |                           | 0.30  | 0.88 |      |        | 1.16  | 0.55  | 0.30  |
| Uniform Delay, d1                 | 42.8  | 42.6  |      | 50.9  | 52.1  |                           | 19.1  | 32.2 |      |        | 34.9  | 21.3  | 5.0   |
| Progression Factor                | 1.00  | 1.00  |      | 1.00  | 1.00  |                           | 1.00  | 1.00 |      |        | 1.00  | 1.00  | 1.00  |
| Incremental Delay, d2             | 33.8  | 28.7  |      | 5.4   | 54.0  |                           | 0.6   | 7.4  |      |        | 103.2 | 0.3   | 0.1   |
| Delay (s)                         | 76.6  | 71.2  |      | 56.3  | 106.1 |                           | 19.7  | 39.5 |      |        | 138.1 | 21.6  | 5.1   |
| Level of Service                  | E     | E     |      | E     | F     |                           | B     | D    |      |        | F     | C     | A     |
| Approach Delay (s)                |       | 73.9  |      |       | 93.4  |                           |       | 38.1 |      |        |       | 41.2  |       |
| Approach LOS                      |       | E     |      |       | F     |                           |       | D    |      |        |       | D     |       |
| Intersection Summary              |       |       |      |       |       |                           |       |      |      |        |       |       |       |
| HCM 2000 Control Delay            |       | 49.3  |      |       |       | HCM 2000 Level of Service |       |      | D    |        |       |       |       |
| HCM 2000 Volume to Capacity ratio |       | 1.11  |      |       |       |                           |       |      |      |        |       |       |       |
| Actuated Cycle Length (s)         |       | 112.0 |      |       |       | Sum of lost time (s)      |       |      | 22.0 |        |       |       |       |
| Intersection Capacity Utilization |       | 89.3% |      |       |       | ICU Level of Service      |       |      | E    |        |       |       |       |
| Analysis Period (min)             |       | 15    |      |       |       |                           |       |      |      |        |       |       |       |
| c Critical Lane Group             |       |       |      |       |       |                           |       |      |      |        |       |       |       |



**HOWARD STEIN HUDSON**

11 Beacon Street, Suite 1010  
Boston, Massachusetts 02108  
617.482.7080

[www.hshassoc.com](http://www.hshassoc.com)

Consultant


  
CORE  
INVESTMENTS, INC.

Key Plan

Notes



PLANNING BOARD SUBMISSION 2023.12.26

Issued/Revision YYYY.MM.DD

Permit/Seal

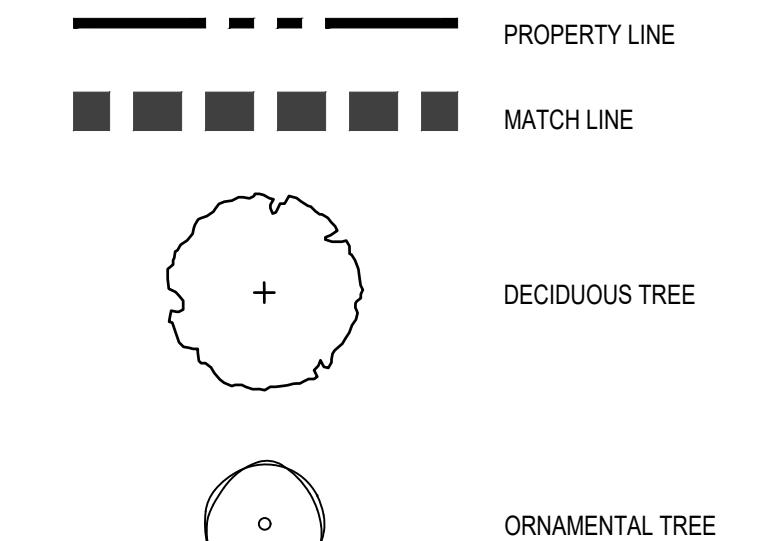
**PRELIMINARY  
NOT FOR  
CONSTRUCTION**

 Scale 1"=20'  
 Project No. 218421418

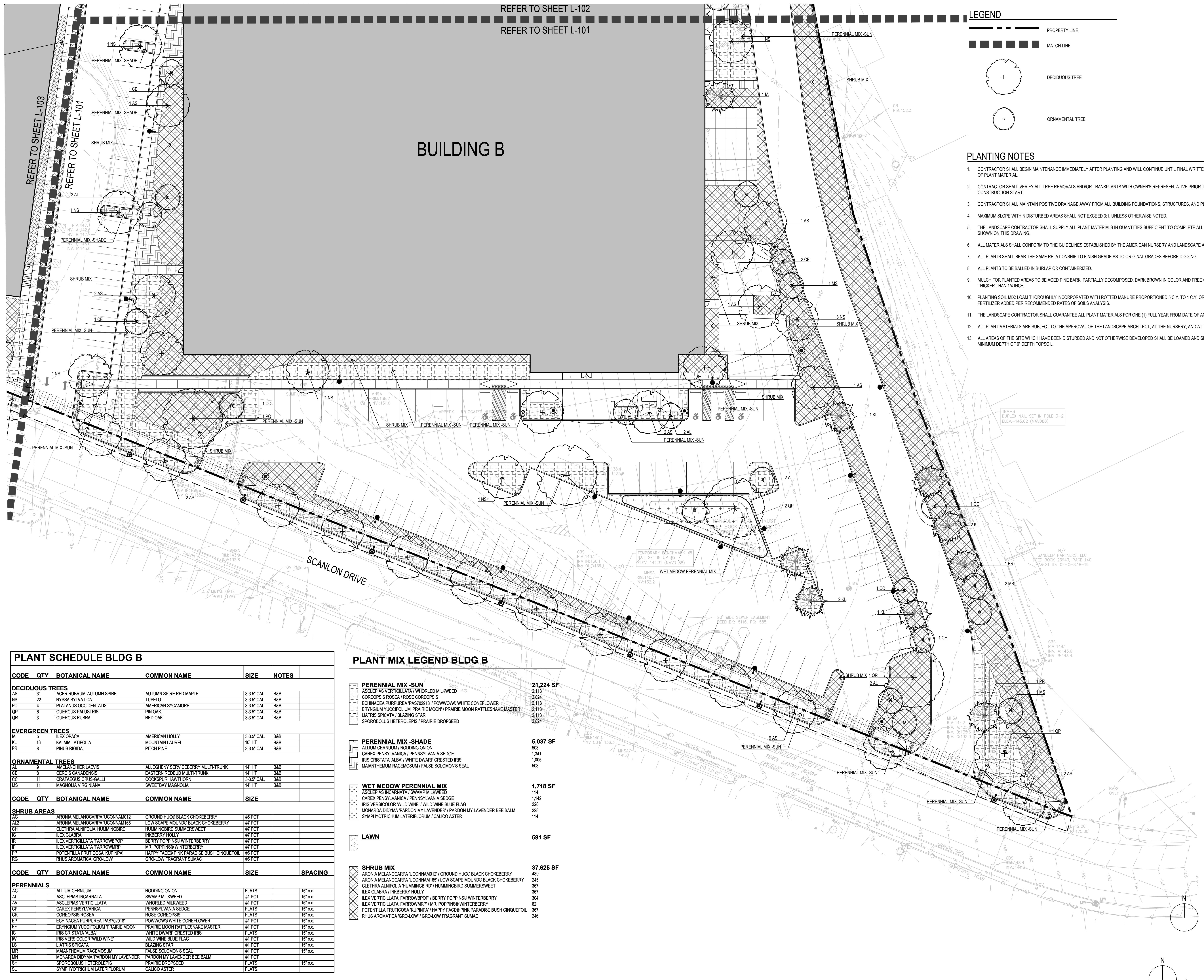
PLANTING PLAN 1

REFER TO SHEET L-102

REFER TO SHEET L-101

**LEGEND****PLANTING NOTES**

- CONTRACTOR SHALL BEGIN MAINTENANCE IMMEDIATELY AFTER PLANTING AND WILL CONTINUE UNTIL FINAL WRITTEN ACCEPTANCE OF PLANT MATERIAL.
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NOTE  
PLANTING SCOPE OUTSIDE OF THE BUILDING A PROPERTY LINE TO BE PRICED WITH BUILDING B; PLANTING COUNTS ARE INCLUDED  
IN THE BUILDING B SCHEDULE; REFER TO SHEET L-121.

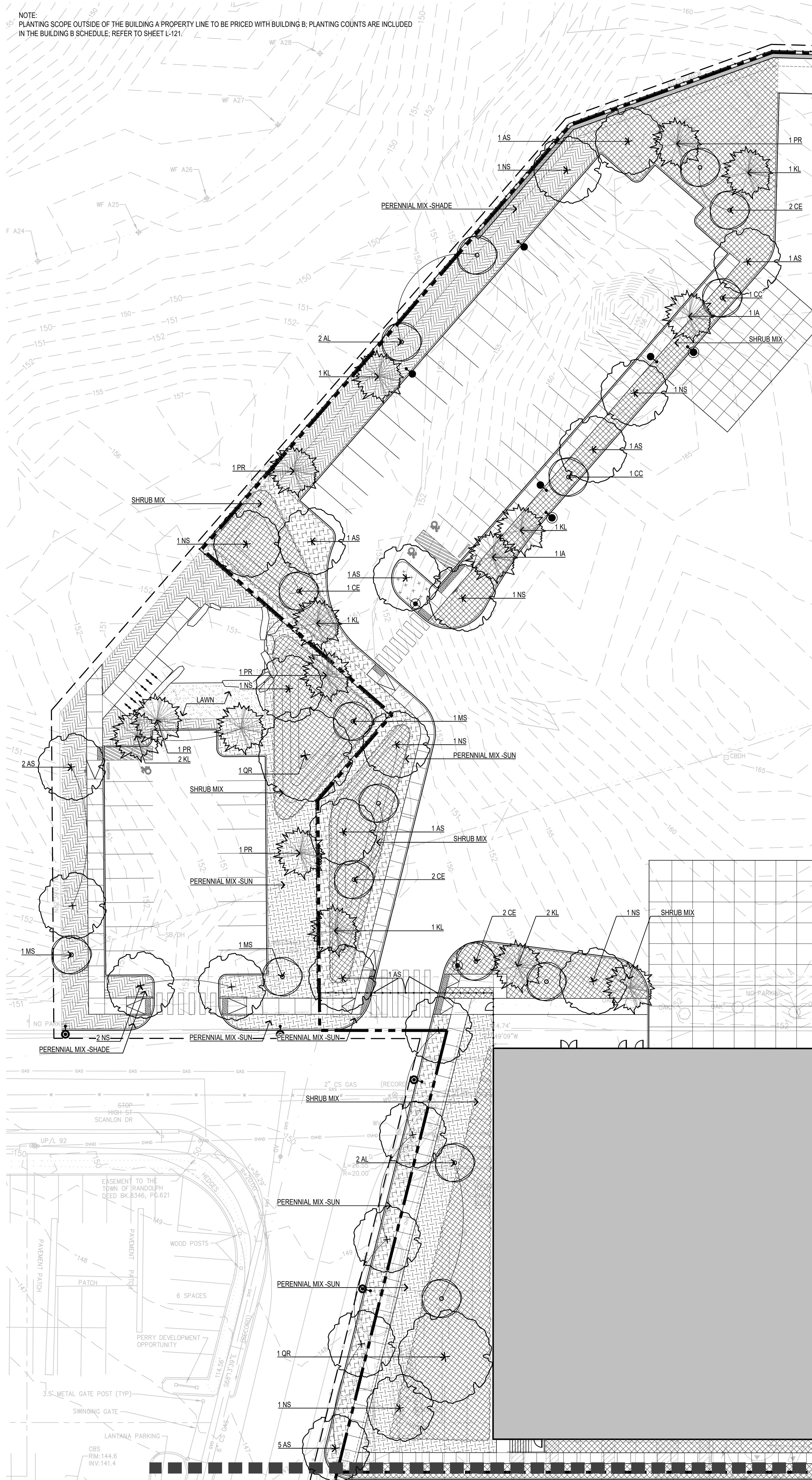
E

D

C

B

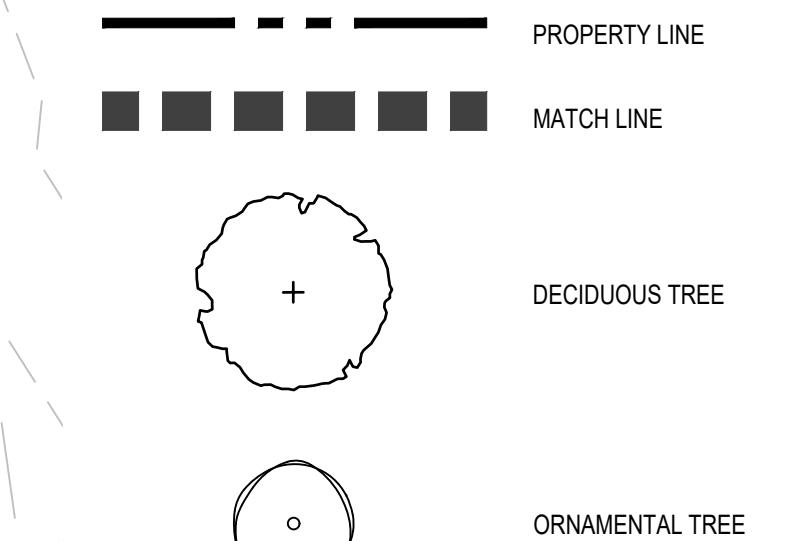
A



### PLANT SCHEDULE BLDG A

| CODE                    | QTY | BOTANICAL NAME                   | COMMON NAME                               | SIZE        | NOTES    |
|-------------------------|-----|----------------------------------|---|-------------|----------|
| <b>DECIDUOUS TREES</b>  |     |                                  |   |             |          |
| AS                      | 12  | AZELIA RUBRUM 'AUTUMN SPIRE'     | AUTUMN SPIRE RED MAPLE                    | 3'-3.5' CAL | B&B      |
| TS                      | 1   | NYSSA SYLVATICA                  | TUPELO                                    | 3'-3.5' CAL | B&B      |
| OR                      | 1   | QUERCUS RUBRA                    | RED OAK                                   | 3'-3.5' CAL | B&B      |
| <b>EVERGREEN TREES</b>  |     |                                  |   |             |          |
| IA                      | 2   | ILEX OPACA                       | AMERICAN HOLLY                            | 3'-3.5' CAL | B&B      |
| KL                      | 7   | KALMA LATIFOLIA                  | MOUNTAIN LAUREL                           | 10' HT      | B&B      |
| PR                      | 2   | PINUS RIGIDA                     | PITCH PINE                                | 3'-3.5' CAL | B&B      |
| <b>ORNAMENTAL TREES</b> |     |                                  |   |             |          |
| AL                      | 1   | LARCAMPHEIUS LAEVIS              | ALLEGHENY SERVICEBERRY MULTI-TRUNK        | 14' HT      | B&B      |
| CE                      | 7   | CERCIS CANADENSIS                | EASTERN REBUD MULTI-TRUNK                 | 14' HT      | B&B      |
| CC                      | 3   | CRATAEGUS CRUS-GALI              | COCKSPUR HAWTHORN                         | 3'-3.5' CAL | B&B      |
| <b>SHRUB AREAS</b>      |     |                                  |   |             |          |
| AG                      |     | ARONIA MELANOCarpa 'UCONNAM012'  | GROUNDSIDE BLACK CHokeBERRY               | #5 POT      |          |
| AZ                      |     | ARONIA MELANOCarpa 'UCONNAM165'  | LOW SCAPE MOUND BLACK CHokeBERRY          | #7 POT      |          |
| GT                      |     | CLETHRA ALNIFolia HUMMINGBIRD    | HUMMINGBIRD SUMMERSWEET                   | #7 POT      |          |
| IG                      |     | ILEX GLabra                      | INKBERRY HOLLY                            | #7 POT      |          |
| IR                      |     | ILEX VERTICILLATA FARROWPOP®     | BERRY POPPIN® WINTERBERRY                 | #7 POT      |          |
| IF                      |     | ILEX VERTICILLATA FARROWWRP®     | MR. POPPIN® WINTERBERRY                   | #7 POT      |          |
| PP                      |     | POTENTILLA FRUTICOSA KUPINPA®    | HAPPY FACE® PINK PARADISE BUSH CINQUEFOIL | #5 POT      |          |
| RG                      |     | RHUS AROMATICA GRO-Low           | GRO-Low FRAGRANT SUMAC                    | #5 POT      |          |
| <b>PERENNIALS</b>       |     |                                  |   |             |          |
| AC                      |     | ALLIUM CERNUM                    | NODDING ONION                             | FLATS       | 15' o.c. |
| AV                      |     | ASCLEPIAS VERTICILLATA           | WHORLED MILKWEED                          | #1 POT      | 15' o.c. |
| CP                      |     | CAREX PENNSYLVANICA              | PENNSYLVANIA SEDGE                        | FLATS       | 15' o.c. |
| CR                      |     | COREOPSIS ROSEA                  | ROSE COREOPSIS                            | FLATS       | 15' o.c. |
| EP                      |     | ECHINACEA PURPUREA 'PAS02918'    | POWWOW® WHITE CONEFLOWER                  | #1 POT      | 15' o.c. |
| EF                      |     | ERYNGIUM 'UCPOLIUM' PRAIRIE MOON | PRairie MOON RATTLESNAKE MASTER           | #1 POT      | 15' o.c. |
| ID                      |     | IRIS 'CANTATA' ALBA              | WHITE DWARF CRESTED IRIS                  | FLATS       | 15' o.c. |
| LS                      |     | LATRIS SPICATA                   | BLAZING STAR                              | #1 POT      | 15' o.c. |
| MR                      |     | MAIANthemum RACEMOSUM            | FAIS SE SOLOMON'S SEAL                    | #1 POT      | 15' o.c. |
| SH                      |     | SPOROBOLUS HETEROLEPIS           | PRairie DROPSeed                          | FLATS       | 15' o.c. |

### LEGEND



### PLANTING NOTES

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### CONCEPT PLANT SCHEDULE BLDG A

|   |           |
|---|-----------|
| <b>PERENNIAL MIX-SUN</b>  | 4,818 SF  |
| ASCLEPIAS VERTICILLATA / WHORLED MILKWEED                                 | 480       |
| COREOPSIS ROSEA / ROSE COREOPSIS  | 641       |
| ECHINACEA PURPUREA 'PAS02918' / POWWOW® WHITE CONEFLOWER                  | 480       |
| IRIS 'UCPOLIUM' PRAIRIE MOON / PRairie MOON RATTLESNAKE MASTER            | 480       |
| LATRIS SPICATA / BLAZING STAR   | 480       |
| SPOROBOLUS HETEROLEPIS / PRairie DROPSeed                                 | 641       |
| <b>PERENNIAL MIX-SHADE</b>  | 2,580 SF  |
| ALLIUM CERNUM / NODDING ONION   | 257       |
| CAREX PENNSYLVANICA / PENNSYLVANIA SEDGE                                  | 686       |
| IRIS CRISTATA 'ALBA' / WHITE DWARF CRESTED IRIS                           | 515       |
| MAIANthemum RACEMOSUM / FALSE SOLOMON'S SEAL                              | 257       |
| <b>SHRUB MIX</b>  | 16,711 SF |
| ARONIA MELANOCarpa 'UCONNAM012' / GROUNDSIDE BLACK CHokeBERRY             | 216       |
| ARONIA MELANOCarpa 'UCONNAM165' / LOW SCAPE MOUND BLACK CHokeBERRY        | 108       |
| CLETHRA ALNIFolia HUMMINGBIRD / HUMMINGBIRD SUMMERSWEET                   | 162       |
| ILEX GLabra / INKBERRY HOLLY  | 162       |
| ILEX VERTICILLATA FARROWPOP® / BERRY POPPIN® WINTERBERRY                  | 136       |
| ILEX VERTICILLATA FARROWWRP® / MR. POPPIN® WINTERBERRY                    | 27        |
| POTENTILLA FRUTICOSA KUPINPA® / HAPPY FACE® PINK PARADISE BUSH CINQUEFOIL | 162       |
| RHUS AROMATICA GRO-Low / GRO-Low FRAGRANT SUMAC                           | 108       |





Planning Board  
Town of Randolph

January 12, 2024

Re: Lantana and Lombardo's Redevelopment

Respectfully submitted,

Please accept this letter on behalf of Comfort Inn Randolph located at 1374 North Main Street. My family purchased the property in 2006. The hotel was built in 1969 and has operated as a hotel for nearly 55 years. We have accounted for a substantial amount of lodging and property tax revenue to the Town. We have hosted countless family events, weddings, corporate meetings, etc. through our years of operating the hotel.

As developers ourselves, we welcome the major redevelopment and the future of this section of Randolph. We have been fortunate to meet the developer and have nothing but positive feedback to provide. The properties are in good hands, and we feel the redevelopment will be great for the Town and the area. However, it has come to our attention the redevelopment of the Lantana and Lombardo's properties would include discontinuances of Billings Street and a portion of High Street. We have yet to review any final plans for the future of the properties, but we know this will have a major impact on our site and will be a disruption to our business.

The entire Northern entrance and exit of our property will be blocked, which will cause major issues with the flow of our site. We often house utility crews and transportation groups that depend on being able to drive through our site to access our main entrance. Without the access to Billings Street, no large vehicle such as Fire engines will be able to turn around on the Route 28 facing portion of our property after entering. I would equate the removal of these streets to one day removing Depot Street or Diauto Drive. The impact may be perceived as limited, but in reality would be substantial to the small businesses these streets serve. The continuation of use of Billings Street and High Street is extremely important to our team and the guests we serve. I appreciate the consideration of our concerns and thank you for your time.

Sincerely,

A handwritten signature in black ink, appearing to read "Jiten Patel".

Jiten Patel  
President  
Jiten Hotel Management



**TOWN OF RANDOLPH**  
MASSACHUSETTS

**FIRE DEPARTMENT**

10 MEMORIAL PARKWAY RANDOLPH, MA 02368-4506

**RONALD J. CASSFORD, CHIEF OF DEPARTMENT**

BUSINESS: 781.961.0991/0992

FAX: 781.961.FIRE (3473)

[WWW.RANDOLPHFIRE.COM](http://WWW.RANDOLPHFIRE.COM)

**MICHAEL J. AUSTRINO**

FIRE CAPTAIN

[FirePrevention1@RandolphFire.com](mailto:FirePrevention1@RandolphFire.com)

**PATRICK J. CONNORS**

FIRE LIEUTENANT

[FirePrevention2@RandolphFire.com](mailto:FirePrevention2@RandolphFire.com)

**OFFICE OF FIRE PREVENTION  
AND CODE ENFORCEMENT**

January 18, 2024

Michelle Tyler  
Director of Planning  
Town of Randolph  
41 South Main Street

Dear Ms. Tyler,

The Randolph Fire Department's Office of Fire Prevention and Code Enforcement has reviewed the Billings/Scanlon/High Street proposal. The fire apparatus mentioned on Exhibit E3.0, identified as the "Spartan Gladiator Star Series Aerial," should be updated to accurately reflect the Randolph Fire Department's utilization of an E-One Typhoon Aerial Platform with slightly larger dimensions. I have attached a specification sheet containing information on turning radius and apparatus dimensions.

After this correction, the designated traffic patterns for the properly identified fire apparatus would be suitable for the proposed occupancies. However, we have concerns regarding access to the hotel property at 1374 North Main Street. Currently, during emergency responses to incidents at this location, a section of Billing Street connecting to the hotel's parking lot is utilized. This access point is crucial for emergency responders as it provides entry to the sprinkler room side of the occupancy.

Blocking or closing this access point would create a dead end for apparatus entering from Scanlon Drive and North Main Street (Rt 28). In such a scenario, apparatus would be required to reverse out of the hotel parking lot, leading to potential traffic congestion, delays in response to other emergencies, possible accidents, and the need for additional personnel to assist or guide apparatus operators exiting the property.

To address these concerns, it is respectfully requested that some form of access point be maintained between the two properties, namely 6 Billing St and 1374 North Main St. Additionally, any design or proposal related to this access point should undergo a thorough fire department review and receive comments prior to obtaining approval.

Respectfully,

*Capt. M. Austrino*

Michael J. Austrino  
Fire Captain  
Office of Fire Prevention and Code Enforcement



| <b>SAE Turning Radius Calculations for Quote No. 98168</b>  |                         |                         |                        |                       |
|---|-------------------------|-------------------------|------------------------|-----------------------|
| Wheelbase:  | 250"                    | Front Bumper Size:      | 10"                    |                       |
| Body Width:   | 100"                    | Front Bumper Extension: | 20"                    |                       |
| Front Axle Kingpin Center:  | 70.66"                  | Front Wheel Type:       | ALUMINUM               |                       |
| Front Axle Track:   | 84.46"                  | Rear Wheel Type:        | ALUMINUM               |                       |
| Front Axle Tire Width:  | 16.6"                   | Tire Brand:             | MICHELIN               |                       |
| Dimension Over Rear Tires:  | 98.59"                  |                         |                        |                       |
| Body Front Overhang:  | 92"                     |                         |                        |                       |
| Inside Cramp Angle  | S. A. E. Turning Radius | Tire Curb Clearance     | Bumper Swing Clearance | Minimum Inside Radius |
| 35  | 41.9'                   | 42.6'                   | 46.6'                  | 28.6'                 |
| 36  | 40.9'                   | 41.6'                   | 45.7'                  | 27.5'                 |
| 37  | 40.1'                   | 40.7'                   | 44.9'                  | 26.5'                 |
| 38  | 39.2'                   | 39.9'                   | 44.2'                  | 25.5'                 |
| 39  | 38.4'                   | 39.1'                   | 43.5'                  | 24.6'                 |
| 40  | 37.7'                   | 38.4'                   | 42.8'                  | 23.7'                 |
| 41  | 37'                     | 37.7'                   | 42.2'                  | 22.8'                 |
| 42  | 36.3'                   | 37'                     | 41.6'                  | 22'                   |
| 43  | 35.7'                   | 36.4'                   | 41'                    | 21.2'                 |
| 44  | 35'                     | 35.7'                   | 40.4'                  | 20.4'                 |
| 45  | 34.5'                   | 35.2'                   | 39.9'                  | 19.7'                 |
| 46  | 33.9'                   | 34.6'                   | 39.4'                  | 19'                   |
| 47  | 33.4'                   | 34.1'                   | 38.9'                  | 18.3'                 |
| 48  | 32.8'                   | 33.5'                   | 38.5'                  | 17.6'                 |
| 49  | 32.4'                   | 33'                     | 38.1'                  | 16.9'                 |
| 50  | 31.9'                   | 32.6'                   | 37.6'                  | 16.3'                 |
| <b>Nominal Cramp Angles:</b>  |                         |                         |                        |                       |
| Meritor FL941 & FL943 axles: up to and including 425/65R22.5 tires  | 45 degrees              |                         |                        |                       |
| Meritor FL941 & FL943 axles: 445/65R22.5 tires  | 38 degrees              |                         |                        |                       |
| Dana 1220W axle: up to and including 445/65R22.5 tires  | 42 degrees              |                         |                        |                       |
| Reyco IFS: up to and including 385/65R22.5 tires  | 48 degrees              |                         |                        |                       |
| Reyco IFS: 425/65R22.5 tires  | 45 degrees              |                         |                        |                       |
| Reyco IFS: 445/65R22.5 tires without front intake   | 42 degrees              |                         |                        |                       |
| Meritor Front Drive Axle: up to and including 425/65R22.5 tires   | 37 degrees              |                         |                        |                       |
| Marmon Herrington Front Drive Axle: up to and including 425/65R22.5 tires   | 42 degrees              |                         |                        |                       |
| <b>This Turning Radius report reflects how the quote was configured. Any succeeding changes may slightly alter the turning radius of the vehicle and the data in this report.</b> |                         |                         |                        |                       |

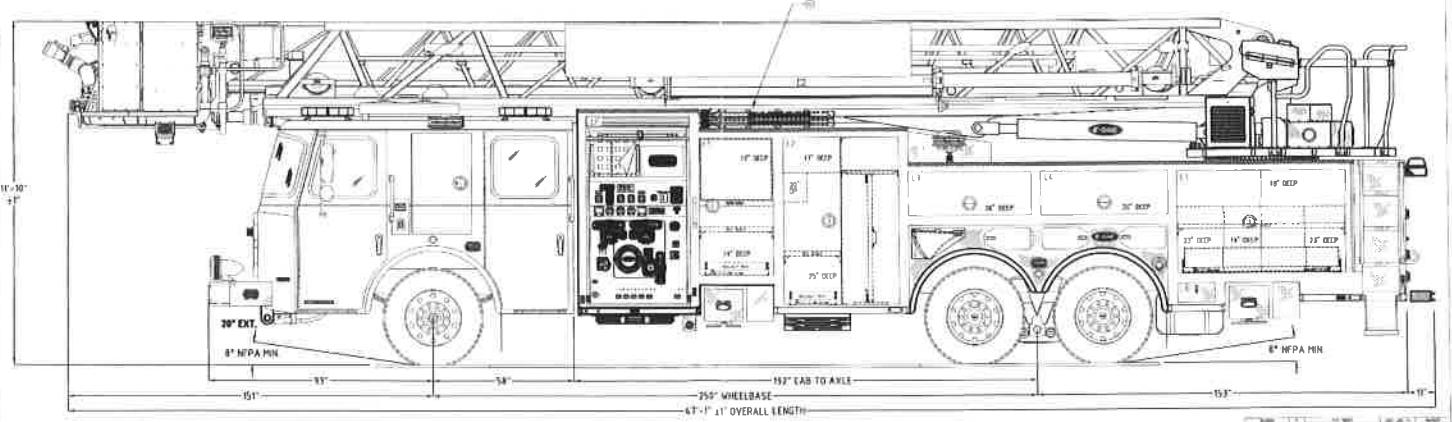
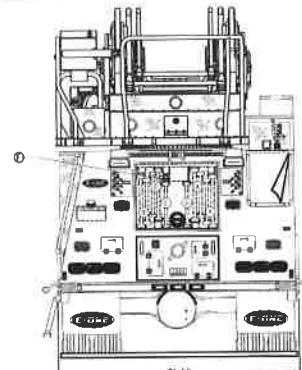
**RANDOLPH FIRE DEPT**  
**RANDOLPH, MA**  
**S.O. 144171/Q 98168**  
**AERIAL BODY**  
**TYphoon 6x4 Chassis**  
**HP 100 Aerial Platform**

This drawing is for reference purposes only. All dimensions are subject to minor variations due to manufacturing processes.  
 Date: 07/04/04 Rev: 001  
 Customer Approval: 002 CMH Revision:

| HOSE LOAD      |         |                    |
|----------------|---------|--------------------|
| 600' OF 4" LDH |         |                    |
| COMPT.         | OPENING | INTERIOR DIMENSION |
| L1/R1          | 31W 51H | 18W 28H            |
| L2/R2          | 48W 7H  | 18W 28H            |
| L3/R3          | 50W 18H | 50W 18H 26D        |
| L4             | 52W 18H | 52W 18H 20D        |
| R4             | 15W 32H | 15W 32H 23D        |
| L5             | 69W 12H | 12H 20D            |
| R5             | 31W 20H | 31W 20H 14D        |
| L6             | 15W 8H  | 15W 8H 23D         |
| R6             | 36W 28H | 36W 28H 23D        |

| GROUND LADDERS |               |              |             |
|----------------|---------------|--------------|-------------|
| ITEM           | LAZZER LENGTH | MODEL NUMBER | QTY         |
| A              | 30' 2-SECT.   | PFL-35       | 2           |
| B              | 28' 2-SECT.   | PFL-28       | 1           |
| C              | 24' 2-SECT.   | PFL-24       | 1           |
| D              | 20' ROOF      | PRL-20       | 1           |
| E              | 18' ROOF      | OFL-18       | 1           |
| F              | 18' FOLDING   | FL-18        | 1           |
| G              | 16' ROOF      | OFL-16       | 1           |
| H              | LITTLE GIANT  | MODEL 17     | 1 ON AERIAL |



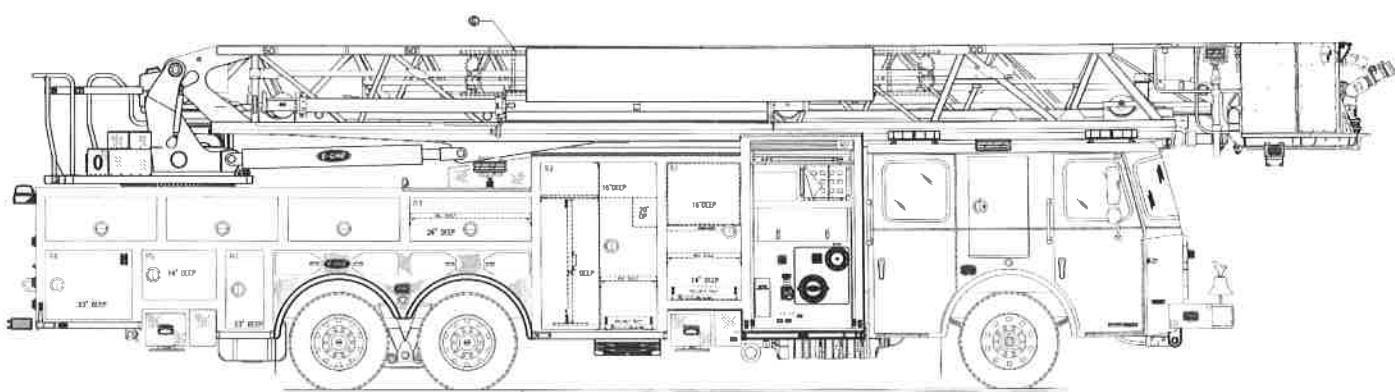
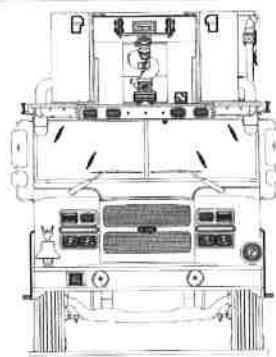
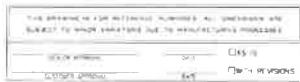
RANDOLPH FIRE DEPT

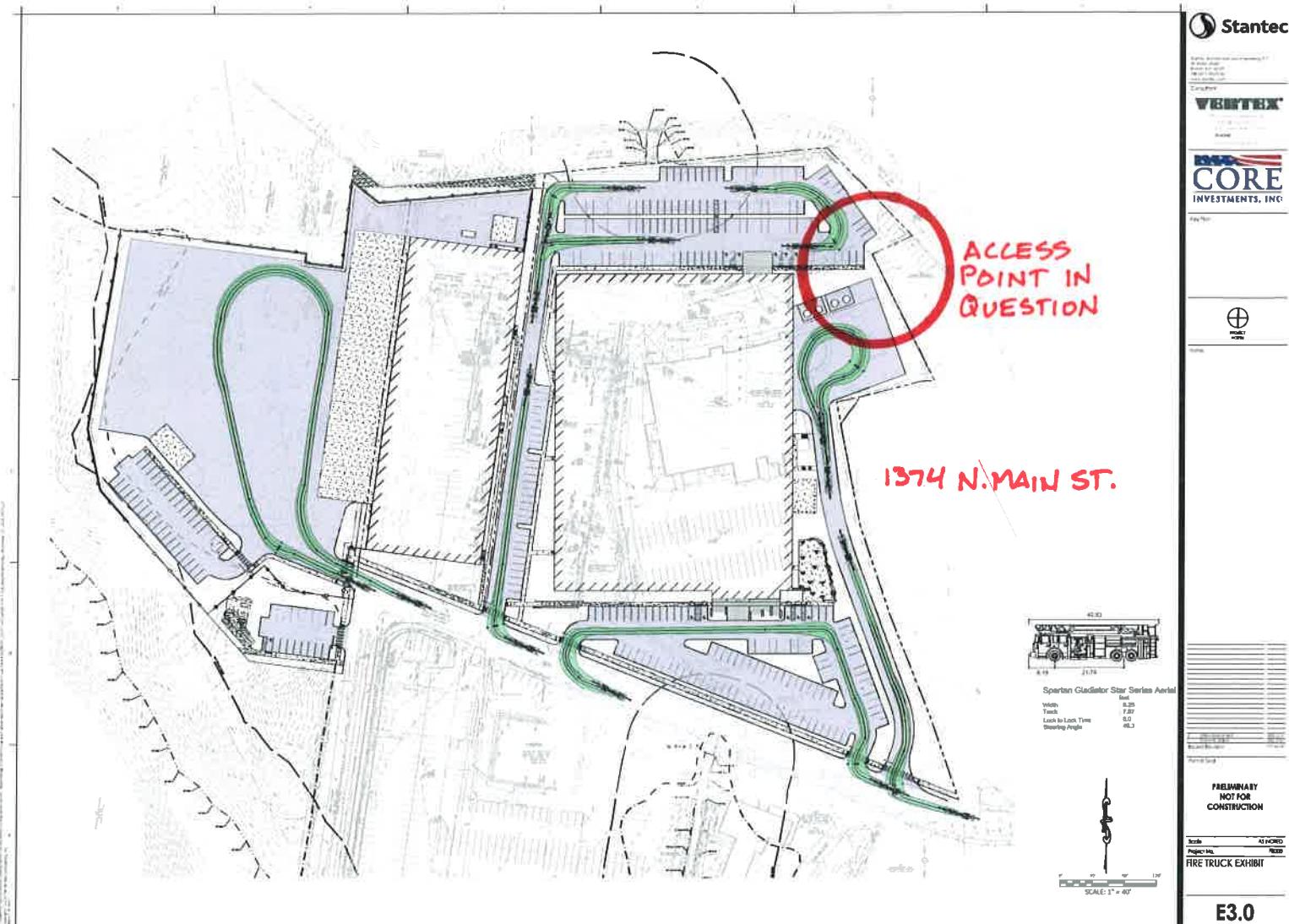
RANDOLPH, MA

S.O. 144171/Q 98168

AERIAL BODY

TYphoon 6x4 Chassis  
HP 100 Aerial Platform



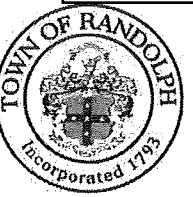


**File Attachments for Item:**

2. Subdivision - Perry Estates - Request for Extension

## PLANNING DEPARTMENT

Section G, Item2.

**FORM K**  
**REQUEST FOR TIME EXTENSION – DEFINITIVE**  
**SUBDIVISION**


|                         |                 |                                |              |
|-------------------------|-----------------|--------------------------------|--------------|
| <b>Subdivision Name</b> | Perry Estates   |                                |              |
| <b>Date of Approval</b> | May 10, 2022    | <b>Initial Expiration Date</b> | May 10, 2024 |
| <b>Requested Date</b>   | January 9, 2024 | <b># Previous Extensions</b>   | 0            |

|                       |                     |              |                       |
|-----------------------|---------------------|--------------|-----------------------|
| <b>Property Owner</b> | Michael Perry Trust |              |                       |
| <b>Address</b>        | 10 Toby Lane        |              |                       |
| <b>Address2</b>       | Randolph, MA 02368  |              |                       |
| <b>Phone</b>          | 781-7279096         | <b>Email</b> | mperry02368@yahoo.com |

|                  |      |              |  |
|------------------|------|--------------|--|
| <b>Applicant</b> | SAME |              |  |
| <b>Address</b>   |      |              |  |
| <b>Address2</b>  |      |              |  |
| <b>Phone</b>     |      | <b>Email</b> |  |

**REASON**

*Describe progress made towards meeting the conditions of approval of the subdivision and reasons for the time extension request*

NO construction activities underway. Applicant  
requests an extension due to health issues

**SURETY CONSENT**

*If performance was secured by a surety, a letter from the Financial Institution must be attached to this request concurring the request of an extension time and shall affirm that the Letter of Credit/Bond issued by them remains in effect and that the terms are valid and binding.*

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Signature of Applicant

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Date

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Printed Name

**PLANNING BOARD DECISION**

Hearing Date \_\_\_\_ / \_\_\_\_ / \_\_\_\_

Approved      New Date of Expiration \_\_\_\_ / \_\_\_\_ / \_\_\_\_

Denied      Reason: \_\_\_\_\_