PLANNING AND ZONING BOARD MEETING

CITY OF LAKE CITY

May 14, 2024 at 5:30 PM Venue: City Hall

AGENDA

The meeting will be held in the City Council Chambers on the second floor of City Hall located at 205 North Marion Avenue, Lake City, FL 32055. Members of the public may also view the meeting on our YouTube channel. YouTube channel information is located at the end of this agenda.

INVOCATION

ROLL CALL

MINUTES

i. Meeting Minutes 04-09-2024

EX PARTE COMMUNICATION

OLD BUSINESS- None

NEW BUSINESS

- **ii. SPR24-05**, Petition submitted by Randall Olney, P.E.. (agent) for Concept Companies (owner), for a Site Plan Review for Dollar General, in the Commercial Intensive Zoning District, and located on parcel 08127-005, which is regulated by the Land Development Regulations section 4.13.
- iii. LDR 24-04; Text amendment to the Land Development Regulations Sections 2.1, 4.2, 4.4, 4.5, and 4.6, more specifically adding definitions and provisions for Accessory Dwelling Units (ADU's) and Tiny Homes for the City of Lake City.

WORKSHOP- None

ADJOURNMENT

YouTube Channel Information

Members of the public may also view the meeting on our YouTube channel at: https://youtube.com/c/CityofLakeCity Pursuant to 286.0105, Florida Statutes, the City hereby advises the public if a person decides to appeal any decision made by the City Council with respect to any matter considered at its meeting or hearings, he or she will need a record of the proceedings, and that, for such purpose, he or she may need to ensure that a verbatim record of the proceedings is made, which record includes the testimony and evidence upon which the appeal is to be based.

Pursuant to 286.26, Florida Statutes, persons needing special accommodations to participate in this meeting should contact the City Manager's Office at (386) 719-5768.

File Attachments for Item:

i. Meeting Minutes 04-09-2024

MEETING MINUTES

DATE: 04/09/2024

ROLL CALL:

Mrs. McKellum- PresentMr. McMahon- PresentMr. Nelson- PresentMr. Lydick- PresentCity Attorney- Clay Martin- Present

MINUTES: March 5, 2024 Planning and Zoning Meeting.

Comments or Revisions: None

Motion to approve 03/05/2024 Meeting Minutes by Mr. Nelson and seconded by Mrs. McKellum.

Ex Parte Communications

Mr. Martin polled the Board if they had any ex parte communications for petitions SPR 24-04, CPA 24-01, and Z 24-01

Mrs. McKellum- No, Mr. McMahon- No, Mr. Nelson- No, and Mr. Lydick- Only the regular exercise of his duties on briefing of the agenda. Mr. Martin asked if it would those conversations affect your ability to render a fair decision.

OLD BUSINESS: None

Petition # LDR 24-03 Presented By: Dave Young, CBO As owner or agent and gives address of: Petitioner is Sworn in by: Clay Martin, City Attorney

Motion to un-table petition LDR 24-03 by; Mr. McMahon and seconded by Mr. Nelson. Approved by hand vote unanimously.

Discussion:

Mr. Young introduced text amendment. He stated that this text amendment is bringing up to date the parking requirements to other communities our size. Mr. Lydick asked if there were any major changes other than, adding section 4.2.15.17. Mr. Young stated no.

Mr. Martin asked about the strike thru's and the addition of where is states see section 4.2.15 is different then the ordinance that is prepared for council. Mr. Martin asked which one do we want to be recommended by the board to go to Council? Mr. Lydick and Mr. Martin discussed briefly. Robert stated that we could go with how the ordinance is prepared. Mr. Martin stated that the would change the verbiage to subsection instead of paragraph and leave the numbering as is.

Public Comment:

Carol Chadwick stated that per the Boards request, she believes that the City did a great job. Mr. Lydick asked if she seen anything that look like it may be a problem. She stated that until you start applying it you will not know.

Motion to close public comment by: Mr. Nelson Seconded by: Mr. McKellum

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MEETING MINUTES

Board Discussion:

Mr. Lydick asked if any of the other departments weighed in on the amendment. Robert stated that the other departments were aware of them but they did not weigh in. Robert stated that they City did send the text amendment out to over 700 businesses in the City. He stated that we only go a handful of comments back, all in support of it. Mr. McMahon asked if this would go on to the City Council once approved.

Motion to approve petition LDR 24-03, with the amendments suggested by council by: Mr. McMahon Motion Seconded By: Mr. Nelson

Mrs. McKellum: Aye Mr. Nelson: Aye Mr. McMahon: Aye Mr. Lydick: Aye

NEW BUSINESS:

Petition # SPR24-03 Presented By: Brandon Stubbs As owner or agent and gives address of: 1450 SW SR 47, Lake City, FL Petitioner is Sworn in by: Mr. Lydick Staff is Sworn in by: Mr. Martin

Discussion:

Mr. Young introduced petition SPR 24-04. He stated that proposed use of the land is for multifamily and is conducive for use per the Land Development Regulations 4.9.2.3. He stated that after review of the site plan that it is consistent with the Land Development Regulations.

Mr. Kurtz the land is currently vacant. He stated that they plan to put one to three bed room town homes. He stated SRWMD has reviewed the project along with the City and they have no concerns. He stated that FDOT said they need a drainage permit. He stated that they will work on that with FDOT.

Mr. McMahon asked about how many units. Mr. Kurtz stated that they want to put in 192 units. Mr. Lydick asked about the size of the large retention pond. Mr. Kurtz stated that due to the slope of the land they had to do two ponds stair stepped to accommodate for the amount of water.

Mr. Martin asked Mr. Young if he was going to move the staff records into evidence. Mr. Young stated yes.

Exhibits introduced: None

Public Comment:

Loretta Nicholas asked about how this is going to affect them as far as traffic, sewer, and water. Mr. Kurtz stated that as far as water and sewer, this will not impact the citizens. He stated as far as traffic they will use Hall of Fame and will not enter Aster Way.

Motion to close public comment by: Mr. Nelson Seconded by: Mrs. McKellum

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MEETING MINUTES

Board Discussion: No comments.

Motion to approve SPR24-04 as submitted by: Mr. McMahon Motion Seconded By: Mr. Nelson

Mrs. McKellum: Aye Mr. Nelson: Aye Mr. McMahon: Aye Mr. Lydick: Aye

Petition # CPA 24-01 Presented By: Carol Chadwick As owner or agent and gives address of: 1208 SW Fairfax Glen Petitioner is Sworn in by: Mr. Lydick Staff is Sworn in by: Mr. Martin

Discussion:

Mr. Young introduced petition CPA 24-01. He stated that the City staff has determined the petition is consistent with the Land Development Regulations. He stated that he is introducing the staff records into the record.

Carol stated that they are planning to change the Future Land Use and Zoning to allow for a second phase of Sugarmill Apartments. She stated that the site will be accessed from the existing site. She stated they are planning on 46 dwelling units. Mr. Lydick asked if the property ever had a City zoning. She stated that it has not. Mr. Martin asked if she was going to introduce her application into the record.

Public Comment:

David Kraft stated that he owns the property next to it. He stated that there is water all in his yard and would like them to address this in the future review. Mr. Lydick asked Robert if this was going to be in front of the board. Robert stated yes.

Exhibits introduced: None

Motion to close public comment by: Mrs. McKellum Seconded by: Mr. Nelson

Board Discussion: None

Motion to approve CPA24-01 as submitted by: Mr. McMahon Motion Seconded By: Mr. Nelson

Mrs. McKellum: Aye	Mr. Nelson: Aye	Mr. McMahon: Aye
Mr. Lydick: Aye		

MEETING MINUTES

Petition # Z 24-01 Presented By: Carol Chadwick As owner or agent and gives address of: 1208 SW Fairfax Glen Petitioner is Sworn in by: Mr. Lydick Staff is Sworn in by: Mr. Martin

Discussion:

Mr. Young introduced petition Z 24-01. He stated that the City staff has determined the petition is consistent with the Land Development Regulations. He stated that he is introducing the staff records into the record.

Carol stated that project is the rezoning for the previous project. She stated that she is introducing her application into the record.

Public Comment: None

Exhibits introduced: None

Motion to close public comment by: Mr. Nelson Seconded by: Mr. Nelson

Board Discussion: None

Motion to approve Z24-01 as submitted by: Mr. Nelson Motion Seconded By: Mr. McMahon

Mrs. McKellum: Aye Mr. Nelson: Aye Mr. McMahon: Aye Mr. Lydick: Aye

WORKSHOP: None

ADJOURNMENT

Mr. Lydick closed the meeting.

Motion to Adjourn by: Mr. McMahon Time: 6:11 pm Motion Seconded By: Mr. Nelson

Mr. Lydick, Board Chairperson

Date Approved

Robert Angelo, Secretary

Date Approved

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MEETING MINUTES

File Attachments for Item:

ii. SPR24-05, Petition submitted by Randall Olney, P.E.. (agent) for Concept Companies (owner), for a Site Plan Review for Dollar General, in the Commercial Intensive Zoning District, and located on parcel 08127-005, which is regulated by the Land Development Regulations section 4.13.



GROWTH MANAGEMENT 205 North Marion Ave. Lake City, FL 32055 Telephone: (386)719-5750 E-Mail: growthmanagement@lcfla.com

OR PLANNING USE ONLY	
pplication # <u></u>	
pplication Fee: <u>\$200.00</u>	
leceiptNo. 2024-00042147	_
iling Date 3/21/24	
Completeness Date	

Site Plan Application

A. PROJECT INFORMATION

- 1. Project Name: Commercial Retail Store Marvin Burnett
- 2. Address of Subject Property: Northwest of the intersection of SR 47 and SW Marvin Burnett Road, Lake City, Florida 32025
- 3. Parcel ID Number(s): 07-48-17-08127-005
- 4. Future Land Use Map Designation: Commerical
- 5. Zoning Designation: Commercial, Intensive
- 6. Acreage: 2.70
- 7. Existing Use of Property: Vacant
- 8. Proposed use of Property: Commercial Retail Store
- 9. Type of Development (Check All That Apply):
 - Increase of floor area to an existing structure: Total increase of square footage_____
 - New construction: Total square footage 10,640

Relocation of an existing structure: Total square footage

B. APPLICANT INFORMATION

1. 2.	Applicant Status Name of Applicant(s	Owner (tit) Randall Olney, P.E.	le holder)	Agent Title: Director of Engineering	
	Company name (if a Mailing Address: 1180	pplicable): <u>CHW</u>			
	City: Alachua		State: Florida	Zip: 32615	
	·	-1976 Fax:()	Email: randyo@chw-inc.com	

PLEASE NOTE: Florida has a very broad public records law. Most written communications to or from government officials regarding government business is subject to public records requests. Your e-mail address and communications may be subject to public disclosure.

3. If the applicant is agent for the property owner*.

Property Owner Name (title holder): Concept Companies

 Mailing Address:
 1449 SW 74th Dr. Suite 200

 City:
 Gainesville

 State:
 Florida

Telephone: (352) 333-3233 Fax:(____) Email:

PLEASE NOTE: Florida has a very broad public records law. Most written communications to or from government officials regarding government business is subject to public records requests. Your e-mail address and communications may be subject to public disclosure. *Must provide an executed Property Owner Affidavit Form authorizing the agent to act on behalf of the property owner.

C. ADDITIONAL INFORMATION

 Is there any additional contract for the sale of, or options to purchase, the subject property? If yes, list the names of all parties involved: <u>St. Johns, LLC, Concept Development, Inc.</u>
 If yes is the contract (option contingent or absolute: Contingent □Absolute)

	if yes, is the contract option	commente	abbolater	S douine Bour Brin	bolute
2.	Has a previous application be	een made on	all or part of t	he subject property	?⊡Yes ∎No_
	Future Land Use Map Amend	lment: (⊐Yes	≡Nc)
	Future Land Use Map Amend	lment Applic	ation No		
	Site Specific Amendment to t	the Official Z	oning Atlas (Re	zoning): □Yes	No
	Site Specific Amendment to t	the Official Z	oning Atlas (Re	zoning) Application	No
	Variance:□Yes		No		
	Variance Application No.				
	Special Exception:	es		■ No	
	Special Exception Application	n No			

D. ATTACHMENT/SUBMITTAL REQUIREMENTS

- 1. Vicinity Map Indicating general location of the site, abutting streets, existing utilities, complete legal description of the property in question, and adjacent land use.
- 2. Site Plan Including, but not limited to the following:
 - a. Name, location, owner, and designer of the proposed development.
 - b. Present zoning for subject site.
 - c. Location of the site in relation to surrounding properties, including the means of ingress and egress to such properties and any screening or buffers on such properties.
 - d. Date, north arrow, and graphic scale not less than one inch equal to 50 feet.
 - e. Area and dimensions of site (Survey).
 - f. Location of all property lines, existing right-of-way approaches, sidewalks, curbs, and gutters.
 - g. Access to utilities and points of utility hook-up.
 - h. Location and dimensions of all existing and proposed parking areas and loading areas.
 - i. Location, size, and design of proposed landscaped areas (including existing trees and required landscaped buffer areas).
 - j. Location and size of any lakes, ponds, canals, or other waters and waterways.
 - k. Structures and major features fully dimensioned including setbacks, distances between structures, floor area, width of driveways, parking spaces, property or lot lines, and percent of property covered by structures.
 - I. Location of trash receptacles.
 - m. For multiple-family, hotel, motel, and mobile home park site plans:
 - i. Tabulation of gross acreage.
 - ii. Tabulation of density.
 - iii. Number of dwelling units proposed.
 - iv. Location and percent of total open space and recreation areas.
 - v. Percent of lot covered by buildings.

City of Lake City – Growth Management Department 205 North Marion Ave, Lake City, FL 32055 ♦ (386) 719-5750

- vi. Floor area of dwelling units.
- vii. Number of proposed parking spaces.
- viii. Street layout.
- ix. Layout of mobile home stands (for mobile home parks only).
- 3. Stormwater Management Plan—Including the following:
 - a. Existing contours at one foot intervals based on U.S. Coast and Geodetic Datum.
 - b. Proposed finished elevation of each building site and first floor level.
 - c. Existing and proposed stormwater management facilities with size and grades.
 - d. Proposed orderly disposal of surface water runoff.
 - e. Centerline elevations along adjacent streets.
 - f. Water management district surface water management permit.
- 4. Fire Department Access and Water Supply Plan: The Fire Department Access and Water Supply Plan must demonstrate compliance with Chapter 18 of the Florida Fire Prevention Code, be located on a separate signed and sealed plan sheet, and must be prepared by a professional fire engineer licensed in the State of Florida. The Fire Department Access and Water Supply Plan must contain fire flow calculations in accordance with the Guide for Determination of Required Fire Flow, latest edition, as published by the Insurance Service Office ("ISO") and/or Chapter 18, Section 18.4 of the Florida Fire Prevention Code, whichever is greater.
- 5. Concurrency Impact Analysis: Concurrency Impact Analysis of impacts to public facilities. For commercial and industrial developments, an analysis of the impacts to Transportation, Potable Water, Sanitary Sewer, and Solid Waste impacts are required.
- 6. Comprehensive Plan Consistency Analysis: An analysis of the application's consistency with the Comprehensive Plan (analysis must identify specific Goals, Objectives, and Policies of the Comprehensive Plan and detail how the application complies with said Goals, Objectives, and Policies).
- 7. Legal Description with Tax Parcel Number (In Word Format).
- 8. Proof of Ownership (i.e. deed).
- 9. Agent Authorization Form (signed and notarized).
- 10. Proof of Payment of Taxes (can be obtained online via the Columbia County Tax Collector's Office).
- 11. Fee. The application fee for a Site and Development Plan Application is \$200.00. No application shall be accepted or processed until the required application fee has been paid.

NOTICE TO APPLICANT

All eleven (11) attachments are required for a complete application. Once an application is submitted and paid for, a completeness review will be done to ensure all the requirements for a complete application have been met. If there are any deficiencies, the applicant will be notified in writing. If an application is deemed to be incomplete, it may cause a delay in the scheduling of the application before the Planning & Zoning Board.

A total of ten (10) copies of proposed site plan application and all support materials must be submitted along with a PDF copy on a CD. See City of Lake City submittal guidelines for additional submittal requirements.

THE APPLICANT ACKNOWLEDGES THAT THE APPLICANT OR AGENT MUST BE PRESENT AT THE PUBLIC HEARING BEFORETHE PLANNING AND ZONING BOARD. AS ADOPTED IN THE BOARD RULES AND PROCEDURES. OTHERWISE THE REQUEST MAY BE CONTINUED TO A FUTURE HEARING DATE.

I hereby certify that all of the above statements and statements contained in any documents or plans submitted herewith are true and accurate to the best of my knowledge and belief.

Randall Olney, P.E.

Applicant/Agent Name (Type or Print)

Applicant/Agent Signature

Applicant/Agent Name (Type or Print)

Applicant/Agent Signature

STATE OF FLORIDA COUNTY OF Alachua

The foregoing instrument was acknowledged before	ore me this 2 day of	3, 2024, by (name o	f person acknowledging).

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	2.76	Notary Public - State of Florida
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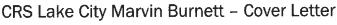
Signature of Notary enno Printed Name of Notary

Date

Date

Personally Known _____ OR Produced Identification _____ Type of Identification Produced

> City of Lake City – Growth Management Department 205 North Marion Ave, Lake City, FL 32055 ♦ (386) 719-5750



JOB NO. 22-0653



March 21, 2024

Robert Angelo Lake City Growth Management

RE: CRS Lake City Marvin Burnett

Dear Robert:

Please find attached the following items for review:

- Check #0018976 in the amount of \$200.00
- Site Plan Application
- Property Appraiser Information
- Agent Authorization Form
- Deed
- Legal Description
- Property Owner Affidavit
- Proof of Tax Payment
- Traffic Study
- Geotechnical Study
- Comprehensive Plan Analysis
- Concurrency Analysis
- Meter Calculations
- Fire Flow Memo
- Lift Station Report
- Stormwater Report
- Signed and Sealed Plans

The ± 2.72 acre site is located on SR 47 and SW Marvin Burnett Road in Lake City, Florida on a portion of tax parcel number 07-4S-17-08127-005. The site is currently undeveloped and heavily wooded. The development intent is to construct a $\pm 10,640$ s.f. commercial retail store on the parcel with the associated parking, stormwater management, and utility connections. Utility connections consist of a gravity sewer lateral to a private onsite lift station and connection to an existing forcemain within SR 47 ROW. Water and fire protection will be provided by extending a 600' water main along the western ROW of SR 47 and crossing via directional drill under SR 47 to wet tap an existing City water main. Offsite roadway improvements consist of a sidewalk along the project frontage, driveway connection and an eastbound left turn lane to Marvin Burnett Road.

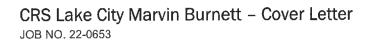
We trust you will find this submittal to be complete for review and approval. If you have any questions, or need additional information, please contact me at (352) 331-1976 or via email at randyo@chw-inc.com.

Sincerely, CHW

Randall Olney, PE Director of Engineering, Land Development

Florida Region

www.chw-inc.com





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Columbia County Property Appraiser Jeff Hampton

Parcel: 🔄 07-48-17-08127-005 (29833) 🛞

2024 Working Values updated: 11/23/2023

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Property & Assessment Values

20	23 Certified Values	20	24 Working Values
Mkt Land	\$266,978	Mkt Land	\$266,978
Ag Land	\$0	Ag Land	\$0
Building	\$0	Building	\$0
XFOB	\$0	XFOB	\$0
Just	\$266,978	Just	\$266,978
Class	\$0	Class	\$0
Appraised	\$266,978	Appraised	\$266,978
SOH Cap [?]	\$0	SOH Cap [?]	\$0
Assessed	\$266,978	Assessed	\$266,978
Exempt	\$0	Exempt	\$0
Total Taxable	county:\$266,978 city:\$266,978 other:\$0 school:\$266,978		county:\$266,978 city:\$266,978 other:\$0 school:\$266,978



Sales History

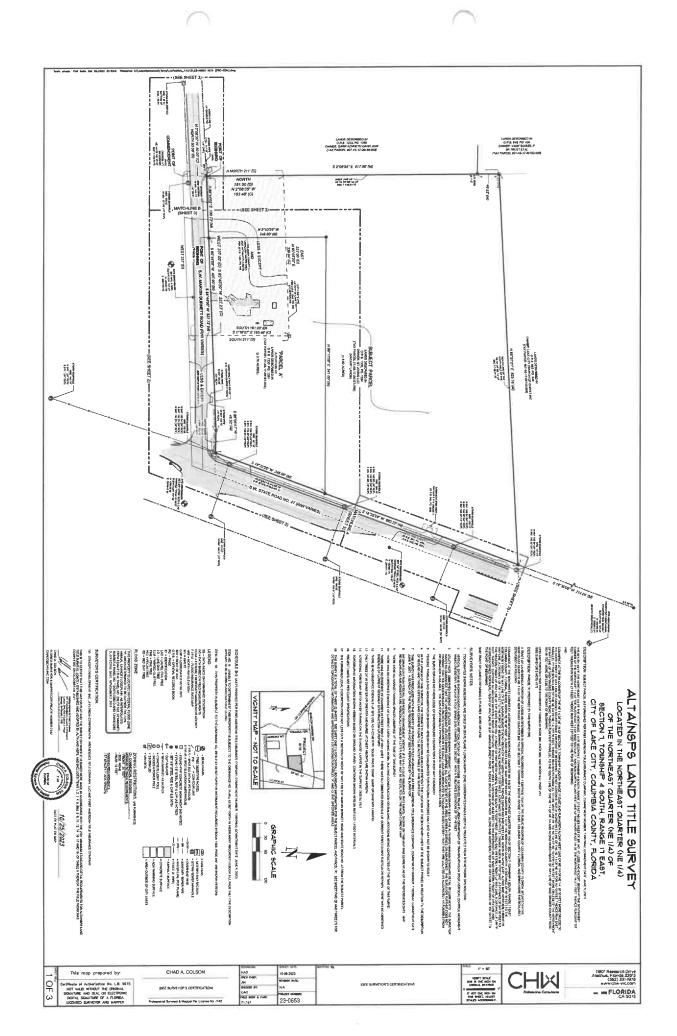
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2/6/2017	\$70,000	1330/1324	WD	I	Q	01
7/7/2016	\$100	1318/0991	LE	1	U	14
4/7/1995	\$727,500	0804/0766	WD	V	U	35
7/31/1990	\$127	1037/1953	WD	V	U	03
7/21/1990	\$127	1036/1953	WD	V	U	03
Building Characteristi	cs					
Bldg Sketch	Description*	Yea	ar Blt	Base SF	Actual SF	Bldg Value
			NONE			
Extra Features & Out	Buildings (Codes)					
Code	Desc	Year Bit		Value	Units	Dims
			NONE			
Land Breakdown						
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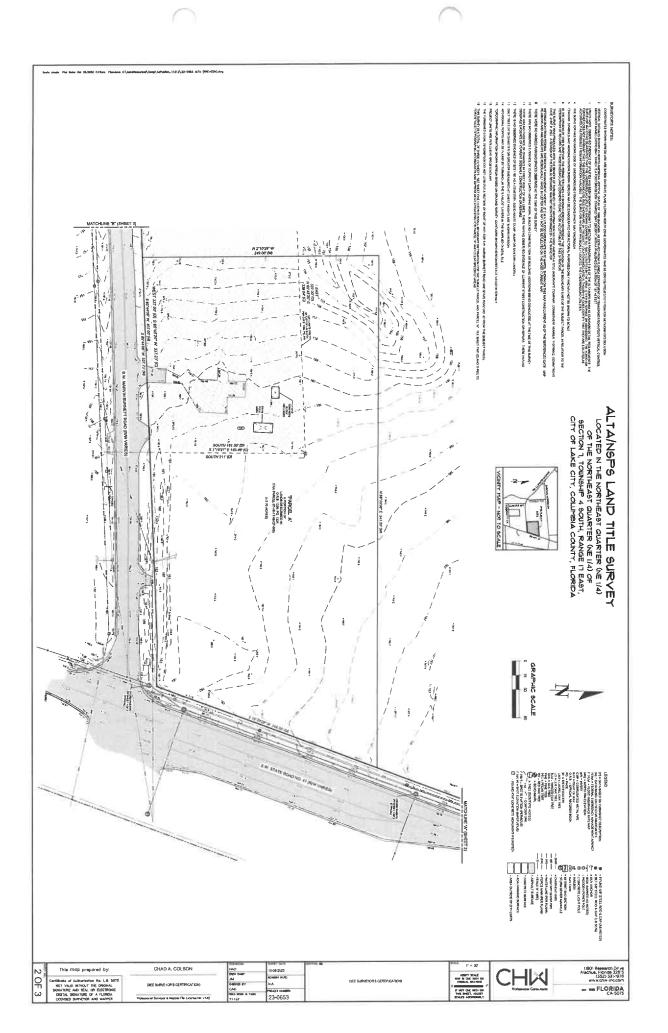
Columbia County Property Appraiser | Jaff Hampton | Lake City, Florida | 386-758-1083

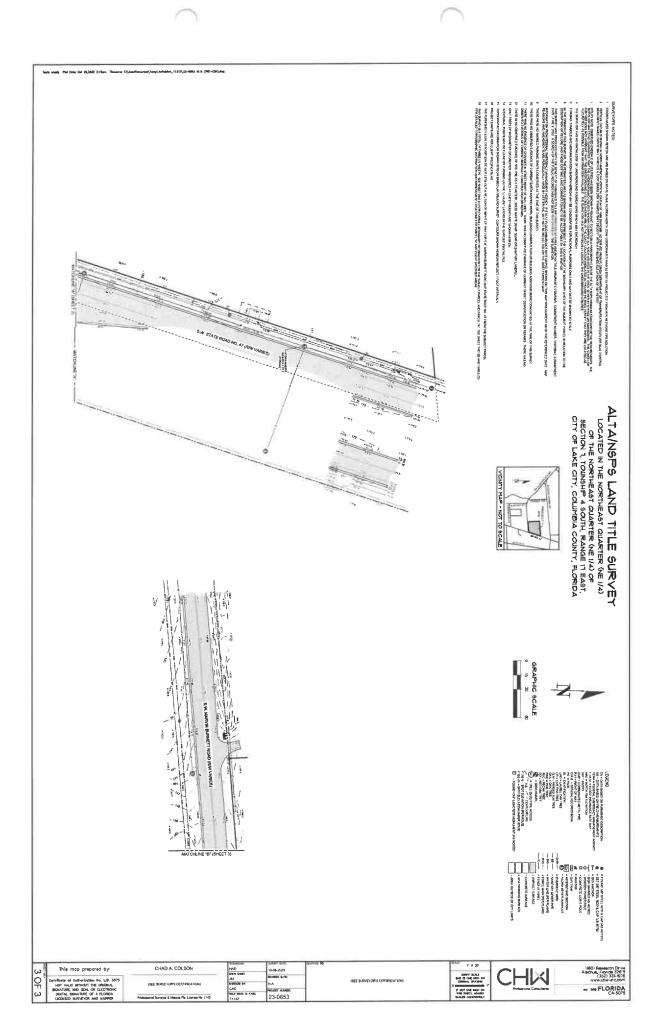
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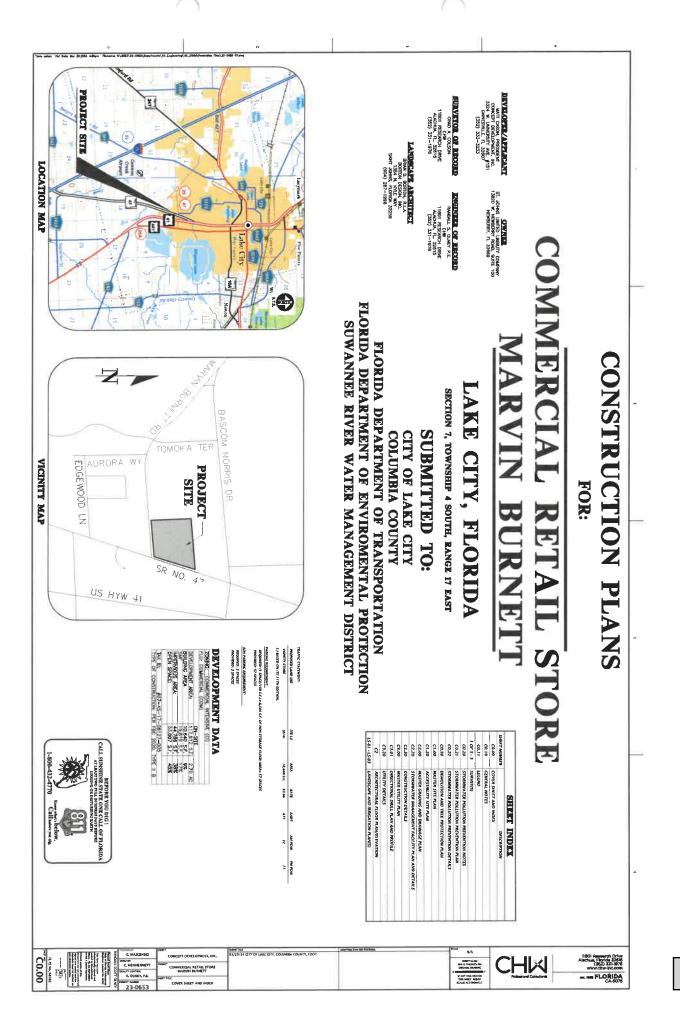
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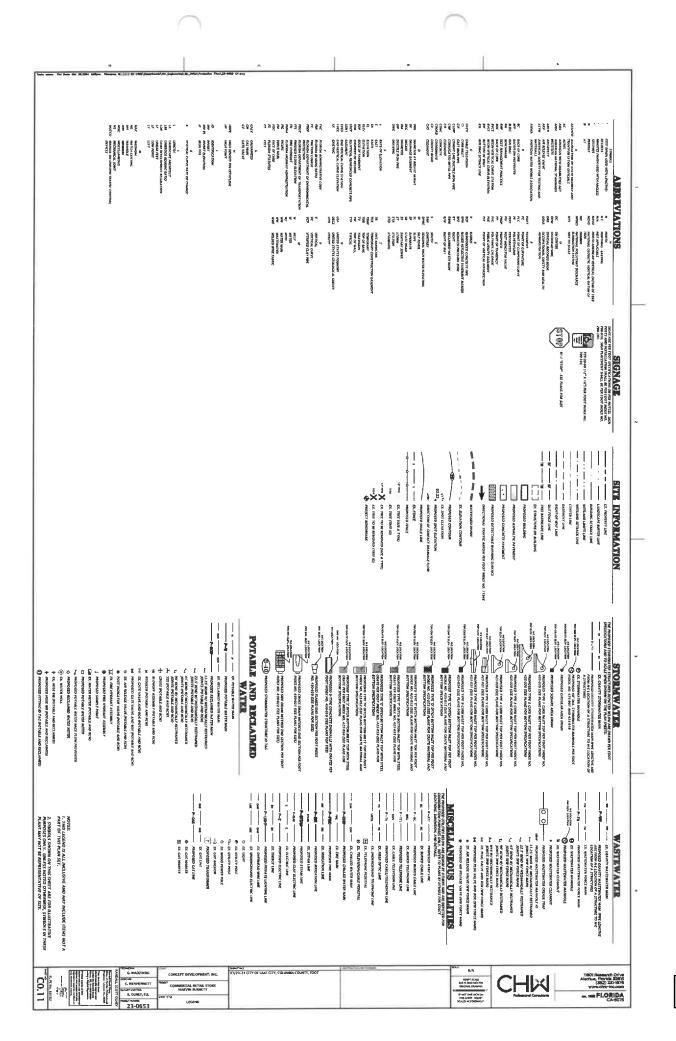






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NOTAL OR OTHER POTENTIAL POLLUTANTS

- NALL MOVIDE LITTER COLLECTION CONTAMERS INTIMU THE MOJECT ADUNDAMESS DUMBAC CONSTRUCTION. CONTRACTON SHALL DEMOSE OF ALL ALS AND CONSTRUCTION DÉBNIS IN ACCORDANCE INTIM ALL ANVILCARLE LOCAL, STATE, AND FEDERAL REQUIREMENTS.
- TT VENCUAN TRACTING OF FEDMENTS AND DUST GENERATION, A STABLEDED CONSTRUCTION BUTRANCE SHALL NE ESTAREDHED NY THE SITE ISAE SEE THE STORINWATER POLLUTION PREVENDON PLAN (CD,21) FOR BETARS AND LOTATION(S).

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статия ная сдания нау прида внерната чатет паг'осога, нау яни со итполития полото се налакоог натенал и сосос Инитита са берново тел. Лита: со соса насног такитока на истоято то тел инистрата. Трасток занид проиог а инитери нотост то тие онних инистате и прои метриалтон са лат зика.

от ракцо продот, встрене солтонныти рац. знаш не паретато от ите солтыство на гласт сомещника или нагластвова 1 май. Води листорат постояте: 1971. Трат. В от 1970. Град. 1971. 1971. От 1971. Постоят

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NUM ACTIVITY DESCRIPTIONS

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терновация от на чисточно, пристички, смощь, дом вличий соплавши лит и ком. начитичкота выш, солотиве, поляст или по на технитити, так соплатитити вызоващие при поляски, таковочно поляски поляски. Полясточи с точнит, та моличие по на тики получие при начитити во поляски, так соотко, сто защи, атехнити на м на полячитити поляски, са поляства по на тики поляски поляски поляски поляски по на поляски на на соотворитити поляски, са поляства по на поляски такова поляски поляски поляски по на поляски на соотворитити поляски сооткахистото мала бизати поляски такова поля на поляски поляски поляски поляски поляс на полячитити поляски сооткахистото мала бизатити поляски поляски поляски поляски поляски поляски поляски поляски натот поляснияти.

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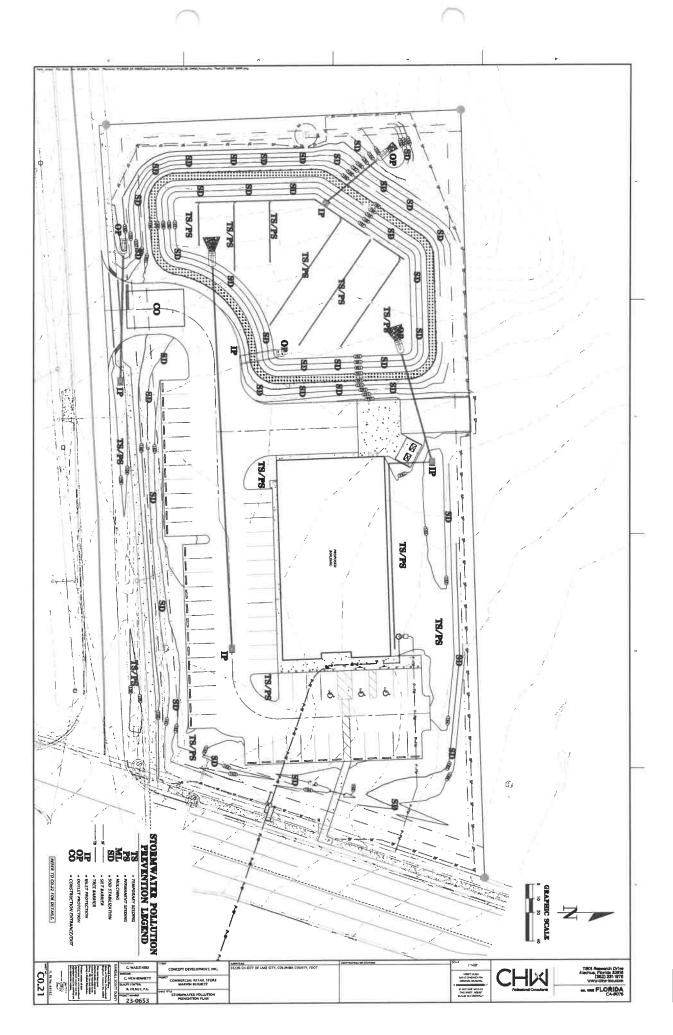
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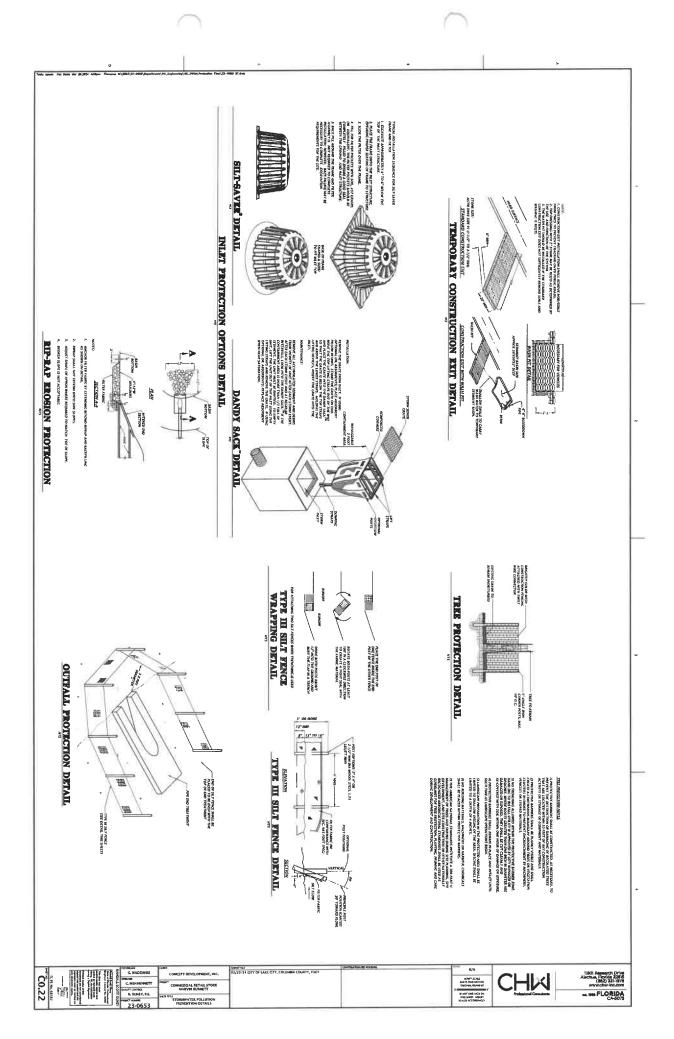
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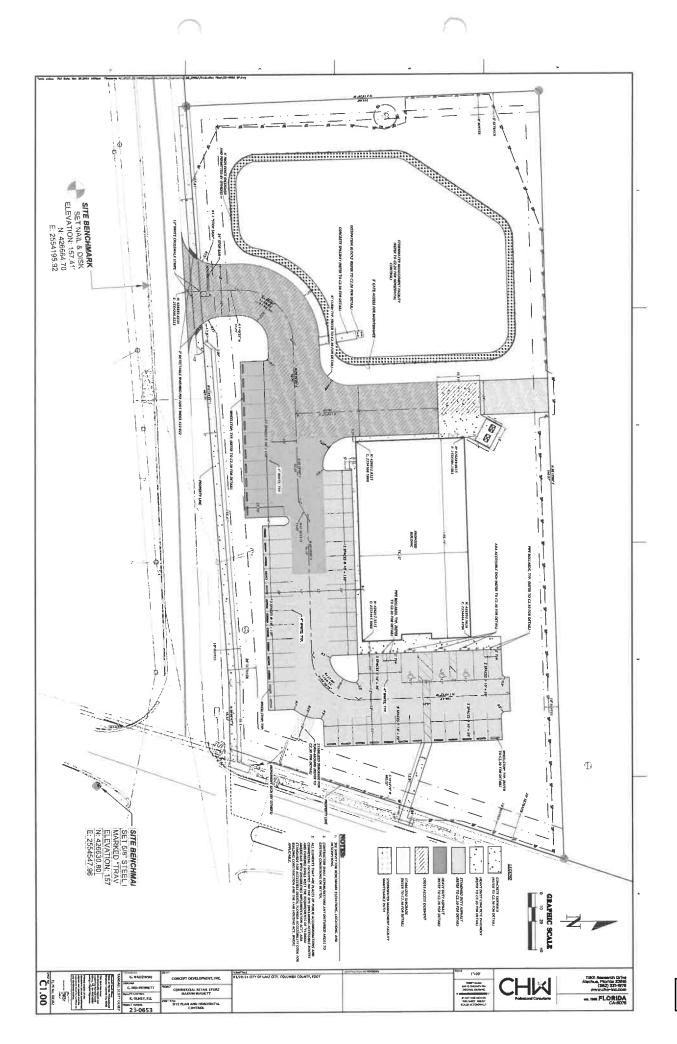
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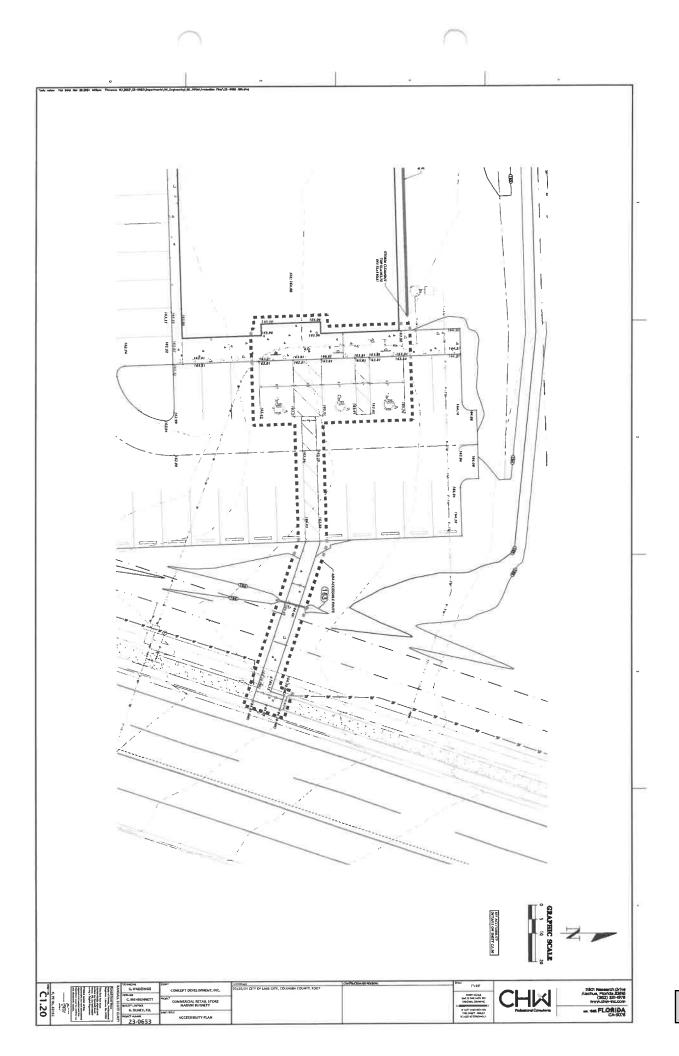
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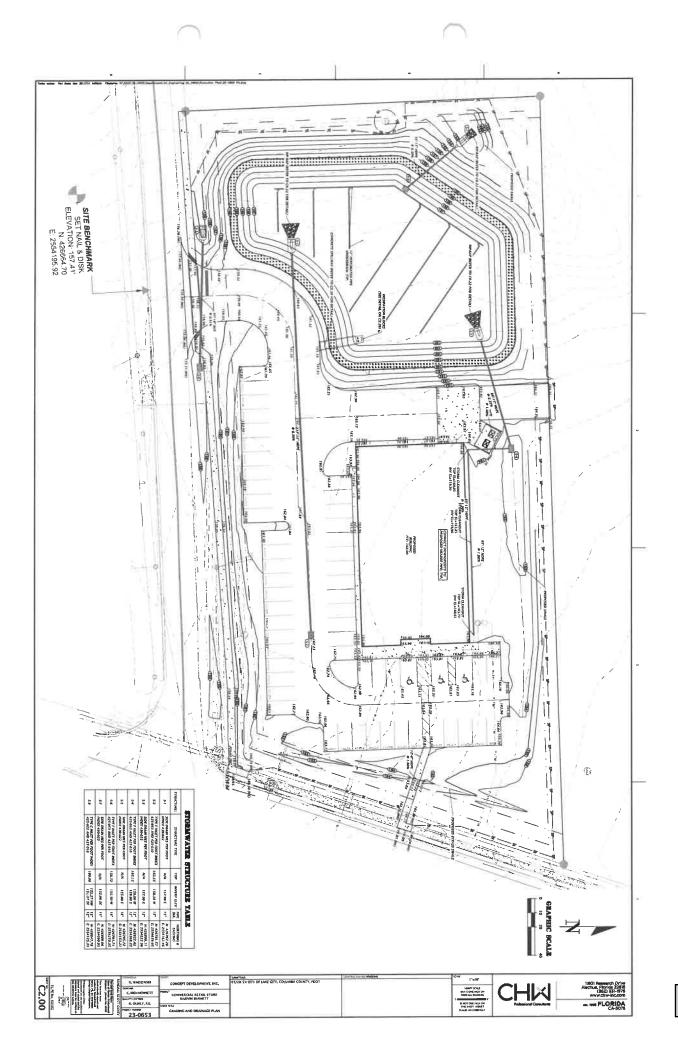


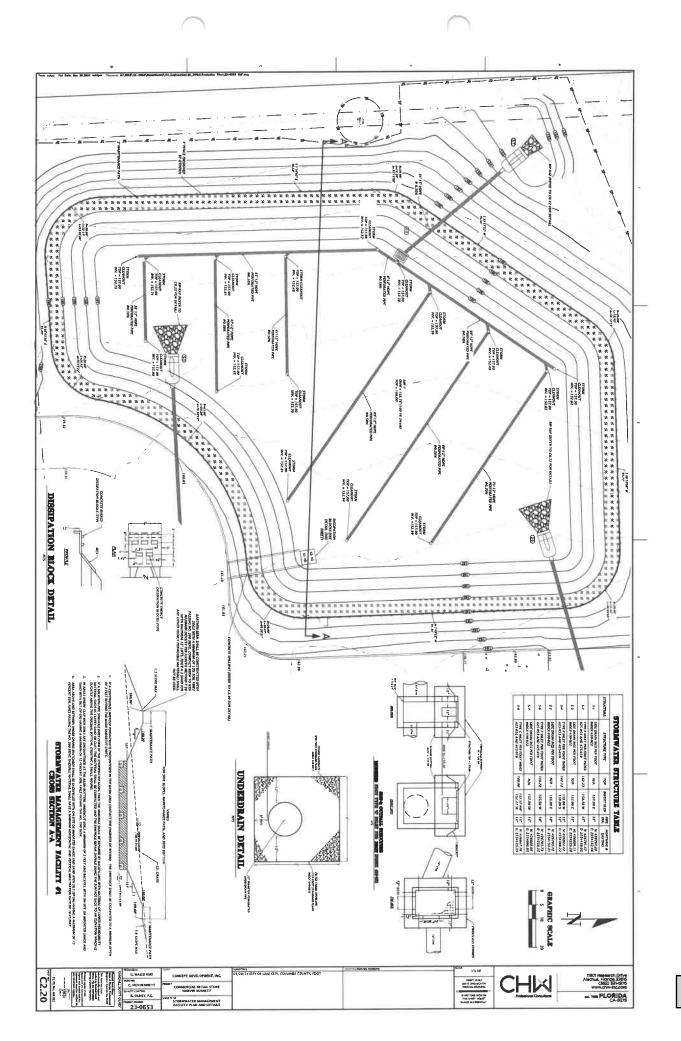


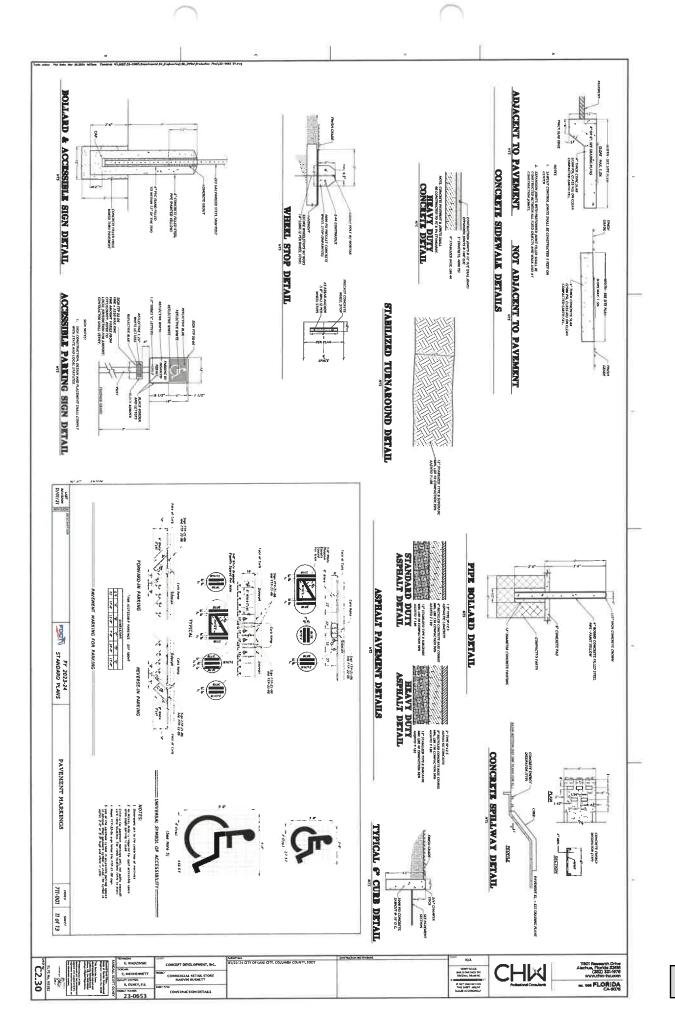


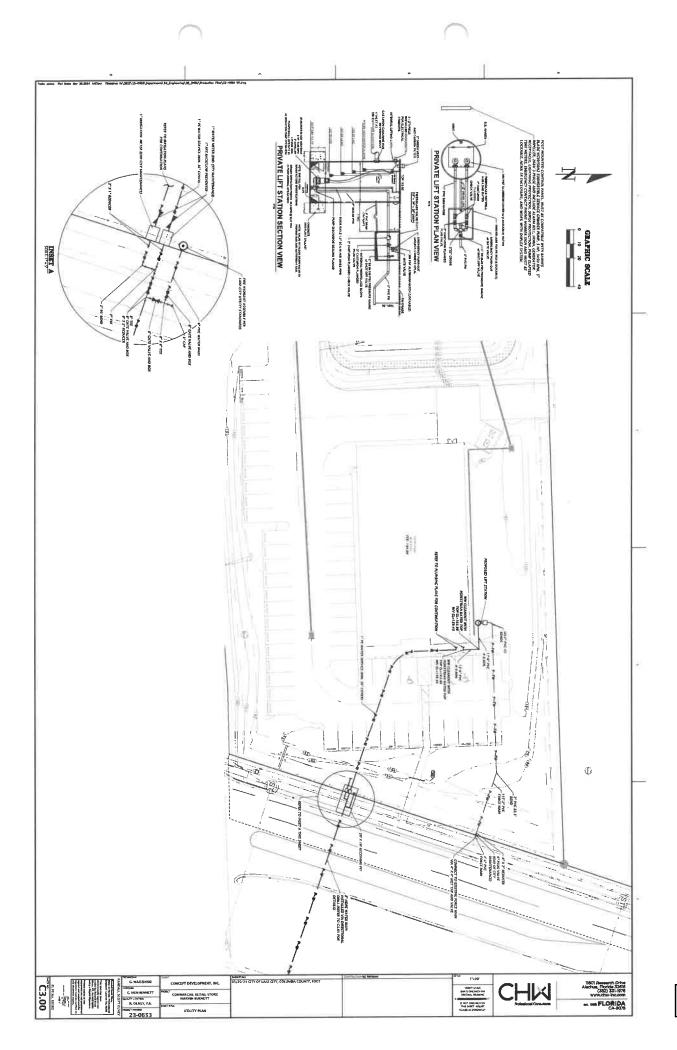


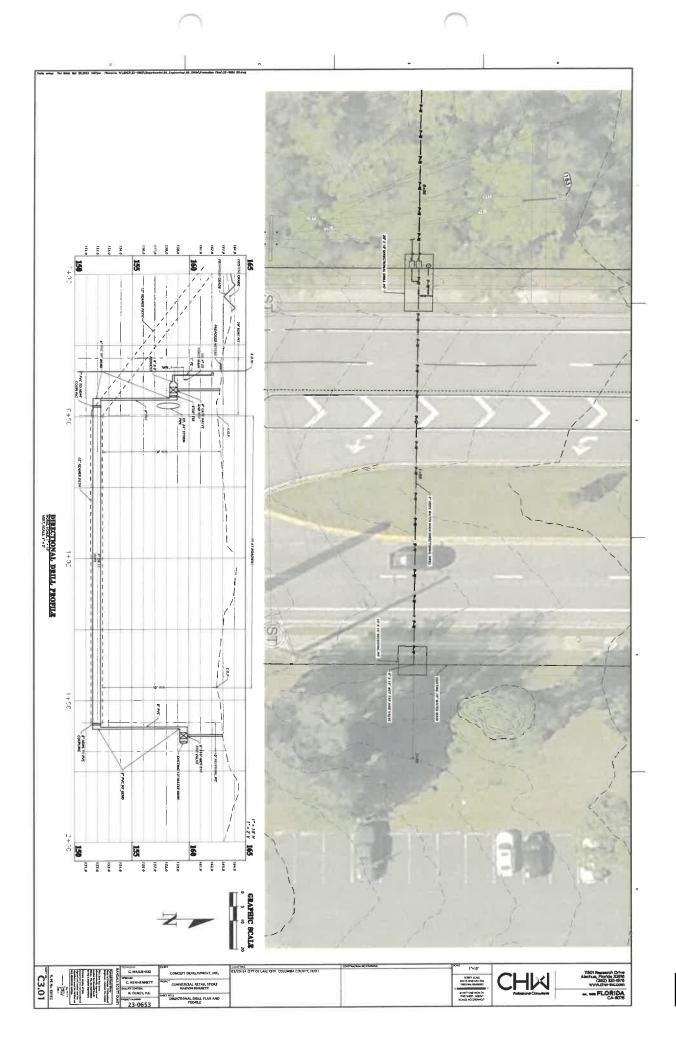


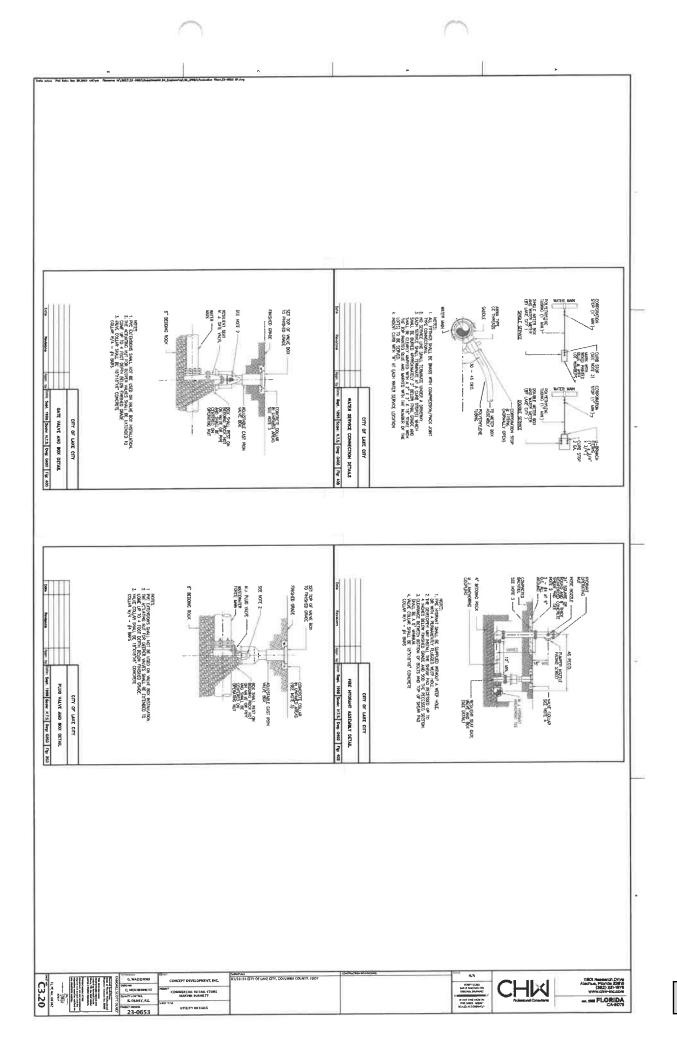


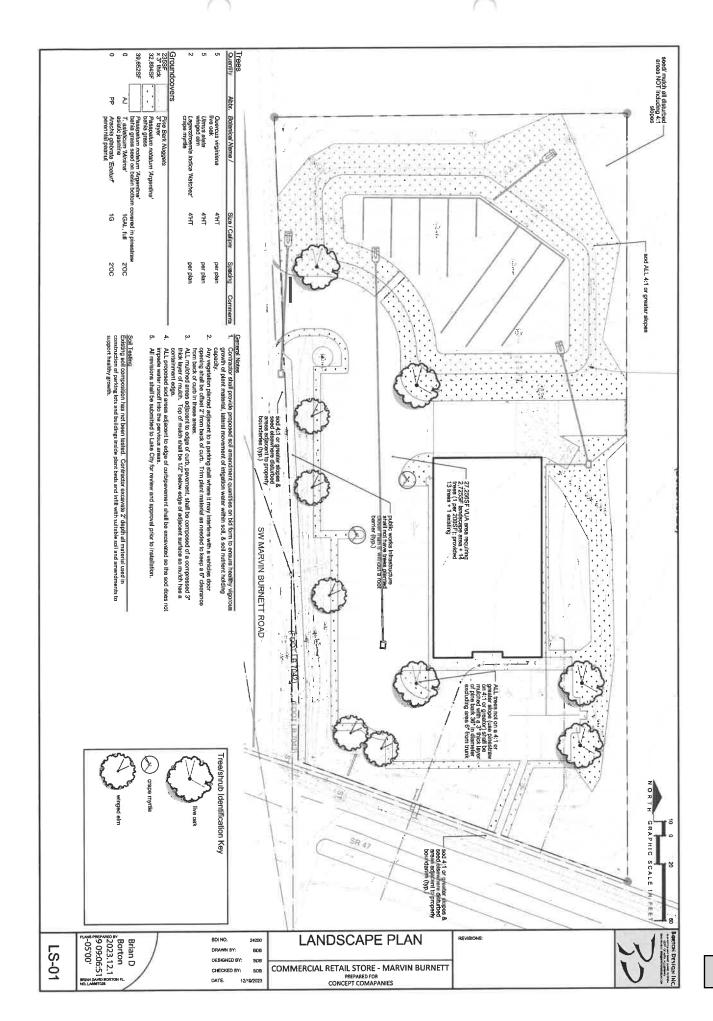


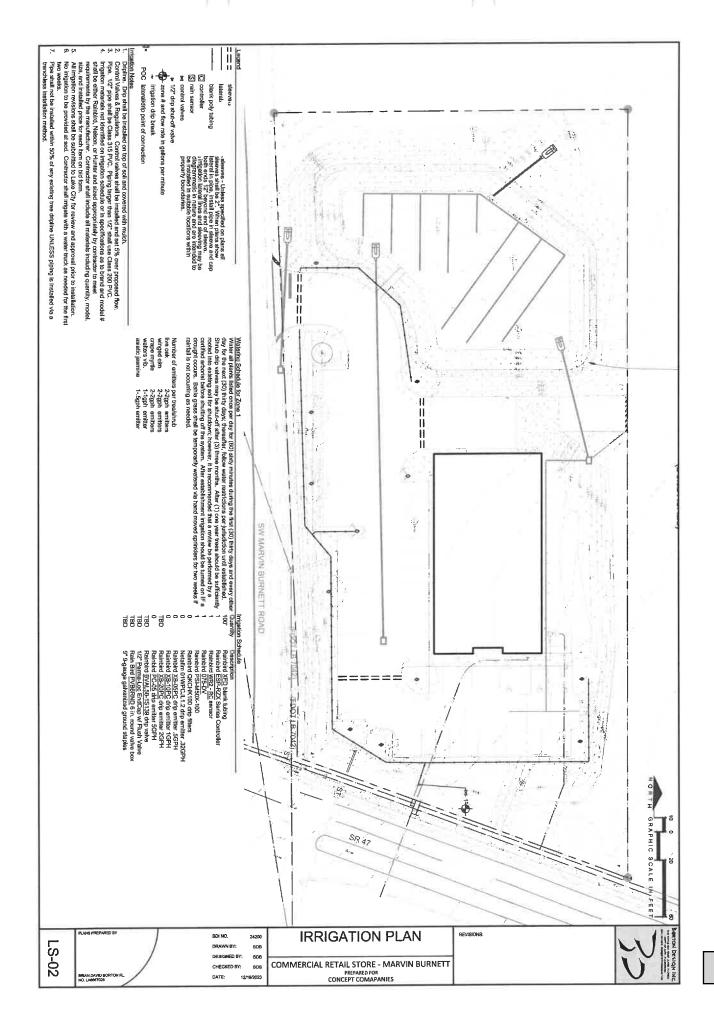


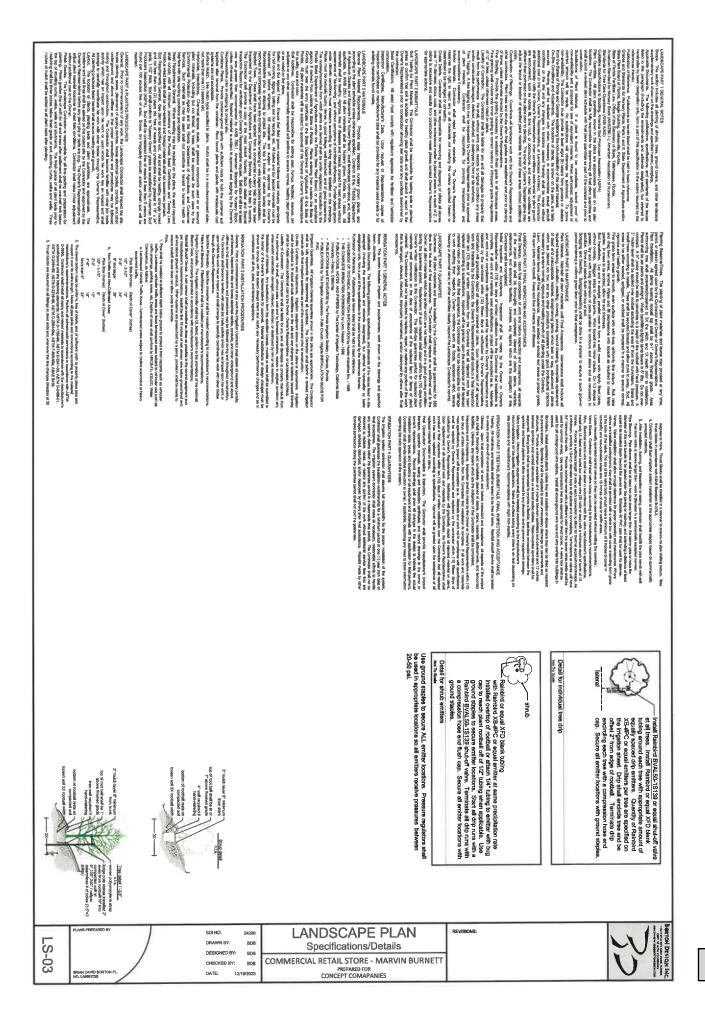


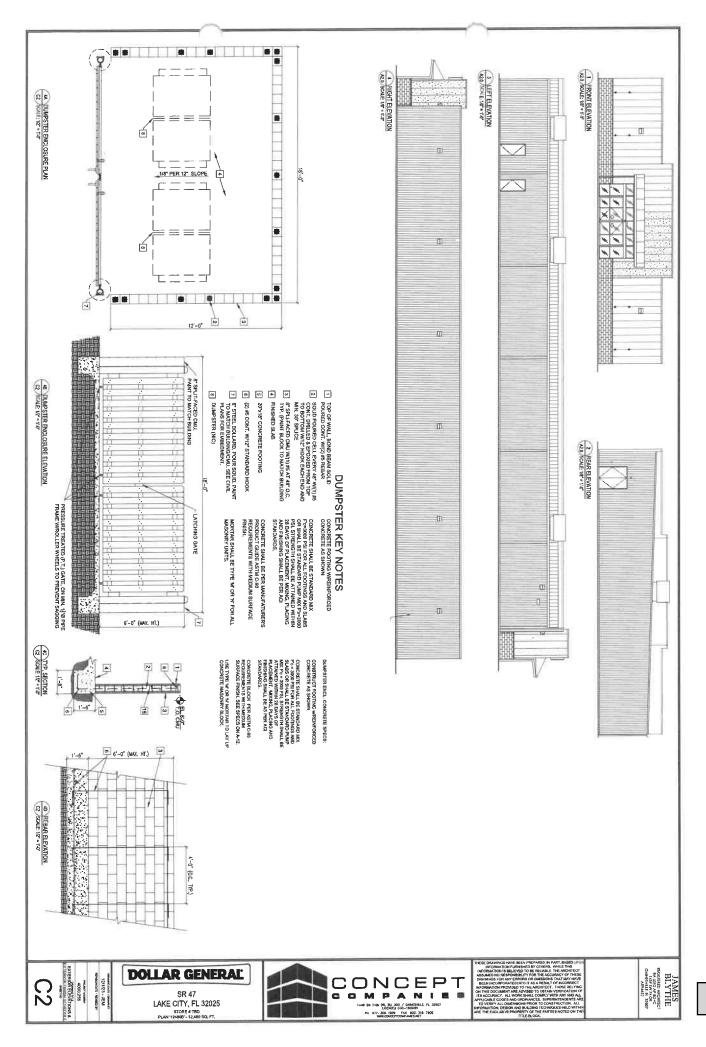














CRS Marvin Burnett 23-0653



RE:	CRS Marvin Burnett – Meter Sizing Calculations
Date:	March 20, 2024
From:	Randall Olney, P.E.
То:	The City of Lake City

The following is a calculation for meter sizing for the proposed project based on the City of Lake City Utility Standards.

CRS Marvin Burnett Building data is based on the information available from the project architect at the time of this memo. Any changes to the building data will void the provided meter sizing calculation and requires a revised analysis to verify calculations are compliant with the City of Lake City Utility Standards criteria.

PROJECT NAME:	CRS Marvin Burnett
PROJECT No.:	23-0653
FILE PATH:	N:\2023\23-0653\Departments\04_Engineering\01_Regulatory Permitting\Utilities\Meter Sizing

ADF and ADF METER SIZING CALCULATIONS

Proposed Average Daily Flow – Stores per Bat	hroom = 200 gpd p	er bath	room per FAC	C 62E-6		
Proposed Average Water Demand	2 bathrooms	Х	200 gpd		400	gpd
				Total=	400	gpd
Proposed Average Water Demand ERC (Eqv. Res Peak Water Demand ERC (PF=4) Peak Flow for Meter Sizing based on ADF (PF =		=350)			1.14 4.6 1.67	ERC ERC gpm
Peak Flow meter size per Lake City Utility Standa	ards 2010				5/8	inch

Use 5/8" Meter with 1" RPZ Backflow Preventer

	Randall Scott Olney, State of Florida, Professional Engineer, License No, 58382
Scott m, JS JO4To7	This item has been electronically signed and sealed by Randall Scott Olney, PE. On 03/21/2024 using a Digital Signature.
68382	Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

Date

OFFICES

Randall Scott Olney

Randall Olney, FL P.E. No.

03/21/2024





CRS Marvin Burnett

Private Lift Station Report 3/20/2024

Prepared for: Florida Department of Environmental Protection City of Lake City Utility Department

Prepared on behalf of:

Concept Development, Inc. 1449 SW 74th Drive. Suite 200 Gainesville, FL 32607

Prepared by: Randall S. Olney CHW

> Departing segment by Randall Soar Oney DH Eventhydigdresen.com, Celefabeli Soci Unite Official Soci Unite Celefabeli Soci Oney, Celefabeli Soci Oney, Celefabeli Soci Oney, Des 2020.13.21 15 51 59.04001

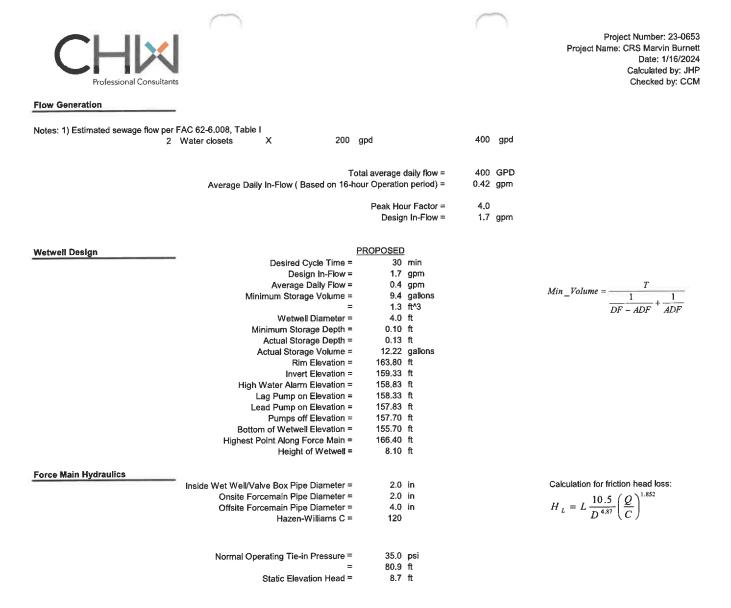
Randall Scott Olney, State of Florida, Professional Engineer, License No. 68382

This item has been electronically signed and sealed by Randall Scott Olney, PE. On 03/21/2024 using a Digital Signature.

Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

23-0653

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Project Number: 23-0653 Project Name: CRS Marvin Burnett Date: 1/16/2024 Calculated by: JHP Checked by: CCM

Equivalent Length of Straight Pipe for Fittings

Fitting Type			Equivalent Length (ft)	x	Quantity	Ē	Subtotal (ft) Eq. Length of same diam. PVC	Subtotal (ft) Eq. Length of 2 in. PVC Pipe	$L_2 = L_1 \left(\frac{D_2}{D_1}\right)^4$
nside Pump Station and Valve	2.00	in							
/ault			40		4	=	12.0	12.0	
Straight Pipe			12	x	1 2	=	6.2	6.2	
0° Bend			3.1	x	2	=	2.6	2.6	
Nug Valve			2.6	x	1	=	6.6	6.6	
ee Branch Flow			6.6	x	1	-	17.0	17.0	
Check Valve			17.0	x		-	1.5	1.5	
ate Valve			1.5	x	1	-	1.5	1,5	
nsite Forcemain	2.00	in							
traight Pipe			155	х	1	=	155.0	155.0	
2.5° Bend			1.7	х	1	=	1.7	1.7	
5° Bend			1.7	x	4	=	6.8	6.8	
0° Bend			3.1	x	0	=	0.0	0.0	
heck Valve			17.0	x	0	=	0.0	0.0	
lug Valve			2.6	x	1	=	2.6	2.6	
ffsite Forcemain (Proposed)	4.00	in							
traight Pipe	4.00		2	x	1	-	2.0	0.1	
1.25° Bend			3.5	x	0	=	0.0	0.0	
2.5° Bend			3.5	x	0	=	0.0	0.0	
5° Bend			3.5	x	0	=	0.0	0.0	
ee Branch Flow			12.0	x	1	=	12.0	0,4	
Check Valve			38.0	x	0	=	0.0	0.0	
Sate Valve			2,5	x	1	=	2.5	0.1	
NORMAL CONDITION:		Total I	Proposed Force Ma	iin Length =			(Includes leng	gth within lift sta	ition)
		Total Proposed	Effective Force Ma	in Length =	213 ft				

Out-Flow Design

Pump Run Time = Design Out-Flow = Design Out-Flow Velocity =

0.50 min 24.4 gpm 2.5 ft/s

(No less than 2.0 ft/s, No more than 8 ft/s)



Normal

CHK Professional Consultants Project Number: 23-0653 Project Name: CRS Marvin Burnett Date: 1/16/2024 Calculated by: JHP Checked by: CCM

System Performance Curve

	Operation
	(with tie-in
	pressure)
Elever (memo)	Head (ft)
Flow (gpm)	89.6
10	90.3
20	92.3
30	95.4
40	99.5
50	104.6
60	110.7
70	117.7
80	125.6
90	134.3
100	144.0
100	154.5
120	165.9
130	178.1
140	191.1
150	204.9
160	219.6
170	235.0
180	251.3
190	268.3
200	286.1
210	304.7
220	324.1
230	344.2
240	365.1
250	386.7
260	409.1
200	432.2
280	456.1
290	480,7
300	506.1
310	532.2
320	559.0
330	586.5
340	614.7
350	643.7
360	673.4
370	703,8
Burnin Cuinia	

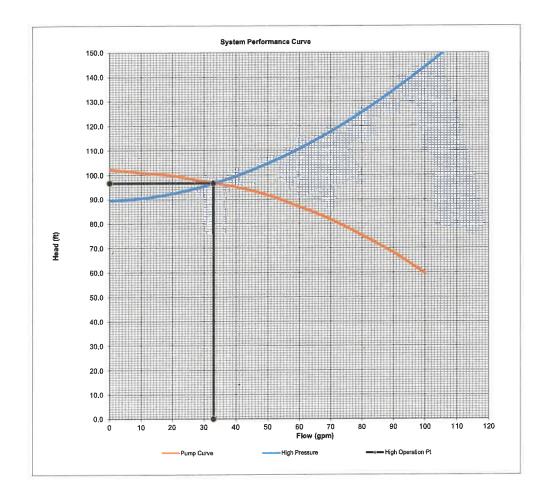
Pump Curve

One Pump - Simplex Flow (gpm)	Head (ft)
0	102.2
10	100.9
20	99.7
30	97.3
40	95,1
50	91.7
60	86,9
70	81.7
80	75.2
90	68.1
100	59.7



Project Number: 23-0653 Project Name: CRS Marvin Burnett Date: 1/16/2024 Calculated by: JHP Checked by: CCM

Pump Specifications:			
Pump: Barnes	Imp Dia:	5	
Model: NGVH50N2	Power:	5	hp
Discharge Flange Dia: 2.5"	Electrial Req:	3 Phase	
Speed: 3450	Voltage:	208	٧





Design Operation Point (1 Pump - Normal Operation)

Flow (gpm)	Velocity (fps) in 2" FM		Head (ft)	-
33.0	3.4		96.6	
System Performance at Norma Forcemain Velocity =	I Operation Design Point		3.37	ft/s
Pump Run Time =			0.37	min
Cycle Time =			29.70 0.49	min hrs
Fiberglass Wetwell				
Displaced Volume =		101.8	cf	
Unit Weight of Water =		62.4	pcf	
Weight of Displaced Water =		6,352	lb	
Bouyant Weight of Concrete = Bouyant Weight of Soil above Co	oncrete Ring =	77.60 47.60	•	
Width of Bouyancy Concrete R	ling =	1	ft	
Required Height of Bouyancy Co	encrete Ring =	1.97	ft	

Pump Run Time =	Storage Volume Design Operation Flow
Cycle Time = Storag	e Volume ADF + Pump Run Time



Specifications:

BLADE Series NGV

18 Frame

Submersible Grinder Pumps

-		
DISCHARG		
	NGV Vertical	. 2" <u>NPT</u>
	NGVH Flange	. 2'/2.50".3", Horizontal
	NGVHH Flange	. 2.50"/3", Horizontal
LIQUID TEN	IPERATURE	. 104°F (40°C) Continuous
VOLUTE		. Cast Iron ASTM A-48, Class 30
MOTOR HO	USING	. Cast Iron ASTM A-48, Class 30
SEAL PLAT	Ε	. Cast Iron ASTM A-48, Class 30
IMPELLER:	Design	. 12 Vane, Vortex, With Pump Out Vanes
		On Back Side. Dynamically Balanced,
		ISO G6.3
		. Cast Iron ASTM A-48, Class 30
SHREDDIN	G RING	. Hardened 440C Stainless Steel,
		Rockwell® C-55
CUTTER		. Hardened 440C Stainless Steel,
		Rockwell® C-55
SHAFT		. 416 Stainless Steel
SQUARE R	NGS	Buna-N
HARDWAR		. 300 Series Stainless Steel
		. Axalta™ Corlar® Epoxy, Two Coats
SEAL:	Design	. Tandem Mechanical, Oil Filled Reservoir
	Material	. Rotating Faces - Carbon
		Stationary Faces - Ceramic
		Elastomer - Buna-N
		Hardware -300 Series Stainless
CORD ENTI	₹ Υ	. Custom Molded, Quick Connected
		for Sealing and Strain Relief . CSA Certified Submersible Power
POWER CO	RD	
UPPER BE/	DINC.	Cable 2000V - Ordered Separately
		. Single Row, Ball, Oil Lubrication
	Load	
LOWER BE		. Naulai
LOWER DE		. Double Row, Ball, Oil Lubrication
	Load	Radial & Thrust
MOTOR:	Design	NEMAB
	Dooign annannann	Three Phase Torque Curve
		Oil-Filled, Squirrel Cage Induction,
		Inverter Duty rated per NEMA MG1
	Insulation	. Class H Varnish & Magnet Wire
SINGLE PH	ASE	. Requires overload protection to be
		included in control panel. Requires start
		components to be included in panel.
		Provided with pump
THREE PHA	\SE	. Requires overload protection to be
		included in control panel
MOISTURE	SENSORS	. Normally Open (N/O), Requires relay
		in control panel
TEMPERAT	URE SENSOR	. Normally Closed (N/C)
		To be wired in series with control circuit
OPTIONAL	EQUIPMENT	. Seal Material, Impeller Trims,
		Cord Length, Leg Kit, 3" Spool Kit









WARNING: CANCER AND REPRODUCTIVE HARM -WWW.P65WARNINGS.CA.GOV



PUMPS & SYSTEMS



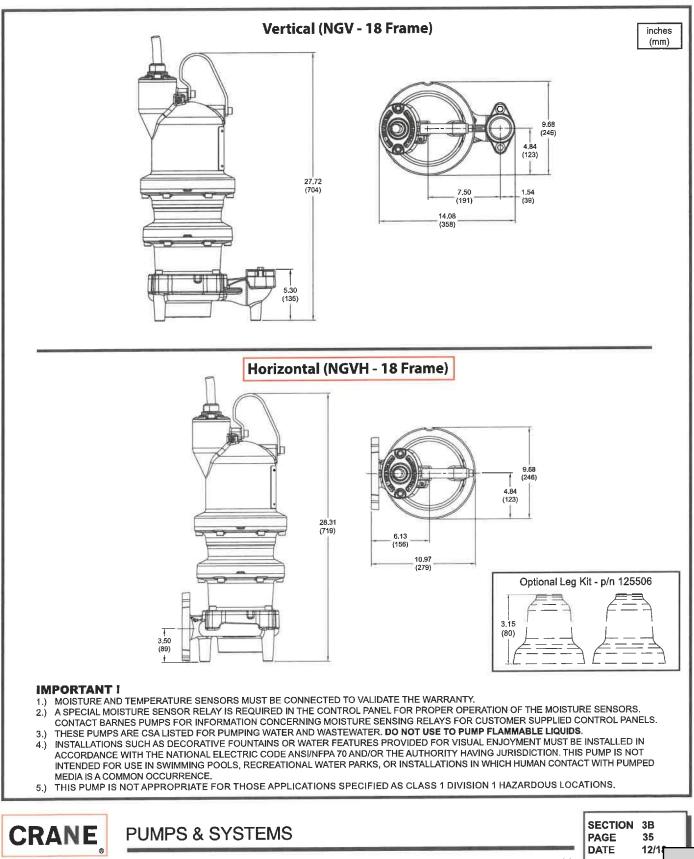
A Crane Co. Company

USA: (937) 778-8947 · Canada: (905) 457-6223 · International: (937) 615-3598





Submersible Grinder Pumps



A Crane Co. Company

USA: (937) 778-8947 · Canada: (905) 457-6223 · International: (937) 615-3598

47

BLADE Series NGJH

Horizontal



Submersible Grinder Pumps

	1	T				T						_	Т	T		
CORD O.D.	.86 ± .02		.86 ± .02		.86 ± .02		1.12 ± .02	.86 ± .02	.86 ± .02	.86 ± .02		.86 ± .02				
CORD SIZE	12/4 - 18/4		12/4 - 18/4	12/4 - 18/4	12/4 - 18/4		8/4 - 18/4	12/4 - 18/4	12/4 - 18/4	12/4 - 18/4		12/4 - 18/4	12/4 - 18/4	12/4 - 18/4		
CORD P/N A	125496		125496	125497	125497		125498	125496	125497	125497		125496	125497	125497		
DRIVER FRAME	18		18		18		18	18		18		ļ	2	18		
3 "]	113.2	131.2 85.4	95.2	47.6	38.1	113.2	131.2	85.4 95.2	47.6	38.1		173.9	201.0	80.4		
SERVICE FACTOR	1.0		1.0		1.0		1.0	1.0		1.0			0.1	10		
FULL Load Amps	25.0	12.2	12.6	6.3	5.0	34.1	29.9	17.8 16.0	8.0	6.4		28.0	28.2	11.3	d en a	
NEMA Start Code	-	M	٩		٩	ш	U	-		7			Σ	M	3 BAF. Provided with	
RPM (Nom)	3450		3450		3450		3450	3450		3450			3450	3450	d for use of a NGVH with a 3x3 e integral to power cord. at motor. XJ - 75 Feet, or XL - 100 Feet. XJ - robe included in panel. P ients to be included in panel. P	
Ř	60		60		60		60	60		80	Ì		ß	09	fa No set, or pow	
Hd	-		ო		3			ო		3			n	m	d for use o e integral t at motor. XJ - 75 Fe ients to be	
логт	208	208	230	460	575	208	230	208 230	460	575		208	230	575	nended for ads are int pltage at π Feet, XJ - omponent;	
4 H	3.0		3.0		3.0		5.0	5.0		5.0		I	c. \	7.5	sor le vv v F - 50 start c	
PART NO	141350N		141351N		141353N		141354N	141355N		141357N			141308N	141360N	ool Kit is re arature sen ation at ± 1 30 Feet, X tely. es require i	
MODEL	NGVH3072		NGVH30N2		NGVH3052		NGVH5072	NGVH50N2		NGVH5052			ZNG/HADN	NGVH7552	 NOTE: A 3" Pipe Spool Kit is recommended for use of a NGVH with a 3x3 BAF. IMPORTANT 1 Moisture and Temperature sensor leads are integral to power cord. Moisture and Temperature sensor leads are integral to power cord. Pump rated for operation at ± 10% voltage at motor. Cord Suffix: XC - 30 Feet, XJ - 75 Feet, or XL - 100 Feet. Cord sold separately. Single Phase pumpes require start components to be included in panel. Provided with pump. 	
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PUMPS & SYSTEMS

CRANE

SECTION 3B

PAGE DATE

38

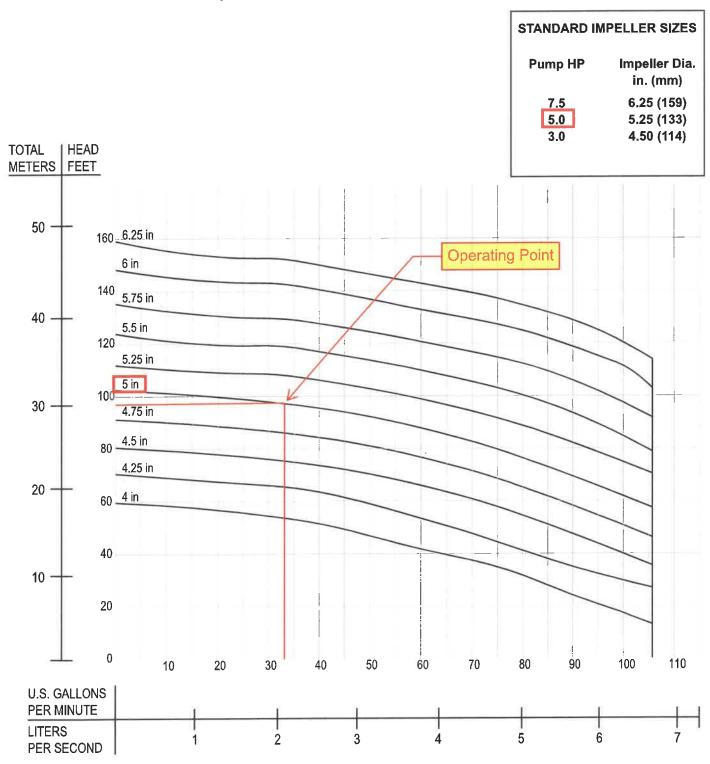
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BLADE Series NGV / NGVH

Performance Curve 3, 5 & 7.5HP, 3450RPM, 60Hz



Submersible Grinder Pumps



Testing is performed with water, specific gravity 1.0 @ 68° F @ (20°C), other fluids may vary performance

SECTION 3B PAGE 40 DATE 12/18



PUMPS & SYSTEMS

MEMORANDUM

CRS Marvin Burnett 23-0653



To:City of Lake CityFrom:Randall S. Olney, PEDate:March 20, 2024RE:CRS Marvin Burnett– Required Fire Flow

The following is a calculation for the required fire flow for the proposed project based on the NFPA 1: Fire Code.

Building data is based on the information available from the project architect at the time of this memo. Any changes to the building data will void the provided fire flow calculation and requires a revised analysis to verify the building complies with the applicable fire protection criteria. The building will not be protected by an approved automatic fire sprinkler system.

NFPA Required Flow Calculations:

Building:Commercial Retail StoreConstruction Type:II (000)Fire Flow Area:±10,640 SF

Required Fire Flow per NFPA Table 18.4.5.1.2: 2,250 gpm

Available Fire Flow:

Based on the hydrant flow data supplied by the City of Lake City, the total available fire flow at 20 PSI is as follows:

Total Available: 2,345 gpm

Minimum Required Fire Flow to be provided: 2,250 gpm

Conclusions:

The total available flow (2,345 GPM) is higher than the minimum required (2,250 GPM).

As part of this development, a new hydrant will be installed onsite.

Randall Scott Olney	Digitally signed by Randell Soch Oney DN: Evrandya@chw-inc.com, CN=Randell Soch Oney, O=Randell Soch Oney, D=Randell Soch Oney, L=Alachus, S=Floride, C=US Date: 2024.03.21 13:51 12-04000
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Date: 03/21/2024

Randall S. Olney, P.E. 68382

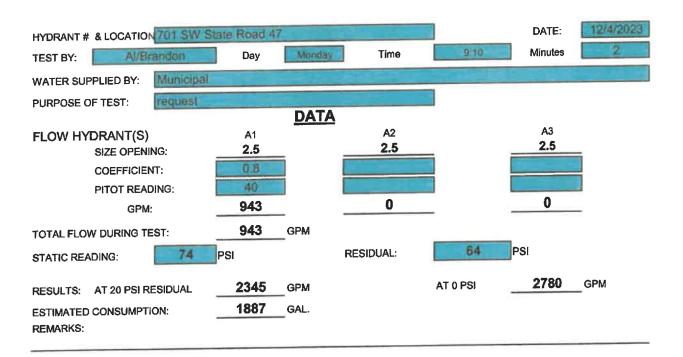
Randall Scott Olney, State of Florida, Professional Engineer, License No. 68382

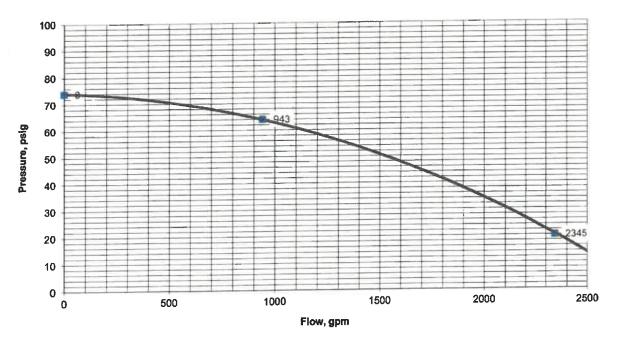
This item has been electronically signed and sealed by Randall Scott Olney, PE. On 03/21/2024 using a Digital Signature.

Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

www.chw-inc.com

City of Lake City Water flow report





	Fire Flow Arc	a ft ² (× 0.0929 for 1	n*)		Fire Flow gpm [†]	{		
I(443), I(332),		IV(2HH), V(111)*	11(000), 111(200)*	V(000)*	(x 3,785 for L/min)	Flow Duration (bours)		
11(222)*	П(111), П1(211)*	0-8200	0-5900	0-3600	1500			
022,700	0-12,700	8201-10,900	5901-7900	3601-4800	1750			
22,701-30,200	12,701-17,000		7901-9800	4801-6200 2000		2		
30,201-38,700	17,001-21,800	10,901-12,900	9801-12,600	6201-7700	2250			
38,701-48,300	21,801-24,200	12,901-17,400	12,601-15,400	7701-9400	2500	I		
48,301-59,000	24,201-33,200	17,401-21,300		9401-11,300	2750			
59,00170,900	33,201-39,700	21,301-25,500	15,401-18,400	11,301-13,400	3000			
70,901-83,700	39,701-47,100	25,501-30,100	18,401-21,800	13,401-15,600	3250	1		
83,701-97,700	47,101-54,900	30,101-35,200	21,801-25,900	15,601-18,000	3500	- 3		
97,701-112,700	54,901-63,400	35,201-40,600	25,901-29,300		3750	1		
112,701-128,700	63,401-72,400	40,601-46,400	29,301-33,500	18,001-20,600	4000			
128,701-145,900	72,401-82,100	46,401-52,500	33,501-37,900	20,601-23,300		-		
145,901-164,200	82,101-92,400	52,501-59,100	37,901-42,700	23,301-26,300	4250 .	-		
164,201-183,400	92,401-103,100	59,101-66,000	42,701-47,700	26,301-29,300		-		
183,401-203,700	103,101-114,600	66,001-73,300	47,701-53,000	29,301-32,600	4750	-		
203,701-225,200	114,601-126,700	73,301-81,100	53,001-58,600	32,601-36,000	5000	-		
	126,701-139,400	81,101-89,200	58,601-65,400	36,001-39,600	5250			
225,201-247,700	139,401-152,600	89,201-97,700	65,401-70,600	39,601-43,400	5500	_		
247,701-271,200	152,601-166,500	97,701-106,500	70,601-77,000	43,401-47,400	5750	-		
271,201-295,900	Greater than 166,500	106,501-115,800	77,001-83,700	47,401-51,500	6000	4		
Greater than 295,900	Greater man rooproo	115,801-125,500	83,701-90,600	51,501-55,700	6250	_		
		125,501-135,500		55,70160,200	6500			
	135,501-145,800		60,201-64,800	6750	_			
	145,801-156,700		64,801-69,600	7000				
	156,701-167,900		69,601-74,600	7250				
		167,901-179,400		74,601-79,800	7500	_		
		179,401-191,400		79,801-85,100	7750			
	Greater than 191,400	Greater than 138,300	Greater than 85,100	8000				

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for Buildings -.....

3

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*Types of construction are based on NFPA 220. *Measured at 20 psi (139.9 kPa).

COMPREHENSIVE PLAN CONSISTENCY ANALYSIS

CRS Marvin Burnett 23-0653

C	ЧX
P	rofessional Consultants

То:	Robert Angelo, City of Lake City Growth Management
From:	Braxton Linton III, Project Planner
Date:	December 7 th , 2023
RE:	CRS Marvin Burnett – Comprehensive Plan Consistency Analysis

This Concurrency Analysis is submitted for CRS Marvin Burnett Lake City. The proposed use is a $\pm 10,640$ -square-foot Commercial Retail Store and associated parking and stormwater. The site is on a portion of tax parcel is 07-4S-17-08127-005 in Columbia County, FL. A lot split is being completed on the site to create a 2.72-acre parcel adjacent to the intersection. One driveway connection will be to Marvin Burnett Road which is a county road. The future land use category is Commercial, and the zoning district is Commercial, Intensive (CI).

The following analysis estimates potential impacts on Lake City public facilities that may result from the proposed development. The following tables include data obtained within the City Comprehensive Plan and Florida Administrative Code (F.A.C.).

Future Land Use Element

Policy I.1.1: The location of higher density residential, high intensity commercial and heavy industrial uses shall be directed to areas adjacent to arterial or collector roads, identified on the Future Traffic Circulation Map, where public facilities are available to support such higher density or intensity.

COMMERCIAL

Lands classified as commercial use consist of areas used for the sale, rental, and Distribution of products or performance of services, as well as public, charter and private elementary, middle and high schools. In addition, off-site signs, churches and other house of worship, private clubs and lodges, residential dwelling units, which existed within this category on the date of adoption of this objective, and other similar uses compatible with commercial uses may be approved as special exceptions and be subject to an intensity of less than or equal to 0.25 floor area ratio except withing the (CG) Commercial, General, (CI) Commercial, Intensive, (C-CBD) Commercial-Central Business District and (CHI) Commercial, Highway Interchange districts being subject to intensity of less than or equal to 1.0 floor area ratio.

The proposed use, a Commercial Retail Store, is considered a retail use, which is consistent with the Commercial FLU category. Development will be consistent with standards set forth by the Commercial FLU category and CI Zoning District.

Objective I.2 The City shall adopt performance standards which regulate the location of land development consistent with topography and soil conditions and the availability of facilities and services.

The site is composed of three soils:

1. Blanton Fine Sand, 0 to 5 percent slopes (hydro group: A) N:2023/23-0653\Departments\02_Planning\Reports\RPT 2301204 Comprehensive Plan Consistency - CRS Marvin Burnett.docx

- 2. Pelham Fine Sand, 0 to 2 percent slopes (hydro group: B/D)
- 3. Ichetucknee Fine Sand, 5 to 8 percent slopes (hydro group: D)

According to the NRCS soil database, these soil types are conducive to the proposed development, which is also demonstrated on adjacent sites with similar uses and soil types.

Currently, there are no buildings located on the project site, there are developments to the north and east of the site.

Objective I.3 The City shall require that all proposed development be approved only where the public facilities meet or exceed the adopted level of service standard

Currently, there is no development on the project site. The proposed commercial retail store does not result in a degradation of Level of Service (LOS) standards, as is demonstrated in the Concurrency Impact Analysis memorandum submitted as part of this application.

Policy I.6.2 The City shall continue to include provisions for drainage, stormwater management, open space and safe and convenient on-site traffic flow including the provisions of needed vehicle parking for all development.

The proposed development will have onsite stormwater management facilities and adhere to all open space requirements set forth in Lake City's LDR. Safe and convenient on-site traffic flow will include one ingress and egress point on Marvin Burnett Road which is a county road. Parking will adhere to standards set in Lake City's LDR.

Objective I.6.5 The City shall continue to require that where a commercial or industrial use is erected or expanded on land abutting a residential district, then the proposed use shall provide a landscaped buffer. A masonry or wood opaque structure may be substituted for the planted buffer.

The subject property, specifically tax parcel 07-4S-17-08127-005, abuts a residential district to on the southwestern boundary. A landscape buffer is provided following guidelines from Lake City's LDR as shown in the landscape plan.

Transportation Element

Objective II.1: Level of Service

The City shall establish a safe, convenient, and efficient level of service standard which shall be maintained for all roadways.

The proposed Commercial Retail Store (Institute of Transportation Engineers (ITE) Land Use Code 814) will not result in a degradation of transportation Level of Service (LOS) standards. Demonstrated in the Concurrency Impact Analysis memorandum submitted as part of this application, there will be 447 net total projected daily trips.

- Policy II.1.2 The City shall control the number and frequency of connection and access points of driveways and roads to arterials and collectors by requiring access points for state roads to be in conformance with Chapter 14-96 and 14-97, Florida Administrative Code, and the following requirements for non-state roads:
 - 1. Permitting 1 access point for ingress and egress purposes to a single property or development.

The subject property includes one ingress and egress point one ingress and egress point on Marvin Burnett Road which is a county road.

Policy II.1.3 The City shall continue to require development to provide safe and convenient on-site traffic flow, which includes the provisions for vehicle parking.

Safe and convenient on-site traffic flow will be achieved by having one ingress and egress point one ingress and egress point on Marvin Burnett Road which is a county road. The parking lot will adhere to parking requirements set forth in Lake City's LDR.

Conservation Element

Policy V.5.2: Soils. The City shall protect soil resources through erosion and sedimentation control, by requiring proper design criteria on specific soils.

In an effort to conserve potable water, that at least 50 percent of the following required landscaped areas be comprised of vegetation native or indigenous to the north Florida area:

1. 10 percent of offstreet parking areas;

Parking area landscaped islands have been provided as shown in the landscape plan.

2. 10 foot buffer between residential and commercial uses;

This buffer has been provided following guidelines from Lake City's LDR as shown in the landscape plan.

3. 15 foot buffer between single family uses and multi-family uses or mobile home parks; and

Not Applicable.

4. 25 foot buffer between residential and industrial uses.

Not Applicable.

Sanitary Sewer, Solid Waste, Drainage, Potable Water and Natural Groundwater aquifer Recharge Element

- Objective IV.3: The City shall coordinate the extension of, or increase in the capacity of facilities by scheduling the completion of public sanitary sewer improvements concurrent with projected demand.
- Policy IV.3.1: The City hereby establishes the following Level of Service standards for sanitary sewer facilities:

FACILITY TYPE City of Lake City Community Sanitary Sewer System LEVEL OF SERVICE STANDARD 135 gallons per capita per day

The proposed development will allow a use of $\pm 10,640$ sq. ft. of nonresidential use. As is demonstrated in the Concurrency Impact Analysis submitted as part of this application, this facility is estimated to use 1,064 Gallons Per day by the proposed use.

- Objective IV.4: The City shall continue to coordinate the extension of, or increase in the capacity of solid waste facilities by scheduling the completion of public facility improvements and requiring that they are concurrent with projected demand.
- Policy IV.4.1: The City hereby establishes the following level of service standards for solid waste disposal facilities:

FACILITY TYPE	LEVEL OF SERVICE STANDARD
Solid Waste Landfill	.85 tons per capita per year
	Residual capacity of landfill

The proposed development will allow a use of $\pm 10,640$ sq. ft. of nonresidential use. As is demonstrated in the Concurrency Impact Analysis submitted as part of this application, this facility is estimated to use 233.02 lbs./day and 42.53 tons/year.

- Objective IV.6: The City shall continue to coordinate the extension of, or increase in the capacity of potable water facilities by scheduling the completion of public facility improvements and requiring that they are concurrent with projected demand.
- Policy IV.4.1: The City hereby establishes the following level of service standards for potable water.

FACILITY TYPE City of Lake City LEVEL OF SERVICE STANDARD 150 gallons per capita per day Residual capacity of landfill

The proposed development will allow a use of $\pm 10,640$ sq. ft. of nonresidential use. As is demonstrated in the Concurrency Impact Analysis submitted as part of this application, this facility is estimated to use 1,064 Gallons Per day by the proposed use.

CONCURRENCY ANALYSIS

CRS Marvin Burnett 23-0653



То:	Robert Angelo, City of Lake City Growth Management
From:	Braxton Linton III, Project Planner
Date:	December 7 th , 2023
Re:	CRS Marvin Burnett – Concurrency Impact Analysis

This Concurrency Analysis is submitted for CRS Marvin Burnett Lake City. The proposed use is a $\pm 10,640$ -square-foot Commercial Retail Store and associated parking and stormwater. The site is on a portion of tax parcel is 07-4S-17-08127-005 in Columbia County, FL. A lot split is being completed on the site to create a 2.72 acre parcel adjacent to the intersection. One driveway connection will be to Marvin Burnett Road which is a county road. The future land use category is Commercial, and the zoning district is Commercial, Intensive (CI).

The following analysis estimates potential impacts on Lake City public facilities that may result from the proposed development. The following tables include data obtained within the City Comprehensive Plan and Florida Administrative Code (F.A.C.).

Roadways / Transportation

Trip generation figures are based on the Institute of Transportation Engineers (ITE) Trip Generation Manual, 11th Edition.

Table 1: Projected Trip Generation

Land Use ¹ (ITE)		Variable KSF Daily Total	AM Peak			PM Peak		
	Variable KSF		Total	In	Out	Total	In	Out
Variety Store (ITE 814)	10.640	677	32	18	14	71	36	35
Pass-by Rate:	= 34%*	230	11	6	5	24	12	12
Net Total Proje	ect Trips	447	21	12	9	47	24	23

1. Source: ITE Trip Generation 11th Edition

* The IT Trip Generation Manual, 11th Edition provides a pass-by rate of 34% during the PM peak but does not provide a pass-by rate for the AM and daily conditions, therefore, a pass-by rate of 34% is applied to the AM and daily scenarios.

Conclusion: Approval of this application may generate **447** daily vehicle trips. This is not anticipated to negatively impact the adopted LOS for adjacent and nearby roadways.

Potable Water / Sanitary Sewer / Solid Waste

Table 2: Projected Potable Water Impacts

Land Use	Maximum Units	Gallons Per Day ¹	Estimated Demand (GPD)
Shopping center without food or laundry	10,640	.01 gallons / sq. ft. / day	1,064

1. Source: Ch. 62E-6.008, Table 1, Florida Administrative Code

Conclusion: The project site will be served by the existing Lake City potable water infrastructure. The subject property is served by Lake City's potable water, and it's anticipated to generate 1,064 Gallons per day.

Table 3: Projected Sanitary Sewer Impacts

Land Use	Maximum Units	Gallons Per Day ¹	Estimated Demand (GPD)
Shopping center without food or laundry	10,640	.01 gallons / sq. ft. / day	1,064

1. Source: Ch. 62E-6.008, Table 1, Florida Administrative Code

Conclusion: The project site will be served by the existing Lake City wastewater infrastructure. The subject property is served by Lake City's sanitary sewer, and it's anticipated to generate 1,064 Gallons per day.

Table 4: Projected Solid Waste Impacts

Land Use	Units	Solid Waste Generated (Ibs/day) ¹	Solid Waste Generated (tons/year) ²
Nonresidential	10,640 sq. ft.	233.02	42.53

1. Formulas per Sincero and Sincero, Environmental Engineering: A Design Approach. Prentice Hall, New Jersey, 1996. a. Formula used, nonresidential: (((12 lbs. / 1,000 sq. ft./day * [10,640 sq. ft.]) * 365)/2,000)

Formula used, pounds per day to tons per year: ([lbs/day] * 0.005) * 365

Conclusion: Solid waste facility capacity exists to adequately serve the intended office development for the subject property. The subject property is served by Lake City's solid waste, and it's anticipated to generate 233.02 pounds per day and 42.53 tons per year.



GSE Engineering & Consulting, Inc.

SUMMARY REPORT OF A GEOTECHNICAL SITE EXPLORATION – REVISION 1

DOLLAR GENERAL – LAKE CITY SW MARVIN BURNETT LAKE CITY, COLUMBIA COUNTY, FLORIDA

GSE PROJECT NO. 16251

Prepared For:

CONCEPT DEVELOPMENT, INC.

DECEMBER 2023



December 7, 2023

Andrea Barnett Concept Development, Inc. 1449 SW 74th Drive, Suite 200 Gainesville, Florida 32607

Subject: Summary Report of a Geotechnical Site Exploration – Revision 1 **Dollar General – Lake City SW Marvin Burnett** Lake City, Columbia County, Florida GSE Project No. 16251

GSE Engineering & Consulting, Inc. (GSE) is pleased to submit this geotechnical site exploration report for the above referenced project.

Presented herein are the findings and conclusions of our exploration, including the geotechnical parameters and recommendations to assist with building foundation, pavement, and stormwater management designs. This revision includes recommended soil parameters for stormwater management design with underdrains.

GSE appreciates this opportunity to have assisted you on this project. If you have any questions or comments concerning this report, please contact us.

Sincerely,

GSE Engineering & Consulting, Inc.

Angelina X. Liu, E.I. Staff Engineer





on the date adjacent to the seal. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

Jason E. Gowland, P.E. Principal Engineer Florida Registration No. 66467

AXL / JEG: tlf Q:\Projects\16251 Dollar General – Lake City SW Marvin Burnett\16251 Rev.1.docx

Distribution: Addressee (1 - Electronic) File (1)

> GSE Engineering & Consulting, Inc. 5590 SW 64th Street, Suite B Gainesville, Florida 32608 (352) 377-3233 Phone * (352) 377-0335 Fax www.gseengineering.com

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- 1. Project Site Location Map
- 2. Site Plan Showing Approximate Locations of Field Tests

1.0 INTRODUCTION

1.1 General

GSE Engineering & Consulting, Inc. (GSE) has completed this geotechnical exploration for the proposed commercial retail store located on SW Marvin Burnett Road in Lake City, Columbia County, Florida. This exploration was performed in accordance with GSE Proposal No. 2023-589 dated September 12, 2023. Ms. Andrea Barnett authorized our services on September 15, 2023.

1.2 Project Description

We understand that you are coordinating due diligence related work related to the development of this site into a commercial retail store. The site is located on the northwest corner of the State Road 47 and SW Marvin Burnett Road intersection in Lake City, Columbia County, Florida. The site is approximately +/-2.72 acres.

You provided GSE with information about the project. We understand the project will consist of an approximate 10,640 square foot building, a parking lot, and a stormwater management facility.

The structure is expected to be a single-story, high wall concrete masonry unit (CMU) and steel frame construction. Structural loads have not been provided but are expected to be on the order of 1 to 2 kips per foot for non-load bearing CMU walls, and less than 50 kips for columns. The finished floor of the structure is anticipated to be constructed within 1 to 2 feet of the existing site grades.

The building will be located in the northern portion of the site. The parking lot will be located west, south, and east of the structure. The stormwater management facility will be located on the western portion of the site.

A recent aerial photograph of the site was obtained and reviewed. The site plan and aerial photograph were used in preparation of this exploration and report.

1.3 Purpose

The purpose of this geotechnical exploration was to determine the general subsurface conditions, evaluate these conditions with respect to the proposed construction, and prepare geotechnical parameters and recommendations to assist with building foundation, stormwater management, and pavement designs.

2.0 FIELD AND LABORATORY TESTS

2.1 General Description

The procedures used for field sampling and testing are in general accordance with industry standards of care and established geotechnical engineering practices for this geographic region. This exploration consisted of performing five (5) Standard Penetration Test (SPT) borings to a depth of 20 feet below land surface (bls) within the proposed building area, five (5) auger borings to a depth of 5 feet bls in the area of the parking lot and driveways, and five (5) auger borings to depths of 15 feet bls in the area of the stormwater management facility.

The soil borings were performed at the approximate locations as shown on Figure 2. The borings were located at the site using the provided site plan, Global Positioning System (GPS) coordinates, and obvious site features as reference. The boring locations should be considered approximate. The soil borings were performed on September 20, 2023.

2.2 Auger Borings

The auger borings were performed in accordance with ASTM D1452. The borings were performed with flight auger equipment that was rotated into the ground in a manner that reduces soil disturbance. After penetrating to the required depth, the auger was retracted and the soils collected on the auger flights were field classified and placed in sealed containers. Representative samples of each stratum were retained from the auger boring. Results from the auger borings are provided in Section 5.1.

2.3 Standard Penetration Test Borings

The soil borings were performed with a drill rig employing mud rotary drilling techniques and Standard Penetration Testing (SPT) in accordance with ASTM D1586. The SPTs were performed continuously to 10 feet and at 5-foot intervals thereafter. Soil samples were obtained at the depths where the SPTs were performed. The soil samples were classified in the field, placed in sealed containers, and returned to our laboratory for further evaluation.

After drilling to the sampling depth, the standard two-inch O.D. split-barrel sampler was seated by driving it 6 inches into the undisturbed soil. The sampler was then driven an additional 12 inches by blows of a 140-pound hammer falling 30 inches. The number of blows required to produce the next 12 inches of penetration were recorded as the penetration resistance (N-value). These values and the complete SPT boring logs are provided in Section 5.2.

Upon completion of the sampling, the boreholes were abandoned in accordance with Water Management District guidelines.

2.4 Soil Laboratory Tests

The soil samples recovered from the soil borings were returned to our laboratory, and examined to confirm the field descriptions. Representative samples were then selected for laboratory testing. The laboratory tests consisted of nine (9) percent soil fines passing the No. 200 sieve, nine (9) natural moisture content determinations, two (2) Atterberg Limits tests, and three (3) constant head hydraulic conductivity tests. These tests were performed in order to aid in classifying the soils and to further evaluate their engineering properties. The laboratory tests are provided in Section 5.3.

3.0 FINDINGS

3.1 Surface Conditions

Karen Roylos with GSE visited the site on September 18, 2023 to observe the site conditions and mark the boring locations. Mr. Jason Kite with Jason Kite, LLC was retained by GSE to clear lanes to allow access to the boring locations for drilling equipment.

The majority of the site is densely vegetated with trees, scattered saw palmettos, shrubs, vines and weedy groundcover. Portions of the site were densely vegetated and more difficult to traverse. To the south of the site is SW Marvin Burnett Road. State Road 47 is located east of the site. Undeveloped wooded land borders the site to the north and west.

The topography at the site is moderately sloping from northeast towards southwest. Regional topography can be characterized as gently to moderately sloping. The Lake City West USGS Topographic Map indicates the ground surface elevations at the site are near 155 to 165 feet¹ NAVD 88.

3.2 Subsurface Conditions

The locations of the auger and SPT borings are provided on Figure 2. Complete logs for the borings are provided in Sections 5.1 and 5.2. Descriptions for the soils encountered are accompanied by the Unified Soil Classification System symbol (SM, SP-SM, etc.) and are based on visual examination of the recovered soil samples and the laboratory tests performed. Stratification boundaries between the soil types should be considered approximate, as the actual transition between soil types may be gradual.

The auger borings located within the proposed parking lot and driveways encountered relatively similar soil conditions. Auger borings A-1 to A-3 encountered poorly graded sand, and sand with silt (SP, SP-SM) to the explored depths of 5 feet bls. Auger borings A-4 and A-5 initially encountered sand with silt (SP-SM) to depths of 1.5 to 3.5 feet bls. This was underlain by clayey to very clayey sand (SC, SC/CL) to the explored depths of 5 feet bls.

The auger borings located within the stormwater management facility encountered relatively consistent soil conditions. Auger boring P-1 encountered 6 feet of silty sand, and poorly graded sand (SM, SP) overlying clayey to very clayey sand, and clay with sand (SC, SC/CL, CL/CH) to the explored depth of 15 feet bls. Auger borings P-2 to P-4 initially encountered poorly graded sand, sand with silt, and silty sand (SP, SP-SM, SM) to depths of 2 to 5 feet bls, overlying silty clayey sand, and clayey to very clayey sand (SM-SC, SC, SC/CL) to depths of 7 to 10.5 feet bls. This was underlain by sand with silt (SP-SM) to depths of 12 to 13.5 feet bls, followed by clayrich soils (CL/CH) to the explored depth of 15 feet of sand with silt (SP-SM) overlying clay with sand (CL/CH) to a depth of 12.5 feet bls. This was underlain by sand with silt (SP-SM) to the explored depth of 15 feet bls.

¹ United States Geological Survey, Lake City West Quadrangle, 2021.

The SPT borings located within the proposed building footprint indicate the soils across these areas are relatively consistent. SPT boring B-1 initially encountered 3 feet of sand with silt (SP-SM), and 4.5 feet of sandy clay (CL) overlying sand with clay, and poorly graded sand (SP-SC, SP) to a depth of 12 feet bls. This was underlain by clay (CL/CH) to the explored depth of 20 feet bls. SPT borings B-2 to B-5 encountered poorly graded sand, sand with silt, sand with clay, silty sand, and silty clayey sand (SP, SP-SM, SP-SC, SM-SC) with some interbedded layers of clayey to very clayey sand (SC, SC/CL) to depths of 13.5 to 17.5 feet bls. This was underlain by clay-rich (CL, CL/CH) soils to the explored depths of 20 feet bls.

The sandy soils (SP, SP-SM, SP-SC) encountered are generally in a very loose to dense condition with N-values ranging from 2 to 45 blows per foot. The silty sand, silty clayey sand, and clayey to very clayey sands (SM, SM-SC, SC, SC/CL) encountered are generally in a very loose to dense condition with N-values ranging from 4 to 38 blows per foot. The sandy clay, clay with sand, and clay (CL/CH, CL) encountered are generally in a very soft to hard condition with N-values ranging from 3 to 33 blows per foot.

Weight-of-rod strength material was encountered in SPT boring B-2 at depth range from 13.5 to 14.5 feet bls. This isolated occurrence is likely related to depositional characteristics of the soil materials and transitions between material types.

The groundwater table was encountered in the auger and SPT borings at depths of 6.1 to 8.8 feet bls at the time of our investigation.

3.3 Review of Published Data

The majority of the site is mapped as three soil series by the Soil Conservation Service (SCS) Soil Survey for Columbia County². The following soil descriptions are from the Soil Survey.

Blanton fine sand, 0 to 5 percent slopes

Map Unit Setting

- *National map unit symbol:* 2w0q2
- Elevation: 30 to 200 feet
- Mean annual precipitation: 51 to 59 inches
- Mean annual air temperature: 64 to 72 degrees F
- *Frost-free period:* 258 to 310 days
- Farmland classification: Not prime farmland

Map Unit Composition

- Blanton and similar soils: 85 percent
- Minor components: 15 percent
- Estimates are based on observations, descriptions, and transects of the map unit.

² Soil Survey of Hamilton County, Florida. Soil Conservation Service, U.S. Department of Agriculture.

Description of Blanton

Setting

- Landform: Knolls on marine terraces, ridges on marine terraces
- Landform position (two-dimensional): Backslope
- Landform position (three-dimensional): Side slope, interfluve, riser
- *Down-slope shape:* Convex
- Across-slope shape: Linear
- Parent material: Sandy and loamy marine deposits

Typical profile

- A 0 to 7 inches: fine sand
- E 7 to 52 inches: fine sand
- Bt 52 to 80 inches: fine sandy loam

Properties and qualities

- *Slope:* 0 to 5 percent
- Depth to restrictive feature: More than 80 inches
- Drainage class: Moderately well drained
- Runoff class: Negligible
- Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 6.00 in/hr)
- Depth to water table: About 42 to 72 inches
- Frequency of flooding: None
- Frequency of ponding: None
- Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
- Sodium adsorption ratio, maximum: 4.0
- Available water supply, 0 to 60 inches: Low (about 3.6 inches)

Interpretive groups

- Land capability classification (irrigated): None specified
- Land capability classification (nonirrigated): 3s
- Hydrologic Soil Group: A
- Forage suitability group: Sandy soils on rises, knolls, and ridges of mesic uplands (G138XA121FL)
- Other vegetative classification: Sandy soils on rises, knolls, and ridges of mesic uplands (G138XA121FL)
- *Hydric soil rating:* No

Minor Components

Albany

- Percent of map unit: 6 percent
- Landform: Ridges on marine terraces
- Landform position (two-dimensional): Shoulder
- Landform position (three-dimensional): Interfluve, talf
- Down-slope shape: Convex
- Across-slope shape: Linear
- Other vegetative classification: Sandy soils on rises and knolls of mesic uplands (G138XA131FL), North Florida Flatwoods (R138XY004FL)
- Hydric soil rating: No

Troup

- *Percent of map unit:* 4 percent
- Landform: Ridges, knolls
- Landform position (two-dimensional): Summit
- Landform position (three-dimensional): Interfluve
- *Down-slope shape:* Convex
- Across-slope shape: Linear
- Other vegetative classification: Sandy soils on ridges and dunes of xeric uplands (G133AA111FL), Longleaf Pine-Turkey Oak Hills (R133AY002FL)
- Hydric soil rating: No

Chipley

- Percent of map unit: 3 percent
- *Landform:* Knolls on marine terraces, rises on marine terraces, flats on marine terraces
- Landform position (two-dimensional): Shoulder, footslope
- Landform position (three-dimensional): Interfluve
- Down-slope shape: Convex
- Across-slope shape: Linear
- Other vegetative classification: Sandy soils on rises and knolls of mesic uplands (G138XA131FL)
- *Hydric soil rating:* No

Alpin

- Percent of map unit: 2 percent
- *Landform:* Flatwoods on marine terraces, knolls on marine terraces, ridges on marine terraces
- Landform position (two-dimensional): Shoulder, backslope
- Landform position (three-dimensional): Interfluve
- Down-slope shape: Convex
- Across-slope shape: Linear
- Other vegetative classification: Sandy soils on ridges and dunes of xeric uplands (G138XA111FL), Sand Pine Scrub (R153AY001FL)
- Hydric soil rating: No

Ichetucknee fine sand, 5 to 8 percent slopes

Map Unit Setting

- National map unit symbol: vrt4
- Elevation: 330 to 660 feet
- *Mean annual precipitation:* 50 to 58 inches
- Mean annual air temperature: 64 to 72 degrees F
- *Frost-free period:* 258 to 288 days
- *Farmland classification:* Not prime farmland

Map Unit Composition

- Ichetucknee and similar soils: 80 percent
- Minor components: 20 percent
- Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Ichetucknee

Setting

- Landform: Hills on marine terraces, ridges on marine terraces
- Landform position (three-dimensional): Interfluve, side slope
- *Down-slope shape:* Convex
- Across-slope shape: Linear
- Parent material: Sandy and clayey marine deposits over limestone

Typical profile

- A 0 to 4 inches: fine sand
- *E 4 to 7 inches:* fine sand
- Bg 7 to 75 inches: clay
- 2*R* 75 to 79 inches: weathered bedrock

Properties and qualities

- *Slope:* 5 to 8 percent
- Depth to restrictive feature: 50 to 75 inches to lithic bedrock
- Drainage class: Somewhat poorly drained
- Runoff class: Negligible
- Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
- Depth to water table: About 18 to 36 inches
- Frequency of flooding: None
- Frequency of ponding: None
- Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
- Sodium adsorption ratio, maximum: 4.0
- Available water supply, 0 to 60 inches: Moderate (about 8.4 inches)

Interpretive groups

- Land capability classification (irrigated): None specified
- Land capability classification (nonirrigated): 6e
- Hydrologic Soil Group: D
- Forage suitability group: Loamy and clayey soils on rises, knolls, and ridges of mesic uplands (G138XA322FL)
- Other vegetative classification: Loamy and clayey soils on rises, knolls, and ridges of mesic uplands (G138XA322FL)
- Hydric soil rating: No

Minor Components

Goldsboro

- Percent of map unit: 10 percent
- Landform: Knolls on marine terraces, ridges on marine terraces
- Landform position (three-dimensional): Interfluve
- *Down-slope shape:* Convex
- Across-slope shape: Linear
- Other vegetative classification: Loamy and clayey soils on flats and rises of mesic lowlands (G138XA331FL)
- *Hydric soil rating:* No

Ocilla

- Percent of map unit: 10 percent
- Landform: Rises on marine terraces
- Landform position (three-dimensional): Interfluve
- Down-slope shape: Convex
- Across-slope shape: Linear
- Other vegetative classification: Sandy over loamy soils on rises and knolls of mesic uplands (G138XA231FL)
- *Hydric soil rating:* No

Pelham fine sand, 0 to 2 percent slopes

Map Unit Setting

- National map unit symbol: 2tg56
- Elevation: 0 to 190 feet
- Mean annual precipitation: 48 to 63 inches
- Mean annual air temperature: 57 to 79 degrees F
- Frost-free period: 251 to 293 days
- Farmland classification: Not prime farmland

Map Unit Composition

- Pelham and similar soils: 75 percent
- Minor components: 25 percent
- Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Pelham

Setting

- Landform: Flatwoods
- Landform position (three-dimensional): Talf
- Down-slope shape: Linear
- Across-slope shape: Linear
- Parent material: Sandy and loamy marine deposits

Typical profile

- A 0 to 6 inches: fine sand
- Eg 6 to 26 inches: fine sand
- Btg1 26 to 42 inches: sandy clay loam
- Btg2 42 to 83 inches: sandy clay loam

Properties and qualities

- *Slope:* 0 to 2 percent
- Depth to restrictive feature: More than 80 inches
- Drainage class: Poorly drained
- Runoff class: High
- Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 5.95 in/hr)
- Depth to water table: About 6 to 12 inches
- Frequency of flooding: None
- Frequency of ponding: None
- Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
- Sodium adsorption ratio, maximum: 4.0
- Available water supply, 0 to 60 inches: Moderate (about 7.0 inches)

Interpretive groups

- Land capability classification (irrigated): None specified
- Land capability classification (nonirrigated): 3w
- *Hydrologic Soil Group:* B/D
- Ecological site: F153AY060NC Wet Loamy Flats and Depressions
- Forage suitability group: Sandy over loamy soils on flats of hydric or mesic lowlands (G153AA241FL)
- Other vegetative classification: Sandy over loamy soils on flats of hydric or mesic lowlands (G153AA241FL)
- *Hydric soil rating:* No

Minor Components

Unnamed

- Percent of map unit: 13 percent
- Landform: Flatwoods
- Landform position (three-dimensional): Talf
- Down-slope shape: Linear
- Across-slope shape: Linear
- Other vegetative classification: Sandy over loamy soils on flats of hydric or mesic lowlands (G153AA241FL)
- *Hydric soil rating:* Yes

Albany

- Percent of map unit: 6 percent
- Landform: Flatwoods
- Landform position (three-dimensional): Talf
- Microfeatures of landform position: Rises
- Down-slope shape: Convex
- Across-slope shape: Convex
- Ecological site: F153AY040NC Moist Loamy Rises and Flats
- Other vegetative classification: Sandy soils on rises and knolls of mesic uplands (G153AA131FL)
- *Hydric soil rating:* No

Meggett

- Percent of map unit: 3 percent
- Landform: Flatwoods
- Landform position (three-dimensional): Talf
- Down-slope shape: Linear
- Across-slope shape: Linear
- Ecological site: F153AY090NC Flooded Mineral Soil Floodplains and Terraces
- Other vegetative classification: Loamy and clayey soils on flats of hydric or mesic lowlands (G153AA341FL)
- Hydric soil rating: Yes

Surrency

- Percent of map unit: 3 percent
- Landform: Drainageways, depressions
- Landform position (three-dimensional): Dip
- Down-slope shape: Linear, concave
- Across-slope shape: Convex, concave
- Ecological site: F153AY060NC Wet Loamy Flats and Depressions
- Other vegetative classification: Sandy over loamy soils on stream terraces, flood plains, or in depressions (G153AA245FL)
- Hydric soil rating: Yes

3.4 Laboratory Soil Analysis

Selected soil samples recovered from the soil borings were analyzed for the percent soil fines passing the No. 200 sieve, natural moisture content, Atterberg Limits, and hydraulic conductivity. Samples selected for laboratory testing were collected at depths ranging from near-surface to 15 feet bls. These tests were performed to confirm visual soil classification and evaluate their engineering properties. The complete laboratory report is provided in Section 5.3.

The laboratory tests indicate the tested soils consist sand with silt, silty sand, silty sand with clay, sand with clay, clayey sand, very clayey sand, and sandy clay. The tested sand with silt (SP-SM) contains approximately 11 percent soil fines passing the No. 200 sieve with a natural moisture content of about 8.7 percent. The tested silty sand, and silty sand with clay (SM, SM-SC) contains approximately 14 to 27 percent soil fines passing the No. 200 sieve with natural moisture contents of about 7.8 to 18 percent. The tested sand with clay (SP-SC) contains approximately 11 percent soil fines passing the No. 200 sieve with a natural moisture content of about 7.8 to 18 percent. The tested sand with clay (SP-SC) contains approximately 11 percent soil fines passing the No. 200 sieve with a natural moisture content of about 17 percent. The tested clayey sand (SC) contains approximately 30 percent soil fines passing the No. 200 sieve with a natural moisture content of about 13 percent. The tested very clayey sand (SC/CL) contains approximately 34 percent soil fines passing the No. 200 sieve with a natural moisture content of about 18 percent. The tested sandy clay (CL) contains approximately 56 to 62 percent soil fines passing the No. 200 sieve with natural moisture content of about 17 to 23 percent.

Atterberg Limits tests indicate the tested sandy clay (CL) has Liquid Limit (LL) values of 35 and 41, Plastic Limit (PL) values of 15 to 18, and Plasticity Index (PI) values of 17 and 26. These values correspond to materials with low potential (LL < 50) to marginal potential (PI \leq 35) for expansive behavior³.

The constant head hydraulic conductivity test results indicate the near-surface silty sand (SM) has hydraulic conductivity values of 0.8 to 1.1 feet per day. The tested clayey sand (SC) has no flow. Tests were not conducted on the deeper very clayey sand due to the limitations of the test method on soils having moderate to high fines content, but these soils are expected to have permeability values at least one order of magnitude lower than the sandy soils.

³ U.S. Department of the Army USA, 1983, Foundations in Expansive Soils, TM 5-818-7, p. 4-1.

4.0 EVALUATION AND RECOMMENDATIONS

4.1 General

The following recommendations are made based upon our understanding of the proposed construction, a review of the attached soil borings and laboratory test data, and experience with similar projects and subsurface conditions. If plans or the location of proposed construction changes from those discussed previously, GSE requests the opportunity to review and possibly amend our recommendations with respect to those changes.

The final design of a foundation system is dependent upon adequate integration of geotechnical and structural engineering considerations. Consequently, GSE must review the final foundation design in order to evaluate the effectiveness and applicability of our initial analyses, and to determine if additional recommendations may be warranted. Without such a review, the recommendations presented herein could be misinterpreted or misapplied resulting in potentially unacceptable performance of the foundation system.

The performance of site improvements may be sensitive to their post-construction relationship to site groundwater levels, seepage zones, or soil/rock characteristics exposed at final site grades. GSE recommends that use of boring information for final design of all site improvements be predicated on proper horizontal and vertical control of borings.

In this section of the report, we present our geotechnical parameters and recommendations to assist with building foundation, stormwater management, and pavement designs as well as our general site preparation guidelines.

4.2 Groundwater

The groundwater table was encountered in the borings at depths of 6.1 to 8.8 feet bls at the time of our exploration. The Soil Survey indicates the groundwater table is typically at a depth of near-surface to 6 feet bls. We anticipate the seasonal high groundwater table will be near depths of 1 to 3.5 feet bls. Estimates for the seasonal high groundwater table are shown on the individual boring logs.

4.3 **Building Foundations**

The SPT borings located within the proposed building footprint indicate the soils across these areas are relatively consistent. SPT boring B-1 initially encountered 3 feet of sand with silt (SP-SM), and 4.5 feet of sandy clay (CL) overlying sand with clay, and poorly graded sand (SP-SC, SP) to a depth of 12 feet bls. This was underlain by clay (CL/CH) to the explored depth of 20 feet bls. SPT borings B-2 to B-5 encountered poorly graded sand, sand with silt, sand with clay, silty sand, and silty clayey sand (SP, SP-SM, SP-SC, SM-SC) with some interbedded layers of clayey to very clayey sand (SC, SC/CL) to depths of 13.5 to 17.5 feet bls. This was underlain by clay-rich (CL, CL/CH) soils to the explored depths of 20 feet bls.

Based upon the soil conditions encountered and our limited understanding of the structural loads and site grading, we recommend the building be supported by conventional, shallow strip and/or spread foundations. We recommend the shallow foundations be designed for a maximum allowable gross bearing pressure of 2,500 psf. The gross bearing pressure is defined as the soil contact pressure that can be imposed from the maximum structural loads, weight of the concrete foundations, and weight of the soil above the foundations. The foundations should be designed based upon the maximum load that could be imposed by all loading conditions.

The foundations should be embedded a minimum of 18 inches below the lowest adjacent grade. Interior foundations or thickened sections should be embedded a minimum of 12 inches. The foundations should have minimum widths of 18 inches for strip footings, and 24 inches for columns, even though the maximum soil bearing pressure may not be fully developed.

Due to the mostly sandy nature of the majority of the near-surface soils, we expect settlement to be mostly elastic in nature. The majority of the settlement will occur on application of the loads, during and immediately following construction. Using the recommended maximum bearing pressure, the assumed maximum structural loads, and the field and laboratory test data which we have correlated into the strength and compressibility characteristics of the subsurface soils, we estimate the total settlements of the structure to be 1 inch or less, with approximately half of it occurring upon load application (during construction).

Differential settlement results from differences in applied bearing pressures and the variations in the compressibility characteristics of the subsurface soils. For the building pad prepared as recommended, we anticipate differential settlement of less than 1/2 inch.

Post-construction settlement of the structures will be influenced by several interrelated factors, such as (1) subsurface stratification and strength/compressibility characteristics of the bearing soils; (2) footing size, bearing level, applied loads, and resulting bearing pressures beneath the foundation; (3) site preparation and earthwork construction techniques used by the contractor, and (4) external factors, including but not limited to vibration from off-site sources and groundwater fluctuations beyond those normally anticipated for the naturally-occurring site and soil conditions which are present.

Our settlement estimates for the structure are based upon our limited understanding of the structural loads and site grading and the use of successful adherence to the site preparation recommendations presented later in this report. Any deviation from our project understanding and/or our site preparation recommendations could result in an increase in the estimated post-construction settlement of the structure.

4.4 Flexible Pavement

Overall soil conditions encountered by our borings at this site are suitable for supporting conventional limerock base and asphalt wearing surface pavements. We have not been provided the anticipated traffic loading conditions; therefore, the following pavement component recommendations should be used only as guidelines. The below recommendations are intended to be minimums. Increasing base course and asphalt thicknesses would increase the design life of the pavement.

The seasonal high groundwater table is estimated to be approximately 12 inches to about 3.5 feet beneath existing grade across the site. We recommend a minimum of either 12 to 24 inches of separation (depending upon the pavement section design) be present between the bottom of the base course and the estimated seasonal high groundwater table. If this separation cannot be achieved by site grading, GSE recommends underdrains be used beneath the base course.

4.4.1 Stabilized Subgrade

If a crushed limerock or recycled concrete base is used, we recommend a stabilized subgrade be located beneath the base. The stabilized subgrade should have a minimum Limerock Bearing Ratio (LBR) of 40, with minimum thicknesses of 6 inches for automobile parking areas and 12 inches for driveways.

The stabilized subgrade can be imported material or a mixture of imported and on-site material. If a mix is proposed, a mix design should be performed to determine the optimum mix proportions. The stabilized subgrade should be compacted to a minimum of 98 percent of the Modified Proctor maximum dry density (ASTM D1557) for soils with less than 15 percent fines content. Soils with 15 percent or greater fines content should be compacted to 100 percent of the Standard Proctor maximum dry density (ASTM D698).

4.4.2 Base Course

The base course can consist of either crushed limerock, soil cement, or recycled concrete. If you should use a soil cement base course, a stabilized subgrade is not required.

Limerock should have an LBR of at least 100, be obtained from a FDOT approved source and meet FDOT gradation requirements. The base course thickness should be a minimum of 6 inches in automobile parking areas, and 8 inches in driveway areas. The base course should be compacted to at least 98 percent of the Modified Proctor maximum dry density (ASTM D1557). We recommend a minimum 24 inches separation between the bottom of the limerock base course and the estimated seasonal high-water table. If site grading does not allow for this separation, we recommend underdrains be considered.

Soil cement can consist of an imported material or a blend of the on-site soils and cement. A mix design should be performed to determine the optimum cement content. We recommend the soil cement have a minimum 28-day compressive strength of 500 psi. Soil cement can be blended off-site (in a pug mill) or on site. Soil cement pills should be cast from each day's production to verify the recommended compressive strength has been achieved at 28 days. We recommend the soil cement base course be a minimum of 8 inches thick throughout the project. We recommend a minimum 18 inches separation between the bottom of the soil cement base course and the estimated seasonal high-water table. If site grading does not allow for this separation, we recommend underdrains be considered.

Recycled concrete should have an LBR of at least 150, be obtained from a FDOT approved source and meet FDOT gradation requirements. The base course thickness should be a minimum of 8 inches. The base course should be compacted to at least 98 percent of the Modified Proctor maximum dry density (ASTM D1557). We recommend a minimum 12 inches separation between the bottom of the recycled concrete base course and the estimated seasonal high-water table. If site grading does not allow for this separation, we recommend underdrains be considered.

4.4.3 Wearing Surface

The asphalt-wearing surface should consist of an FDOT Type SP Hot Mix Asphalt mixture. For automobile parking areas, the thickness should be a minimum of 1.5 inches. For driveway areas, the thickness should be a minimum of 2 inches. The asphalt-wearing surface should consist of an SP-12.5 mix. The asphalt should be compacted to at least 95 percent of the mix design density.

The constructability of differing asphalt thicknesses may be difficult, and having a uniform 2-inch thick asphalt wearing surface may be more practical.

4.5 Rigid Pavement

Concrete pavement is a rigid pavement that results in smaller load transfers to the subgrade soils than flexible pavement. For concrete pavement subgrade, we recommend using the existing surficial sands or recommended clean sand (SP) fill, compacted to at least 98 percent of the Modified Proctor maximum dry density without additional stabilization with the following stipulations:

- 1. Subgrade soils must be compacted to at least 98 percent of Modified Proctor maximum dry density to a depth of at least 2 feet prior to placement of concrete.
- 2. The surface of the subgrade soils must be smooth and any disturbances or wheel rutting corrected prior to placement of the concrete.
- 3. The subgrade soils must be moistened prior to placement of concrete.
- 4. Concrete pavement thickness should be uniform throughout, with the exception of thickened edges (curb or footing).
- 5. The bottom of the pavement should be separated from the estimated seasonal high groundwater level by at least 18 inches.
- 6. Limerock or any other impermeable base is not suitable unless it meets the minimum recommended permeability of 10 ft/day.
- 7. The upper 12 inches of subgrade underlying the base course must also be "freedraining" and water that enters the base and subgrade must be allowed to seep out by gravity or if this is not possible, underdrains must be incorporated into the subgrade. A "bathtub" condition within the base/subgrade must be avoided.

Our recommendations for slab thickness for both light-duty and heavy-duty concrete pavements is based on a.) subgrade soils are compacted to 98 percent of the Modified Proctor maximum dry density, b.) modulus of subgrade reaction (k) of 200 pounds per cubic inch, c.) a 20-year design life, and d.) previously stated design parameters. For an anticipated light-duty traffic group, a minimum pavement thickness of 5.5 inches is recommended, using Table 2.4 from the ACI 330 Guide for Design and Construction of Concrete Parking Lots, ACI 330R-01. For an anticipated heavy-duty traffic group, a minimum pavement thickness of 8 inches is recommended, using Table 3.4 from the FDOT *Rigid Pavement Design Manual*, January 2019.

We recommend using concrete with a minimum 28-day compressive strength of 4,000 pounds per square inch and a minimum 28-day flexural strength (modulus of rupture) of at least 600 pounds per square inch based on the third point loading of concrete beam test samples. Maximum control joint spacing of 12.5 by 12.5 feet is suggested for light-duty concrete pavements. Maximum control joint spacing of 15 by 15 feet is suggested for heavy-duty concrete pavements. Layout of sawcut control joints should form square panels, and the depth of sawcut joint should be at least 1/4 of the concrete slab thickness. The joints should be sawed within six hours of concrete placement or as soon as the concrete has developed sufficient strength to support workers and equipment.

For further details on concrete pavement construction, refer to "Guide to Jointing Non-reinforced Concrete Pavements" published by the Florida Concrete and Products Associates, Inc. and "Building Quality Concrete Parking Areas", published by the Portland Cement Association.

4.6 Site Preparation

The soils at this site should be suitable for supporting the proposed construction using normal, good practice site preparation procedures. The following recommendations are our general guidelines for site preparation.

4.6.1 Stripping

Strip the construction limits and 10 feet beyond the perimeter of all grass, roots, topsoil, and other deleterious materials. You should expect to strip to depths of 12 or more inches. Deeper stripping will likely be necessary due to major root systems present at the site.

4.6.2 Dewatering

Temporary dewatering may be necessary for this project. If needed, we anticipate dewatering can be accomplished with sumps placed near the construction area, or with underdrains connected to a vacuum pump.

In any case, the site should always be graded to promote runoff and limit the amount of ponding. Localized ponding of stormwater is expected without proper grading during construction, and could render previously acceptable surfaces unacceptable.

4.6.3 Proof-Rolling

Proof-roll the subgrade with heavy rubber-tired equipment, such as a loaded front-end loader or dump truck, to identify any loose or soft zones not found by the soil borings. The proof-rolling should be monitored by a geotechnical engineer or qualified technician. Undercut or otherwise treat these zones as recommended by the geotechnical engineer in this report.

4.6.4 Proof Compaction

Compact the subgrade to a density of at least 95 percent of the Modified Proctor maximum dry density (ASTM D1557). The specified compaction should be obtained to a depth of 1 foot below the foundation bottoms and the existing grade prior to placing fill. Vibratory roller equipment should not be used within approximately 100 feet of existing structures. Lighter "walk-behind" compaction equipment may be used to achieve the degree of compaction.

Should clayey sand be encountered at the bearing surface, this material should be probed and visually confirmed to be unyielding in the upper 12 inches in lieu of density testing. If the foundation excavations penetrate the clayey sand, the excavation should be performed in a manner that reduces soil disturbance. Clayey sand soils (with fines content in excess of 15 percent) that are removed and replaced or appreciably disturbed need to be re-compacted to 98 percent of the Standard Proctor maximum dry density (ASTM D698).

4.6.5 Fill Placement

Imported fill placed to raise the site grades should consist of clean sand having less than 10 percent passing the No. 200 sieve. On-site soils meeting the requirements of Section 4.9 may also be used as structural fill. The fill should be placed in maximum 12-inch loose lifts that are compacted to at least 95 percent of the Modified Proctor maximum dry density (ASTM D1557). If lighter "walk-behind" compaction equipment is used, this may require lifts of 4 inches or less to achieve the required degree of compaction.

4.7 Quality Control and Construction Materials Testing

It should be noted that the geotechnical engineering design does not end with the advertisement of the construction documents. As the geotechnical engineer of record, GSE is the most qualified to perform the construction materials testing that will be required for this project. The benefits of having the geotechnical engineer of record also perform the construction materials testing are numerous. If GSE continues to be involved with the project through construction, we will be able to constantly re-evaluate and possibly alter our geotechnical recommendations in a timely and cost effective manner once final design and construction techniques are developed. This often results in cost savings for the project.

We recommend performing compaction testing beneath the concrete floor slab and the building foundations. We recommend one test be performed every 50 linear feet of continuous footing and every other column footing, per foot depth of fill or native material. We recommend a compaction test be performed for each 2,500 square feet of floor area or 10,000 square feet of pavement area per foot of fill or native material, or a minimum of three tests each, whichever is greater. Test all footing excavations to a depth of 12 inches at the frequencies stated above.

4.8 Stormwater Management

The auger borings located within the stormwater management facility encountered relatively consistent soil conditions. Auger boring P-1 encountered 6 feet of silty sand, and poorly graded sand (SM, SP) overlying clayey to very clayey sand, and clay with sand (SC, SC/CL, CL/CH) to the explored depth of 15 feet bls. Auger borings P-2 to P-4 initially encountered poorly graded sand, sand with silt, and silty sand (SP, SP-SM, SM) to depths of 2 to 5 feet bls, overlying silty clayey sand, and clayey to very clayey sand (SM-SC, SC, SC/CL) to depths of 7 to 10.5 feet bls. This was underlain by sand with silt (SP-SM) to depths of 12 to 13.5 feet bls, followed by clayrich soils (CL/CH) to the explored depth of 15 feet of sand with silt (SP-SM) overlying clay with sand (CL/CH) to a depth of 12.5 feet bls. This was underlain by sand with silt (SP-SM) to the explored depth of 15 feet bls.

The water table was encountered in the auger borings at depths of 7.5 to 8.8 feet bls at the time of our exploration. We anticipate the seasonal high groundwater table to be at depths of 1 to 2.5 feet bls.

The laboratory permeability tests indicate the surficial layers of silty sand (SM) has hydraulic conductivity values of 0.8 to 1.1 feet per day, and clayey sand (SC) has no flow. The deeper very clayey sand encountered below the surficial sandy soils is friable and will have permeability values at least one order of magnitude lower than the sandy soils. The underlying dense soils and clayrich soils are expected to be confining soils.

Mr. Cole Menhennett with CHW confirmed the proposed stormwater management facility as a dry pond via email. We understand that the current design will consider underdrains. We understand that imported clean sand will be used for the backfill for the underdrains. This revision includes soil parameters considering and underdrain design with clean sand backfill.

Based upon our findings and test results, our recommended soil parameters for the stormwater management design in the explored areas are presented below. The recommended parameters consider the results of the permeability tests, wash 200 determinations, and our experience with these types of soils. The parameters below do not consider a factor of safety.

Proposed Stormwater Management Facility

- 1. Base elevation of effective or mobilized aquifer (average depth of confining layer) equal to 8 feet bls.
- 2. Unsaturated vertical infiltration rate of 10 foot per day.
- 3. Horizontal hydraulic conductivity equal to 10 feet per day.
- 4. Specific yield (fillable porosity) of 20 percent.
- 5. Average seasonal high groundwater table depth equal to 2 feet bls.
- 6. Average seasonal low groundwater table depth equal to 6 feet bls.

In areas where clay-rich soils are present at the basin bottom, we recommend these soils be undercut a minimum of 2 feet and backfilled with the on-site sands and sands with silt (SP, SP-SM) having a maximum of 12 percent soil fines passing the No. 200 sieve. This fill should also be used above the bottom of the underdrains. The intent of this undercutting and replacement is to provide a more uniform sand "blanket" at the basin bottom that allows the migration of water to the underdrains. This sand blanket will also reduce the potential for clay-fines leaching out of the soils when water is present in the basin that can result in a thin layer of confining type material on the basin bottom that can reduce the effectiveness of the basin.

4.9 Fill Suitability

The soils encountered at this site within the explored depths range from sands (SP) to clays (CL/CH). A discussion of the suitability for reuse as structural fill for each soil classification according to the Unified Soil Classification System (USCS) designation is provided below.

SP, SP/SM – Sands (SP) and sand with silt (SP/SM) have less than 5 percent and 12 percent soil fines passing the No. 200 sieve, respectively, and are typically well draining soils that are suitable for reuse as structural fill. The sands with silt may require moisture conditioning (drying) to make the material more workable. These soils will require stockpiling and drying before they are reused if they are excavated from below the water table.

SM – Silty sands (SM) can have between 12 percent and 50 percent soil fines passing the No. 200 sieve. Silty sands are typically non-plastic or have low plasticity, and can be reused as structural fill with precautions. Silty sands can be moisture sensitive and difficult to work and compact and can rut if the moisture content is near or above the optimum moisture content. We recommend these soils be moisture content. Aerating and exposure to the sun is typically the most effective methods of drying these soils. It may not be practical to reuse these materials during the wet season, as frequent rain showers may not allow these soils to dry to a workable moisture content. Suitable silty sands are limited to soil having less than 30 percent soil fines passing the No. 200 sieve. Silty sands with more than 30 percent soil fines are especially moisture sensitive, and are not recommended for reuse as structural fill. These soils will behave more as sandy silt, and for this reason, very silty sands having more than 30 percent soil fines passing the No. 200 sieve have been assigned a dual classification of SM/ML. Silty sand soils that are excavated from below the water table are not recommended for reuse as structural fill due to the amount of time that will be required to dry these soils to a workable condition.

SC - Clayey sand (SC) soils can have between 12 percent and 50 percent soil fines passing the No. 200 sieve. Clayey sands can have a high range of plasticity, varying from a PI of 7 or greater and plotting above the A-line to highly plastic. Friable clayey sands are typically suitable for use as structural fill with precautions. Clayey sands will be moisture sensitive and difficult to work and compact and can rut during placement if the moisture content is near or above the natural moisture content. We recommend these soils be moisture conditioned (dried) so that the moisture content during use is at or below the optimum moisture content. Aerating and exposure to the sun is typically the most effective methods of drying these soils. It may not be practical to reuse these materials during the wet season, as frequent rain showers may not allow these soils to dry to a workable moisture content. Suitable clayey sands are limited to soil having less than 30 percent soil fines passing the No. 200 sieve. Clayey sands with more than 30 percent soil fines passing the No. 200 sieve are especially moisture sensitive and are typically highly plastic, and are not recommended for reuse as structural fill. These soils will behave more as sandy clay, and for this reason, very clayey sands having more than 30 percent soil fines passing the No. 200 sieve have been assigned a dual classification of SC/CH or SC/CL. Clayey sand soils that are excavated from below the water table are not recommended for reuse as structural fill due to the amount of time that will be required to dry these soils to a workable condition.

ML, MH, CL, CH - Silts and clays are not suitable materials for reuse as structural fill.

When using on-site soils as fill materials, we recommend the silty and clayey sand soils (SM, SC) be used in the lower depths of the fill. Sand and sand with silt (SP, SP-SM) should be used in the upper portions of the fill. We recommend a minimum of 2 feet of sand (SP, SP-SM) cover the silty and clayey sand fill materials to reduce the potential for soggy surface conditions due to the low permeability characteristics of the silty and clayey sand materials.

4.10 Surface Water Control and Landscaping

Roof gutters should be considered to divert runoff away from the building. The gutter downspouts should discharge a minimum of 10 feet from the structure to reduce the amount of water collecting around the foundations. Where possible, the gutter downspouts should discharge directly into the storm sewer system or onto the asphalt paved areas in order to reduce the amount of water collecting around the foundations. Grading of the site should be such that water is diverted away from the building on all sides to reduce the potential for erosion and water infiltration along the foundation.

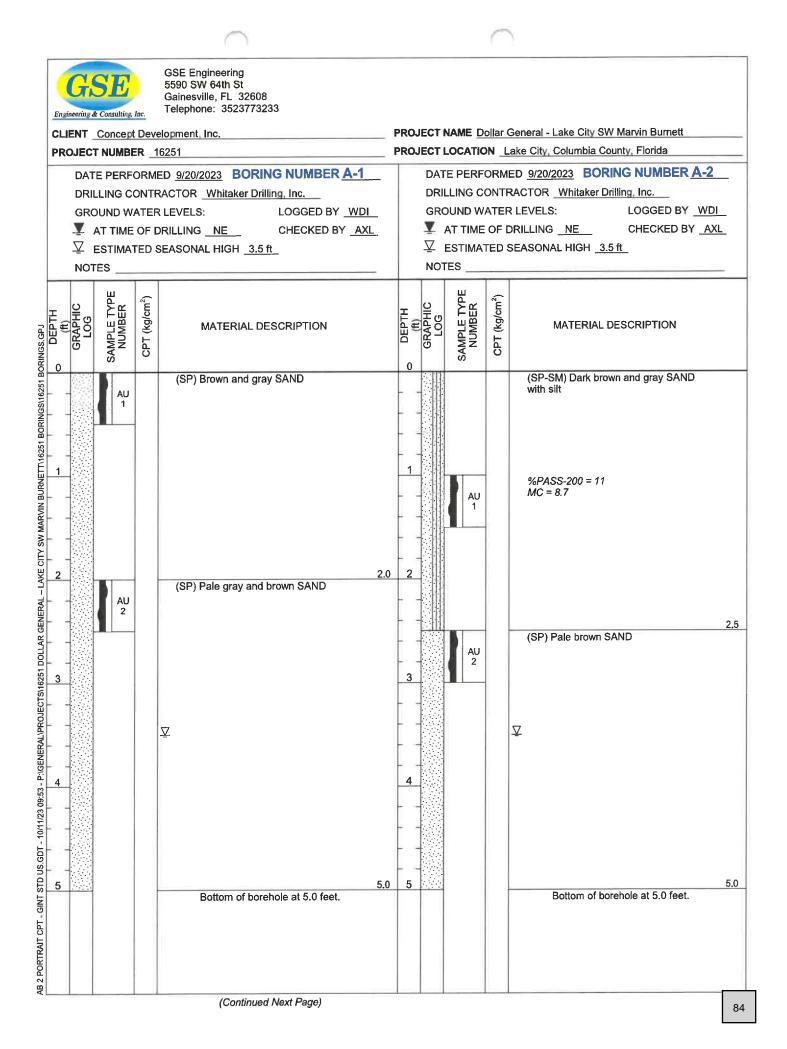
With respect to landscaping, it is recommended that any trees and large "tree-like" shrubbery with potential for developing large root systems be planted a minimum distance of half their mature height, and preferably their expected final height, away from the structure. The purpose of this is to reduce the potential for foundation or slab movements from the growth of root systems as the landscaping matures.

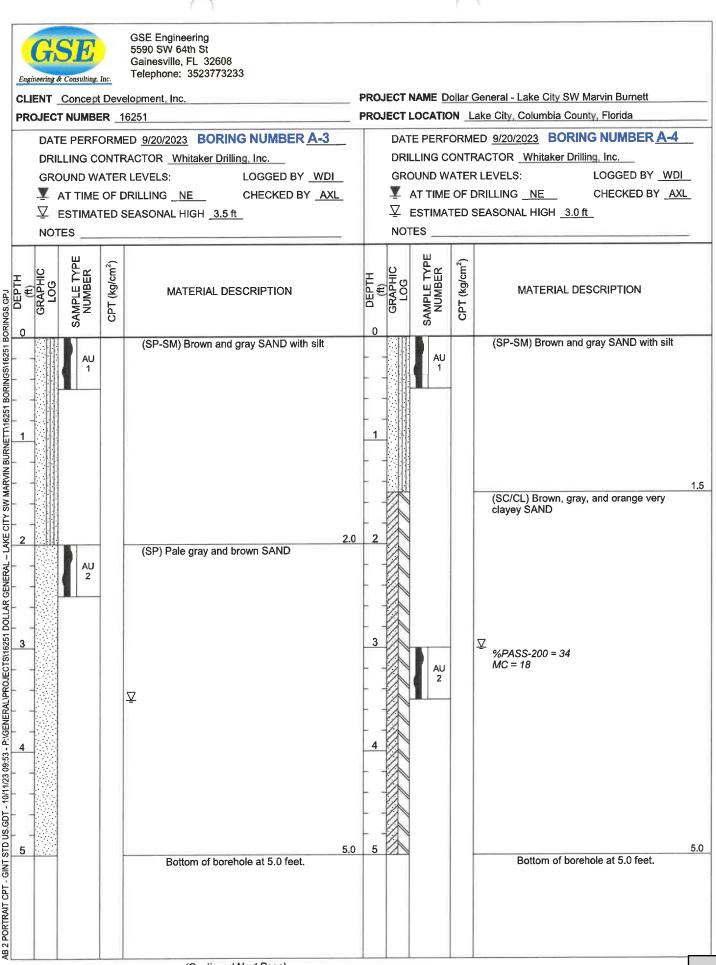
FIELD DATA 5.0

December 7, 2023

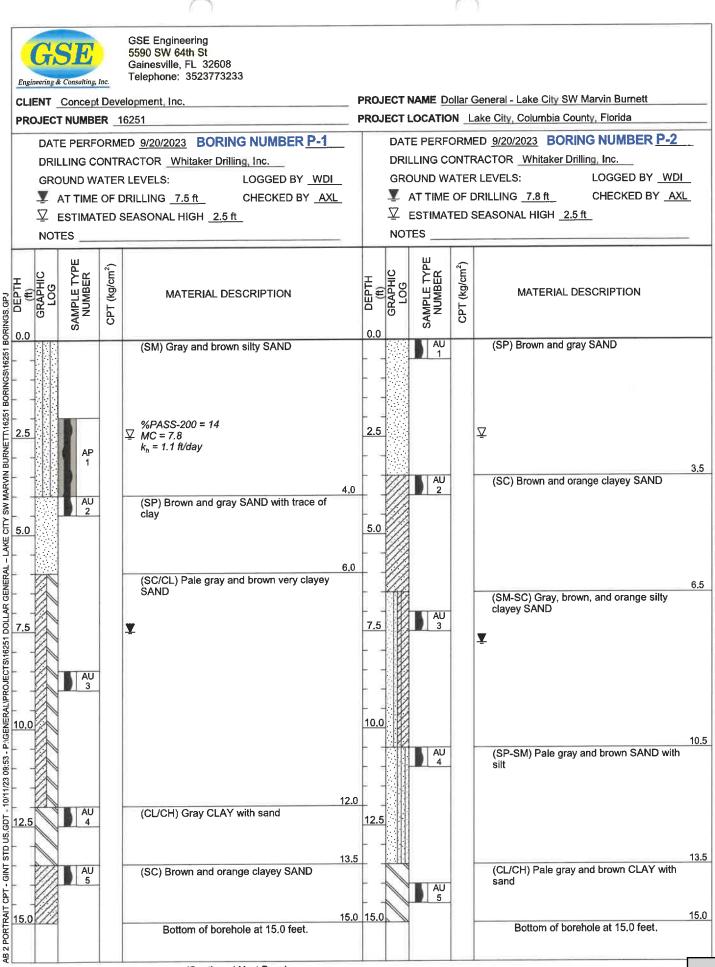
Summary Report of a Geotechnical Site Exploration – Revision 1 Dollar General – Lake City SW Marvin Burnett Lake City, Columbia County, Florida GSE Project No. 16251

5.1 Auger Boring Logs

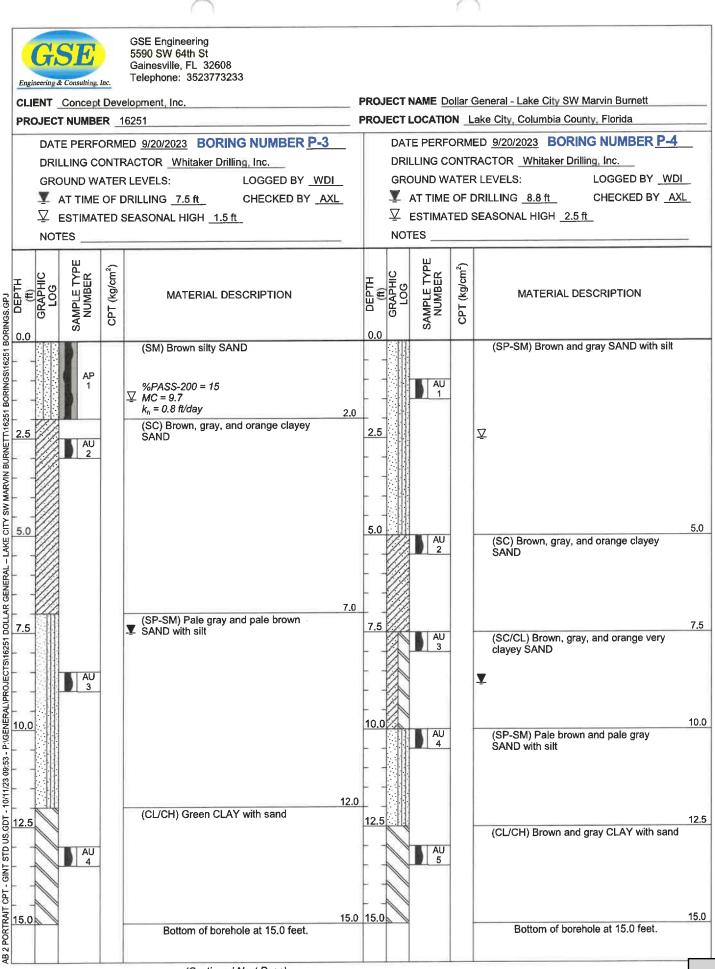




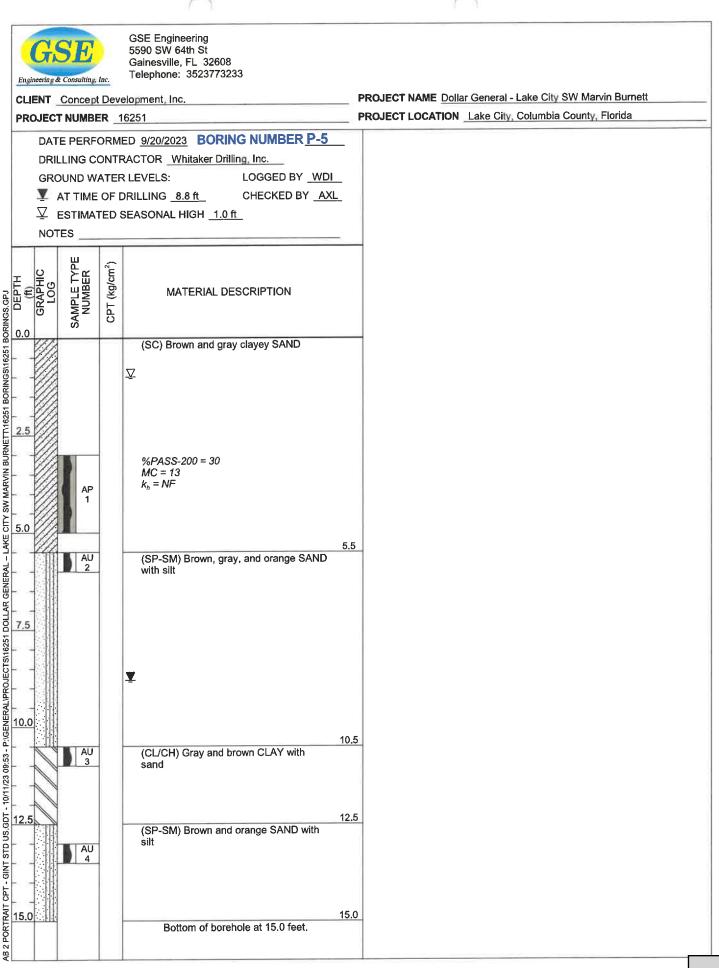
GSE Engineering 5590 SW 64th St Gainesville, FL 32608 Telephone: 3523773233	
ENT Concept Development, Inc.	PROJECT NAME Dollar General - Lake City SW Marvin Burnett
DIECT NUMBER 16251	PROJECT LOCATION Lake City, Columbia County, Florida
DATE PERFORMED 9/20/2023 BORING NUMBER A-5	
DRILLING CONTRACTOR Whitaker Drilling, Inc.	
GROUND WATER LEVELS: LOGGED BY WDI	<u> </u>
AT TIME OF DRILLING <u>NE</u> CHECKED BY <u>AXI</u>	
NOTES	<u>-</u>
GRAPHIC CPT (kg/cm ²) SAMPLE TYPE NUMBER Round CPT (kg/cm ²)	
CI SA CI	
(SP-SM) Brown and gray SAND with silt	
(SC) Brown and gray clayey SAND	3.5
AU 2	
	5.0
Bottom of borehole at 5.0 feet.	



(Continued Next Page)



(Continued Next Page)



December 7, 2023

5.2 Standard Penetration Test Soil Boring Logs

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LIENT ROJEC ATE ST RILLIN RILLIN OGGEL OTES	<u>Co</u> CT NI TART IG CO IG MI D BY	Incept Development, Inc. UMBER 16251 TED 9/20/23 COMPLETED 9/20/23 ONTRACTOR Whitaker Drilling, Inc.	PR		NAME Dolla	0								
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ATE ST RILLING OGGEL OTES	TART IG CO IG MI D BY	TED _9/20/23 COMPLETED _9/20/23 ONTRACTOR _Whitaker Drilling, Inc.			OCATION									
	ig Co ig Mi D By	ONTRACTOR Whitaker Drilling, Inc.						_				_		
	IG MI													
OTES (#)	_	ETHOD Flight Auger			ME OF DRI			ft						
(ft) GRAPHIC		WDI CHECKED BY AXL	e - 1	⊈ esti l	MATED SE	ASON	AL HI	GH_3	3.5 ft					
	2													_
		MATERIAL DESCRIPTION	CONTACT DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX	PERCENT PASS NO. 200 SIEVE	MOISTURE CONTENT, %		PT N V		
0	11	(SP-SM) Very loose brown SAND with silt	-								20	40	<u>60 8</u>	<u>su</u>
				SPT 1	1-1-1 (2)					3			- - - - - - - - - - - - - - - -	
			3	SPT 2	1-2-3 (5)						ł		· · · ·	•
5				SPT 3	4-6-9 (15)	35	18	17	56	17		32		
		Ţ		SPT 4	7-10-11 (21)	-							-	
		(SP-SC) Medium dense brown, gray, and orange SAND with clay	7.5	SPT 5	8-11-12 (23)							395		
		(SP) Medium dense pale gray and brown SAND	9.5	SPT 6	9-10-14 (24)								1	•
10												ļ		
			12									з	8	
		(CL/CH) Firm to stiff green and orange CLAY										51 C		
				SPT 7	3-4-5 (9)							9 3	8	
15	ľ												<u>.</u>	
												97°		
	1												000	
	I													
20			20	SPT 8	2-3-4 (7)						•	7		
		Bottom of borehole at 20.0 feet.												

	-				_			-				
-	S	Telephone: 3523773233						BC	DRI	NG	NUMBER B-2	
		nsuling, Inc.	DD				oral	Laka	City S	337 M	anvin Rumott	
		UMBER _16251										
		TED 9/20/23 COMPLETED 9/20/23									E	
		ONTRACTOR Whitaker Drilling, Inc.									3 	
		ETHOD Flight Auger					6.1	ft				
.OGG	SED B	WDI CHECKED BY AXL		⊈ ESTII	MATED SE	ASON/	AL HIG	GH _3	.5 ft	_		
IOTE	s											
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	CONTACT DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX	PERCENT PASS NO. 200 SIEVE	MOISTURE CONTENT, %	▲ SPT N VALUE ▲ 20 40 60 80	
0		(SP-SM) Very loose gray and brown SAND with silt										
3				SPT 1	1-2-2 (4)						^	
		$\underline{\nabla}$ (SM-SC) Very loose to medium dense gray, brown, and orange silty clayey SAND	3	SPT 2	1-2-2 (4)					3	•	
5				SPT 3	2-4-6 (10)							
3		⊻		SPT 4	7-9-8 (17)	-					Ì	
a			8.5	SPT 5	7-8-10 (18)	-						
10		(SP-SC) Very loose to medium dense pale gray and brown SAND with clay		SPT 6	7-9-10 (19)							
20 E		Weight-of-Rod from 13.5 to 14.5 ft bls.		SDT	0-0-3	-						
15		(CL/CH) Soft gray sandy CLAY	14.5	SPT 7	(3)	-					^	
10	111	(CL/CH) Firm green and orange CLAY	16.5									
3	Ill'			SPT	3-3-4 (7)							
20		Bottom of borehole at 20.0 feet.	20	8	(7)							

Enginee.	T Co	Telephone: 3523773233 ncept Development, Inc.						Lake	City S	SW Ma	NUMBER	B-3
		UMBER	PROJECT LOCATION Lake City, Columbia County, Florida									
DATE	STAR	TED 9/20/23 COMPLETED 9/20/23	GR	OUND E	LEVATION	_			HOL	E SIZ	Æ	
RILL	ING C	ONTRACTOR Whitaker Drilling, Inc.										
		ETHOD Flight Auger										_
		WDI CHECKED BY AXL		¥ ESTI	MATED SE/	ASON	AL HI	GH 3	3.5 ft			
OTE	s											
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	CONTACT DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX	PERCENT PASS NO. 200 SIEVE	MOISTURE CONTENT, %	▲ SPT N VAL	
0		(SP-SM) Very loose gray and brown SAND with silt									20 40 00	
			2.5	SPT 1	1-1-1 (2)						Î.	i e
		(SP) Loose pale gray SAND ⊈		SPT 2	1-2-4 (6)							
5	V	(SP-SC) Loose to gray and brown SAND with clay	4.5	SPT 3	2-4-5 (9)							
		(SC/CL) Medium dense to dense gray, brown, and orange very clayey SAND	6	SPT 4	6-2-9 (11)							1000
				SPT 5	7-9-11 (20)							
-				SPT 6	14-16-22 (38)							
1. J.			13.5									24
5		(CL) Firm gray sandy CLAY		SPT 7	2-3-3 (6)	41	15	26	62	23		
-		(CL/CH) Green and orange CLAY	16									2
1	J											2 2
												20
20	10	Bottom of borehole at 20.0 feet.	20									
												12

GSE S590 SW 64th St Gainesville, FL 32608 Telephone: 3523773233 CLIENT Concept Development, Inc. PROJECT NAME Dollar General - Lake City SW N PROJECT NUMBER 16251 PROJECT LOCATION Lake City, Columbia Cour DATE STARTED 9/20/23 COMPLETED 9/20/23 DRILLING CONTRACTOR Whitaker Drilling, Inc. GROUND WATER LEVELS: DRILLING METHOD Flight Auger Y AT TIME OF DRILLING 6.5 ft	nty, Florida
PROJECT NUMBER 16251 PROJECT LOCATION Lake City, Columbia Count DATE STARTED 9/20/23 COMPLETED 9/20/23 DRILLING CONTRACTOR Whitaker Drilling, Inc. GROUND WATER LEVELS: DRILLING METHOD Flight Auger Image: Complete Co	nty, Florida
DATE STARTED 9/20/23 COMPLETED 9/20/23 GROUND ELEVATION HOLE SI DRILLING CONTRACTOR Whitaker Drilling, Inc. GROUND WATER LEVELS: Image: Complete Si Image: Complete Si DRILLING METHOD Flight Auger Image: Complete Si Image: Complete Si Image: Complete Si	IZE
DRILLING CONTRACTOR Whitaker Drilling, Inc. GROUND WATER LEVELS: DRILLING METHOD Flight Auger Image: Contraction of the contraction of	
DRILLING METHOD Flight Auger	
∇	
DEPTH (f) (f) (f) (f) (f) (f) (f) (f)	
0 (SP-SM) Very loose gray and brown SAND with silt	20 40 60 80
SPT 1-1-2 1 (3)	1
SPT 2 (SP) Medium dense pale gray and brown SAND 2 4-7-11 (18)	
5 SPT 7-5-6 3 (11)	4
6 SPT 3-4-5 orange silty SAND with clay (9)	
SPT 5-7-14 5 (21) 27 18	3
9 SPT 12-10-9	
(SC) gray and brown clayey SAND	
13 (SP-SC) Medium dense gray, brown, and orange SAND	
with clay	
(CL/CH) Firm green and gray sandy CLAY	
20 SPT 3-3-4 8 (7)	4
20 Bottom of borehole at 20.0 feet.	

-	F S ring & Co.	GSE Engineering 5590 SW 64th St Gainesville, FL 32608 Telephone: 3523773233						BC	ORI	NG	NUMBER B-5
-		procept Development, Inc.	PR	JECT		ar Gen	eral -	Lake	City S	SW Ma	arvin Burnett
		UMBER 16251		OJECT	LOCATION	Lake	City,	Colur	nbia (County	/, Florida
DATE	STAR	TED 9/20/23 COMPLETED 9/20/23	GR	OUND E	LEVATION				HOL	E SIZ	E
RILI	ING C	ONTRACTOR Whitaker Drilling, Inc.	GR	OUND V	VATER LEV	ELS:					
RILI	ING M	ETHOD Flight Auger									
OGC	GED B	WDI CHECKED BY AXL		⊈ ESTI	MATED SE/	ASON/	AL HI	GH _3	.5 ft		
IOTE	s						_				
0 (f)	GRAPHIC LOG	MATERIAL DESCRIPTION	CONTACT DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX	PERCENT PASS NO. 200 SIEVE	MOISTURE CONTENT, %	▲ SPT N VALUE ▲ 20 40 60 80
0		(SP-SM) Very loose brown and gray SAND with silt									
				SPT 1	1-1-2 (3)						N
-		$\overline{\mathcal{V}}$ (SP) Medium dense pale brown and pale gray SAND	3	SPT 2	4-7-8 (15)						Y
5				SPT 3	10-11-13 (24)						
1		Ţ		SPT 4	10-8-9 (17)						
-	e	(SP-SC) Medium dense to dense brown and orange SAND with clay	8	SPT 5	7-8-11 (19)						
-			10	SPT 6	17-21-24 (45)				11	17)
		(SP) Medium dense pale brown and gray SAND									
15				SPT 7	5-7-9 (16)						
		(CL/CH) Hard pale gray sandy CLAY	17.5								
- 20		Bottom of borehole at 20.0 feet.	20	SPT 8	8-14-19 (33)						.

5.3 Laboratory Results

GSE Engineering & Consulting, Inc.

SUMMARY REPORT OF LABORATORY TEST RESULTS

Project Number: 16251

Project Name: Dollar Genera

Dollar General - Lake City SW Marvin Burnett

			Natural Moisture				Percent	Oreanic	Hvidraulic	
Boring Number	Depth (ft)	Soil Description	Content (%)	Liquid Limit	Plastic Limit	Plasticity Index	No. 200 Sieve	Content (%)	Conductivity (ft/dav)	Unified Soil Classification
A-2	1-1.5	Dark brown and gray SAND with silt	8.7				11			SP-SM
A-4	3-3.5	Brown, gray, and orange very clayey SAND	18				34			sc/cl
B-1	4-5.5	Brown, gray, and orange sandy CLAY	17	35	18	17	56			C
B-3	13.5-15	Gray sandy CLAY	23	41	15	26	62			cr
B-4	7-8.5	Gray, brown, and orange silty SAND with clay	18				27			SM-SC
B-5	8.5-10	Pale brown and gray SAND with clay	17				11			SP-SC
P-1	2-4	Gray and brown silty SAND	7.8				14		1.1	SM
P-3	0-2	Brown silty SAND	9.7				15		0.8	SM
P-5	3-5	Brown and gray clayey SAND	13				30		NF	sc

5.4 Key to Soil Classification

· · · · · ·	- Andreading Channel 1	and Group Manager II	sing Laboratory Tests	SYM	BOLS	GROUP NAME	
Criteria f	or Assigning Group Symbol	s and Group Names U	sing Laboratory Tests	GRAPHIC	LETTER	UKUUP NAME	
COARSE-GRAINED SOILS	Gravels	Clean Gravels	$Cu \ge 4$ and $1 \le Cc \le 3$	2.24	GW	Well graded GRAVEL	
fore than 50% retained	More than 50% of coarse	Less than 5% fines	Cu < 4 and/or 1 > Cc > 3	20:20	GP	Poorly graded GRAVE	
n No. 200 sieve	fraction retained on No. 4 sieve	Gravels with fines	Fines classify as ML or MH	1200	GM	Silty GRAVEL	
	SIEVE	More than 12% fines	Fines classify as CL or CH	1972 - 17 - 17 - 17 - 17 - 17 - 17 - 17 -	GC	Clayey GRAVEL	
	Sands	Clean Sands	$Cu \ge 6$ and $1 \le Cc \le 3$		SW	Well graded SAND	
	50% or more of coarse	Less than 5% fines	Cu < 6 and/or 1 > Cc > 3	and the second s	SP	Poorly graded SAND	
	fraction passes No. 4 sieve	Sand with fines	Fines classify as ML or MH		SP-SM	SAND with silt	
		$5\% \le \text{fines} < 12\%$	Fines classify as CL or CH		SP-SC	SAND with clay	
		Sand with fines	Fines classify as ML or MH		SM	Silty SAND	
		$12\% \le \text{fines} < 30\%$	Fines classify as CL or CH	Ale - Charles	SC	Clayey SAND	
		Sand with fines	Fines classify as ML or MH		SM	Very silty SAND	
		30% fines or more	Fines classify as CL or CH		SC	Very clayey SAND	
TINE-GRAINED SOILS	Clays	inorganic	50% ≤ fines < 70%		CL/CH	Sandy CLAY	
50% or more passes the			70% ≤ fines < 85%	000	CL/CH	CLAY with sand	
No. 200 sieve			fines $\geq 85\%$	000	CL/CH	CLAY	
	Silts and Clays	inorganic	PI > 7 and plots on/above "A" line		CL	Lean CLAY	
	Liquid Limit less than 50	·	PI < 4 or plots below "A" line		ML	SILT	
		organic	Liquid Limit - oven dried < 0.7		OL	Organic clay	
			Liquid Limit - not dried		UL	Organic silt	
	Silts and Clays	inorganic	PI plots on or above "A" line		СН	Fat CLAY	
	Liquid Limit 50 or more		PI plots below "A" line		MH	Elastic SILT	
		organic	Liquid Limit - oven dried < 0.75		ОН	Organic clay	
			Liquid Limit - not dried			Organic silt	
CORRE	LATION OF PENETR	ATION RESISTAL	NCE WITH RELATIVE DEN	SITY AND	CONSIST	ENCY	
			NT		C N CO	NSISTENCY	
No. OF B	,	LATIVE DENSITY	INC). UF BLUW	S, N CO		
0 -		Van Lagar					
5		Very Loose		0 - 2		Very Soft	
5 -	10	Loose	SILTS	0 - 2 3 - 4		Very Soft Soft	
SANDS: 11 -	10 · 30	Loose Medium dense	SILTS &	0 - 2 3 - 4 5 - 8		Very Soft Soft Firm	
SANDS: 11 - 31 -	10 30 50	Loose Medium dense Dense	SILTS	0 - 2 3 - 4 5 - 8 9 - 15		Very Soft Soft Firm Stiff	
SANDS: 11 -	10 30 50	Loose Medium dense	SILTS &	0 - 2 3 - 4 5 - 8		Very Soft Soft Firm	
SANDS: 11 - 31 -	10 30 50 R 50	Loose Medium dense Dense	SILTS &	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30		Very Soft Soft Firm Stiff Very Stiff	
SANDS: 11 - 31 - OVE	10 30 50 R 50 LOWS, N RELA	Loose Medium dense Dense Very Dense	SILTS &	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50		Very Soft Soft Firm Stiff Very Stiff Hard	
SANDS: 11 - 31 - OVE No. OF BL	10 - 30 - 50 R 50 LOWS, N RELA - 8	Loose Medium dense Dense Very Dense	SILTS &	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50		Very Soft Soft Firm Stiff Very Stiff Hard Very Hard	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 -	10 30 50 R 50 LOWS, N RELA 8 18	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft	SILTS & CLAYS: <u>SAMPLE G</u>	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50		Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 -	10 30 50 R 50 LOWS, N RELA 8 18 32 N	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft	SILTS & CLAYS: SAMPLE G Location	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50	YPE LEGI	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 - LIMESTONE: 19 -	10 30 50 R 50 LOWS, N RELA 8 18 32 N 50	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard	SILTS & CLAYS: SAMPLE G Location	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50	YPE LEGI	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 - LIMESTONE: 19 - 33 - OVE	10 30 50 R 50 COWS, N RELA 8 18 32 N 50 R 50	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard	SILTS & CLAYS: SAMPLE G Location of SPT	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50	YPE LEGI	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location of Auger	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 - LIMESTONE: 19 - 33 - OVE	10 30 50 R 50 LOWS, N RELA 8 18 32 N 50	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard	SILTS & CLAYS: SAMPLE G Location of SPT Sample	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY	YPE LEG	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location of Auger Sample	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 - LIMESTONE: 19 - 33 - OVE <u>PARTICLE</u>	10 30 50 R 50 COWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATION	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON	SILTS & CLAYS: SAMPLE G Location of SPT Sample	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50	YPE LEG	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location of Auger Sample	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 - LIMESTONE: 19 - 33 - OVE <u>PARTICLE</u> BOULDERS:	10 30 50 R 50 COWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATION Greater than 30	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON	SILTS & CLAYS: SAMPLE G Location of SPT Sample LABORA	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY	YPE LEGI	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location of Auger Sample	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 - LIMESTONE: 19 - 33 - OVE <u>PARTICLE</u> BOULDERS: COBBLES:	10 30 50 R 50 COWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATION Greater than 30 75 mm to 300	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON	SILTS & CLAYS: SAMPLE G Location of SPT Sample LABORA	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY TORY TES	YPE LEGI	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location of Augen Sample	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 - LIMESTONE: 19 - 33 - OVE <u>PARTICLE</u> BOULDERS: COBBLES: GRAVEL: Coarse	10 30 50 R 50 COWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATION Greater than 30 75 mm to 300 5 - 19.0 mm to 75	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON 00 mm 0 mm	SILTS & CLAYS: SAMPLE G Location of SPT Sample LABORA LL = PL =	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY TORY TES	YPE LEGI	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location of Auge Sample	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 - LIMESTONE: 19 - 33 - OVE <u>PARTICLE</u> BOULDERS: COBBLES: GRAVEL: Coarse Fine	10 30 50 R 50 COWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATION Greater than 30 75 mm to 300 2 - 19.0 mm to 75 3 - 4.75 mm to 19	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON 00 mm 0 mm 5 mm 0 mm	SILTS & CLAYS: SAMPLE G Location of SPT Sample LABORA LL = PL = PL = PI =	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY TORY TES	YPE LEGI	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location of Augen Sample D Sample	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 - LIMESTONE: 19 - 33 - OVE <u>PARTICLE</u> BOULDERS: COBBLES: GRAVEL: Coarse Fine SANDS: Coarse	10 30 50 R 50 COWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATION Greater than 30 75 mm to 300 - 19.0 mm to 75 - 4.75 mm to 19. - 2.00 mm to 4.7	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON 00 mm 0 mm 5 mm .0 mm 25 mm	SILTS & CLAYS: SAMPLE G Location of SPT Sample LABORA LL = PL = PI = PI = % PASS - 200 =	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY TORY TES Li Pl Pla Percent Pas	YPE LEGI T LEGEN quid Limit astic Limit sticity Inde ssing the N	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location of Auger Sample D 5, % 5, % 5, % 5, %	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 - LIMESTONE: 19 - 33 - OVE <u>PARTICLE</u> BOULDERS: COBBLES: GRAVEL: Coarse Fine SANDS: Coarse Medium	10 30 50 R 50 COWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATION Greater than 30 75 mm to 300 2 19.0 mm to 75 2 4.75 mm to 19 2 2.00 mm to 4.7 4 5.00 mm to 4.7 4 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 2.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 2.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON 0 mm 5 mm 0 mm 5 mm 0 mm	SILTS & CLAYS: SAMPLE G Location of SPT Sample LABORA LL = PL = PL = PI = % PASS - 200 = MC =	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY TORY TES Li Pl Pla Percent Pa: Moi:	YPE LEGI T LEGEN quid Limit astic Limit sticity Inde ssing the N sture Conte	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location of Auger Sample D s, % s, % sx, % to. 200 Sieve ent, %	
SANDS: 11 - 31 - OVE No. OF BI 0 - 9 - LIMESTONE: 19 - 33 - OVE <u>PARTICLE</u> BOULDERS: COBBLES: GRAVEL: Coarse Fine SANDS: Coarse	10 30 50 R 50 COWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATION Greater than 30 75 mm to 300 2 19.0 mm to 75 2 4.75 mm to 19 2 2.00 mm to 4.7 4 5.00 mm to 4.7 4 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 2.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 2.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm to 2.00 mm to 4.7 5 5.00 mm	Loose Medium dense Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON 00 mm 5 mm 00 mm 5 mm 00 mm 25 mm 00 mm	SILTS & CLAYS: SAMPLE G Location of SPT Sample LABORA LL = PL = PL = PI = PI = % PASS - 200 = MC = ORG =	0 - 2 3 - 4 5 - 8 9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY TORY TES Li Pl Pla Percent Pa: Moi: Org	YPE LEGI T LEGEN quid Limit astic Limit sticity Inde ssing the N sture Conte anic Conte	Very Soft Soft Firm Stiff Very Stiff Hard Very Hard END Location of Auge Sample D s, % s, % sx, % to. 200 Sieve ent, %	

KEY TO SOIL CLASSIFICATION CHART

6.0 LIMITATIONS

6.1 Warranty

This report has been prepared for our client for their exclusive use, in accordance with generally accepted soil and foundation engineering practices, and makes no other warranty either expressed or implied as to the professional advice provided in the report.

6.2 Auger and SPT Borings

The determination of soil type and conditions was performed from the ground surface to the maximum depth of the borings, only. Any changes in subsurface conditions that occur between or below the borings would not have been detected or reflected in this report.

Soil classifications that were made in the field are based upon identifiable textural changes, color changes, changes in composition or changes in resistance to penetration in the intervals from which the samples were collected. Abrupt changes in soil type, as reflected in boring logs and/or cross sections may not actually occur, but instead, be transitional.

Depth to the water table is based upon observations made during the performance of the auger and SPT borings. This depth is an estimate and does not reflect the annual variations that would be expected in this area due to fluctuations in rainfall and rates of evapotranspiration.

6.3 Site Figures

The measurements used for the preparation of the figures in this report were made using the provided site plan and by estimating distances from existing structures and site features. Figures in this report were not prepared by a licensed land surveyor and should not be interpreted as such.

6.4 Unanticipated Soil Conditions

The analysis and recommendations submitted in this report are based upon the data obtained from soil borings performed at the locations indicated on Figure 2. This report does not reflect any variations that may occur between these borings.

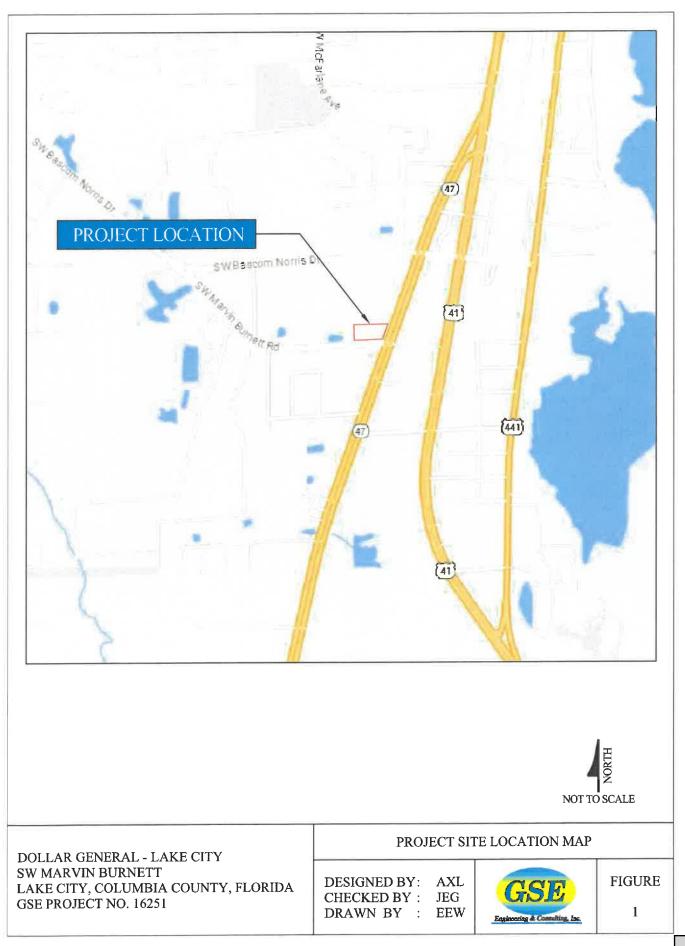
The nature and extent of variations between borings may not become known until excavation begins. If variations appear, we may have to re-evaluate our recommendations after performing on-site observations and noting the characteristics of any variations.

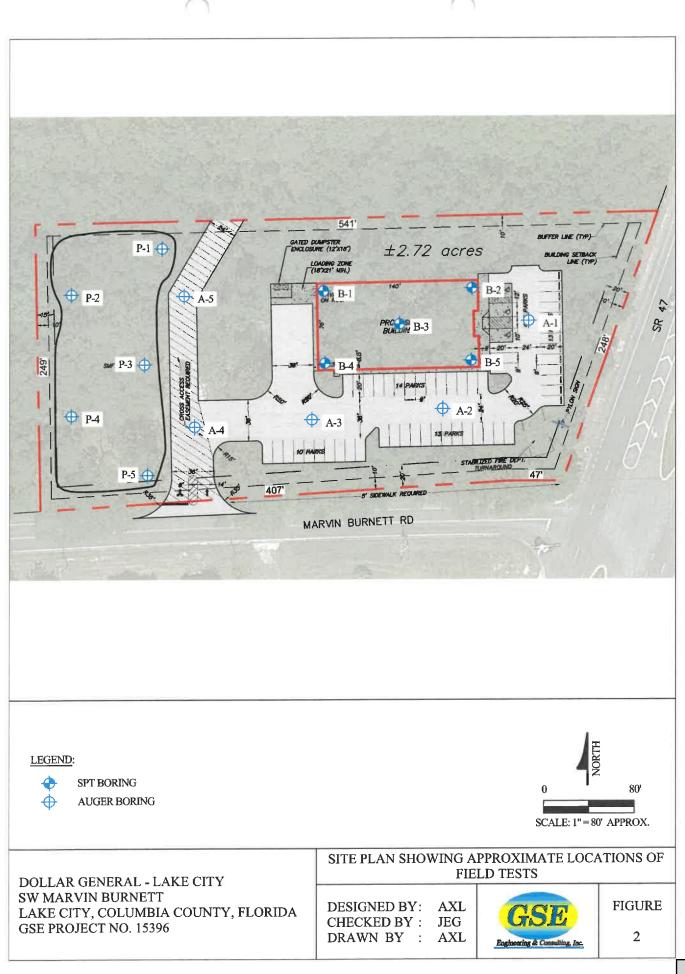
6.5 Misinterpretation of Soil Engineering Report

GSE Engineering & Consulting, Inc. is responsible for the conclusions and opinions contained within this report based upon the data relating only to the specific project and location discussed herein. If others make the conclusions or recommendations based upon the data presented, those conclusions or recommendations are not the responsibility of GSE.

December 7, 2023

FIGURES





LEGAL DESCRIPTION

23-0653



DATE: OCTOBER 25, 2023 PROJECT NAME: DG LAKE CITY ALTA PROJECT NO: 23-0653 DESCRIPTION FOR: PARCEL A

A TRACT OF LAND BEING A PORTION OF LANDS AS DESCRIBED IN OFFICIAL RECORDS BOOK 1330 PAGE 1324 OF THE PUBLIC RECORDS OF COLUMBIA COUNTY, FLORIDA, SITUATED IN THE NORTHEAST QUARTER (NE 1/4) OF THE NORTHEAST QUARTER (NE 1/4) OF SECTION 7, TOWNSHIP 4 SOUTH, RANGE 17 EAST, COLUMBIA COUNTY, FLORIDA, AND BEING MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCE AT THE SOUTHWEST CORNER OF AFOREMENTIONED NORTHEAST QUARTER (NE 1/4) OF THE NORTHEAST QUARTER (NE 1/4) OF SECTION 7, TOWNSHIP 4 SOUTH, RANGE 17 EAST, COLUMBIA COUNTY, FLORIDA; THENCE NORTH 02°08'35" WEST, ALONG WEST LINE OF SAID NORTHEAST QUARTER (NE 1/4) OF THE NORTHEAST QUARTER, A DISTANCE OF 50.00 FEET TO THE NORTHERLY RIGHT OF WAY LINE OF S.W. MARVIN BURNETT ROAD (RIGHT OF WAY WIDTH VARIES); THENCE DEPARTING SAID WEST LINE, NORTH 85°44'05" EAST, ALONG SAID NORTHERLY RIGHT OF WAY LINE, A DISTANCE OF 130.73 FEET TO THE **POINT OF BEGINNING**; THENCE NORTH 02°10'29" WEST, A DISTANCE OF 249.00 FEET; THENCE NORTH 88°10'08" EAST, A DISTANCE OF 541.00 FEET TO THE WESTERLY RIGHT OF WAY LINE OF S.W. STATE ROAD NO. 47 (RIGHT OF WAY WIDTH VARIES); THENCE SOUTH 18°32'28" WEST, ALONG SAID WESTERLY RIGHT OF WAY LINE, A DISTANCE OF 248.00 FEET; THENCE, CONTINUE ALONG SAID WESTERLY RIGHT OF WAY LINE, A DISTANCE OF 248.00 FEET; THENCE, CONTINUE ALONG SAID WESTERLY RIGHT OF WAY LINE, SOUTH 89°06'47" WEST, A DISTANCE OF 46.52 FEET TO THE INTERSECTION OF SAID WESTERLY RIGHT OF WAY LINE AND AFOREMENTIONED NORTHERLY RIGHT OF WAY LINE OF S.W. MARVIN BURNETT ROAD; THENCE SOUTH 85°44'05" WEST, ALONG SAID NORTHERLY RIGHT OF WAY LINE A DISTANCE OF 248.00 FEET; ALONG SAID NORTHERLY RIGHT OF WAY LINE A DISTANCE OF 544.'05" WEST, ALONG SAID NORTHERLY RIGHT OF WAY LINE A DISTANCE OF 544.'05" WEST, ALONG SAID NORTHERLY RIGHT OF WAY LINE A DISTANCE OF 44'05" WEST,

SAID TRACT OF LAND CONTAINING 2.70 ACRES, MORE OR LESS.

PROPERTY OWNER AFFIDAVIT Owner Mailing Address: Property Owner Name: 13820 W. Newberry Road, Suite 100 St. Johns Limited Liability Company Newberry, FL 32669 **Owner phone: Owner email:** Property County: Columbia Parcel ID #: 07-4S-17-08127-005 Agent: Concept Development, Inc. and Concept Construction of North Florida, Inc. 1449 SW 74th Drive, Suite 200 Gainesville, FL 32607 (352) 333-3233 **Authorized Actions of Agent:** Design and submission of documentation, forms and plans and application for all permits as required from those regulatory agencies having jurisdiction over the Property (e.g. County, City, Water Management District, FDOT, FDEP, etc.) and on-site access for inspections, testing, data collection, etc. I hereby certify that I am the owner of record. I hereby authorize the above listed agents to act on my behalf for the purposes of any and all applications and securing the above requested actions. St. Johns Limited Liability Company, a Florida limited liability company William B. Martin Its: Manager STATE OF FLORIDA COUNTY OF HELACHUN The foregoing instrument was acknowledged before me this 3 all day of June, 2023, by William. B. Martin, as Manager of St. Johns Limited Liability Company, a Florida limited liability company, on behalf of said company who is as identification. personally known to me or has produced JAMES D. SALTER Commission # HH 253673 Nota Public, State of Florida at Large

Page 15 of 15

Expires May 30, 2026

This instrument prepared by and after recording return to:

John C. Bovay, Attorney at Law 901 N.W. 57th Street Gainesville, Florida 32605

Inst:2005003121 Date:02/09/2005 Time:15:12 Doc Stamp-Deed : 0.70 _____DC,P.DeWitt Cason,Columbia County B:1037 P:1953

07-4S-

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Property Appraiser's Parcel Identification Number(s)

WARRANTY DEED

The Grantor, William B. Martin, as Trustee of the William B. Martin Trust, dated July 31, 1990, in consideration of Ten and grants and conveys to the Grantee, St. Johns, LLC (a Florida limited liability company), whose mailing address is 2841 NW 41st Street, Gainesville, Florida 32606, the real property in Columbia County, Florida, described as follows:

The South ½ of the Northeast ¼ of the Northeast ¼ of Section 7, Township 4 South, Range 17 East as lies West of S.R. No. 47; LESS AND EXCEPT: Begin at the Southwest Corner of the Northeast ¼ of the Northeast ¼ of said Section 7, and run North along West Line of said Northeast ¼ of the Northeast ¼ 211 feet; thence run East 337 feet; thence run South 211 feet; thence run West 337 feet to the Point of Beginning.

The Grantor warrants that the property is free of all encumbrances, except the lien for real estate taxes not yet due and payable and restrictions, reservations, and easements of record, and that lawful seisin of and good right to convey the property are vested in the Grantor. The Grantor hereby fully warrants the title to the property and will defend the same against the lawful claims of all persons.

This deed was prepared without examination of title or legal opinion, but upon information, including the legal description and the ownership interest, supplied by the Grantor.

* *********

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The interest conveyed is not the homestead of the Grantor.

Inst:2005003121 Date:02/09/2005 Time:15:12 Doc Stamp-Deed : 0.70 ____DC,P.DeWitt Cason,Columbia County B:1037 P:1954

Signed on February 4, 2005.

Signed in the presence of: Print Name:

Prin Name:

William B. Martin, as Trustee of the William B. Martin Trust, dated July 31, 1990 2841 NW 41st Street

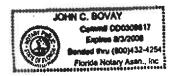
Gainesville, Florida 32606

Two witnesses as to William B. Martin, as Trustee of the William B. Martin Trust, dated July 31, 1990

STATE OF FLORIDA COUNTY OF ALACHUA

The foregoing instrument was acknowledged before me on February $\underline{4}$, 2005, by William B. Martin.

Personally Known ______ Produced Identification ______ Type of Identification ______





GROWTH MANAGEMENT DEPARTMENT 205 North Marion Ave, Lake City, FL 32055 Phone: 386-719-5750 E-mail: growthmanagement@lcfla.com

AGENT AUTHORIZATION FORM

I.MatthewCason_____(owner name), owner of property parcel

number 07-4S-17-08127-005 (parcel number), do certify that

the below referenced person(s) listed on this form is/are contracted/hired by me, the owner, or, is an officer of the corporation; or, partner as defined in Florida Statutes Chapter 468, and the said person(s) is/are authorized to sign, speak and represent me as the owner in all matters relating to this parcel.

Printed Name of Person Authorized	Signature of Authorized Person
1. Randall Olney (CHW)	1. 19
2.	2.
3.	3.
4.	4.
5.	5.

I, the owner, realize that I am responsible for all agreements my duly authorized agent agrees with, and I am fully responsible for compliance with all Florida Statutes, City Codes, and Land Development Regulations pertaining to this parcel.

If at any time the person(s) you have authorized is/are no longer agents, employee(s), or officer(s), you must notify this department in writing of the changes and submit a new letter of authorization form, which will supersede all previous lists. Failure to do so may allow unauthorized persons to use your name and/or license number to obtain permits.

2-15-2023 **Owner** Signature (Notarized) Nato **NOTARY INFORMATION:** COUNTY OF: Alachua STATE OF: Florida The above person, whose name is Ma ason personally appeared before me and is known by me or has produced identification 20 23 on this 15 day of December (type of I.D.) OTARY'S SIGNATL (Seal/Stamp) Notary Public State of Florida Sonia R. Hopewell My Commission HH 428758 CO HIN Expires 8/2/2027



Department of State / Division of Corporations / Search Records / Search by Entity Name /

Detail by Entity Name

Florida Limited Liability Cor ST. JOHNS LIMITED LIABI			
Filing Information			
Document Number	L0500000431		
FEI/EIN Number	20-3739691		
Date Filed	12/23/2004		
Effective Date	01/01/2005		
State	FL		
Status	ACTIVE		
Principal Address			
13820 W Newberry Rd			
Suite 100			
GAINESVILLE, FL 32669			
Changed: 01/14/2018			
Mailing Address			
13820 W Newberry Rd			
Suite 100			
GAINESVILLE, FL 32669			
Changed: 01/14/2018			
Registered Agent Name & A	ddress		
Martin, William B			
13820 W Newberry Road			
Suite 100			
Newberry, FL 32669			
·			
Name Changed: 03/10/201	9		
Address Changed: 02/10/2/	010		
Address Changed: 03/10/20			
Authorized Person(s) Detail			
Name & Address			

Title MGR

Banks, Judith 13820 W Newberry Road Suite 100 Newberry, FL 32669

Title MGR

Martin, William B 13820 W Newberry Rd Suite 100 GAINESVILLE, FL 32669

Annual Reports

Report Year	Filed Date
2022	02/23/2022
2023	02/08/2023
2024	02/12/2024

Document Images

02/12/2024 ANNUAL REPORT	View image in PDF format
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02/23/2022 - ANNUAL REPORT	View image in PDF format
01/24/2021 ANNUAL REPORT	View image in PDF format
01/18/2020 ANNUAL REPORT	View image in PDF format
03/10/2019 ANNUAL REPORT	View image in PDF format
01/14/2018 ANNUAL REPORT	View image in PDF format
01/14/2017 ANNUAL REPORT	View image in PDF format
03/02/2016 - ANNUAL REPORT	View image in PDF format
01/25/2015 ANNUAL REPORT	View image in PDF format
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03/12/2009 ANNUAL REPORT	View image in PDF format
02/25/2008 ANNUAL REPORT	View image in PDF format
02/27/2007 - ANNUAL REPORT	View image in PDF format
06/21/2006 ANNUAL REPORT	View image in PDF format
12/23/2004 Florida Limited Liabilites	View image in PDF format





Department of State / Division of Corporations / Search Records / Search by Entity Name /

Detail by Entity Name

Florida Profit Corporation CONCEPT COMPANIES, I	NC.
Filing Information	
Document Number	P14000067003
FEI/EIN Number	47-1672849
Date Filed	08/07/2014
Effective Date	07/08/2009
State	FL
Status	ACTIVE
Last Event	CONVERSION
Event Date Filed	08/07/2014
Event Effective Date	NONE
Principal Address	
1449 SW 74th Drive	
Suite 200	
Gainesville, FL 32607	
Changed: 04/18/2022	
Mailing Address	
1449 SW 74th Drive	
Suite 200	
Gainesville, FL 32607	
Changed: 04/18/2022	
Registered Agent Name & A	ddress
Burch, Stephanie	
1449 SW 74th Drive	
Suite 200	
Gainesville, FL 32607	
Name Changed: 04/18/202	22
Address Changed: 04/18/2	022
Officer/Director Detail	

Name & Address

Title Founder and Principal

Crawford, Brian S 1449 SW 74th Drive Suite 200 Gainesville, FL 32607

Title President

Cason, Matthew 1449 SW 74th Drive Suite 200 Gainesville, FL 32607

Title CEO

Banks, Nick 1449 SW 74th Drive Suite 200 Gainesville, FL 32607

Annual Reports

Report Year	Filed Date
2022	04/18/2022
2023	03/03/2023
2024	03/11/2024

Document Images

03/11/2024 ANNUAL REPORT	View image in PDF format
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04/18/2022 ANNUAL REPORT	View image in PDF format
04/02/2021 - ANNUAL REPORT	View image in PDF format
06/09/2020 - ANNUAL REPORT	View image in PDF format
02/13/2019 - ANNUAL REPORT	View image in PDF format
04/26/2018 - ANNUAL REPORT	View image in PDF format
04/27/2017 ANNUAL REPORT	View image in PDF format
04/15/2016 ANNUAL REPORT	View image in PDF format
04/22/2015 ANNUAL REPORT	View image in PDF format
- 08/07/2014 Domestic Profit	View image in PDF format

Florida Department of State: Division of Corporations

Tax Record

Last Update: 3/20/2024 3:02:58 PM EDT

Register for eBill

Ad Valorem Taxes and Non-Ad Valorem Assessments

The information contained herein does not constitute a title search and should not be relied on as such.

	Account Number		Tax T	уре	Тах	Year
	R08127-005		REAL E	STATE	2	023
ST JOI 13820	n g Address HNS LLC W NEWBERRY RD STE RRY FL 32669	100	Propert	y Address		
				08127-005		
	Exempt Amount		Taxable			
	See Below		See Be	elow		
NO EXI	t ion Detail EMPTIONS Description (clic)	Millage 001 k for full d			crow Code	2
07-4S- LE 131	-17 0000/00009.69 1 18-991, DC 1327- 12 394- 679, 912-1064,	Acres S1/2 0 297, DC 1327	F NE1/4 O	F NE1/4 W OF		
7007	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		em Taxes			
Taxing 2	Authority	Rate	Assessed Value	Exemption	Taxable Value	Taxe: Levied
TTY OF LA	AKE CITY	4.9000	266,978	0	\$266,978	\$1,308.19
	COUNTY COMMISSIONERS	7.8150	266,978	0	\$266,978	\$2,086.43
	COUNTY SCHOOL BOARD		0.00 070	0	0000 070	\$199.70
	VARY	0.7480 3.2170	266,978 266,978	0	\$266,978 \$266,978	\$858.87
		3.2170		0	\$266,978	\$400.47
OCAL	TET AV	1 5000			42001010	+100111
COCAL		1.5000	266,978	0	\$266,978	\$83.11
OCAL CAPITAL OU SUWANNEE P	ITLAY RIVER WATER MGT DIST E HOSPITAL AUTHORITY	1.5000 0.3113 0.0001	266,978 266,978 266,978		\$266,978 \$266,978	•
LOCAL CAPITAL OU SUWANNEE P	RIVER WATER MGT DIST E HOSPITAL AUTHORITY	0.3113	266,978 266,978	0	\$266,978	\$83.11 \$0.03 4,936.80
OCAL CAPITAL OU SUWANNEE P	RIVER WATER MGT DIST E HOSPITAL AUTHORITY Total Millage	0.3113 0.0001 18.4914	266, 978 266, 978 T e	0 0 otal Taxes	\$266,978	\$0.03
GOCAL CAPITAL OU SUWANNEE P	NIVER WATER MGT DIST E HOSPITAL AUTHORITY Total Millage	0.3113 0.0001 18.4914 on-Ad Valore	266, 978 266, 978 T e	0 0 otal Taxes	\$266,978	\$0.03
JOCAL CAPITAL OU SUWANNEE H LAKE SHORE	NIVER WATER MGT DIST E HOSPITAL AUTHORITY Total Millage No. Levying Autho	0.3113 0.0001 18.4914 on-Ad Valore ority	266, 978 266, 978 T e	0 0 otal Taxes	\$266,978	\$0.03 4,936.80
LAKE SHORE	NIVER WATER MGT DIST E HOSPITAL AUTHORITY Total Millage No. Levying Autho	0.3113 0.0001 18.4914 on-Ad Valore ority	266, 978 266, 978 T e	0 0 otal Taxes	\$266,978	\$0.03 4,936.80 Amount
COCAL CAPITAL OU SUWANNEE F LAKE SHORE	NIVER WATER MGT DIST E HOSPITAL AUTHORITY Total Millage No. Levying Autho	0.3113 0.0001 18.4914 on-Ad Valore ority	266, 978 266, 978 Te	otal Taxes ments	\$266,978 \$	\$0.03 4,936.80 Amount \$61.26
COCAL CAPITAL OU SUWANNEE F LAKE SHORE	NIVER WATER MGT DIST E HOSPITAL AUTHORITY Total Millage No. Levying Autho	0.3113 0.0001 18.4914 on-Ad Valore ority	266, 978 266, 978 Te	0 0 otal Taxes	\$266,978 \$	\$0.03 4,936.80 Amount
COCAL CAPITAL OU SUWANNEE F LAKE SHORE	NIVER WATER MGT DIST E HOSPITAL AUTHORITY Total Millage No. Levying Autho	0.3113 0.0001 18.4914 on-Ad Valore ority	266, 978 266, 978 Tem Assess Tota	otal Taxes ments	\$266,978 \$	\$0.03 4,936.80 Amount \$61.26
LOCAL CAPITAL OU SUWANNEE F LAKE SHORE	NIVER WATER MGT DIST E HOSPITAL AUTHORITY Total Millage No. Levying Autho	0.3113 0.0001 18.4914 on-Ad Valore ority	266, 978 266, 978 Tem Assess Tota	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	\$266,978 \$ \$ \$ \$	\$0.03 4,936.80 Amount \$61.26 \$61.26

Date Paid	Transaction	Receipt	Item	Amount Paid
11/27/2023	PAYMENT	9921508.0001	2023	\$4,798.14

Prig	Year	Taxes	Due
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NO DELINQUENT TAXES

TRAFFIC IMPACT STUDY

Variety Retail Store Marvin Burnett Road Lake City, Florida

October 3, 2023

prepared for: FLORIDA DOT DISTRICT 2 and THE CITY OF LAKE CITY

submitted on behalf of: Concept Development, Inc.





PROFESSIONAL ENGINEER ENDORSEMENT

I hereby certify that I am a Registered Professional Engineer in the State of Florida and currently practicing as the principal of Hagen Consulting Services, LLC.

Hagen Consulting Services, LLC is authorized via Registry No: 27955 to operate as an Engineering Business by the Florida Board of Professional Engineers, State of Florida, Department of Professional Regulation.

I have prepared or supervised the preparation of the evaluation, findings, conclusions, recommendations, and professional opinions/advice contained in this document. My endorsement constitutes my approval of these items.

PROJECT: Marvin Burnett Road Retail Store **LOCATION:** Lake City, Florida **CLIENT:** Concept Development, Inc.

The results contained in this report were developed using procedures and references standard to the transportation engineering practice. These references and procedures were applied using professional judgment and experience.

Name: Lawrence T. Hagen, P.E., PTOE, RSP Florida P.E. No.: 43968



Lawrence T Hagen Digitally signed by Lawrence T Hagen Date: 2023.10.03 08:20:11 -04'00'

This item has been digitally signed and sealed by Lawrence T. Hagen on the date adjacent to the seal.

Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.



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EXECUTIVE SUMMARY

The results of the traffic impact analysis for the proposed variety retail store location at the intersection of State Road 47 and SW Marvin Burnett Road near the City of Lake City show that the traffic generated by the development will not have a significant impact on the operation of the roadway network surrounding it. The existing STOP-Controlled intersection adjacent to the project site will continue to operate well with the addition of the projected traffic from the development. Additionally, the nearby intersection of SW Bascom Norris Drive and SW Marvin Burnett Road will also continue to operate well.

The project location is within Columbia County south of the City of Lake City, Florida and State Road 47 is under the jurisdiction of the Florida DOT, District 2. This study utilized turning movement count data for the AM and PM Peak Hours collected by Hagen Consulting Services in July of 2023. The turning movement count information for the AM and PM Peak Hours of traffic were adjusted using a seasonal adjustment factor from FDOT's Peak Season Factor Category Report and a growth factor was applied to adjust traffic volumes to the build-out year (2024). The adjusted traffic volumes were then analyzed with and without the project traffic utilizing the Highway Capacity Manual (HCM) procedures.

The project traffic was developed using the Institute of Transportation Engineers (ITE) *Trip Generation* – 11^{th} Edition. The ITE Land Use Code for a variety retail store was used to estimate the trips generated by the proposed 12,480 square foot building. The trips were then distributed on the transportation network to estimate the traffic impacts.

The HCM analysis showed that the intersections, and hence the roadway network adjacent to the site, will be able to accommodate the traffic from the proposed development without a significant degradation in operational performance. Traffic conditions in the area will continue to operate at a very good level that meets the needs of the traveling public.



INTRODUCTION

Hagen Consulting Services, LLC is assisting Concept Development, Inc. with the transportation impacts for the proposed new 10,640 square foot variety retail store in Columbia County, Florida. The site will serve the southern Lake City area. The proposed retail store site is located on SW Marvin Burnett Road, at the intersection with State Road 47. State Road 47 is under the jurisdiction of the Florida Department of Transportation, District Two. The proposed site will have a connection to SW Marvin Burnett Road. The site currently is undeveloped and heavily wooded. There is a single family home foundation and accessory shed and propane tank on the site. The project location is shown in **Figure 1** below.

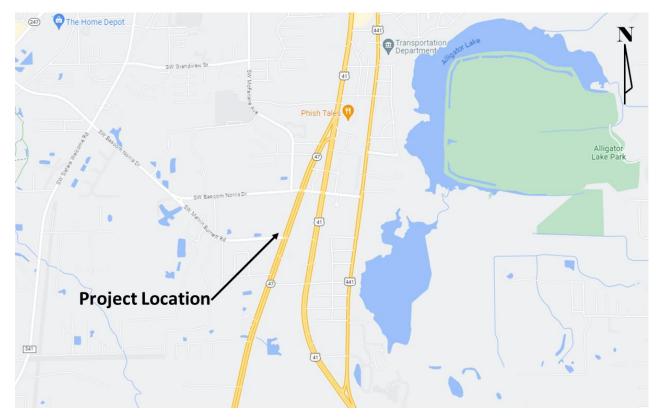


Figure 1 - Project Location Map

The preliminary site plan for the proposed retail store is shown in **Figure 2** on the following page.



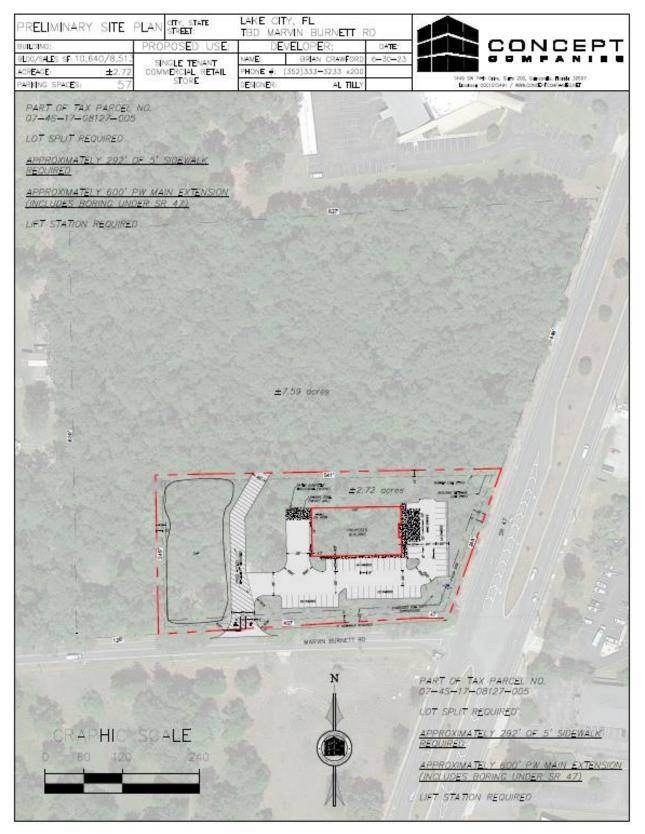


Figure 2 - Preliminary Site Plan



The 11th Edition of the Institute of Transportation Engineers (ITE) <u>*Trip Generation*</u> is the recognized authoritative source for estimating the trips generated by developments such as the proposed variety retail store facility. According to *Trip Generation*, a variety retail facility such as proposed here falls under ITE Land Use Code 814 – Variety Store. The assessment of the traffic impacts of the proposed variety retail store will be based on the impacts to traffic in the AM and PM peak hour periods.

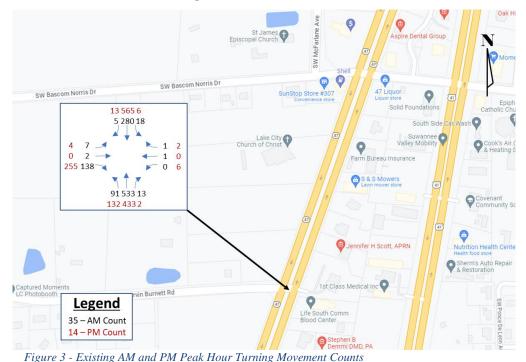
The traffic impacts of the proposed development will be based on a Highway Capacity Software analysis of the operation of the signalized intersection adjoining the site both with and without the traffic generated by the development. A comparison of the delay and Level Of Service (LOS) with and without the project traffic will serve as the basis of the analysis.



EXISTING CONDITIONS

State Road 47 is a four-lane divided highway with an urban typical section (curb and gutter). The posted speed limit in the vicinity of the project site is 45 miles per hour. There are existing bike lanes and sidewalks on both sides of the roadway. State Road 47 is classified as an Urban Minor Arterial. There are existing NB and SB left turn lanes at the Marvin Burnett Road intersection. Marvin Burnett Road is a two-lane roadway that is functionally classified as a minor collector rural with a posted speed of 35 miles per hour. The cross-section features a flush shoulder on the north side of the road and the south side has raised curb. There are currently no bike lanes or sidewalks present.

Existing AM and PM Peak Hour turning movement counts were collected at the intersection of State Road 47 and Marvin Burnett Road. Two hours of AM Peak data (7:00 AM – 9:00 AM) and two hours of PM Peak data (4:00 PM – 6:00 PM) were collected. From these counts, the AM Peak Hour (7:30 – 8:30 AM) and PM Peak Hour (4:30 – 5:30 PM) turning movement counts were determined. The AM and PM Peak Hour turning movement counts are shown in **Figure 3** below.



The raw turning movement count data for the AM and PM Peak Hour is included in Appendix A.



TRIP GENERATION

The Institute of Transportation Engineers (ITE) *Trip Generation* 11th Edition was used to calculate the project trip estimates for the new land use at the project site. Trip generations estimates are shown in terms of daily traffic, as well as the AM and PM peak hours. The proposed Variety Retail Store falls under ITE Land Use Code 814 – Variety Store. The trip generation information for the proposed Variety Retail Store is shown in Table 1 below.

TABLE 1: Trip GenerationVariety Retail Store – ITE Land Use 814 – 10,640 SFLake City, Florida

				Distril	oution	Trips			
Period	ITE Rate	Units	Trips	%In	% Out	In	Out	Net	
Weekday	T = 63.66 (X)	10.64	677	50%	50%	339	338	677	
AM Peak	T = 3.04 (X)	10.64	32	55%	45%	18	14	32	
PM Peak	T = 6.70 (X)	10.64	71	51%	49%	36	35	71	

Source: ITE 11th Edition of Trip Generation - Units: 1,000 square feet Gross Floor Area

The 2021 Pass-By Tables for ITE's *Trip Generation* indicate a 34% pass-by rate for Land Use 814. This means that 34% of the trips generated are existing pass-by trips, and the net new trips represent 66% of the estimated *Trip Generation* number.

TABLE 2: Net Trip Generation with Pass-By Reduction

				Distri				
Period	Trips	Pass-By	Net Trips	% In	% Out	In	Out	Net
Weekday	677	34%	447	50%	50%	224	224	447
AM Peak	32	34%	21	55%	45%	12	10	21
PM Peak	71	34%	47	51%	49%	24	23	47

The trip generation data is then used to develop the external distribution of project trips onto the adjacent roadway network from the project site. The next section of the report presents information on the trip distribution.



TRIP DISTRIBUTION

The distribution of project trips on the roadway network is a manual assignment derived from the AM and PM peak period traffic data collected on the adjacent roadway and a review of existing locations of interacting land-uses. The distribution is based on engineering judgment of the expected routes that patrons would take to / from the proposed development. The project has access just on SW Marvin Burnett Road. The AM and PM Peak Hour Project Trip Distribution is shown in **Figure 4** below.

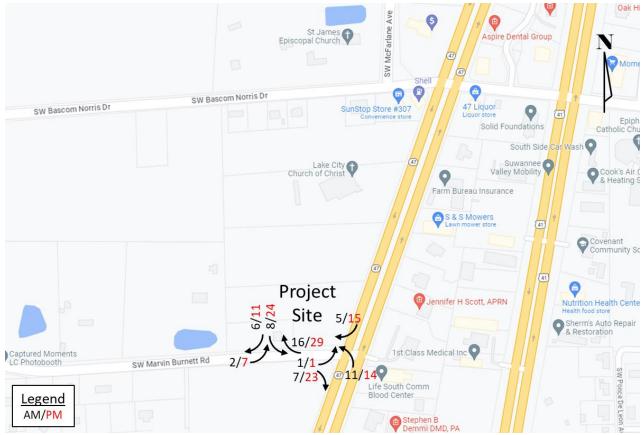


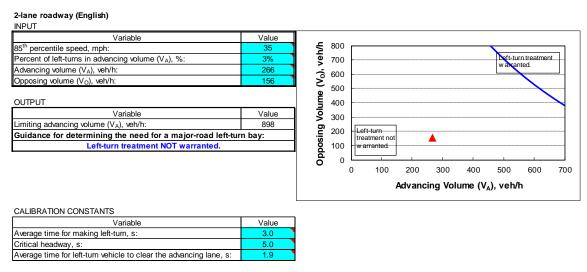
Figure 4 - Peak Hour Project Trip Distribution



LEFT TURN LANE ANALYSIS - Marvin Burnett Road

The criteria for evaluating left turn lanes are established in *NCHRP Report 457: Evaluating Intersection Improvements: An Engineering Study Guide.* The highest left turning volume into the project site from Marvin Burnett Road is the PM Peak Hour left turn volume of 7 vehicles. The left + through + right turn volumes are added together to compute the "advancing volume." The through + right turning volumes opposing the left turn are used as the "opposing volume."

Figure 2 - 5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.



RIGHT TURN LANE ANALYSIS – Marvin Barnett Road

Similarly, the criteria for evaluating right turn lanes are established in *NCHRP Report 457: Evaluating Intersection Improvements: An Engineering Study Guide*. For this analysis, we need to enter the major road speed, the major road volume (through + right), and the right turn volume.

Figure 2 - 6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-cor	ntrolled intersection.
--	------------------------

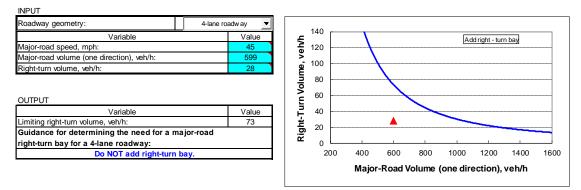
INPUT										
Roadway geometry:	2-lane roadw ay 🔹									
Variable	Value	ع ا	140				Ac	ld right - tur	n hav	
Major-road speed, mph:	35	eh/h	120				7.0	a right tu	ii buy	
Major-road volume (one direction), veh/h:	156	>	100		_ \					
Right-turn volume, veh/h:	29	je je	100							
		Volume,	80							
OUTPUT		urn Vo	60							
Variable	Value	12	40			<u> </u>				
Limiting right-turn volume, veh/h:	14198	Right-T	20							
Guidance for determining the need for a major	-road	ß	20							
right-turn bay for a 2-lane roadway:			0							
Do NOT add right-turn bay.			200	400	600	800	1000	1200	1400	1600
				Major	r-Road V	/olume	(one dire	ection),	veh/h	



RIGHT TURN LANE ANALYSIS – State Road 47

As indicated previously, the criteria for evaluating right turn lanes are established in *NCHRP Report 457: Evaluating Intersection Improvements: An Engineering Study Guide.* For this analysis, we need to enter the major road speed, the major road volume (left + through + right), and the right turn volume.







INTERSECTION LEVEL OF SERVICE (LOS) ANALYSIS

The roadway Level Of Service (LOS) analysis is conducted using the procedures outlined in the Transportation Research Board's *Highway Capacity Manual* (HCM). The HCM procedures represent the state-of-the-practice for the analysis of transportation facilities.

Existing turning movement count data was collected on Tuesday, July 18, 2023 at the intersection of State Road 47 and SW Marvin Burnett Road. Two hours of turning movement count data were collected for both the AM peak period (7 AM to 9 AM) and the PM peak period (4 PM to 6 PM). Out of that two-hours of data collection in each period, the overall AM peak hour of 7:30 AM to 8:30 AM and the overall PM peak hour of 4:30 PM to 5:30 PM were used in the analysis. A seasonal adjustment of 1.02 is then applied based on FDOT Peak Season Factor Category Report for Columbia County (included in Appendix A). A growth factor of 3% is then added to the volumes to convert to 2024 (expected build-out year) volumes. The AM peak hour volumes along with the assigned new project trips are provided in **Table 3** below. The PM peak hour volumes along with the assigned new project trips are provided in **Table 4** below.

Roadway			State R	Road 47	7		SW Marvin Burnett Road					
Approach	Northbound			Southbound			Eastbound			Westbound		
Movement	Lt	Thru	Rt	Lt	Thru	Rt	Lt	Thru	Rt	Lt	Thru	Rt
2023	91	533	13	18	280	5	7	2	138	0	1	1
Seasonal	93	544	13	18	286	5	7	2	141	0	1	1
2024	96	560	14	19	294	5	7	2	145	0	1	1
Project	11	0	0	0	0	5	1	0	7	0	0	0
Total	107	560	14	19	294	10	8	2	152	0	1	1

Table 3 – AM Peak Hour Volumes

Roadway			State R	Road 47	7		SW Marvin Burnett Road						
Approach	Northbound			Southbound			Ea	Eastbound			Westbound		
Movement	Lt	Thru	Rt	Lt	Thru	Rt	Lt	Thru	Rt	Lt	Thru	Rt	
2023	132	433	2	6	565	13	4	0	255	6	0	2	
Seasonal	135	442	2	6	576	13	4	0	260	6	0	2	
2024	139	455	2	6	594	14	4	0	268	6	0	2	
Project	14	0	0	0	0	15	1	0	23	0	0	0	
Total	153	455	2	6	594	29	5	0	291	6	0	2	



The Highway Capacity Software (HCS) Two-Way Stop-Controlled intersection module was utilized in analyzing the no-build and the build-out traffic volumes at the intersection of SR 47 and Marvin Burnett Road. The results from the HCS analyses are summarized in **Table 5** and **Table 6** below. The outputs from HCS are included in Appendix B.

Table 5 – Intersection Level Of Service (AM)											
Roadway	• •	State R	load 47	,	SW Marvin Burnett Road						
Approach	North	bound	South	bound	Eastb	ound	Westbound				
MOE	Delay LOS Delay LOS [Delay	LOS	Delay	LOS					
No-Build	8.3	А	9.0	А	11.3	В	19.4	С			
Build	8.3	А	9.0	А	11.5	В	20.1	С			
	Roadway Approach MOE No-Build	RoadwayApproachMOEDelayNo-Build8.3	RoadwayState RApproachNorthboundMOEDelayLOSNo-Build8.3A	RoadwayState Road 47ApproachNorthboundSouthMOEDelayLOSDelayNo-Build8.3A9.0	RoadwayState Road 47ApproachNorthboundSouthboundMOEDelayLOSDelayLOSNo-Build8.3A9.0A	RoadwayState Road 47SW MApproachNorthboundSouthboundEastbMOEDelayLOSDelayLOSDelayNo-Build8.3A9.0A11.3	RoadwayState Road 47SW Marvin EApproachNorthboundSouthboundEastboundMOEDelayLOSDelayLOSDelayLOSNo-Build8.3A9.0A11.3B	RoadwayState Road 47SW Marvin BurnettApproachNorthboundSouthboundEastboundWestboundMOEDelayLOSDelayLOSDelayLOSDelayNo-Build8.3A9.0A11.3B19.4			

 Table 5 – Intersection Level Of Service (AM)

Table	Table 0 – Intel section Level Of Service (TWI)												
Roadway		State F	Road 47	,	SW Marvin Burnett Road								
Approach	North	bound	South	bound	Eastb	ound	Westbound						
MOE	Delay LOS Delay LOS		Delay	LOS	Delay	LOS							
No-Build	9.8	А	8.5	А	15.9	С	28.8	D					
Build	10.0	В	8.5	А	17.2	С	35.0	Е					

Table 6 – Intersection Level Of Service (PM)

The HCS analyses show that the impacts of the proposed variety retail store development on the operation of the intersection are minimal in the AM period. In the PM period, the westbound approach degrades from LOS D to LOS E, despite the fact that the project assigns no trips to the westbound approach. The westbound approach is a minor approach to the intersection and even in the LOS E scenario is operating at a volume to capacity ratio of 0.07 with an hourly flow rate of just nine vehicles. The HCS two-way stop-controlled analysis is well known for being overly pessimistic, and this is an example of that. An average delay of 35 seconds is not an intolerable scenario for those vehicles.



The City of Lake City requested that the intersection of SW Bascom Norris Drive and SW Marvin Burnett Road also be analyzed for this project. Existing turning movement count data was also collected on Tuesday, July 18, 2023 at this intersection. Two hours of turning movement count data were collected for both the AM peak period (7 AM to 9 AM) and the PM peak period (4 PM to 6 PM). Out of that two-hours of data collection in each period, the overall AM peak hour of 7:30 AM to 8:30 AM and the overall PM peak hour of 4:45 PM to 5:45 PM were used in the analysis. A seasonal adjustment of 1.02 is then applied based on FDOT Peak Season Factor Category Report for Columbia County. A growth factor of 3% is then added to the volumes to convert to 2024 (expected build-out year) volumes. The AM peak hour volumes along with the assigned new project trips are provided in **Table 8** below. For this analysis, a worst-case scenario where all of the project trips from the proposed retail site are presumed to make a northbound left at the intersection.

Roadway		SW Marvin Burnett Road						SW Bascom Norris Drive					
Approach	Northbound			Southbound			Eastbound			Westbound			
Movement	Lt	Thru	Rt	Lt	Thru	Rt	Lt	Thru	Rt	Lt	Thru	Rt	
2023	102	0	0	-	-	-	0	234	0	0	249	0	
Seasonal	104	0	0	-	-	-	0	239	0	0	254	0	
2024	107	0	0	-	-	-	0	246	0	0	262	0	
Project	6	0	0	-	-	-	0	0	0	0	0	0	
Total	113	0	0	-	-	-	0	246	0	0	262	0	

 Table 7 – AM Peak Hour Volumes

Table 8 – PM Peak Hour Volumes

Roadway		SW M	arvin E	Burnet	t Road		SW Bascom Norris Drive						
Approach	No	Northbound			Southbound			Eastbound			Westbound		
Movement	Lt	Thru	Rt	Lt	Thru	Rt	Lt	Thru	Rt	Lt	Thru	Rt	
2023	145	0	2	-	-	-	0	205	0	0	422	0	
Seasonal	148	0	2	-	-	-	0	209	0	0	430	0	
2024	152	0	2	-	-	-	0	215	0	0	443	0	
Project	11	0	0	-	-	-	0	0	0	0	0	0	
Total	163	0	2	-	-	-	0	215	0	0	443	0	



The intersection of Bascom Norris Drive and Marvin Burnett Road is a somewhat unusual T-intersection: Bascom Norris Drive is the major street that does not stop, and Marvin Burnett Road intersects and is controlled by a STOP sign. However, the left turn from Bascom Norris Drive WB onto Marvin Burnett Road is prohibited, and the right turn from Bascom Norris Drive EB onto Marvin Burnett Road is a free-flowing movement that is channelized and unimpeded. Thus, the only movement that has any control delay is the northbound left or right turn from Marvin Barnett Road onto Bascom Norris Drive. The layout of the intersection is shown in **Figure 5** below.



Figure 5 - SW Bascom Norris Dr & SW Marvin Burnett Rd

The results from the HCS analyses are summarized in **Table 9** and **Table 10** below. The outputs from HCS are included in Appendix B.



I able	/ 11	1101 50							
Roadway	SW M	larvin E	Burnett	Road	SW Bascom Norris Drive				
Approach	North	bound	South	bound	Eastb	ound	Westbound		
MOE	Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS	
No-Build	15.8	С	-	-	-	-	-	-	
Build	16.1	С	-	-	-	-	-	-	

 Table 9 – Intersection Level Of Service (AM)

Table 1	10 – Inters	section Lev	el Of Serv	vice (PM)
Roadway	SW Marvin I	Burnett Road	SW Bascom	Norris Drive

Roadway	SW M	larvin E	Burnett	Road	SW Bascom Norris Drive							
Approach	North	bound	South	bound	Eastb	ound	Westbound					
MOE	Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS				
No-Build	24.6	С	-	I	-	-	-	-				
Build	26.0	D	-	I	-	-	-	-				

The HCS analyses show that the impact of the project traffic on the intersection of SW Marvin Burnett Road and SW Bascom Norris Drive is minimal. Although in the PM period the LOS does go from C to D, it is only an increase of 1.4 seconds of delay per vehicle. This movement operates with a volume to capacity ratio of just 0.54 in the PM period with the project traffic.



CONCLUSIONS AND RECOMMENDATIONS

Based on the foregoing data and analysis provided, the following conclusions and recommendations are offered:

Conclusions:

- The proposed variety retail store is estimated to generate 32 trips in the AM Peak Hour and 71 trips in the PM Peak Hour. To be conservative in the analyses, these numbers were used. If the pass-by reductions from ITE are used, the net trips would be 21 in the AM Peak Hour and 47 in the PM Peak Hour.
- The additional traffic generated by the proposed variety retail store will not have a noticeable impact on the adjoining STOP-controlled intersections and will not degrade the performance of the transportation network.
- Neither left-turn lanes nor right-turn lanes are warranted on either State Road 47 or on SW Marvin Burnett Road. There is very little disruption to traffic with the addition of the project driveways and the generated project traffic.

Recommendations:

• Approve the project for construction and approve the associated driveway connection onto SW Marvin Burnett Road.

APPENDIX A: TURNING MOVEMENT COUNTS

Tue Jul 18, 2023

Full Length (7 AM-9 AM, 4 PM-6 PM) All Classes (Lights and Motorcycles, Heavy)

All Movements

ID: 1091860, Location: 30.160196, -82.645384, Site Code: SR 47 & Marvin Burnett



Provided by: Hagen Consulting Services 361 Strawder Road, Ray City, GA, 31645, US

Leg	Marvir	1 Burne	tt Road	1		Radiati	on Onc	ology (Grp		SR 47					SR 47					
Direction	Eastbo	und				Westbo	ound				Northb	ound				South	oound				
Time	L	Т	R	U	Арр	L	Т	R	U	Арр	L	Т	R	U	Арр	L	Т	R	U	Арр	Int
2023-07-18 7:00AM	0	0	17	0	17	0	0	0	0	0	13	91	2	0	106	0	58	1	1	60	183
7:15AM	1	0	16	0	17	0	0	0	0	0	16	140	2	0	158	0	42	0	0	42	217
7:30AM	2	0	34	0	36	0	0	0	0	0	20	163	3	0	186	2	63	1	4	70	292
7:45AM	0	0	35	0	35	0	1	0	0	1	27	150	3	0	180	1	82	2	4	89	305
Hourly Total	3	0	102	0	105	0	1	0	0	1	76	544	10	0	630	3	245	4	9	261	997
8:00AM	2	0	31	0	33	0	0	1	0	1	23	121	5	0	149	0	63	2	4	69	252
8:15AM	3	2	38	0	43	0	0	0	0	0	20	99	2	1	122	1	72	0	2	75	240
8:30AM	0	1	33	0	34	0	1	2	0	3	28	117	1	0	146	0	54	1	2	57	240
8:45AM	3	0	40	1	44	0	0	2	0	2	32	137	1	0	170	1	65	0	2	68	284
Hourly Total	8	3	142	1	154	0	1	5	0	6	103	474	9	1	587	2	254	3	10	269	1016
4:00PM	2	0	51	0	53	1	0	0	0	1	33	90	0	1	124	0	124	3	2	129	307
4:15PM	3	0	71	0	74	1	1	0	0	2	27	92	0	1	120	0	103	3	1	107	303
4:30PM	1	0	64	0	65	3	0	0	0	3	21	117	1	1	140	0	141	3	4	148	356
4:45PM	0	0	67	0	67	0	0	1	0	1	35	96	0	3	134	0	137	0	1	138	340
Hourly Total	6	0	253	0	259	5	1	1		7	116	395	1	6	518	0	505	9	8	522	1306
5:00PM	1	0	63	0	64	3	0	0	0	3	36	133	1	9	179	0	147	7	0	154	400
5:15PM	2	0	61	0	63	0	0	1	0	1	21	97	0	6	124	0	140	3	1	144	332
5:30PM	2	0	66	1	69	3	0	0	0	3	36	88	0	6	130	1	148	4	1	154	356
5:45PM	0	0	79	0	79	0	0	0	0	0	24	76	1	1	102	0	99	1	1	101	282
Hourly Total	5	0	269	1	275	6	0	1	0	7	117	394	2	22	535	1	534	15	3	553	1370
Total	22	3	766	2	793	11	3	7	0	21	412	1807	22	29	2270	6	1538	31	30	1605	4689
% Approach	2.8%	0.4%	96.6%	0.3%	-	52.4%	14.3%	33.3%	0%	-	18.1%	79.6%	1.0%	1.3%	-	0.4%	95.8%	1.9%	1.9%	-	-
% Total	0.5%	0.1%	16.3%	0%	16.9%	0.2%	0.1%	0.1%	0%	0.4%	8.8%	38.5%	0.5%	0.6%	48.4%	0.1%	32.8%	0.7%	0.6%	34.2%	-
Lights and Motorcycles	21	3	759	2	785	11	2	7	0	20	410	1743	22	28	2203	6	1489	28	29	1552	4560
% Lights and Motorcycles	95.5%	100%	99.1%	100%	99.0%	100%	66.7%	100%	0%	95.2%	99.5%	96.5%	100% 9	96.6%	97.0%	100%	96.8%	90.3%	96.7%	96.7%	97.2%
Heavy	1	0	7	0	8	0	1	0	0	1	2	64	0	1	67	0	49	3	1	53	129
% Heavy	4.5%	0%	0.9%	0%	1.0%	0%	33.3%	0%	0%	4.8%	0.5%	3.5%	0%	3.4%	3.0%	0%	3.2%	9.7%	3.3%	3.3%	2.8%

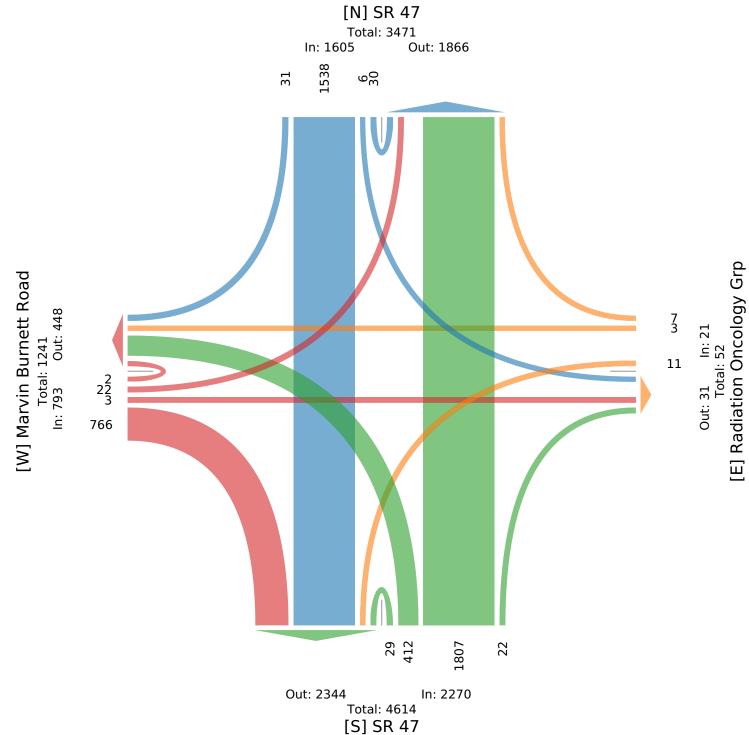
*L: Left, R: Right, T: Thru, U: U-Turn

Tue Jul 18, 2023 Full Length (7 AM-9 AM, 4 PM-6 PM)

All Classes (Lights and Motorcycles, Heavy)

All Movements

ID: 1091860, Location: 30.160196, -82.645384, Site Code: SR 47 & Marvin Burnett



6

ING

SERVICES, LLC

Provided by: Hagen Consulting Services

361 Strawder Road, Ray City, GA, 31645, US

AGEN Consulting Services, LLC

AM Peak (7:30 AM - 8:30 AM) All Classes (Lights and Motorcycles, Heavy)

All Movements

Tue Jul 18, 2023

ID: 1091860, Location: 30.160196, -82.645384, Site Code: SR 47 & Marvin Burnett

Provided by: Hagen Consulting Services 361 Strawder Road, Ray City, GA, 31645, US

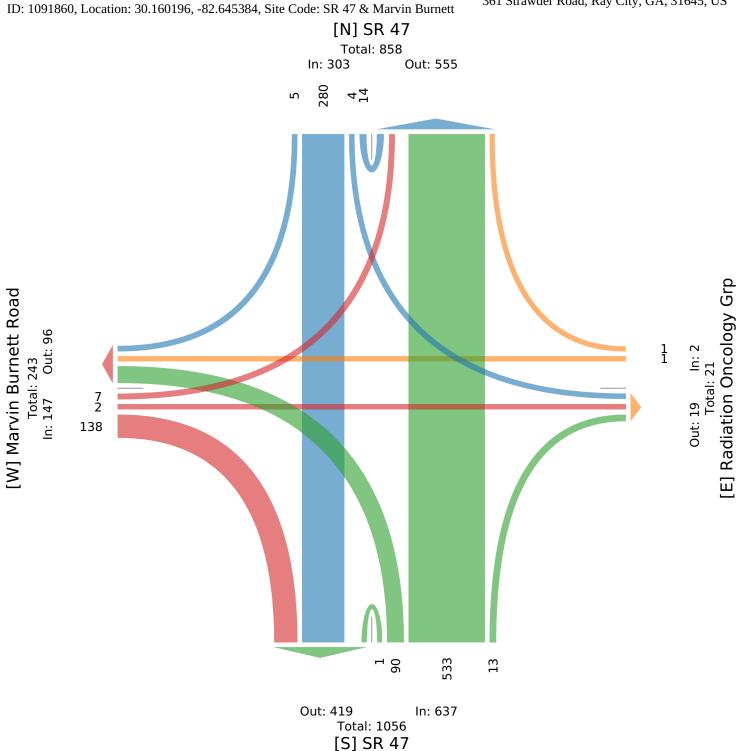
Leg	Marvii	n Burn	ett Road	1		Rad	iation C	ncolog	y Gr	p	SR 47					SR 47					
Direction	Eastbo	ound				Wes	stbound				Northb	ound				Southb	ound				
Time	L	Т	R	U	Арр	L	Т	R	U	Арр	L	Т	R	U	Арр	L	Т	R	U	Арр	Int
2023-07-18 7:30AM	2	0	34	0	36	0	0	0	0	0	20	163	3	0	186	2	63	1	4	70	292
7:45AM	0	0	35	0	35	0	1	0	0	1	27	150	3	0	180	1	82	2	4	89	305
8:00AM	2	0	31	0	33	0	0	1	0	1	23	121	5	0	149	0	63	2	4	69	252
8:15AM	3	2	38	0	43	0	0	0	0	0	20	99	2	1	122	1	72	0	2	75	240
Total	7	2	138	0	147	0	1	1	0	2	90	533	13	1	637	4	280	5	14	303	1089
% Approach	4.8%	1.4%	93.9%	0%	-	0%	50.0%	50.0%	0%	-	14.1%	83.7%	2.0%	0.2%	-	1.3%	92.4%	1.7%	4.6%	-	-
% Total	0.6%	0.2%	12.7%	0%	13.5%	0%	0.1%	0.1%	0%	0.2%	8.3%	48.9%	1.2%	0.1%	58.5%	0.4%	25.7%	0.5%	1.3%	27.8%	-
PHF	0.583	0.250	0.908	-	0.855	-	0.250	0.250	-	0.500	0.833	0.817	0.650	0.250	0.856	0.500	0.854	0.625	0.875	0.851	0.893
Lights and Motorcycles	7	2	137	0	146	0	0	1	0	1	89	515	13	1	618	4	272	3	13	292	1057
% Lights and Motorcycles	100%	100%	99.3%	0%	99.3%	0%	0%	100%	0%	50.0%	98.9%	96.6%	100%	100%	97.0%	100%	97.1%	60.0%	92.9%	96.4%	97.1%
Heavy	0	0	1	0	1	0	1	0	0	1	1	18	0	0	19	0	8	2	1	11	32
% Heavy	0%	0%	0.7%	0%	0.7%	0%	100%	0%	0%	50.0%	1.1%	3.4%	0%	0%	3.0%	0%	2.9%	40.0%	7.1%	3.6%	2.9%

*L: Left, R: Right, T: Thru, U: U-Turn

Tue Jul 18, 2023 AM Peak (7:30 AM - 8:30 AM) All Classes (Lights and Motorcycles, Heavy) All Movements



Provided by: Hagen Consulting Services 361 Strawder Road, Ray City, GA, 31645, US



Tue Jul 18, 2023 PM Peak (4:30 PM - 5:30 PM) - Overall Peak Hour All Classes (Lights and Motorcycles, Heavy) All Movements

ID: 1091860, Location: 30.160196, -82.645384, Site Code: SR 47 & Marvin Burnett



Provided by: Hagen Consulting Services 361 Strawder Road, Ray City, GA, 31645, US

Leg	Marvin	Bur	nett Roa	ıd		Radiatio	n O	ncology	/ Gr)	SR 47					SR -	47				
Direction	Eastbo	und				Westbou	ind				Northbo	ound				Sou	thbound				
Time	L	Т	R	U	Арр	L	Т	R	U	Арр	L	Т	R	U	Арр	L	Т	R	U	Арр	Int
2023-07-18 4:30PM	1	0	64	0	65	3	0	0	0	3	21	117	1	1	140	0	141	3	4	148	356
4:45PM	0	0	67	0	67	0	0	1	0	1	35	96	0	3	134	0	137	0	1	138	340
5:00PM	1	0	63	0	64	3	0	0	0	3	36	133	1	9	179	0	147	7	0	154	400
5:15PM	2	0	61	0	63	0	0	1	0	1	21	97	0	6	124	0	140	3	1	144	332
Total	4	0	255	0	259	6	0	2	0	8	113	443	2	19	577	0	565	13	6	584	1428
% Approach	1.5%	0%	98.5%	0%	-	75.0%	0%	25.0%	0%	-	19.6%	76.8%	0.3%	3.3%	-	0%	96.7%	2.2%	1.0%	-	-
% Total	0.3%	0%	17.9%	0%	18.1%	0.4%	0%	0.1%	0%	0.6%	7.9%	31.0%	0.1%	1.3%	40.4%	0%	39.6%	0.9%	0.4%	40.9%	-
PHF	0.500	-	0.951	-	0.966	0.500	-	0.500	-	0.667	0.785	0.833	0.500	0.528	0.806	-	0.961	0.464	0.375	0.948	0.893
Lights and Motorcycles	3	0	253	0	256	6	0	2	0	8	113	430	2	18	563	0	549	12	6	567	1394
% Lights and Motorcycles	75.0%	0%	99.2%	0%	98.8%	100%	0%	100%	0%	100%	100%	97.1%	100%	94.7%	97.6%	0%	97.2%	92.3%	100%	97.1%	97.6%
Heavy	1	0	2	0	3	0	0	0	0	0	0	13	0	1	14	0	16	1	0	17	34
% Heavy	25.0%	0%	0.8%	0%	1.2%	0%	0%	0%	0%	0%	0%	2.9%	0%	5.3%	2.4%	0%	2.8%	7.7%	0%	2.9%	2.4%

*L: Left, R: Right, T: Thru, U: U-Turn

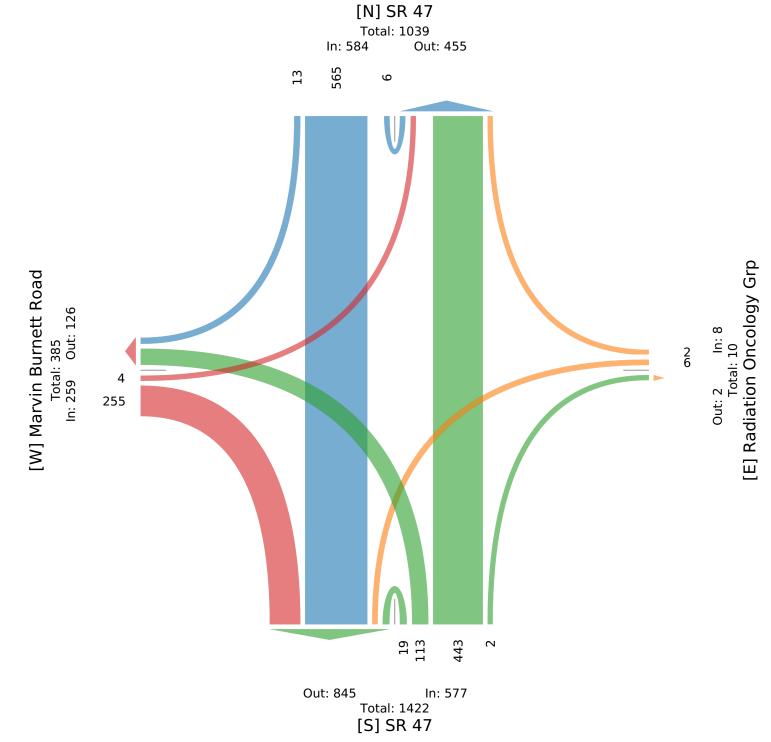
Tue Jul 18, 2023

PM Peak (4:30 PM - 5:30 PM) - Overall Peak Hour

All Classes (Lights and Motorcycles, Heavy)

All Movements

ID: 1091860, Location: 30.160196, -82.645384, Site Code: SR 47 & Marvin Burnett



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Marvin Burnett & Bascom Norris - TMC

Tue Jul 18, 2023 Full Length (7 AM-9 AM, 4 PM-6 PM) All Classes (Lights and Motorcycles, Heavy)

All Movements

ID: 1091861, Location: 30.163397, -82.655082, Site Code: Marvin Burnett & Bascom Norris



Provided by: Hagen Consulting Services 361 Strawder Road, Ray City, GA, 31645, US

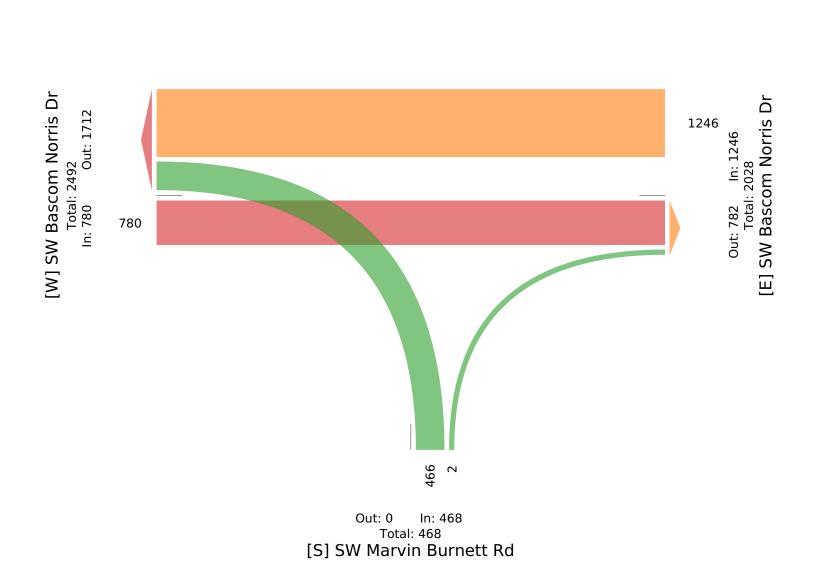
Leg	SW Bascom	Norris	Dr		SW Base	com Norris	Dr		SW Marvin I	Burnett Rd	1		
Direction	Eastbound				Westbou	ind			Northbound				
Time	Т	R	U	Арр	L	Т	U	Арр	L	R	U	Арр	Int
2023-07-18 7:00AM	33	0	0	33	0	27	0	27	16	0	0	16	76
7:15AM	31	0	0	31	0	48	0	48	16	0	0	16	95
7:30AM	59	0	0	59	0	63	0	63	21	0	0	21	143
7:45AM	78	0	0	78	0	63	0	63	34	0	0	34	175
Hourly Total	201	0	0	201	0	201	0	201	87	0	0	87	489
8:00AM	41	0	0	41	0	58	0	58	24	0	0	24	123
8:15AM	56	0	0	56	0	65	0	65	23	0	0	23	144
8:30AM	49	0	0	49	0	57	0	57	26	0	0	26	132
8:45AM	41	0	0	41	0	74	0	74	38	0	0	38	153
Hourly Total	187	0	0	187	0	254	0	254	111	0	0	111	552
4:00PM	43	0	0	43	0	103	0	103	36	0	0	36	182
4:15PM	1 52	0	0	52	0	107	0	107	38	0	0	38	197
4:30PM	48	0	0	48	0	97	0	97	20	0	0	20	165
4:45PM	48	0	0	48	0	95	0	95	32	0	0	32	175
Hourly Total	191	0	0	191	0	402	0	402	126	0	0	126	719
5:00PM	I 52	0	0	52	0	142	0	142	35	0	0	35	229
5:15PM	I 58	0	0	58	0	98	0	98	22	1	0	23	179
5:30PM	[47	0	0	47	0	87	0	87	56	1	0	57	191
5:45PM	[44	0	0	44	0	62	0	62	29	0	0	29	135
Hourly Total	201	0	0	201	0	389	0	389	142	2	0	144	734
Total	780	0	0	780	0	1246	0	1246	466	2	0	468	2494
% Approach	100%	0%	0%	-	0%	100%	0%	-	99.6%	0.4%	0%	-	-
% Total	31.3%	0%	0%	31.3%	0%	50.0%	0%	50.0%	18.7%	0.1%	0%	18.8%	-
Lights and Motorcycles	759	0	0	759	0	1221	0	1221	461	2	0	463	2443
% Lights and Motorcycles	97.3%	0%	0%	97.3%	0%	98.0%	0%	98.0%	98.9%	100%	0%	98.9%	98.0%
Неаvy	21	0	0	21	0	25	0	25	5	0	0	5	51
% Heavy	2.7%	0%	0%	2.7%	0%	2.0%	0%	2.0%	1.1%	0%	0%	1.1%	2.0%

*L: Left, R: Right, T: Thru, U: U-Turn

Marvin Burnett & Bascom Norris - TMC

Tue Jul 18, 2023 Full Length (7 AM-9 AM, 4 PM-6 PM) All Classes (Lights and Motorcycles, Heavy) All Movements ID: 1091861, Location: 30.163397, -82.655082, Site Code: Marvin Burnett & Bascom Norris





Marvin Burnett & Bascom Norris - TMC

Tue Jul 18, 2023 AM Peak (7:30 AM - 8:30 AM) All Classes (Lights and Motorcycles, Heavy) All Movements ID: 1091861, Location: 30.163397, -82.655082, Site Code: Marvin Burnett & Bascom Norris



Provided by: Hagen Consulting Services 361 Strawder Road, Ray City, GA, 31645, US

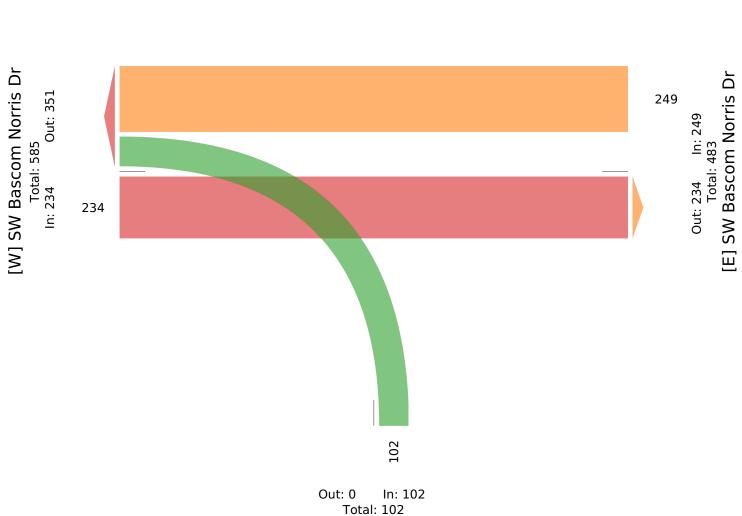
Leg	SW Bascom	Norris	Dr		SW Base	com Norris	Dr		SW Marvin E	Burnett	Rd		
Direction	Eastbound				Westbou	ınd			Northbound				
Time	Т	R	U	Арр	L	Т	U	Арр	L	R	U	Арр	Int
2023-07-18 7:30AM	59	0	0	59	0	63	0	63	21	0	0	21	143
7:45AM	78	0	0	78	0	63	0	63	34	0	0	34	175
8:00AM	41	0	0	41	0	58	0	58	24	0	0	24	123
8:15AM	56	0	0	56	0	65	0	65	23	0	0	23	144
Total	234	0	0	234	0	249	0	249	102	0	0	102	585
% Approach	100%	0%	0%	-	0%	100%	0%	-	100%	0%	0%	-	-
% Total	40.0%	0%	0%	40.0%	0%	42.6%	0%	42.6%	17.4%	0%	0%	17.4%	-
PHF	0.750	-	-	0.750	-	0.958	-	0.958	0.750	-	-	0.750	0.836
Lights and Motorcycles	222	0	0	222	0	240	0	240	99	0	0	99	561
% Lights and Motorcycles	94.9%	0%	0%	94.9%	0%	96.4%	0%	96.4%	97.1%	0%	0%	97.1%	95.9%
Heavy	12	0	0	12	0	9	0	9	3	0	0	3	24
% Heavy	5.1%	0%	0%	5.1%	0%	3.6%	0%	3.6%	2.9%	0%	0%	2.9%	4.1%

*L: Left, R: Right, T: Thru, U: U-Turn

Marvin Burnett & Bascom Norris - TMC

Tue Jul 18, 2023 AM Peak (7:30 AM - 8:30 AM) All Classes (Lights and Motorcycles, Heavy) All Movements ID: 1091861, Location: 30.163397, -82.655082, Site Code: Marvin Burnett & Bascom Norris





[S] SW Marvin Burnett Rd

Marvin Burnett & Bascom Norris - TMC

Tue Jul 18, 2023 PM Peak (4:45 PM - 5:45 PM) - Overall Peak Hour All Classes (Lights and Motorcycles, Heavy) All Movements ID: 1091861, Location: 30.163397, -82.655082, Site Code: Marvin Burnett & Bascom Norris



Provided by: Hagen Consulting Services 361 Strawder Road, Ray City, GA, 31645, US

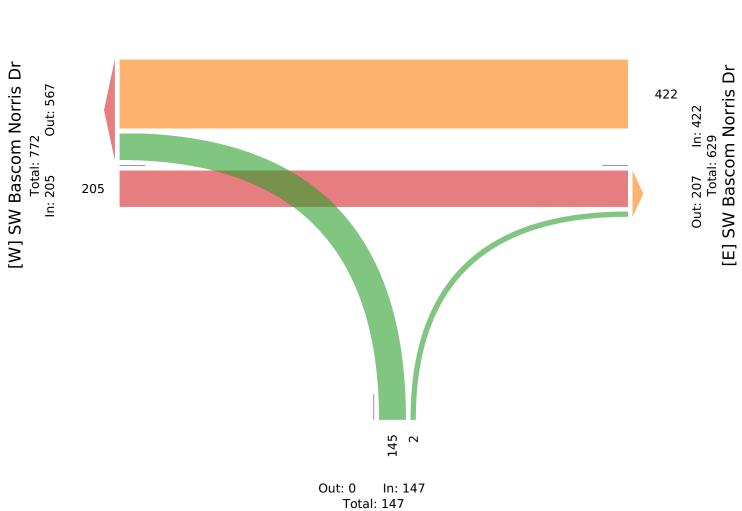
Leg	SW Bascom	Norris	Dr			com Norris	Dr		SW Marvin I	Burnett Rd	l		
Direction	Eastbound				Westbou	ina			Northbound				
Time	Т	R	U	Арр	L	Т	U	Арр	L	R	U	Арр	Int
2023-07-18 4:45PM	48	0	0	48	0	95	0	95	32	0	0	32	175
5:00PM	52	0	0	52	0	142	0	142	35	0	0	35	229
5:15PM	58	0	0	58	0	98	0	98	22	1	0	23	179
5:30PM	47	0	0	47	0	87	0	87	56	1	0	57	191
Total	205	0	0	205	0	422	0	422	145	2	0	147	774
% Approach	100%	0%	0%	-	0%	100%	0%	-	98.6%	1.4%	0%	-	-
% Total	26.5%	0%	0%	26.5%	0%	54.5%	0%	54.5%	18.7%	0.3%	0%	19.0%	-
PHF	0.884	-	-	0.884	-	0.743	-	0.743	0.647	0.500	-	0.645	0.845
Lights and Motorcycles	204	0	0	204	0	416	0	416	144	2	0	146	766
% Lights and Motorcycles	99.5%	0%	0%	99.5%	0%	98.6%	0%	98.6%	99.3%	100%	0%	99.3%	99.0%
Heavy	1	0	0	1	0	6	0	6	1	0	0	1	8
% Heavy	0.5%	0%	0%	0.5%	0%	1.4%	0%	1.4%	0.7%	0%	0%	0.7%	1.0%

*L: Left, R: Right, T: Thru, U: U-Turn

Marvin Burnett & Bascom Norris - TMC

Tue Jul 18, 2023 PM Peak (4:45 PM - 5:45 PM) - Overall Peak Hour All Classes (Lights and Motorcycles, Heavy) All Movements ID: 1091861, Location: 30.163397, -82.655082, Site Code: Marvin Burnett & Bascom Norris





[S] SW Marvin Burnett Rd

2022 PEAK SEASON FACTOR CATEGORY REPORT - REPORT TYPE: ALL CATEGORY: 2900 COLUMBIA COUNTYWIDE

CATEGORI. 2900 COHOMBIA COON		MOCF: 0.98
WEEK DATES	SF	PSCF
WEEK DATES 1 01/01/2022 - 01/08/202 2 01/02/2022 - 01/08/202 3 01/09/2022 - 01/22/202 4 01/16/2022 - 01/22/202 5 01/23/2022 - 02/05/202 7 02/06/2022 - 02/12/202 8 02/13/2022 - 02/19/202 9 02/20/2022 - 03/05/202 10 02/27/2022 - 03/05/202 *11 03/06/2022 - 03/12/202 *12 03/13/2022 - 03/26/202 *13 03/20/2022 - 04/02/202 *14 03/27/2022 - 04/02/202 *15 04/03/2022 - 04/30/202 *16 04/10/2022 - 04/30/202 *17 04/17/2022 - 05/21/202 *18 04/24/2022 - 05/21/202 *20 05/08/2022 - 05/21/202 *21 05/15/2022 - 05/28/202 *22 05/22/2022 - 06/11/202 *23 05/29/2022 - 06/25/202 *24 06/05/2022 - 07/02/202 *24 06/05/2022 - 07/02/202 *25 06/12/2022 - 07/23/202 31 07/24/2022 - 08/27/202 <td>SF 2 1.02 2 1.05 2 1.07 2 1.05 2 1.03 2 1.00 2 1.00 2 1.00 2 0.99 2 0.99 2 0.98 2 0.98 2 0.97 2 0.99 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 1.01 2 1.01 2 1.01 2 1.01 2 1.00 2 1.01 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 0.99 2 /td> <td>$\begin{array}{c} 1.04\\ 1.07\\ 1.10\\ 1.09\\ 1.07\\ 1.05\\ 1.04\\ 1.02\\ 1.02\\ 1.02\\ 1.01\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 1.00\\ 1.01\\ 1.02\\ 1.02\\ 1.02\\ 1.03\\ 1.04\\ 1.05\\ 1.04\\ 1.03\\ 1.02\\ 1.01\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.03\\ 1.02\\ 1.01\\ 1.02\\ 1.00$</td>	SF 2 1.02 2 1.05 2 1.07 2 1.05 2 1.03 2 1.00 2 1.00 2 1.00 2 0.99 2 0.99 2 0.98 2 0.98 2 0.97 2 0.99 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 1.01 2 1.01 2 1.01 2 1.01 2 1.00 2 1.01 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 1.00 2 0.99 2	$ \begin{array}{c} 1.04\\ 1.07\\ 1.10\\ 1.09\\ 1.07\\ 1.05\\ 1.04\\ 1.02\\ 1.02\\ 1.02\\ 1.01\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 1.00\\ 1.01\\ 1.02\\ 1.02\\ 1.02\\ 1.03\\ 1.04\\ 1.05\\ 1.04\\ 1.03\\ 1.02\\ 1.01\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.03\\ 1.02\\ 1.01\\ 1.02\\ 1.00$
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	2 0.98 2 0.99 2 1.00 2 1.01 2 1.02 2 1.05	1.00
53 12/25/2022 - 12/31/202	2 1.08	1.10

* PEAK SEASON

23-FEB-2023 09:11:19

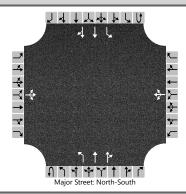
830UPD

2_2900_PKSEASON.TXT

APPENDIX B: HIGHWAY CAPACITY ANALYSES

		Stop Control Report	
General Information		Site Information	
Analyst	L. Hagen	Intersection	SR 47 & Marvin Burnett Road
Agency/Co.	Hagen Consulting Services	Jurisdiction	Columbia County
Date Performed	10/2/2023	East/West Street	SW Marvin Burnett Road
Analysis Year	2024	North/South Street	SR 47
Time Analyzed	AM Peak Period	Peak Hour Factor	0.89
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description	No-build scenario		

Lanes

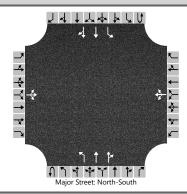


Vehicle Volumes and Adjustments Approach Eastbound Westbound Northbound Southbound U U U L т R L т R U L Т R L т R Movement 7 2 Priority 10 11 12 8 9 1U 1 3 4U 4 5 6 2 Number of Lanes 0 1 0 0 1 0 0 1 0 0 1 2 0 LTR LTR Configuration L Т TR L Т TR Volume (veh/h) 7 145 96 294 2 0 1 1 0 560 14 0 19 5 3 3 Percent Heavy Vehicles (%) 3 3 3 3 3 3 3 3 **Proportion Time Blocked** 0 0 Percent Grade (%) **Right Turn Channelized** Median Type | Storage Left Only 1 **Critical and Follow-up Headways** Base Critical Headway (sec) 7.5 6.5 6.9 7.5 6.5 6.9 4.1 4.1 Critical Headway (sec) 7.56 6.56 6.96 7.56 6.56 6.96 4.16 4.16 3.3 3.5 4.0 3.3 3.5 2.2 2.2 Base Follow-Up Headway (sec) 4.0 Follow-Up Headway (sec) 3.53 4.03 3.33 3.53 4.03 3.33 2.23 2.23 Delay, Queue Length, and Level of Service Flow Rate, v (veh/h) 2 108 173 21 Capacity, c (veh/h) 743 252 1213 929 v/c Ratio 0.23 0.01 0.09 0.02 0.9 0.3 0.1 95% Queue Length, Q₉₅ (veh) 0.0 Control Delay (s/veh) 11.3 19.4 8.3 9.0 Level of Service (LOS) В С А А Approach Delay (s/veh) 11.3 19.4 1.2 0.5 Approach LOS В С А А

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	TICS 100-00ay		
General Information		Site Information	
Analyst	L. Hagen	Intersection	SR 47 & Marvin Burnett Road
Agency/Co.	Hagen Consulting Services	Jurisdiction	Columbia County
Date Performed	10/2/2023	East/West Street	SW Marvin Burnett Road
Analysis Year	2024	North/South Street	SR 47
Time Analyzed	AM Peak Period	Peak Hour Factor	0.89
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description	Build scenario		

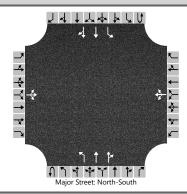
Lanes



Approach		Eastb	ound			West	oound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	1	2	0	0	1	2	0
Configuration			LTR				LTR			L	Т	TR		L	Т	TF
Volume (veh/h)		8	2	152		0	1	1	0	107	560	14	0	19	294	10
Percent Heavy Vehicles (%)		3	3	3		3	3	3	3	3			3	3		
Proportion Time Blocked																
Percent Grade (%)			0)									
Right Turn Channelized																
Median Type Storage				Left	Only								1			
Critical and Follow-up H	eadwa	ys														
Base Critical Headway (sec)		7.5	6.5	6.9		7.5	6.5	6.9		4.1				4.1		
Critical Headway (sec)		7.56	6.56	6.96		7.56	6.56	6.96		4.16				4.16		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.53	4.03	3.33		3.53	4.03	3.33		2.23				2.23		
Delay, Queue Length, an	d Leve	l of Se	ervice													
Flow Rate, v (veh/h)			182				2			120				21		
Capacity, c (veh/h)			732				241			1207				929		
v/c Ratio			0.25				0.01			0.10				0.02		
95% Queue Length, Q ₉₅ (veh)			1.0				0.0			0.3				0.1		
Control Delay (s/veh)			11.5				20.1			8.3				9.0		
Level of Service (LOS)			В				С			A				A		
Approach Delay (s/veh)		- 1'	1.5			20).1			1	.3		0.5			
Approach LOS	1		В			(2				4				4	

		Stop Control Report	
General Information		Site Information	
Analyst	L. Hagen	Intersection	SR 47 & Marvin Burnett Road
Agency/Co.	Hagen Consulting Services	Jurisdiction	Columbia County
Date Performed	10/2/2023	East/West Street	SW Marvin Burnett Road
Analysis Year	2024	North/South Street	SR 47
Time Analyzed	PM Peak Period	Peak Hour Factor	0.89
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description	No-build scenario		

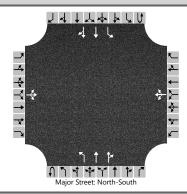
Lanes



Vehicle Volumes and Adjustments Approach Eastbound Westbound Northbound Southbound U U U L т R L т R U L Т R L R Movement Т 7 Priority 10 11 12 8 9 1U 1 2 3 4U 4 5 6 2 Number of Lanes 0 1 0 0 1 0 0 1 0 0 1 2 0 LTR Configuration LTR L Т TR L Т TR 2 139 455 594 Volume (veh/h) 4 0 268 6 0 0 2 0 6 14 3 3 Percent Heavy Vehicles (%) 3 3 3 3 3 3 3 3 **Proportion Time Blocked** 0 0 Percent Grade (%) **Right Turn Channelized** Median Type | Storage Left Only 1 **Critical and Follow-up Headways** Base Critical Headway (sec) 7.5 6.5 6.9 7.5 6.5 6.9 4.1 4.1 Critical Headway (sec) 7.56 6.56 6.96 7.56 6.56 6.96 4.16 4.16 3.3 3.5 4.0 3.3 3.5 2.2 2.2 Base Follow-Up Headway (sec) 4.0 Follow-Up Headway (sec) 3.53 4.03 3.33 3.53 4.03 3.33 2.23 2.23 Delay, Queue Length, and Level of Service Flow Rate, v (veh/h) 306 9 156 7 Capacity, c (veh/h) 634 160 899 1041 v/c Ratio 0.48 0.06 0.17 0.01 2.6 0.2 0.6 0.0 95% Queue Length, Q_{95} (veh) Control Delay (s/veh) 15.9 28.8 9.8 8.5 С Level of Service (LOS) D А А Approach Delay (s/veh) 15.9 28.8 2.3 0.1 Approach LOS С D А А

General Information		Site Information	
Analyst	L. Hagen	Intersection	SR 47 & Marvin Burnett Road
Agency/Co.	Hagen Consulting Services	Jurisdiction	Columbia County
Date Performed	10/2/2023	East/West Street	SW Marvin Burnett Road
Analysis Year	2024	North/South Street	SR 47
Time Analyzed	PM Peak Period	Peak Hour Factor	0.89
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description	Build scenario		

Lanes



Vehicle Volumes and Adj	ustme	nts														
Approach		Eastb	ound			West	bound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority		10	11	12		7	8	9	10	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	1	2	0	0	1	2	0
Configuration			LTR				LTR			L	Т	TR		L	Т	TR
Volume (veh/h)		5	0	291		6	0	2	0	153	455	2	0	6	594	29
Percent Heavy Vehicles (%)		3	3	3		3	3	3	3	3			3	3		
Proportion Time Blocked																
Percent Grade (%)		0 0														
Right Turn Channelized																
Median Type Storage				Left	Only								1			
Critical and Follow-up H	eadwa	ys														
Base Critical Headway (sec)		7.5	6.5	6.9		7.5	6.5	6.9		4.1				4.1		
Critical Headway (sec)		7.56	6.56	6.96		7.56	6.56	6.96		4.16				4.16		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.53	4.03	3.33		3.53	4.03	3.33		2.23				2.23		
Delay, Queue Length, an	d Leve	l of Se	ervice													
Flow Rate, v (veh/h)			333				9			172				7		
Capacity, c (veh/h)			622				129			886				1041		
v/c Ratio			0.53				0.07			0.19				0.01		
95% Queue Length, Q ₉₅ (veh)			3.2				0.2			0.7				0.0		
Control Delay (s/veh)			17.2				35.0			10.0				8.5		
Level of Service (LOS)			С				E			В				A		
Approach Delay (s/veh)		17	7.2			3!	5.0	-		2	.5		0.1			
Approach LOS		(С				E			1	4				Ą	

		ŀ		ſwo-	Way	Stop	o-Cor	ntrol	Repo	ort						
General Information							Site	Inforr	natio	n						
Analyst	L. Hag	gen					Inters	ection			Basco	om Norri	s & Mar	vin Burn	ett	
Agency/Co.	Hage	n Consu	lting Ser	vices			Jurisc	liction			Colur	nbia Cou	unty			
Date Performed	10/2/	2023					East/	Nest Str	eet		Basco	om Norri	s Drive			
Analysis Year	2024						North	/South	Street		Marv	in Burne	tt Road			
Time Analyzed	AM P	eak					Peak	Hour Fac	tor		0.84					
Intersection Orientation	East-\	Nest					Analy	sis Time	Period (hrs)	0.25					
Project Description	No-b	uild scer	nario													
Lanes																
						۲۲ مr Street: Ea		1 1 1 1 1 4 4 1 1								
Vehicle Volumes and A	Adjustme	nts														
Approach		Eastb	ound			West	bound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	1
Number of Lanes	0	0	1	0	0	0	1	0		0	1	0		0	0	(
Configuration			Т				Т				LR					
Volume (veh/h)			246				262			107		0				

Percent Heavy Vehicles (%)								3		3		
Proportion Time Blocked												
Percent Grade (%)								()			
Right Turn Channelized												
Median Type Storage				Undi	vided							
Critical and Follow-up H	leadwa	ys										
Base Critical Headway (sec)								7.1		6.2		Γ
Critical Headway (sec)								6.43		6.23		
Base Follow-Up Headway (sec)								3.5		3.3		
Follow-Up Headway (sec)								3.53		3.33		
Delay, Queue Length, an	d Leve	l of Se	ervice									
Flow Rate, v (veh/h)									127			Γ
Capacity, c (veh/h)									459			
v/c Ratio									0.28			
95% Queue Length, Q ₉₅ (veh)									1.1			
Control Delay (s/veh)									15.8			
Level of Service (LOS)									С			
Approach Delay (s/veh)								15	5.8			
Approach LOS								(2			

	_	ŀ	_					_		_	_	_				_
General Information							Site	Inforr	natio	า						
Analyst	L. Hag	gen					Inters	ection			Basco	om Norri	s & Marv	/in Burne	ett	
Agency/Co.	Hagei	n Consul	lting Ser	vices			Jurisd	liction			Colun	nbia Cou	inty			
Date Performed	10/2/	2023					East/\	West Stre	eet		Basco	om Norri	s Drive			
Analysis Year	2024						North	n/South S	Street		Marvi	n Burne	tt Road			
Time Analyzed	AM Pe	eak					Peak	Hour Fac	tor		0.84					
Intersection Orientation	East-V	Vest					Analy	sis Time	Period (hrs)	0.25					
Project Description	Build	scenario)													
Lanes																
				2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4				1 1 7 4 7 7 P								
Vehicle Volumes and Ad	djustme			\rightarrow		Y • Y or Street: Ea	st-West	1 7 4 1 6								
	djustme		oound	\rightarrow		*Y1	st-West	174200		North	bound			South	bound	
Approach Movement	U	Eastb L	Т	→ ×	Majo	Westl	oound T	R	U	L	Т	R	U	L	Т	-
Approach Movement Priority	U 1U	Eastb L 1	T 2	R 3	U 4U	Westl L	oound T 5	R 6	U	L 7	Т 8	9	U	L 10	T 11	R 12
Approach Movement Priority Number of Lanes	U	Eastb L	T 2 1	→ ×	Majo	Westl	bound T 5 1	R	U	L	T 8 1		U	L	Т	12
Approach Movement Priority Number of Lanes Configuration	U 1U	Eastb L 1	T 2 1 T	R 3	U 4U	Westl L	bound T 5 1 T	R 6	U	L 7 0	Т 8	9		L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h)	U 1U	Eastb L 1	T 2 1	R 3	U 4U	Westl L	bound T 5 1	R 6	U	L 7 0 113	T 8 1	9 0 0	U	L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h) Percent Heavy Vehicles (%)	U 1U	Eastb L 1	T 2 1 T	R 3	U 4U	Westl L	bound T 5 1 T	R 6		L 7 0	T 8 1	9		L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h) Percent Heavy Vehicles (%) Proportion Time Blocked	U 1U	Eastb L 1	T 2 1 T	R 3	U 4U	Westl L	bound T 5 1 T	R 6	U	L 7 0 113 3	T 8 1 LR	9 0 0	U 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h) Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%)	U 1U	Eastb L 1	T 2 1 T	R 3	U 4U	Westl L	bound T 5 1 T	R 6		L 7 0 113	T 8 1 LR	9 0 0		L 10	T 11	1
Approach Movement	U 1U	Eastb L 1	T 2 1 T	R 3 0	U 4U	Westl L	bound T 5 1 T	R 6		L 7 0 113 3	T 8 1 LR	9 0 0		L 10	T 11	-

Critical and Follow-up He	aawa	ys									
Base Critical Headway (sec)							7.1		6.2		
Critical Headway (sec)							6.43		6.23		
Base Follow-Up Headway (sec)							3.5		3.3		
Follow-Up Headway (sec)							3.53		3.33		
Delay, Queue Length, and	l Leve	l of Se	ervice								
Flow Rate, v (veh/h)								135			
Capacity, c (veh/h)								459			
v/c Ratio								0.29			
95% Queue Length, Q ₉₅ (veh)								1.2			
Control Delay (s/veh)								16.1			
Level of Service (LOS)								С			
Approach Delay (s/veh)							16	5.1			
Approach LOS							(C			

		L		Бмо- ¹		Stor	-Cor	otrol	Ponc	ort						
							o-Control Report Site Information									
Analyst	L. Had	gen					Intersection Bascom Norris & Marvin Burnett						ett			
Agency/Co.	· · · · ·	-	lting Ser	vices			Jurisc	liction			Colur	nbia Cou	unty			
Date Performed	10/2/						East/	West Str	eet			om Norri				
Analysis Year	2024						North	n/South :	Street		Marvi	n Burne	tt Road			
Time Analyzed	PM P	eak					Peak	Hour Fac	ctor		0.84					
Intersection Orientation	East-\	Vest					Analy	sis Time	Period (hrs)	0.25					
Project Description	No-b	uild scer	nario													
Lanes																
					<u>Ъ</u> Ч _{Мај}	۲ ۲ or Street: Ea	st-West	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1								
Vehicle Volumes and Adju	ustme															
Approach		_	ound	D		1	bound	D			bound			-	bound	
Movement	U	L 1	T	R 3	U	L	Т 5	R 6	U	L 7	Т 8	R 9	U	L	T	R
Priority Number of Lanes	1U 0	0	2	3	4U 0	4	5	0		0	8	9		10 0	11 0	12 0
Configuration	0	0	T	0	0	0	T	0		0	LR	0		0	0	0
Volume (veh/h)			215				443			152	LIX	0				
Percent Heavy Vehicles (%)			215							3		3				
Proportion Time Blocked										5						
Percent Grade (%)			1					0								
Right Turn Channelized																
-																

Median Type | Storage

Critical and Follow-up Headways																
Base Critical Headway (sec)										7.1		6.2				
Critical Headway (sec)										6.43		6.23				
Base Follow-Up Headway (sec)										3.5		3.3				
Follow-Up Headway (sec)										3.53		3.33				
Delay, Queue Length, and Level of Service																
Flow Rate, v (veh/h)											181					
Capacity, c (veh/h)											361					
v/c Ratio											0.50					
95% Queue Length, Q ₉₅ (veh)											2.7					
Control Delay (s/veh)											24.6					
Level of Service (LOS)											С					
Approach Delay (s/veh)								24.6								
Approach LOS									С							

Undivided

		H	HCS ⁻	Гwo-	Way	Stop	-Cor	ntrol	Repo	ort						
General Information							Site Information									
Analyst	L. Hag	L. Hagen					Intersection Bascom Norris & Marvin Burnett									
Agency/Co.	Hage	n Consu	Iting Ser	vices			Jurisd	iction			Colur	nbia Cou	unty			
Date Performed	10/2/	2023					East/\	Nest Stre	eet		Basco	om Norri	s Drive			
Analysis Year	2024						North	/South S	Street		Marvi	n Burne	tt Road			
Time Analyzed	PM P	eak					Peak	Hour Fac	tor		0.84					
Intersection Orientation	East-\	Vest					Analy	sis Time	Period (hrs)	0.25					
Project Description	Build	scenario)													
Lanes																
					 	↓⋏∊	k k l									
Vehicle Volumes and Adjustments																
Vehicle Volumes and Adj	ustme	nts			Majo		st-West									
Vehicle Volumes and Adj Approach	ustme		pound		Majc	or Street: Ea	st-West Dound			North	bound			South	bound	
-	ustme		oound T	R	U	or Street: Ea		R	U	North	bound T	R	U	South	bound T	R
Approach		Eastl	1	R 3		or Street: Ea	bound	R 6	U		1	R 9	U			R 12
Approach Movement	U	Eastl	Т		U	Westl	oound T		U	L	Т		U	L	Т	
Approach Movement Priority	U 1U	Easth L 1	Т 2	3	U 4U	Westl	oound T 5	6	U	L 7	Т 8	9	U	L 10	T 11	12
Approach Movement Priority Number of Lanes	U 1U	Easth L 1	T 2 1	3	U 4U	Westl	Dound T 5 1	6	U	L 7	T 8 1	9	U	L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration	U 1U	Easth L 1	T 2 1 T	3	U 4U	Westl	T 5 1 T	6	U	L 7 0	T 8 1	9	U	L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h)	U 1U	Easth L 1	T 2 1 T	3	U 4U	Westl	T 5 1 T	6		L 7 0 163	T 8 1	9 0 0		L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h) Percent Heavy Vehicles (%)	U 1U	Easth L 1	T 2 1 T	3	U 4U	Westl	T 5 1 T	6		L 7 0 163 3	T 8 1	9 0 0		L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h) Percent Heavy Vehicles (%) Proportion Time Blocked	U 1U	Easth L 1	T 2 1 T	3	U 4U	Westl	T 5 1 T	6		L 7 0 163 3	T 8 1 LR	9 0 0		L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h) Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%)	U 1U	Easth L 1	T 2 1 T	3 0	U 4U	Westl	T 5 1 T	6		L 7 0 163 3	T 8 1 LR	9 0 0		L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h) Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%) Right Turn Channelized	U U 1U 0 Image: Constraint of the second seco	Easth L 0	T 2 1 T	3 0	U 4U 0	Westl	T 5 1 T	6		L 7 0 163 3	T 8 1 LR	9 0 0		L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h) Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%) Right Turn Channelized Median Type Storage	U U 1U 0 Image: Constraint of the second seco	Easth L 0	T 2 1 T	3 0	U 4U 0	Westl	T 5 1 T	6		L 7 0 163 3	T 8 1 LR	9 0 0		L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h) Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%) Right Turn Channelized Median Type Storage	U U 1U 0 Image: Constraint of the second seco	Easth L 0	T 2 1 T	3 0	U 4U 0	Westl	T 5 1 T	6		L 7 0 163 3	T 8 1 LR	9 0 3		L 10	T 11	12
Approach Movement Priority Number of Lanes Configuration Volume (veh/h) Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%) Right Turn Channelized Median Type Storage Critical and Follow-up He Base Critical Headway (sec)	U U 1U 0 Image: Constraint of the second seco	Easth L 0	T 2 1 T	3 0	U 4U 0	Westl	T 5 1 T	6		L 7 0 163 3	T 8 1 LR	9 0 3 6.2		L 10	T 11	12

Delay, Queue Length, and Level of Service

Delay, Queue Length, and Level of Service														
Flow Rate, v (veh/h)											194			
Capacity, c (veh/h)											361			
v/c Ratio											0.54			
95% Queue Length, Q ₉₅ (veh)											3.0			
Control Delay (s/veh)											26.0			
Level of Service (LOS)											D			
Approach Delay (s/veh)										26	5.0			
Approach LOS										[)			

Stormwater Management • System Report

CRS Marvin Burnett



Prepared For: Concept Development, Inc.

Submitted To: City of Lake City and Suwannee River Water Management District

Date: 03/20/2024 PN# 23-0653 PM: Randall S. Olney, P.E. Address: 1449 SW 74th Drive Suite 200 Gainesville, Florida 32607



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Engineer's Certification Statement

I hereby certify that the design of the stormwater management systems for the project known as <u>CRS Marvin Burnett</u> has been designed substantially in accordance with the City of Lake City, the Suwannee River Water Management District, and the Florida Department of Transportation applicable rules and regulations.

Randall Scott Olney, State of Florida, Professional Engineer, License No. 68382	Digitally signed by Randall Scott Olney DN: E=randy0 @chw-inc.com, CN=Randall Scott Olney, O=Randail Scott Olney, L=Alachua, S=Florida, C=US Date: 2024.03.21 13:52:58-04000'
This item has been electronically signed and sealed by Randall Scott Olney, PE. On 03/21/2024 using a Digital Signature.	Randall S. Olney, FL PE No. 68382
Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.	03/21/2024 Date

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Site Characteristics	2
Drainage Analysis	3
Summary and Conclusions	6

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- 3 Aerial Map
- 4 NRCS Soils Map
- 5 FEMA Flood Map
- 6 Pre-Development Drainage Map
- 7 Post-Development Drainage Map

Appendices

- A. Drainage Calculations and Computer Model Output
- B. Operation and Maintenance Requirements and Erosion and Sedimentation Control Requirements
- C. Geotechnical Report

Introduction

The CRS Marvin Burnett project proposes the development of a $\pm 10,640$ sf commercial retail store with associated parking, stormwater, and utility infrastructure. The total proposed site area is ± 2.70 acres, located along the northwest corner of the intersection of State Road 47 and SW Marvin Burnett Road in Lake City, Florida.

The project site is located on a portion of tax parcel #07-4S-17-08127-005 according to the Columbia County Property Appraiser's website. Figure 1 provides a Location Map and Figure 2 depicts the site on a portion of the Lake City West USGS Quadrangle Map. The site is located in Section 7, Township 4 South, Range 17 East in Columbia County, Florida.

Refer to the accompanying engineering plans for details about the proposed construction and demolition regarding this project.

Design Criteria

The design criteria for the proposed stormwater management facility (SMF) is based upon the criteria set forth by the City of Lake City (CLC), the Suwannee River Water Management District (SRWMD), and the Florida Department of Transportation (FDOT) for a dry retention system design in a closed watershed. The criteria are as follows:

- 1. <u>Provide Peak Discharge Rate Attenuation</u>: Attenuate the post-development peak discharge rates to be less than the pre-development peak discharge rates for:
 - a. The 100 year 1 hour, 100 year 2 hour, 100 year 4 hour, 100 year 8 hour, 100 year 24 hour storm events (SRWMD).
 - b. The 3, 5, 10, 25, 50, and 100-year frequency analysis of the 1, 2, 4, 8, 24, 72, 168, and 240-hr storm events (FDOT).
- 2. <u>Provide Peak Discharge Volume Attenuation</u>: Attenuate the post-development peak discharge volumes to be less than the pre-development peak discharge volume for:
 - a. The 100 year -1 hour, 100 year -2 hour, 100 year -4 hour, 100 year -8 hour, 100 year -24 hour storm events (SRWMD).
 - b. The 3, 5, 10, 25, 50, and 100-year frequency analysis of the 1, 2, 4, 8, 24, 72, 168, and 240-hr storm events (FDOT).
- 3. <u>Provide Water Quality Treatment Volume (WQTV)</u>: The minimum stormwater treatment volume shall be the runoff from the first 2.0 inch of runoff from the design storm. WQTV must be recovered within 72 hours (SRWMD).
- 4. <u>Freeboard:</u> Retention ponds shall have a freeboard of 1 foot above the maximum stage in order to function properly during storms greater than the design storm (SRWMD).
- 5. <u>Provide Volume Recovery:</u> Retention systems must have one-half of the total volume available within 7 days following the end of the design storm event, and the total volume must be recovered within 30 days following the end of the storm event (SRWMD and FDOT).

Alternatively, if recovery requirements cannot be met, back-to-back storms can be routed through the system (SRWMD).

6. <u>Fencing:</u> Any water retention areas that have a potential of holding water in excess of one (1) foot depth to be fenced with a four (4) foot high fence and screened by trees or shrubbery (CLC).

City of Lake City, SRWMD, and FDOT also require that best management practices be employed to control erosion, sedimentation, and that an operation and maintenance entity be established.

Site Characteristics

Physical characteristics of the site are described in the following sections. Additional details are provided in the accompanying Engineering plans.

Site Topography

The existing site is undeveloped and heavily wooded with existing pavement and structures that are to be removed. The project site is bordered by a single-family residence to the west, a church to the north, State Road 47 to the east, and Marvin Burnett Road to the south. The site is sloped from the northeast to the southwest. Site topography ranges from EL. ± 167.00 ' (NAVD 88) in the northeast corner of the site to EL. ± 152.60 ' (NAVD 88) in the southwest corner.

Please refer to the accompanying engineering plans for details.

Pre-Development Drainage

Pre-development drainage consists of two watersheds: Pre-Development Watershed #1 (Pre DA-1) and Pre-Development Watershed #2 (Pre DA-2). Pre DA-1 is ± 2.03 acres in size and includes a portion of offsite area to the north of the site as well as most of the western portion of the project site. Stormwater runoff from Pre DA-1 flows via sheet flow and shallow concentrated flow to a natural low area along the western boundary of the site. Pre DA-2 is ± 1.79 acres in size and includes offsite area to the north as well as the eastern portion of the project site. Stormwater runoff from Pre DA-2 flows via sheet flow into the SR-47 (FDOT) storm sewer system.

Refer to Figure 4 for a NRCS Soils Map. Refer to Figure 6 for more information on the predevelopment watershed.

Post-Development Drainage

Post-Development drainage consists of two watersheds: Post-Development Watershed #1 (Post DA-1) and Post-Development Watershed #2 (Post DA-2). Post DA-1 comprises ± 3.29 acres including ± 0.93 acres of impervious area as well as a portion of offsite area. Stormwater runoff from Post DA-1 will be routed via sheet flow and shallow concentrated flow to a stormwater pipe conveyance system and into the proposed stormwater management facility (SMF-1). Post DA-2 comprises

 ± 0.53 acres including ± 0.02 acres of impervious area from a small portion of sidewalk. Stormwater runoff from Post DA-2 will be routed via sheet flow and shallow concentrated flow to the SR-47 (FDOT) storm sewer system as in the pre-development condition. The drainage area discharging to the FDOT system is greatly reduced in comparison to pre-development. Additionally, the CN of this area did not increase. Therefore, it is assumed that runoff rates and volumes have been reduced for each design storm event and these watersheds were not included in the drainage model.

SMF-1 is designed as a dry retention facility that will retain and infiltrate the difference between pre-development and post-development runoff volume. The top of bank for SMF-1 is set at EL. 160.00' while the bottom of pond is at EL. 157.00' with 4:1 side slope. The resulting total storage volume is \pm 49,744 cf. An underdrain system is proposed to lower the seasonal high-water table and meet recovery requirements. An outfall structure has been provided, which enables discharge to the existing depression beyond the western border of the site, mimicking the pre-development drainage patterns.

Refer to Figure 7 for more information on the post-development watershed.

Soils Information

The National Resource Conservation Service (NRCS) Soil Survey for Columbia County describes the near surface soil profile for the project area as *Blanton fine sand* (0-5% slopes) of hydrologic soil group rating of 'A', *Ichetucknee fine sand* (5-8% slopes) of hydrologic soil group rating of 'D', *Mascotte fine sand* of hydrologic soil group rating of 'B/D', *Pelham fine sand* (0-2% slopes) of hydrologic soil group rating of 'B/D'. Refer to Figure 4 for the NRCS Soils Map.

A site-specific soils investigation was conducted by GSE Engineering & Consulting, Inc. on October 11th, 2023 and the report was later revised on December 7th, 2023. Based on the Summary Report of Geotechnical Site Exploration, the following design parameters were recommended for the stormwater management facility calculations. Refer to Appendix C for further details.

SMF-1

- Average ground elevation of borings within proposed SMF-1 area: 156.70' (NAVD 88)
- Base elevation of effective or mobilized aquifer: 148.70' (NAVD 88)
- Average seasonal high groundwater table elevation: *152.99' (NAVD 88)
- Horizontal hydraulic conductivity: 10 feet per day (5 feet per day used in calculations)
- Unsaturated vertical infiltration rate: 10 feet per day (5 feet per day used in calculations)
- Specific yield (fillable porosity): 20%

*Seasonal high-water table established based on highest invert of the underdrain system.

Drainage Analysis

The proposed stormwater management system (SMF-1) has been designed to provide attenuation of the discharge rates and volumes for the 100 year -1 hour, 100 year -2 hour, 100 year -4 hour, 100 year -8 hour, and 100 year -24 hour storm events. Since the portion of the site draining towards the FDOT ROW (Post DA-2) is minimal and has been reduced from its pre- development

condition (Pre DA-2), the FDOT storms were not modeled. SMF-1 should recover one-half of the total volume available within 7 days following the end of the design storm event, and the total volume must be recovered within 30 days. Additionally, the stormwater management system is designed to retain the water quality treatment volume and recover this volume within 72 hours.

Appendix A contains details and calculations as well as a section for routing results, recovery analysis, hydraulic calculations, and general drainage calculations.

Analysis Methodology

The drainage analysis was conducted using the computer program PONDS (v3.3) to generate runoff hydrographs and route the runoff hydrographs through the proposed stormwater system. The required storm events were analyzed using SRWMD rainfall amounts for the predevelopment and post-development watersheds.

Unit Hydrograph Parameters

Unit hydrograph parameters required for the drainage analysis include run-off curve number (CN), time of concentration (Tc), and drainage area. Values used in the analysis are summarized as follows:

Pre-Development Watershed #1 (Pre DA-1):	
Watershed Area =	2.03 ac.
Impervious Area (Existing) =	0.02 ac.
Woods (Good, Type 'A' Soil) =	0.47 ac.
Woods (Good, Type 'D' Soil) =	1.55 ac.

CN = 66 Tc = 29 min.

Post-Development Watershed #1 (Post DA-1):	
Watershed Area =	3.29 ac.
Impervious Area =	0.93 ac.
Stormwater Management Facility =	0.45 ac.
Open Space (Good, Type 'A' Soil) =	1.29 ac.
Open Space (Good, Type 'D' Soil) =	0.62 ac.

CN = 72 Tc = 10 min.*

*Time of Concentration is assumed to be 10 minutes. *Pond Storage*

Stage-storage values for the proposed stormwater management facilities are provided in Appendix A.

Water Quality Treatment Volume (WQTV)

Per SRWMD, the required water quality treatment volume (WQTV) required for a dry retention system is 2.0 inch of runoff over the drainage area, that must draw down within 72 hours. The WQTV calculations and modeling results are summarized in Table 1, additional details can be found in appendix A.

Stormwater Management Facility	Required WQTV (cf)	Peak Elevation at WQTV (ft)	Time to Recover WQTV (hours)
SMF-1	12,483	157.87	< 6

Run-off and Facility Routing Results

The routing results for Pre DA-1 and Post DA-1 (SMF-1) are summarized in Tables 2 and 3. Table 2 displays the peak stage, freeboard, and recovery time for the analyzed storm events, while Table 3 displays the discharge rates and volumes for pre and post-development. Detailed results and calculations are provided in Appendix A.

Table 2:	Pre DA-1	vs. Post DA-1	Routing Results
----------	----------	---------------	-----------------

Storm Event	Peak Stage (ft.)	Freeboard (ft)	Full Volume Recovery (days after storm)	
SRWMD 100YR-1HR	158.14	1.86	< 1	
SRWMD 100YR-2HR	158.35	1.65	< 1	
SRWMD 100YR-4HR	158.46	1.54	< 1	
SRWMD 100YR-8HR	158.61	1.39	< 4	
SRWMD 100YR-24HR	158.78	1.22	< 7	

Table 3: Pre DA-1 vs. Post DA-1 Attenuation Results

Storm Event	Discharge Rates (cfs)			Discharge Volumes (cf)		
	Pre	Post	Change	Pre	Post	Change
SRWMD 100YR-1HR	4.27	0.31	-3.96	8,901	463	-8439
SRWMD 100YR-2HR	5.47	1.28	-4.19	13,242	4,512	-8730
SRWMD 100YR-4HR	6.46	1.93	-4.53	18,428	10,552	-7876
SRWMD 100YR-8HR	7.25	3.00	-4.25	25,727	17,171	-8556
SRWMD 100YR-24HR	6.67	4.28	-2.39	40,983	37,974	-3009

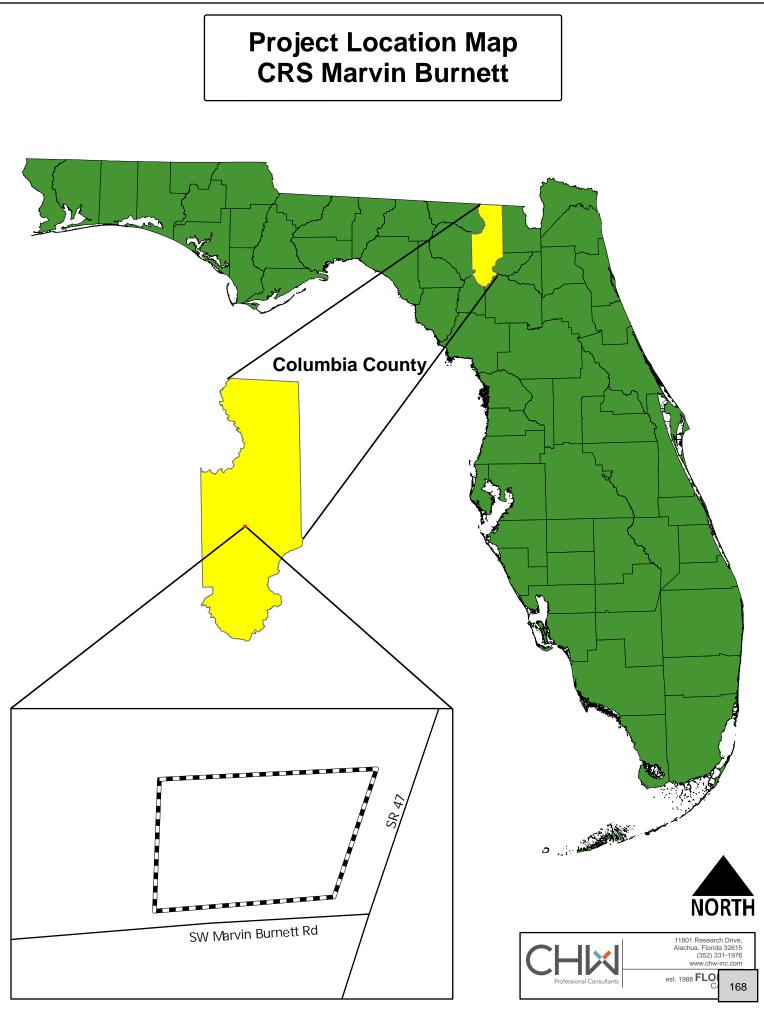
Summary and Conclusions

The proposed drainage system meets CLC, SRWMD, and FDOT criteria for dry retention system designs in a closed watershed. The criteria are as follows:

- 1. <u>Provide Peak Discharge Rate Attenuation</u>: SMF-1 attenuates the post-development peak discharge rates to be less than the pre-development peak discharge rates for:
 - a. The 100 year -1 hour, 100 year -2 hour, 100 year -4 hour, 100 year -8 hour, 100 year -24 hour storm events (SRWMD).
 - b. The 3, 5, 10, 25, 50, and 100-year frequency analysis of the 1, 2, 4, 8, 24, 72, 168, and 240-hr storm events (FDOT).
- 2. <u>Provide Peak Discharge Volume Attenuation</u>: SMF-1 attenuates the post-development peak discharge volumes to be less than the pre-development peak discharge volume for:
 - a. The 100 year -1 hour, 100 year -2 hour, 100 year -4 hour, 100 year -8 hour, 100 year -24 hour storm events (SRWMD).
 - b. The 3, 5, 10, 25, 50, and 100-year frequency analysis of the 1, 2, 4, 8, 24, 72, 168, and 240-hr storm events (FDOT).
- 3. <u>Provide Water Quality Treatment Volume (WQTV)</u>: SMF-1 has been designed to retain the runoff from the first 2.0 inch of runoff from the design storm. WQTV is recovered within 72 hours. (SRWMD).
- 4. <u>Freeboard:</u> SMF-1 provides 1 foot of freeboard above the maximum stage in order to function properly during storms greater than the design storm (SRWMD).
- 5. <u>Provide Volume Recovery:</u> SMF-1 provides half of the total available volume within 7 days after the end of all storm events, and provides the total available volume within 30 days after the end of all storm events (SRWMD and FDOT).
- 6. <u>Fencing:</u> SMF-1 has the potential to hold water in excess of one (1) foot depth, therefore a (4) foot high fence and sufficient screening by trees and shrubbery is proposed. (CLC).

Based on the information provided, the project is eligible for approval by City of Lake City, SRWMD, and FDOT.

Project Location Map



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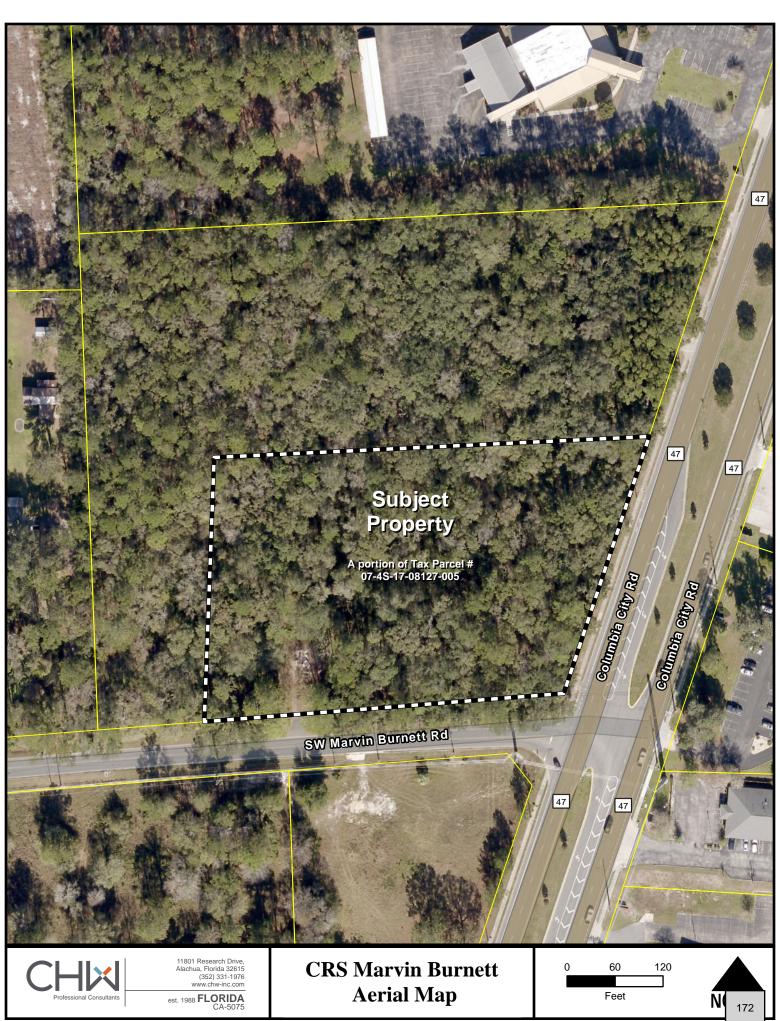
USGS Quadrangle Map



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Prepared by Employee ###

Aerial Map

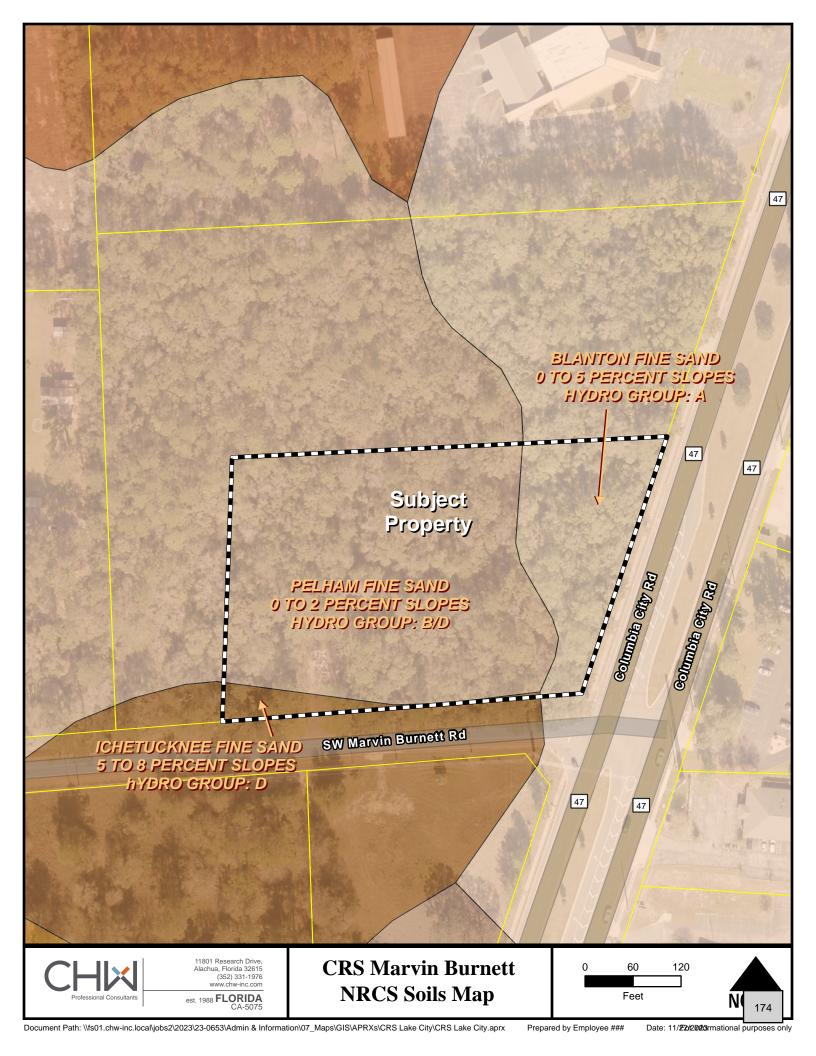


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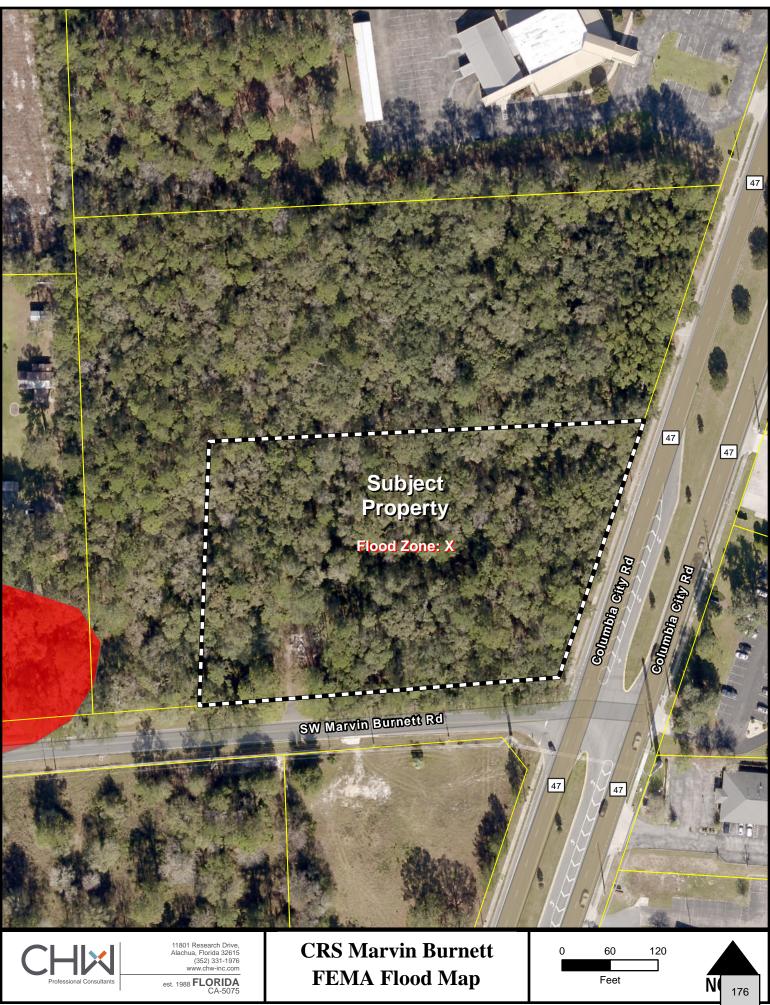
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NRCS Soils Map



FEMA Flood Map



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Prepared by Employee ### Date: 11/22/20

Date: 11/22/20/20/rmational purposes only

Pre-Development Drainage Map

LEGEND

PRE-DEVELOPMENT WATERSHED 1 (PRE DA-1) BOUNDARY:

PRE-DEVELOPMENT WATERSHED 2 (PRE DA-2) BOUNDARY:

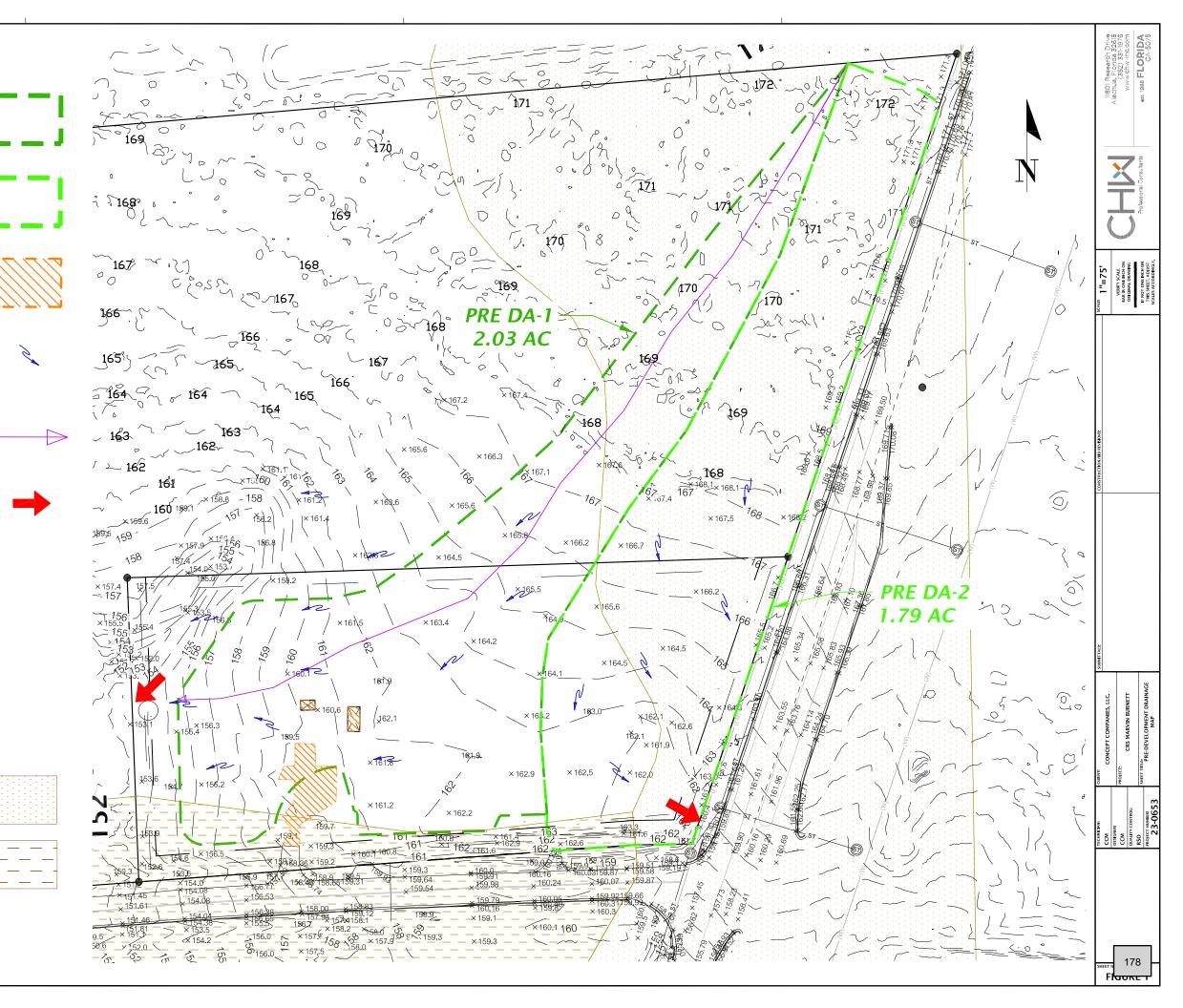
EXISTING IMPERVIOUS AREA TO BE REMOVED:

PRE-DEVELOPMENT DRAINAGE FLOW PATTERNS:

PRE-DEVELOPMENT TIME OF CONCENTRATION

PRE-DEVELOPMENT DISCHARGE POINT:

TYPE 'A' SOILS



TYPE 'D' SOILS

NOTE: ALL SOILS ARE TYPE 'B/D' UNLESS OTHERWISE NOTED

Post-Development Drainage Map

LEGEND

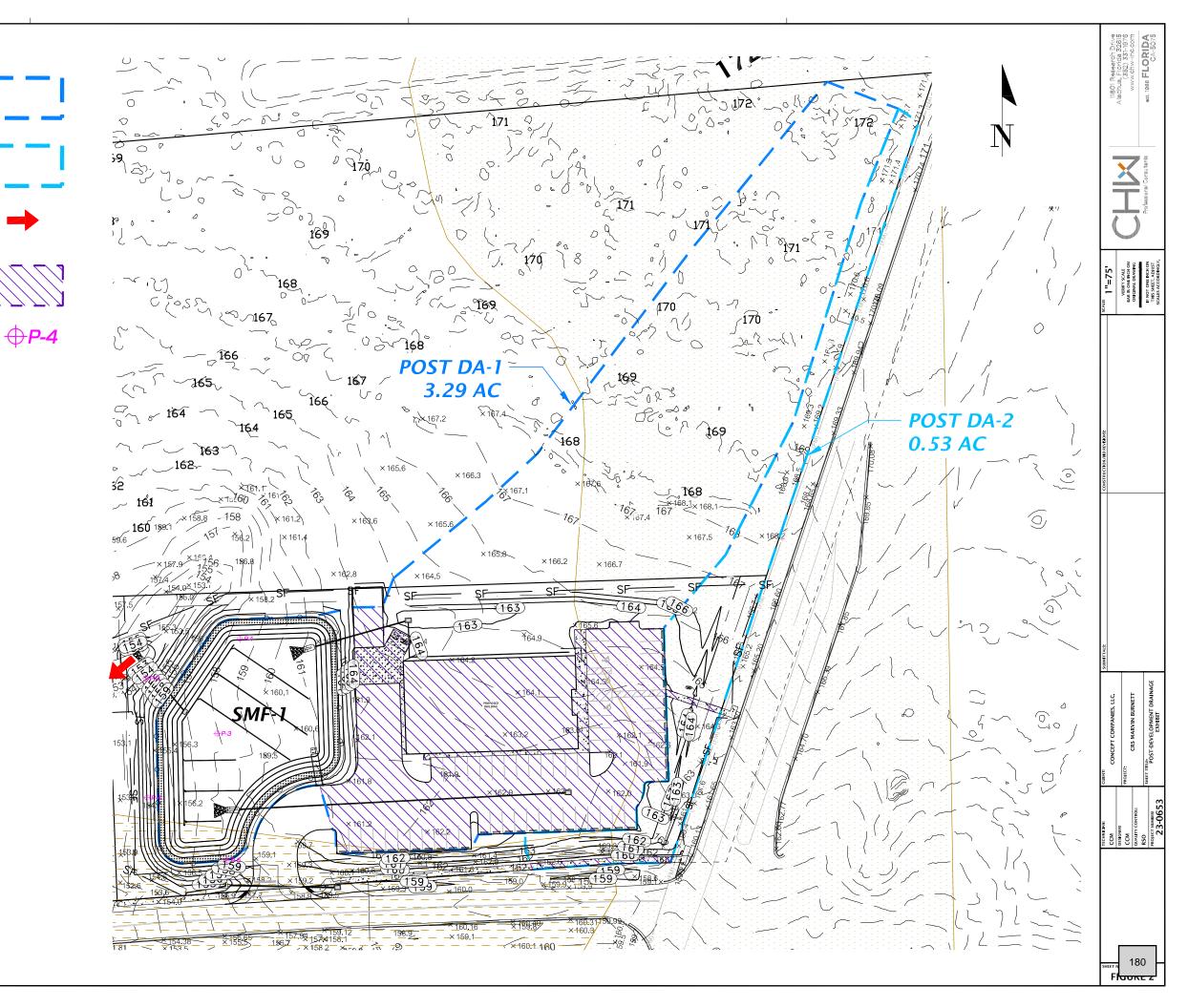
POST-DEVELOPMENT WATERSHED 1 (POST DA-1) BOUNDARY:

POST-DEVELOPMENT WATERSHED 2 (POST DA-2) BOUNDARY:

POST-DEVELOPMENT DISCHARGE POINT:

PROPOSED ONSITE IMPERVIOUS AREA:

SOIL BORING LOCATION:



Appendix A

Drainage Calculations and Computer Model Output



CURVE NUMBER CALCULATIONS:

Pre DA-1									
Total Area:	88,582	s.f.	2.03	ac.	CN	CN * Area	С	C * Area	
Woods (Good, Group "A" Soil)	20,340	s.f.	0.47	ac.	30	610200	0.2	4068	
Woods (Good, Group "D" Soil)	67,311	s.f.	1.55	ac.	77	5182947	0.2	13462.2	
Exisitng Impervious Area	931	s.f.	0.02	ac.	98	91238	0.95	884.45	

Weighted C: 0.21

Weighted CN: 66

Time of Concentration:

: **29**

Post DA-1								
Total Area:	143,411	s.f.	3.29	ac.	CN	CN * Area	С	C * Area
Open Space (Good, Group "A" Soil)	56,007	s.f.	1.29	ac.	39	2184273	0.2	11201.4
Open Space (Good, Group "D" Soil)	27,102	s.f.	0.62	ac.	80	2168160	0.2	5420.4
Impervious Area	40,483	s.f.	0.93	ac.	98	3967334	0.95	38458.85
Stormwater Management Facility	19,819	s.f.	0.45	ac.	100	1981900	1	19819

minutes

Weighted C: 0.52

Weighted CN:

Time of Concentration:

10 minutes

WQTV CALCULATIONS: SMF-1 (Dry Retention)

72

SRWMD WQTV Calculation:								
Runoff from the first 2.0" of rainfall								
2" x Drainage Area:	23901.83	c.f.						
C =	0.52							
SRWMD WQTV:	12,483	c.f.						

Pre DA-2										
Total Area:	77,911	s.f.	1.79	ac.	CN	CN * Area				
Woods (Good, Group "A" Soil)	62,699	s.f.	1.44	ac.	30	1880970				
Woods (Good, Group "D" Soil)	15,212	s.f.	0.35	ac.	77	1171324				

Weighted CN: 39

Post DA-2							
Total Area:	23,090	s.f.	0.53	ac.	CN	CN * Area	
Woods (Good, Group "A" Soil)	9,873	s.f.	0.23	ac.	30	296190	
Open Space (Good, Group "A" Soil)	11,246	s.f.	0.26	ac.	39	438594	
Open Space (Good, Group "D" Soil)	1,162	s.f.	0.03	ac.	80	92960	
Impervious Area	809	s.f.	0.02	ac.	98	79282	

Weighted CN: 39



Project Number: 23-0653 Project Name: CRS Marvin Burnett Calculated by: JHP Checked by: CCM Date: 1/4/2024

Tc CALCULATIONS:

		SHEE	T FLOW		SH	SHALLOW CONCENTRATED FLOW CHANNEL / PIPE FLOW															
		Flow	2-Year	Land		Paved	Flow	Water-	Avg.		Cross-	Wetted	Hydraulic	Pipe		Avg.	Flow				
BASIN	Manning's	Length	24-Hour	Slope	Tt1	or	Length	course	Velocity		Section	Perim.	Radius	Slope	Manning	Velocity	Length	Tt3	ID	Tc	Тс
	n	L	Rain, P2			Unpvd.	L	Slope, s	V		Area, a	Pw	r		n		L				
	()	(ft)	(in)	(ft/ft)	(hr)	(P or U)	(ft)	(ft/ft)	(ft/s)	(hr)	(ft^2)	(ft)	(ft)	(ft/ft)	()	(ft/s)	(ft)	(hr)	#	(hr)	(min)
Pre DA-1	0.4	100	4.2	0.011	0.40	U	694	0.023	2.44	0.08	-	-	-	-	-	-	-	-	PRE DA-1	0.48	29

If Tc less than 10 minutes, 10 minutes was assumed per FDOT standards

TIME OF CONCENTRATION VALUES DETERMINED USING TR-55 METHODOLOGY.

SHEET FLOW:

 $Tt = \frac{0.007 (nL)^{0.8}}{(P2)^{0.5} s^{0.4}}$

SHALLOW CONCENTRATED FLOW: 1. For slopes < 0.005 ft/ft Unpaved V=16.1345 s^{0.5} V=20.3282 s^{0.5} Paved

2. For slopes > 0.005 ft/ft Velocity per Figure 3-1, TR-55

CHANNEL/PIPE FLOW: $V = \underbrace{\frac{1.49r^{2/3}s^{1/2}}{n}}_{Tt = \underbrace{L}_{3600 \text{ V}}}$

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STAGE-STORAGE CALCULATIONS:

Post-Development: SMF-1 Stage-Storage Relationship										
ELEV.	AREA (SF)	AREA (AC.)	STORAGE (CF)	STORAGE VOLUME (AC-FT)						
157.00	13,469	0.3092	0	0.00	1					
158.00	15,494	0.3557	14,482	0.33						
159.00	17,606	0.4042	31,032	0.71						
160.00	19,819	0.4550	49,744	1.14]					
WQTV =	12,483	cf	SHWT =	*152.99	ft					
WQTV EL. =	157.86	ft	Confining Layer =	148.70	ft					
			Kv =	5.00	ft/da					
Weir Elevation =	158.00	ft	Kh =	5.00	ft/day					
			Porosity =	20	%					
Eq. Length =	200	ft								
Eq. Width =	83	ft	Depth =	3.00	ft					
			Perimeter =	566	ft					

Geotech Borings						
Boring #	Ex. Grade EL.					
P-1	158.50					
P-2	154.00					
P-3	158.00					
P-4	154.75					
P-5	158.25					
Avg.	156.70					

*Established based on Invert of Underdrain System



PIPE CALCS: CRS Marvin Burnett (23-0653)

Structu	ure No.	Invert	Elev.	Length	Slope	Dia.	с	Тс	i	А	А	Q (cfs) Actual	Q Allowed	Pipe A	V - Full Flow	Pipe R	Minor Loss	Minor Loss	Loss	H	GL	ToG/ EoP	F.B.
From	То	U.S.	D.S.	(ft)	(ft/foot)	(in)		(min)	(in/hr)	(sf)	(ac)	Inc	Cumul	(cfs)	(sq-ft)	(fps)	(ft)	Coeff.	(ft)	(ft)	U.S.	D.S.		(in)
S-2	S-1	158.38	157.00	277	0.0050	15	0.95	10	6.2	18163	0.42	2.5	2.5	4.94	1.2	4.0	0.31	0.5	0.03	0.3	158.51	158.14	162.23	45
C/O-1	C/O-2	160.61	159.96	65	0.0100	12	0.95	10	6.2	3547	0.08	0.5	0.5	3.86	0.8	4.9	0.25	0.5	0.00	0.0	160.93	160.91	163.72	34
C/O-2	C/O-3	159.96	159.30	65	0.0102	12	0.95	10	6.2	3547	0.08	0.5	1.0	3.89	0.8	5.0	0.25	0.5	0.01	0.0	160.91	160.86	163.85	35
C/O-3	S-4	159.30	159.00	30	0.0100	12	0.95	10	6.2	3547	0.08	0.5	1.4	3.86	0.8	4.9	0.25	0.8	0.04	0.0	160.86	160.78	164.03	38
S-4	S-3	159.00	157.00	86	0.0233	15	0.80	10	6.2	76339	1.75	8.7	10.1	10.67	1.2	8.7	0.31	0.8	0.85	1.8	160.78	158.14	162.12	16

1. ToG = Top of Grate/EoP = Edge of Pavement

2. FB = Free Board

3. Rainfall intensity is based on the FDOT Zone 3 Rainfall Intensity-Duration-Frequency curve for the 3 year - 10 min storm event (6.2 inches/hr)

4. The tailwater condition was set at the peak stage for the 100 year - 1 hour storm event of the receiving SMF.

Pre-Development Model

Project Data

Project Name:	CRS Marvin Burnett
Simulation Description:	Pre-Development
Project Number:	23-0653
Engineer :	Jarrett Pearson
Supervising Engineer:	Cole Menhennett
Date:	12-28-2023

Scenario Input Data

Scenario 1 :: SRWMD 100YR-1HR

Hydrograph Type: • Modflow Routing: Repetitions:	Inline SCS Not routed 1	
Basin Area (acres) Time Of Concentration DCIA (%) Curve Number Design Rainfall Depth (Design Rainfall Duratio Shape Factor Rainfall Distribution	(inches)	2.030 29.0 0.0 66 4.2 1.0 UHG 484 SCS Type II Florida Modified

Initial ground water level (ft datum) 154.70 (default)

Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)
0.250	6.250	12.250	18.250	24.250
0.500	6.500	12.500	18.500	24.500
0.750	6.750	12.750	18.750	24.750
1.000	7.000	13.000	19.000	25.000
1.250	7.250	13.250	19.250	25.250
1.500	7.500	13.500	19.500	25.500
1.750	7.750	13.750	19.750	25.750
2.000	8.000	14.000	20.000	26.000
2.250	8.250	14.250	20.250	26.250
2.500	8.500	14.500	20.500	26.500
2.750	8.750	14.750	20.750	26.750
3.000	9.000	15.000	21.000	27.000
3.250	9.250	15.250	21.250	27.250
3.500	9.500	15.500	21.500	27.500
3.750	9.750	15.750	21.750	27.750
4.000	10.000	16.000	22.000	28.000
4.250	10.250	16.250	22.250	28.250
4.500	10.500	16.500	22.500	28.500
4.750	10.750	16.750	22.750	28.750
5.000	11.000	17.000	23.000	29.000
5.250	11.250	17.250	23.250	29.250
5.500	11.500	17.500	23.500	29.500
5.750	11.750	17.750	23.750	29.750
6.000	12.000	18.000	24.000	30.000

Scenario 2 :: SRWMD 100YR-2HR

Hydrograph Type: • Modflow Routing: Repetitions:	Inline SCS Not routed 1	
Basin Area (acres) Time Of Concentration DCIA (%) Curve Number Design Rainfall Depth (Design Rainfall Duratio Shape Factor Rainfall Distribution	(inches)	2.030 29.0 0.0 66 5.1 2.0 UHG 484 SCS Type II Florida Modified

Initial ground water level (ft datum) 154.70 (default)

Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)
0.250	6.250	12.250	18.250	24.250
0.500	6.500	12.500	18.500	24.500
0.750	6.750	12.750	18.750	24.750
1.000	7.000	13.000	19.000	25.000
1.250	7.250	13.250	19.250	25.250
1.500	7.500	13.500	19.500	25.500
1.750	7.750	13.750	19.750	25.750
2.000	8.000	14.000	20.000	26.000
2.250	8.250	14.250	20.250	26.250
2.500	8.500	14.500	20.500	26.500
2.750	8.750	14.750	20.750	26.750
3.000	9.000	15.000	21.000	27.000
3.250	9.250	15.250	21.250	27.250
3.500	9.500	15.500	21.500	27.500
3.750	9.750	15.750	21.750	27.750
4.000	10.000	16.000	22.000	28.000
4.250	10.250	16.250	22.250	28.250
4.500	10.500	16.500	22.500	28.500
4.750	10.750	16.750	22.750	28.750
5.000	11.000	17.000	23.000	29.000
5.250	11.250	17.250	23.250	29.250
5.500	11.500	17.500	23.500	29.500
5.750	11.750	17.750	23.750	29.750
6.000	12.000	18.000	24.000	30.000

Scenario 3 :: SRWMD 100YR-4HR

Hydrograph Type: • Modflow Routing: Repetitions:	Inline SCS Not routed 1	
Basin Area (acres) Time Of Concentration DCIA (%) Curve Number Design Rainfall Depth (Design Rainfall Duratio Shape Factor Rainfall Distribution	(inches)	2.030 29.0 0.0 66 6.1 4.0 UHG 484 SCS Type II Florida Modified

Initial ground water level (ft datum) 154.70 (default)

Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)
0.250	6.250	12.250	18.250	24.250
0.500	6.500	12.500	18.500	24.500
0.750	6.750	12.750	18.750	24.750
1.000	7.000	13.000	19.000	25.000
1.250	7.250	13.250	19.250	25.250
1.500	7.500	13.500	19.500	25.500
1.750	7.750	13.750	19.750	25.750
2.000	8.000	14.000	20.000	26.000
2.250	8.250	14.250	20.250	26.250
2.500	8.500	14.500	20.500	26.500
2.750	8.750	14.750	20.750	26.750
3.000	9.000	15.000	21.000	27.000
3.250	9.250	15.250	21.250	27.250
3.500	9.500	15.500	21.500	27.500
3.750	9.750	15.750	21.750	27.750
4.000	10.000	16.000	22.000	28.000
4.250	10.250	16.250	22.250	28.250
4.500	10.500	16.500	22.500	28.500
4.750	10.750	16.750	22.750	28.750
5.000	11.000	17.000	23.000	29.000
5.250	11.250	17.250	23.250	29.250
5.500	11.500	17.500	23.500	29.500
5.750	11.750	17.750	23.750	29.750
6.000	12.000	18.000	24.000	30.000

Scenario 4 :: SRWMD 100YR-8HR

Hydrograph Type: • Modflow Routing: Repetitions:	Inline SCS Not routed 1	
Basin Area (acres) Time Of Concentration DCIA (%) Curve Number Design Rainfall Depth Design Rainfall Duratic Shape Factor Rainfall Distribution	(inches)	2.030 29.0 0.0 66 7.4 8.0 UHG 484 SCS Type II Florida Modified

Initial ground water level (ft datum) 154.70 (default)

Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)
0.250	6.250	12.250	18.250	24.250
0.500	6.500	12.500	18.500	24.500
0.750	6.750	12.750	18.750	24.750
1.000	7.000	13.000	19.000	25.000
1.250	7.250	13.250	19.250	25.250
1.500	7.500	13.500	19.500	25.500
1.750	7.750	13.750	19.750	25.750
2.000	8.000	14.000	20.000	26.000
2.250	8.250	14.250	20.250	26.250
2.500	8.500	14.500	20.500	26.500
2.750	8.750	14.750	20.750	26.750
3.000	9.000	15.000	21.000	27.000
3.250	9.250	15.250	21.250	27.250
3.500	9.500	15.500	21.500	27.500
3.750	9.750	15.750	21.750	27.750
4.000	10.000	16.000	22.000	28.000
4.250	10.250	16.250	22.250	28.250
4.500	10.500	16.500	22.500	28.500
4.750	10.750	16.750	22.750	28.750
5.000	11.000	17.000	23.000	29.000
5.250	11.250	17.250	23.250	29.250
5.500	11.500	17.500	23.500	29.500
5.750	11.750	17.750	23.750	29.750
6.000	12.000	18.000	24.000	30.000

Scenario 5 :: SRWMD 100YR-24HR

Hydrograph Type: • Modflow Routing: Repetitions:	Inline SCS Not routed 1	
Basin Area (acres) Time Of Concentration DCIA (%) Curve Number Design Rainfall Depth Design Rainfall Duratic Shape Factor Rainfall Distribution	(inches)	2.030 29.0 0.0 66 9.8 24.0 UHG 484 SCS Type II Florida Modified

Initial ground water level (ft datum) 154.70 (default)

Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)
0.250	6.250	12.250	18.250	24.250
0.500	6.500	12.500	18.500	24.500
0.750	6.750	12.750	18.750	24.750
1.000	7.000	13.000	19.000	25.000
1.250	7.250	13.250	19.250	25.250
1.500	7.500	13.500	19.500	25.500
1.750	7.750	13.750	19.750	25.750
2.000	8.000	14.000	20.000	26.000
2.250	8.250	14.250	20.250	26.250
2.500	8.500	14.500	20.500	26.500
2.750	8.750	14.750	20.750	26.750
3.000	9.000	15.000	21.000	27.000
3.250	9.250	15.250	21.250	27.250
3.500	9.500	15.500	21.500	27.500
3.750	9.750	15.750	21.750	27.750
4.000	10.000	16.000	22.000	28.000
4.250	10.250	16.250	22.250	28.250
4.500	10.500	16.500	22.500	28.500
4.750	10.750	16.750	22.750	28.750
5.000	11.000	17.000	23.000	29.000
5.250	11.250	17.250	23.250	29.250
5.500	11.500	17.500	23.500	29.500
5.750	11.750	17.750	23.750	29.750
6.000	12.000	18.000	24.000	30.000

Sort-By-Category Report

Scenarios Considered: 1 to 5

Discharge - Rate - Maximum Positive

Rank	Scenario Number	Maximum Positive Discharge Rate (ft³/s)	Time (hours)	Description
1	4	7.25	4.25	SRWMD 100YR-8HR
2	5	6.67	12.12	SRWMD 100YR-24HR
3	3	6.46	2.32	SRWMD 100YR-4HR
4	2	5.47	1.35	SRWMD 100YR-2HR
5	1	4.27	0.84	SRWMD 100YR-1HR

Discharge - Cumulative Volume - Maximum Positive

Rank	Scenario Number	Maximum Positive Cumulative Discharge Volume (ft³)	Time (hours)	Description	
1	5	40983.17	25.58	SRWMD 100YR-24HR	
2	4	25726.74	9.60	SRWMD 100YR-8HR	
3	3	18428.31	5.54	SRWMD 100YR-4HR	
4	2	13241.67	3.61	SRWMD 100YR-2HR	
5	1	8901.35	2.58	SRWMD 100YR-1HR	

Post-Development Model

Project Data

Project Name:	CRS Marvin Burnett
Simulation Description:	Post-Development DA-1
Project Number:	23-0653
Engineer :	Jarrett Pearson
Supervising Engineer:	Cole Menhennett
Date:	01-04-2024

Aquifer Data

Base Of Aquifer Elevation, [B] (ft datum):	148.70
Water Table Elevation, [WT] (ft datum):	152.99
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day):	5.00
Fillable Porosity, [n] (%):	20.00
Unsaturated Vertical Infiltration Rate, [Iv] (ft/day):	5.0
Maximum Area For Unsaturated Infiltration, [Av] (ft²):	19819.0

Geometry Data

Equivalent Pond Length, [L] (ft):	200.0	
Equivalent Pond Width, [W] (ft):	83.0	

Ground water mound is expected to intersect the pond bottom

Stage vs Area Data

Stage (ft datum)	Area (ft²)
157.00	13469.0
158.00	15494.0
159.00	17606.0
160.00	19819.0

Discharge Structures

Discharge Structure #1 is active as weir

Structure Parameters

Description: WQTV

Weir elevation, (ft datum):	158.00
Weir coefficient:	3.13
Weir length, (ft):	2
Weir exponent:	1.5

Tailwater - disabled, free discharge

Discharge Structure #2 is inactive

Discharge Structure #3 is inactive

Scenario Input Data

Scenario 1 :: SRWMD 100YR-1HR

Hydrograph Type: Modflow Routing: Repetitions:	Inline SCS Routed with 1	h infiltration
Basin Area (acres) Time Of Concentration DCIA (%) Curve Number Design Rainfall Depth Design Rainfall Duratio Shape Factor Rainfall Distribution	(inches)	3.290 10.0 0.0 72 4.2 1.0 UHG 484 SCS Type II Florida Modified

Initial ground water level (ft datum) 152.99 (default)

Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)
0.250	6.250	12.250	18.250	24.250
0.500	6.500	12.500	18.500	24,500
0.750	6.750	12.750	18.750	24.750
1.000	7.000	13.000	19.000	25.000
1.250	7.250	13.250	19.250	25.250
1.500	7.500	13.500	19.500	25.500
1.750	7.750	13.750	19.750	25.750
2.000	8.000	14.000	20.000	26.000
2.250	8.250	14.250	20.250	26.250
2.500	8.500	14.500	20.500	26.500
2.750	8.750	14.750	20.750	26.750
3.000	9.000	15.000	21.000	27.000
3.250	9.250	15.250	21.250	27.250
3.500	9.500	15.500	21.500	27.500
3.750	9.750	15.750	21.750	27.750
4.000	10.000	16.000	22.000	28.000
4.250	10.250	16.250	22.250	28.250
4.500	10.500	16.500	22.500	28.500
4.750	10.750	16.750	22.750	28.750
5.000	11.000	17.000	23.000	29.000
5.250	11.250	17.250	23.250	29.250
5.500	11.500	17.500	23.500	29.500
5.750	11.750	17.750	23.750	29.750
6.000	12.000	18.000	24.000	30.000

Scenario 2 :: SRWMD 100YR-2HR

Hydrograph Type: Modflow Routing: Repetitions:	Inline SCS Routed witl 1	n infiltration
Basin Area (acres) Time Of Concentration DCIA (%) Curve Number Design Rainfall Depth Design Rainfall Duration Shape Factor Rainfall Distribution	(inches)	3.290 10.0 0.0 72 5.1 2.0 UHG 484 SCS Type II Florida Modified

Initial ground water level (ft datum) 152.99 (default)

Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)
0.250	6.250	12.250	18.250	24.250
0.500	6.500	12.500	18.500	24.500
0.750	6.750	12.750	18.750	24.750
1.000	7.000	13.000	19.000	25.000
1.250	7.250	13.250	19.250	25.250
1.500	7.500	13.500	19.500	25.500
1.750	7.750	13.750	19.750	25.750
2.000	8.000	14.000	20.000	26.000
2.250	8.250	14.250	20.250	26.250
2.500	8.500	14.500	20.500	26.500
2.750	8.750	14.750	20.750	26.750
3.000	9.000	15.000	21.000	27.000
3.250	9.250	15.250	21.250	27.250
3.500	9.500	15.500	21.500	27.500
3.750	9.750	15.750	21.750	27.750
4.000	10.000	16.000	22.000	28.000
4.250	10.250	16.250	22.250	28.250
4.500	10.500	16.500	22.500	28.500
4.750	10.750	16.750	22.750	28.750
5.000	11.000	17.000	23.000	29.000
5.250	11.250	17.250	23.250	29.250
5.500	11.500	17.500	23.500	29.500
5.750	11.750	17.750	23.750	29.750
6.000	12.000	18.000	24.000	30.000

Scenario 3 :: SRWMD 100YR-4HR

Hydrograph Type: Modflow Routing: Repetitions:	Inline SCS Routed with 1	h infiltration
Basin Area (acres) Time Of Concentration DCIA (%) Curve Number Design Rainfall Depth Design Rainfall Duration Shape Factor Rainfall Distribution	(inches)	3.290 10.0 0.0 72 6.1 4.0 UHG 484 SCS Type II Florida Modified

Initial ground water level (ft datum) 152.99 (default)

Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)
0.250	6.250	12.250	18.250	24.250
0.500	6.500	12.500	18.500	24,500
0.750	6.750	12.750	18.750	24.750
1.000	7.000	13.000	19.000	25.000
1.250	7.250	13.250	19.250	25.250
1.500	7.500	13.500	19.500	25.500
1.750	7.750	13.750	19.750	25.750
2.000	8.000	14.000	20.000	26.000
2.250	8.250	14.250	20.250	26.250
2.500	8.500	14.500	20.500	26.500
2.750	8.750	14.750	20.750	26.750
3.000	9.000	15.000	21.000	27.000
3.250	9.250	15.250	21.250	27.250
3.500	9.500	15.500	21.500	27.500
3.750	9.750	15.750	21.750	27.750
4.000	10.000	16.000	22.000	28.000
4.250	10.250	16.250	22.250	28.250
4.500	10.500	16.500	22.500	28.500
4.750	10.750	16.750	22.750	28.750
5.000	11.000	17.000	23.000	29.000
5.250	11.250	17.250	23.250	29.250
5.500	11.500	17.500	23.500	29.500
5.750	11.750	17.750	23.750	29.750
6.000	12.000	18.000	24.000	30.000

Scenario 4 :: SRWMD 100YR-8HR

Hydrograph Type: Modflow Routing: Repetitions:	Inline SCS Routed witl 1	n infiltration
Basin Area (acres) Time Of Concentration DCIA (%) Curve Number Design Rainfall Depth Design Rainfall Duratio Shape Factor Rainfall Distribution	(inches)	3.290 10.0 0.0 72 7.4 8.0 UHG 484 SCS Type II Florida Modified

Initial ground water level (ft datum) 152.99 (default)

Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)
0.250	6.250	12.250	18.250	24.250
0.500	6.500	12.500	18.500	24.500
0.750	6.750	12.750	18.750	24.750
1.000	7.000	13.000	19.000	25.000
1.250	7.250	13.250	19.250	25.250
1.500	7.500	13.500	19.500	25.500
1.750	7.750	13.750	19.750	25.750
2.000	8.000	14.000	20.000	26.000
2.250	8.250	14.250	20.250	26.250
2.500	8.500	14.500	20.500	26.500
2.750	8.750	14.750	20.750	26.750
3.000	9.000	15.000	21.000	27.000
3.250	9.250	15.250	21.250	27.250
3.500	9.500	15.500	21.500	27.500
3.750	9.750	15.750	21.750	27.750
4.000	10.000	16.000	22.000	28.000
4.250	10.250	16.250	22.250	28.250
4.500	10.500	16.500	22.500	28.500
4.750	10.750	16.750	22.750	28.750
5.000	11.000	17.000	23.000	29.000
5.250	11.250	17.250	23.250	29.250
5.500	11.500	17.500	23.500	29.500
5.750	11.750	17.750	23.750	29.750
6.000	12.000	18.000	24.000	30.000

Scenario 5 :: SRWMD 100YR-24HR

Hydrograph Type: Modflow Routing: Repetitions:	Inline SCS Routed with 1	n infiltration
Basin Area (acres) Time Of Concentration DCIA (%) Curve Number Design Rainfall Depth Design Rainfall Duration Shape Factor Rainfall Distribution	(inches)	3.290 10.0 0.0 72 9.8 24.0 UHG 484 SCS Type II Florida Modified

Initial ground water level (ft datum) 152.99 (default)

Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)
0.250	6.250	12.250	18.250	24.250
0.500	6.500	12.500	18.500	24,500
0.750	6.750	12.750	18.750	24.750
1.000	7.000	13.000	19.000	25.000
1.250	7.250	13.250	19.250	25.250
1.500	7.500	13.500	19.500	25.500
1.750	7.750	13.750	19.750	25.750
2.000	8.000	14.000	20.000	26.000
2.250	8.250	14.250	20.250	26.250
2.500	8.500	14.500	20.500	26.500
2.750	8.750	14.750	20.750	26.750
3.000	9.000	15.000	21.000	27.000
3.250	9.250	15.250	21.250	27.250
3.500	9.500	15.500	21.500	27.500
3.750	9.750	15.750	21.750	27.750
4.000	10.000	16.000	22.000	28.000
4.250	10.250	16.250	22.250	28.250
4.500	10.500	16.500	22.500	28.500
4.750	10.750	16.750	22.750	28.750
5.000	11.000	17.000	23.000	29.000
5.250	11.250	17.250	23.250	29.250
5.500	11.500	17.500	23.500	29.500
5.750	11.750	17.750	23.750	29.750
6.000	12.000	18.000	24.000	30.000

Scenario 6 :: WQTV

Hydrograph Type: Modflow Routing:	Slug Load Routed with	infiltration
Treatment Volume (ft ³))	12483
Initial ground water lev	el (ft datum)	152.99 (default)

Scenario 6 (cont'd.) :: Slug Load :: WQTV

Time After	Time After
Storm Event	Storm Event
(days)	(days)
0.100	2.000
0.250	2.500
0.500	3.000
1.000	3.500
1.500	4.000

Sort-By-Category Report

Scenarios Considered: 1 to 6

Stage - Maximum

Rank	Scenario Number	Maximum Stage (ft datum)	Time (hours)	Description	
1	5	158.78	12.58	SRWMD 100YR-24HR	
2	4	158.61	4.47	SRWMD 100YR-8HR	
3	3	158.46	2.64	SRWMD 100YR-4HR	
4	2	158.35	1.89	SRWMD 100YR-2HR	
5	1	158.14	1.13	SRWMD 100YR-1HR	
6	6	157.87	0.00	WQTV	

Discharge - Rate - Maximum Positive

Rank	Scenario Number	Maximum Positive Discharge Rate (ft³/s)	Time (hours)	Description
1	5	4.28	12.58	SRWMD 100YR-24HR
2	4	3.00	4.47	SRWMD 100YR-8HR
3	3	1.93	2.64	SRWMD 100YR-4HR
4	2	1.28	1.89	SRWMD 100YR-2HR
5	1	0.31	1.13	SRWMD 100YR-1HR
6	6	None	N.A.	WQTV

Discharge - Cumulative Volume - Maximum Positive

Rank	Scenario Number	Maximum Positive Cumulative Discharge Volume (ft³)	Time (hours)	Description
1	5	37974.45	30.58	SRWMD 100YR-24HR
2	4	17170.97	8.47	SRWMD 100YR-8HR
3	3	10552.48	4.58	SRWMD 100YR-4HR
4	2	4512.00	2.58	SRWMD 100YR-2HR
5	1	462.72	1.58	SRWMD 100YR-1HR
6	6	None	N.A.	WQTV

Detailed Results :: Scenario 1 :: SRWMD 100YR-1HR

Elapsed Time (hours)	Inflow Rate (ft³/s)	Outside Recharge (ft/day)	Stage Elevation (ft datum)	Infiltration Rate (ft³/s)	Overflow Discharge (ft³/s)	Cumulative Inflow Volume (ft³)	Cumulative Infiltration Volume (ft ³)	Cumulative Discharge Volume (ft³)	Flow Type
0.000	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	N.A.
0.022	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	U
0.044	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	U
0.067 0.089	0.0000 0.0000	0.0000 0.0000	152.990	0.00000 0.00000	0.00000 0.00000	0.0 0.0	0.0 0.0	0.0 0.0	U U
0.009	0.0000	0.0000	152.990 152.990	0.00000	0.00000	0.0	0.0	0.0	U
0.133	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	Ŭ
0.156	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	U
0.178	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	U
0.200	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	U
0.222	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	U U
0.244 0.267	0.0000 0.0000	0.0000 0.0000	152.990 152.990	0.00000 0.00000	0.00000 0.00000	0.0 0.0	0.0 0.0	0.0 0.0	U
0.289	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	Ŭ
0.311	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	U
0.333	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	U
0.356	0.0000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	U
0.378	0.0000	0.0000	152.990	0.00000	0.00000 0.00000	0.0	0.0	0.0 0.0	U U
0.400 0.422	0.0000 0.0048	0.0000 0.0000	152.990 152.990	0.00120 0.01123	0.00000	0.0 0.2	0.0 0.2	0.0	U
0.444	0.0353	0.0000	152.990	0.05641	0.00000	1.8	1.8	0.0	Ŭ
0.467	0.1503	0.0000	152.992	0.28887	0.00000	9.2	9.2	0.0	U
0.489	0.8197	0.0000	153.002	0.63289	0.00000	48.0	48.0	0.0	U
0.511	3.0541	0.0000	157.007	0.78234	0.00000	203.0	110.5	0.0	U/P
0.533 0.556	7.3661 13.2100	0.0000 0.0000	157.033 157.089	0.78715 0.79551	0.00000 0.00000	619.8 1442.8	173.2 236.4	0.0 0.0	U/P U/P
0.578	18.1747	0.0000	157.176	0.80685	0.00000	2698.2	300.5	0.0	U/P
0.600	20.6736	0.0000	157.283	0.81971	0.00000	4252.1	365.5	0.0	U/P
0.622	20.8533	0.0000	157.395	0.83258	0.00000	5913.2	431.6	0.0	U/P
0.644	19.2460	0.0000	157.502	0.84432	0.00000	7517.2	498.7	0.0	U/P
0.667	16.5416	0.0000	157.596	0.85437	0.00000	8948.7	566.7	0.0	U/P
0.689 0.711	13.9483 11.8984	0.0000 0.0000	157.674 157.738	0.86274 0.86972	0.00000 0.00000	10168.3 11202.2	635.4 704.8	0.0 0.0	U/P U/P
0.733	10.2784	0.0000	157.793	0.87561	0.00000	12089.2	704.8	0.0	U/P
0.756	8.9361	0.0000	157.839	0.88063	0.00000	12857.8	844.9	0.0	U/P
0.778	7.8660	0.0000	157.879	0.88496	0.00000	13529.9	915.5	0.0	U/P
0.800	6.9880	0.0000	157.913	0.88872	0.00000	14124.1	986.4	0.0	U/P
0.822	6.2744	0.0000	157.943	0.89202	0.00000	14654.6	1057.7	0.0	U/P
0.844 0.867	5.6997 5.2272	0.0000 0.0000	157.969 157.993	0.89496 0.89764	0.00000 0.00000	15133.5 15570.6	1129.2 1200.9	0.0 0.0	U/P U/P
0.889	4.8274	0.0000	158.014	0.90011	0.00000	15972.8	1200.9	0.0	U/P
0.911	4.4846	0.0000	158.033	0.90236	0.03797	16345.3	1344.9	2.4	U/P
0.933	4.1987	0.0000	158.051	0.90441	0.07132	16692.6	1417.2	6.7	U/P
0.956	3.9662	0.0000	158.067	0.90628	0.10723	17019.2	1489.6	13.9	U/P
0.978	3.7655	0.0000	158.081	0.90800	0.14413	17328.5	1562.2	23.9	U/P
1.000 1.022	3.5795 3.3573	0.0000 0.0000	158.094 158.106	0.90957 0.91097	0.18099 0.21671	17622.2 17899.7	1634.9 1707.7	36.9 52.8	U/P U/P
1.022	3.0563	0.0000	158.117	0.91215	0.24959	18156.3	1780.6	71.5	U/P
1.067	2.6439	0.0000	158.125	0.91306	0.27735	18384.3	1853.6	92.6	U/P
1.089	2.1539	0.0000	158.131	0.91365	0.29779	18576.2	1926.7	115.6	U/P
1.111	1.6654	0.0000	158.135	0.91394	0.30981	18729.0	1999.8	139.9	U/P
1.133	1.2315	0.0000	158.136	0.91396	0.31371	18844.8	2073.0	164.8	U/P
1.156 1.178	0.8803 0.6289	0.0000 0.0000	158.135 158.133	0.91376 0.91341	0.31073 0.30262	18929.3 18989.7	2146.1 2219.2	189.8 214.3	U/P U/P
1.200	0.4528	0.0000	158.129	0.91294	0.29108	19032.9	2292.2	238.1	U/P
1.222	0.3260	0.0000	158.125	0.91240	0.27735	19064.1	2365.2	260.8	U/P
1.244	0.2330	0.0000	158.121	0.91182	0.26226	19086.5	2438.2	282.4	U/P
1.267	0.1669	0.0000	158.116	0.91119	0.24642	19102.5	2511.1	302.7	U/P
1.289 1.311	0.1190 0.0845	0.0000 0.0000	158.111	0.91055 0.90990	0.23026 0.21408	19113.9 19122.0	2584.0 2656.8	321.8 339.6	U/P U/P
1.333	0.0645	0.0000	158.105 158.100	0.90990	0.21408	19122.0	2050.0	356.1	U/P U/P
1.356	0.0421	0.0000	158.095	0.90857	0.18244	19131.9	2802.3	371.3	U/P
1.378	0.0293	0.0000	158.089	0.90791	0.16723	19134.7	2874.9	385.3	U/P
1.400	0.0201	0.0000	158.084	0.90725	0.15251	19136.7	2947.5	398.1	U/P
1.422	0.0134	0.0000	158.079	0.90660	0.13835	19138.0	3020.1	409.7	U/P
1.444	0.0086	0.0000	158.074	0.90595	0.12475	19138.9	3092.6	420.2	U/P
1.467 1.489	0.0049 0.0023	0.0000 0.0000	158.068 158.063	0.90531 0.90468	0.11175 0.09934	19139.5 19139.8	3165.1 3237.5	429.7 438.1	U/P U/P
1.469	0.0023	0.0000	158.058	0.90408	0.09934	19139.9	3309.8	438.1	U/P
1.533	0.0007	0.0000	158.053	0.90343	0.07638	19139.9	3382.1	452.2	U/P
1.556	0.0000	0.0000	158.048	0.90282	0.06584	19139.9	3454.4	457.9	U/P
1.578	0.0000	0.0000	158.043	0.90177	0.05593	19139.9	3526.6	462.7	U/P
7.578	0.0000	0.0000	156.339	0.35071	0.00000	19139.9	18677.2	462.7	U/S
13.578	0.0000	0.0000	156.032	0.00000	0.00000	19139.9	18677.2	462.7	S

Detailed Results (cont,d.) :: Scenario 2 :: SRWMD 100YR-2HR

Elapsed Time (hours)	Inflow Rate (ft³/s)	Outside Recharge (ft/day)	Stage Elevation (ft datum)	Infiltration Rate (ft³/s)	Overflow Discharge (ft³/s)	Cumulative Inflow Volume (ft³)	Cumulative Infiltration Volume (ft³)	Cumulative Discharge Volume (ft³)	Flow Type
1.644	2.8768	0.0000	158.329	0.93836	1.18168	23236.3	2444.0	1097.9	U/P
1.667	2.8113	0.0000	158.333	0.93878	1.20074	23463.9	2519.1	1193.2	U/P
1.689	2.7507	0.0000	158.336	0.93914	1.21770	23686.3	2594.2	1289.9	U/P
1.711	2.6872	0.0000	158.339	0.93946	1.23263 1.24535	23903.9	2669.4	1387.9	U/P U/P
1.733 1.756	2.6123 2.5262	0.0000 0.0000	158.341 158.343	0.93973 0.93993	1.24535	24115.8 24321.4	2744.5 2819.7	1487.1 1587.1	U/P
1.778	2.4400	0.0000	158.344	0.94008	1.26331	24520.0	2894.9	1687.9	U/P
1.800	2.3649	0.0000	158.345	0.94018	1.26864	24712.2	2970.1	1789.1	U/P
1.822	2.3054	0.0000	158.346	0.94024	1.27203	24899.0	3045.4	1890.8	U/P
1.844	2.2636	0.0000	158.346	0.94027	1.27397	25081.8	3120.6	1992.6	U/P
1.867 1.889	2.2352 2.2139	0.0000 0.0000	158.346 158.346	0.94029 0.94029	1.27492 1.27517	25261.7 25439.7	3195.8 3271.0	2094.6 2196.6	U/P U/P
1.009	2.1931	0.0000	158.346	0.94029	1.27485	25616.0	3346.2	2190.0	U/P
1.933	2.1665	0.0000	158.346	0.94024	1.27390	25790.4	3421.5	2400.5	U/P
1.956	2.1306	0.0000	158.346	0.94019	1.27214	25962.3	3496.7	2502.4	U/P
1.978	2.0834	0.0000	158.345	0.94011	1.26931	26130.8	3571.9	2604.0	U/P
2.000	2.0249	0.0000	158.344	0.94000	1.26515	26295.1	3647.1	2705.4	U/P U/P
2.022 2.044	1.9305 1.7813	0.0000 0.0000	158.343 158.342	0.93982 0.93956	1.25906 1.24989	26453.4 26601.8	3722.3 3797.5	2806.4 2906.7	U/P
2.044	1.5542	0.0000	158.339	0.93917	1.23598	26735.3	3872.6	3006.2	U/P
2.089	1.2738	0.0000	158.335	0.93863	1.21577	26848.4	3947.7	3104.2	U/P
2.111	0.9890	0.0000	158.330	0.93793	1.18876	26938.9	4022.8	3200.4	U/P
2.133	0.7342	0.0000	158.324	0.93710	1.15562	27007.8	4097.8	3294.2	U/P
2.156	0.5253	0.0000	158.317	0.93616	1.11765	27058.2	4172.7	3385.1	U/P U/P
2.178 2.200	0.3755 0.2706	0.0000 0.0000	158.309 158.301	0.93515 0.93410	1.07648 1.03363	27094.2 27120.1	4247.6 4322.4	3472.9 3557.3	U/P
2.222	0.1954	0.0000	158.293	0.93303	0.99016	27120.1	4397.0	3638.2	U/P
2.244	0.1399	0.0000	158.284	0.93195	0.94675	27152.1	4471.6	3715.7	U/P
2.267	0.1004	0.0000	158.275	0.93087	0.90387	27161.7	4546.2	3789.7	U/P
2.289	0.0717	0.0000	158.267	0.92980	0.86184	27168.6	4620.6	3860.4	U/P
2.311 2.333	0.0511	0.0000 0.0000	158.258 158.250	0.92874	0.82086	27173.5 27177.0	4694.9 4769.2	3927.7 3991.7	U/P U/P
2.355	0.0363 0.0255	0.0000	158.241	0.92770 0.92667	0.78106 0.74251	27179.5	4843.4	4052.7	U/P
2.378	0.0177	0.0000	158.233	0.92566	0.70526	27181.2	4917.5	4110.6	U/P
2.400	0.0121	0.0000	158.225	0.92467	0.66930	27182.4	4991.5	4165.6	U/P
2.422	0.0081	0.0000	158.217	0.92370	0.63462	27183.2	5065.4	4217.7	U/P
2.444	0.0052	0.0000	158.210	0.92275	0.60121	27183.8	5139.3	4267.2	U/P
2.467 2.489	0.0030 0.0014	0.0000 0.0000	158.202 158.195	0.92182 0.92090	0.56904 0.53807	27184.1 27184.3	5213.0 5286.8	4314.0 4358.3	U/P U/P
2.409	0.0005	0.0000	158.188	0.92090	0.50827	27184.3	5360.4	4338.3	U/P
2.533	0.0000	0.0000	158.180	0.91913	0.47960	27184.3	5434.0	4439.6	U/P
2.556	0.0000	0.0000	158.173	0.91826	0.45203	27184.3	5507.4	4476.9	U/P
2.578	0.0000	0.0000	158.167	0.91737	0.42553	27184.3	5580.9	4512.0	U/P
<u>8.578</u> 14.578	0.0000	0.0000 0.0000	<u>156.340</u> 156.033	0.39564	0.00000	27184.3 27184.3	22672.3 22672.3	4512.0 4512.0	U/S
20.578	0.0000	0.0000	155.832	0.00000	0.00000	27184.3	22672.3	4512.0	S S S S S S S S
26.578	0.0000	0.0000	155.680	0.00000	0.00000	27184.3	22672.3	4512.0	S
32.578	0.0000	0.0000	155.558	0.00000	0.00000	27184.3	22672.3	4512.0	S
38.578	0.0000	0.0000	155.455	0.00000	0.00000	27184.3	22672.3	4512.0	S
44.578 50.578	0.0000 0.0000	0.0000 0.0000	155.366 155.288	0.00000 0.00000	0.00000 0.00000	27184.3 27184.3	22672.3 22672.3	4512.0 4512.0	S
56.578	0.0000	0.0000	155.219	0.00000	0.00000	27184.3	22672.3	4512.0	S
62.578	0.0000	0.0000	155.156	0.00000	0.00000	27184.3	22672.3	4512.0	S
68.578	0.0000	0.0000	155.099	0.00000	0.00000	27184.3	22672.3	4512.0	S
74.578	0.0000	0.0000	155.047	0.00000	0.00000	27184.3	22672.3	4512.0	S
80.578 86.578	0.0000 0.0000	0.0000 0.0000	154.998 154.954	0.00000 0.00000	0.00000 0.00000	27184.3 27184.3	22672.3	4512.0 4512.0	S S
92.578	0.0000	0.0000	154.954	0.00000	0.00000	27184.3	22672.3 22672.3	4512.0	S
98.578	0.0000	0.0000	154.873	0.00000	0.00000	27184.3	22672.3	4512.0	S
104.578	0.0000	0.0000	154.836	0.00000	0.00000	27184.3	22672.3	4512.0	S
110.578	0.0000	0.0000	154.801	0.00000	0.00000	27184.3	22672.3	4512.0	S
116.578	0.0000	0.0000	154.768	0.00000	0.00000	27184.3	22672.3	4512.0	S
122.578	0.0000	0.0000	154.737	0.00000 0.00000	0.00000 0.00000	27184.3 27184.3	22672.3	4512.0 4512.0	S S
128.578 134.578	0.0000 0.0000	0.0000 0.0000	154.708 154.680	0.00000	0.00000	27184.3 27184.3	22672.3 22672.3	4512.0	S S
140.578	0.0000	0.0000	154.653	0.00000	0.00000	27184.3	22672.3	4512.0	S
146.578	0.0000	0.0000	154.628	0.00000	0.00000	27184.3	22672.3	4512.0	S
152.578	0.0000	0.0000	154.603	0.00000	0.00000	27184.3	22672.3	4512.0	S
158.578	0.0000	0.0000	154.580	0.00000	0.00000	27184.3	22672.3	4512.0	S
164.578 170.578	0.0000 0.0000	0.0000 0.0000	154.557 154.536	0.00000 0.00000	0.00000 0.00000	27184.3 27184.3	22672.3 22672.3	4512.0 4512.0	S S
170.578	0.0000	0.0000	154.536	0.00000	0.00000	27184.3 27184.3	22672.3	4512.0	S S
182.578	0.0000	0.0000	154.495	0.00000	0.00000	27184.3	22672.3	4512.0	S
188.578	0.0000	0.0000	154.476	0.00000	0.00000	27184.3	22672.3	4512.0	S

Detailed Results (cont,d.) :: Scenario 3 :: SRWMD 100YR-4HR

Elapsed Time (hours)	Inflow Rate (ft³/s)	Outside Recharge (ft/day)	Stage Elevation (ft datum)	Infiltration Rate (ft³/s)	Overflow Discharge (ft³/s)	Cumulative Inflow Volume (ft³)	Cumulative Infiltration Volume (ft ³)	Cumulative Discharge Volume (ft³)	Flow Type
3.289	1.6884	0.0000	158.378	0.94412	1.45726	32414.7	5467.0	6451.7	U/P
3.311	1.6908	0.0000	158.375	0.94370	1.43741	32549.9	5542.5	6567.5	U/P
3.333	1.6865	0.0000	158.372	0.94328	1.41816	32685.0	5618.0	6681.7	U/P
3.356 3.378	1.6727 1.6482	0.0000 0.0000	158.368 158.365	0.94286 0.94245	1.39929 1.38050	32819.4 32952.2	5693.5 5768.9	6794.4 6905.6	U/P U/P
3.400	1.6107	0.0000	158.362	0.94202	1.36146	33082.5	5844.2	7015.3	U/P
3.422	1.5651	0.0000	158.358	0.94157	1.34190	33209.6	5919.6	7123.4	U/P
3.444	1.5196	0.0000	158.355	0.94112	1.32172	33333.0	5994.9	7230.0	U/P
3.467	1.4789	0.0000	158.351	0.94065	1.30104	33452.9	6070.2	7334.9	U/P
3.489	1.4456	0.0000	158.347	0.94017	1.28002	33569.9	6145.4	7438.1	U/P U/P
3.511 3.533	1.4219 1.4055	0.0000 0.0000	158.343 158.339	0.93969 0.93921	1.25892 1.23796	33684.6 33797.7	6220.6 6295.8	7539.7 7639.6	U/P U/P
3.556	1.3939	0.0000	158.336	0.93874	1.21731	33909.6	6370.9	7737.8	U/P
3.578	1.3855	0.0000	158.332	0.93828	1.19706	34020.8	6445.9	7834.3	U/P
3.600	1.3799	0.0000	158.328	0.93782	1.17726	34131.4	6521.0	7929.3	U/P
3.622	1.3760	0.0000	158.325	0.93737	1.15798	34241.7	6596.0	8022.7	U/P
3.644 3.667	1.3736 1.3720	0.0000 0.0000	158.321 158.318	0.93694 0.93651	1.13922 1.12099	34351.7 34461.5	6671.0 6745.9	8114.6 8205.0	U/P U/P
3.689	1.3720	0.0000	158.314	0.93610	1.10330	34571.2	6820.8	8294.0	U/P
3.711	1.3706	0.0000	158.311	0.93569	1.08615	34680.9	6895.7	8381.6	U/P
3.733	1.3704	0.0000	158.308	0.93530	1.06951	34790.5	6970.5	8467.8	U/P
3.756	1.3702	0.0000	158.305	0.93492	1.05338	34900.1	7045.3	8552.7	U/P
3.778	1.3677	0.0000	158.302	0.93454	1.03771	35009.7	7120.1	8636.4	U/P
3.800 3.822	1.3606 1.3466	0.0000 0.0000	158.299 158.296	0.93417 0.93380	1.02239 1.00726	35118.8 35227.1	7194.9 7269.6	8718.8 8799.9	U/P U/P
3.844	1.3273	0.0000	158.293	0.93342	0.99218	35334.0	7344.3	8879.9	U/P
3.867	1.3057	0.0000	158.290	0.93305	0.97704	35439.4	7418.9	8958.7	U/P
3.889	1.2832	0.0000	158.287	0.93267	0.96182	35542.9	7493.6	9036.3	U/P
3.911	1.2614	0.0000	158.284	0.93228	0.94650	35644.7	7568.2	9112.6	U/P
3.933	1.2401	0.0000	158.281	0.93190	0.93112	35744.8	7642.7	9187.7	U/P
3.956 3.978	1.2168 1.1871	0.0000 0.0000	158.278 158.274	0.93150 0.93110	0.91566 0.90001	35843.0 35939.2	7717.3 7791.8	9261.6 9334.2	U/P U/P
4.000	1.1521	0.0000	158.271	0.93069	0.88406	36032.8	7866.2	9405.5	U/P
4.022	1.1018	0.0000	158.268	0.93025	0.86757	36122.9	7940.7	9475.6	U/P
4.044	1.0235	0.0000	158.264	0.92977	0.85005	36207.9	8015.1	9544.3	U/P
4.067	0.8987	0.0000	158.260	0.92923	0.83066	36284.8	8089.4	9611.5	U/P
4.089	0.7409	0.0000	158.256	0.92861	0.80857	36350.4	8163.8	9677.1	U/P
4.111 4.133	0.5789 0.4312	0.0000 0.0000	158.250 158.244	0.92790 0.92713	0.78349 0.75569	36403.2 36443.6	8238.0 8312.2	9740.8 9802.4	U/P U/P
4.155	0.3085	0.0000	158.238	0.92629	0.72579	36473.2	8386.4	9861.6	U/P
4.178	0.2204	0.0000	158.231	0.92542	0.69459	36494.3	8460.4	9918.4	U/P
4.200	0.1588	0.0000	158.224	0.92453	0.66288	36509.5	8534.4	9972.7	U/P
4.222	0.1147	0.0000	158.217	0.92363	0.63120	36520.4	8608.3	10024.5	U/P
4.244	0.0820	0.0000	158.209	0.92273	0.59988	36528.3	8682.2	10073.7	U/P U/P
4.267 4.289	0.0589 0.0420	0.0000 0.0000	158.202 158.195	0.92183 0.92094	0.56915 0.53917	36533.9 36538.0	8756.0 8829.7	10120.5 10164.8	U/P
4.311	0.0299	0.0000	158.188	0.92007	0.51003	36540.9	8903.3	10206.8	U/P
4.333	0.0213	0.0000	158.181	0.91920	0.48180	36542.9	8976.9	10246.5	U/P
4.356	0.0150	0.0000	158.174	0.91835	0.45450	36544.4	9050.4	10283.9	U/P
4.378	0.0104	0.0000	158.167	0.91751	0.42815	36545.4	9123.8	10319.2	U/P U/P
4.400 4.422	0.0071 0.0048	0.0000 0.0000	158.161 158.154	0.91668 0.91587	0.40273 0.37825	36546.1 36546.6	9197.2 9270.5	10352.5 10383.7	U/P
4.444	0.0031	0.0000	158.148	0.91507	0.35468	36546.9	9343.7	10413.0	U/P
4.467	0.0018	0.0000	158.141	0.91429	0.33200	36547.1	9416.9	10440.5	U/P
4.489	0.0009	0.0000	158.135	0.91351	0.31019	36547.2	9490.0	10466.2	U/P
4.511	0.0003	0.0000	158.129	0.91276	0.28922	36547.2	9563.1	10490.2	U/P
4.533	0.0000	0.0000	158.123	0.91201	0.26909	36547.2	9636.1	10512.5	U/P U/P
4.556 4.578	0.0000 0.0000	0.0000 0.0000	158.117 158.111	0.91128 0.90990	0.24976 0.23121	36547.2 36547.2	9709.0 9781.9	10533.3 10552.5	U/P
10.578	0.0000	0.0000	157.182	0.35377	0.00000	36547.2	23509.0	10552.5	U/S
16.578	0.0000	0.0000	157.069	0.05754	0.00000	36547.2	25065.0	10552.5	S
22.578	0.0000	0.0000	156.950	0.02152	0.00000	36547.2	25994.7	10552.5	S
28.578	0.0000	0.0000 0.0000	156.719	0.00000	0.00000	36547.2	25994.7 25994.7	10552.5	S
34.578 40.578	0.0000 0.0000	0.0000	156.537 156.387	0.00000 0.00000	0.00000 0.00000	36547.2 36547.2	25994.7 25994.7	10552.5 10552.5	S S
46.578	0.0000	0.0000	156.259	0.00000	0.00000	36547.2	25994.7	10552.5	S
52.578	0.0000	0.0000	156.147	0.00000	0.00000	36547.2	25994.7	10552.5	S
58.578	0.0000	0.0000	156.048	0.00000	0.00000	36547.2	25994.7	10552.5	S
64.578	0.0000	0.0000	155.958	0.00000	0.00000	36547.2	25994.7	10552.5	S
70.578 76.578	0.0000	0.0000	155.878	0.00000	0.00000	36547.2	25994.7	10552.5	S
76.578 82.578	0.0000 0.0000	0.0000 0.0000	155.804 155.736	0.00000 0.00000	0.00000 0.00000	36547.2 36547.2	25994.7 25994.7	10552.5 10552.5	S S
88.578	0.0000	0.0000	155.673	0.00000	0.00000	36547.2	25994.7	10552.5	S
94.578	0.0000	0.0000	155.614	0.00000	0.00000	36547.2	25994.7	10552.5	S

Detailed Results (cont,d.) :: Scenario 4 :: SRWMD 100YR-8HR

Elapsed Time (hours)	Inflow Rate (ft³/s)	Outside Recharge (ft/day)	Stage Elevation (ft datum)	Infiltration Rate (ft³/s)	Overflow Discharge (ft³/s)	Cumulative Inflow Volume (ft³)	Cumulative Infiltration Volume (ft³)	Cumulative Discharge Volume (ft³)	Flow Type
8.222	0.0696	0.0000	158.052	0.90330	0.07386	49421.5	16989.3	17144.9	U/P
8.244	0.0498	0.0000	158.047	0.90272	0.06409	49426.3	17061.5	17150.4	U/P
8.267	0.0358	0.0000	158.042	0.90214	0.05471	49429.7	17133.7	17155.2	U/P
8.289	0.0255	0.0000	158.038	0.90156	0.04582	49432.1	17205.8	17159.2	U/P
8.311	0.0182	0.0000	158.033	0.90097	0.03747	49433.9	17277.9	17162.5	U/P
8.333	0.0129	0.0000	158.028	0.90039	0.02971	49435.1	17350.0	17165.2	U/P
8.356	0.0091	0.0000	158.024	0.89981	0.02260	49436.0	17422.0	17167.3	U/P
8.378	0.0064	0.0000	158.019	0.89924	0.01619	49436.6	17494.0	17168.8	U/P
8.400	0.0044	0.0000	158.014	0.89866	0.01056	49437.1	17565.9	17169.9	U/P
8.422	0.0030	0.0000	158.010	0.89809	0.00581	49437.4	17637.8	17170.6	U/P
8.444	0.0020	0.0000	158.005	0.89752	0.00213	49437.5	17709.6	17170.9	U/P
8.467	0.0011	0.0000	158.000	1.15253	0.00002	49437.7	17781.4	17171.0	U/P
8.489	0.0006	0.0000	157.993	1.05693	0.00000	49437.7	17894.0	17171.0	U/S
8.511	0.0002	0.0000	157.989	0.70395	0.00000	49437.8	17950.5	17171.0	S
8.533	0.0000	0.0000	157.986	0.69816	0.00000	49437.8	18006.6	17171.0	S
8.556	0.0000	0.0000	157.982	0.68940	0.00000	49437.8	18062.2	17171.0	S
8.578	0.0000	0.0000	157.979	0.68240	0.00000	49437.8	18116.9	17171.0	S
14.578	0.0000	0.0000	157.750	0.12199	0.00000	49437.8	21590.3	17171.0	S
20.578	0.0000	0.0000	157.630	0.07204	0.00000	49437.8	23387.1	17171.0	S
26.578	0.0000 0.0000	0.0000	157.540	0.05534	0.00000	49437.8	24702.6	17171.0	S S
32.578 38.578	0.0000	0.0000 0.0000	157.466 157.401	0.04630 0.04039	0.00000 0.00000	49437.8 49437.8	25777.7 26702.7	17171.0 17171.0	S
30.578 44.578	0.0000	0.0000	157.343	0.03613	0.00000	49437.8	27522.5	17171.0	S
44.578 50.578	0.0000	0.0000	157.343	0.03286	0.00000	49437.8	28263.3	17171.0	S
50.578 56.578	0.0000	0.0000	157.291	0.03286	0.00000	49437.8	28942.2	17171.0	S
62.578	0.0000	0.0000	157.242	0.02812	0.00000	49437.8	20942.2 29570.6	17171.0	S
68.578	0.0000	0.0000	157.157	0.02632	0.00000	49437.8	30157.0	17171.0	S
74.578	0.0000	0.0000	157.115	0.02032	0.00000	49437.8	30707.7	17171.0	S
80.578	0.0000	0.0000	157.077	0.02345	0.00000	49437.8	31227.6	17171.0	S
86.578	0.0000	0.0000	157.040	0.02227	0.00000	49437.8	31720.5	17171.0	S
92.578	0.0000	0.0000	157.006	0.01265	0.00000	49437.8	32189.6	17171.0	S
98.578	0.0000	0.0000	156.905	0.00179	0.00000	49437.8	32266.8	17171.0	S
104.578	0.0000	0.0000	156.803	0.00000	0.00000	49437.8	32266.8	17171.0	S
110.578	0.0000	0.0000	156.711	0.00000	0.00000	49437.8	32266.8	17171.0	S
116.578	0.0000	0.0000	156.626	0.00000	0.00000	49437.8	32266.8	17171.0	S
122.578	0.0000	0.0000	156.548	0.00000	0.00000	49437.8	32266.8	17171.0	S
128.578	0.0000	0.0000	156.475	0.00000	0.00000	49437.8	32266.8	17171.0	S
134.578	0.0000	0.0000	156.407	0.00000	0.00000	49437.8	32266.8	17171.0	S
140.578	0.0000	0.0000	156.343	0.00000	0.00000	49437.8	32266.8	17171.0	S
146.578	0.0000	0.0000	156.283	0.00000	0.00000	49437.8	32266.8	17171.0	S
152.578	0.0000	0.0000	156.226	0.00000	0.00000	49437.8	32266.8	17171.0	S
158.578	0.0000	0.0000	156.172	0.00000	0.00000	49437.8	32266.8	17171.0	S
164.578	0.0000	0.0000	156.121	0.00000	0.00000	49437.8	32266.8	17171.0	S
170.578	0.0000	0.0000	156.072	0.00000	0.00000	49437.8	32266.8	17171.0	S
176.578	0.0000	0.0000	156.026	0.00000	0.00000	49437.8	32266.8	17171.0	S
182.578	0.0000	0.0000	155.981	0.00000	0.00000	49437.8	32266.8	17171.0	S
188.578	0.0000	0.0000	155.938	0.00000	0.00000	49437.8	32266.8	17171.0	S
194.578	0.0000	0.0000	155.897	0.00000	0.00000	49437.8	32266.8	17171.0	S
200.578	0.0000	0.0000	155.858	0.00000	0.00000	49437.8	32266.8	17171.0	S
206.578	0.0000	0.0000	155.820	0.00000	0.00000	49437.8	32266.8	17171.0	S
212.578	0.0000	0.0000	155.783	0.00000	0.00000	49437.8	32266.8	17171.0	S
218.578	0.0000	0.0000	155.748	0.00000	0.00000	49437.8	32266.8	17171.0	S
224.578	0.0000	0.0000	155.714	0.00000	0.00000	49437.8	32266.8	17171.0	S
230.578	0.0000	0.0000	155.681	0.00000	0.00000	49437.8	32266.8	17171.0	S
236.578	0.0000	0.0000	155.650	0.00000	0.00000	49437.8	32266.8	17171.0	S
242.578	0.0000	0.0000	155.619	0.00000	0.00000	49437.8	32266.8	17171.0	S
248.578	0.0000	0.0000	155.589	0.00000	0.00000	49437.8	32266.8	17171.0	S
254.578	0.0000	0.0000	155.560	0.00000	0.00000	49437.8	32266.8	17171.0	S
260.578	0.0000	0.0000	155.532	0.00000	0.00000	49437.8	32266.8	17171.0	S
266.578	0.0000	0.0000	155.505	0.00000	0.00000	49437.8	32266.8	17171.0	S
272.578	0.0000	0.0000	155.479	0.00000	0.00000	49437.8	32266.8	17171.0	S
278.578	0.0000	0.0000	155.453	0.00000	0.00000	49437.8	32266.8	17171.0	S
284.578	0.0000	0.0000	155.428	0.00000	0.00000	49437.8	32266.8	17171.0	S
290.578	0.0000	0.0000	155.404	0.00000	0.00000	49437.8	32266.8	17171.0	S
296.578	0.0000	0.0000	155.380	0.00000	0.00000	49437.8	32266.8	17171.0	S
302.578	0.0000	0.0000	155.357	0.00000	0.00000	49437.8	32266.8	17171.0	S
308.578	0.0000	0.0000	155.335	0.00000	0.00000	49437.8	32266.8	17171.0	S
314.578	0.0000	0.0000	155.313	0.00000	0.00000	49437.8	32266.8	17171.0	S
320.578	0.0000	0.0000	155.292	0.00000	0.00000	49437.8	32266.8	17171.0	S
326.578	0.0000	0.0000	155.271	0.00000	0.00000	49437.8	32266.8	17171.0	S
332.578	0.0000	0.0000	155.251	0.00000	0.00000	49437.8	32266.8	17171.0	S
000 570	0.0000	0.0000	155.231	0.00000	0.00000	49437.8	32266.8	17171.0	S
338.578									
338.578 344.578 350.578	0.0000 0.0000	0.0000 0.0000	155.211 155.192	0.00000 0.00000	0.00000 0.00000	49437.8 49437.8	32266.8 32266.8	17171.0 17171.0	S S

Detailed Results (cont,d.) :: Scenario 5 :: SRWMD 100YR-24HR

Elapsed Time (hours)	Inflow Rate (ft³/s)	Outside Recharge (ft/day)	Stage Elevation (ft datum)	Infiltration Rate (ft³/s)	Overflow Discharge (ft³/s)	Cumulative Inflow Volume (ft³)	Cumulative Infiltration Volume (ft ³)	Cumulative Discharge Volume (ft³)	Flow Type
48.578	0.0000	0.0000	157.790	0.04142	0.00000	75765.1	26523.4	37974.5	S
54.578	0.0000	0.0000	157.733	0.03772	0.00000	75765.1	27373.4	37974.5	S
60.578	0.0000	0.0000	157.681	0.03474	0.00000	75765.1	28152.7	37974.5	S
66.578 72.578	0.0000 0.0000	0.0000 0.0000	157.632 157.586	0.03228 0.03021	0.00000 0.00000	75765.1 75765.1	28874.2 29547.2	37974.5 37974.5	S S
78.578	0.0000	0.0000	157.543	0.02843	0.00000	75765.1	30179.2	37974.5	S
84.578	0.0000	0.0000	157.502	0.02689	0.00000	75765.1	30775.5	37974.5	S S
90.578	0.0000	0.0000	157.463	0.02554	0.00000	75765.1	31340.8	37974.5	S S S
96.578	0.0000	0.0000	157.425	0.02433	0.00000	75765.1	31878.7	37974.5	S
102.578	0.0000	0.0000	157.389	0.02325	0.00000	75765.1	32392.0	37974.5	
108.578 114.578	0.0000 0.0000	0.0000 0.0000	157.355 157.322	0.02228 0.02140	0.00000 0.00000	75765.1 75765.1	32883.3 33354.6	37974.5 37974.5	S S S
120.578	0.0000	0.0000	157.289	0.02059	0.00000	75765.1	33807.7	37974.5	S
126.578	0.0000	0.0000	157.258	0.01985	0.00000	75765.1	34244.2	37974.5	S
132.578	0.0000	0.0000	157.228	0.01917	0.00000	75765.1	34665.4	37974.5	S S S
138.578	0.0000	0.0000	157.199	0.01854	0.00000	75765.1	35072.5	37974.5	S
144.578 150.578	0.0000 0.0000	0.0000 0.0000	157.170 157.143	0.01795 0.01741	0.00000 0.00000	75765.1 75765.1	35466.4 35848.2	37974.5 37974.5	S S
156.578	0.0000	0.0000	157.116	0.01690	0.00000	75765.1	36218.5	37974.5	s
162.578	0.0000	0.0000	157.089	0.01642	0.00000	75765.1	36578.1	37974.5	S
168.578	0.0000	0.0000	157.064	0.01597	0.00000	75765.1	36927.7	37974.5	S
174.578	0.0000	0.0000	157.039	0.01554	0.00000	75765.1	37267.9	37974.5	S
180.578	0.0000	0.0000	157.014 156.967	0.01210 0.00443	0.00000	75765.1 75765.1	37599.1 37790.6	37974.5 37974.5	S S
<u>186.578</u> 192.578	0.0000	0.0000	156.889	0.00000	0.00000	75765.1	37790.6	37974.5	S
198.578	0.0000	0.0000	156.818	0.00000	0.00000	75765.1	37790.6	37974.5	S
204.578	0.0000	0.0000	156.752	0.00000	0.00000	75765.1	37790.6	37974.5	S
210.578	0.0000	0.0000	156.690	0.00000	0.00000	75765.1	37790.6	37974.5	S
216.578	0.0000	0.0000	156.632	0.00000	0.00000	75765.1	37790.6	37974.5	S S S
222.578 228.578	0.0000 0.0000	0.0000 0.0000	156.577 156.525	0.00000 0.00000	0.00000 0.00000	75765.1 75765.1	37790.6 37790.6	37974.5 37974.5	5
234.578	0.0000	0.0000	156.475	0.00000	0.00000	75765.1	37790.6	37974.5	S S
240.578	0.0000	0.0000	156.428	0.00000	0.00000	75765.1	37790.6	37974.5	S
246.578	0.0000	0.0000	156.382	0.00000	0.00000	75765.1	37790.6	37974.5	S S S
252.578	0.0000	0.0000	156.338	0.00000	0.00000	75765.1	37790.6	37974.5	
258.578	0.0000	0.0000	156.296	0.00000	0.00000	75765.1	37790.6	37974.5	S S S
264.578 270.578	0.0000 0.0000	0.0000 0.0000	156.256 156.216	0.00000 0.00000	0.00000 0.00000	75765.1 75765.1	37790.6 37790.6	37974.5 37974.5	S
276.578	0.0000	0.0000	156.179	0.00000	0.00000	75765.1	37790.6	37974.5	S
282.578	0.0000	0.0000	156.142	0.00000	0.00000	75765.1	37790.6	37974.5	S S S
288.578	0.0000	0.0000	156.107	0.00000	0.00000	75765.1	37790.6	37974.5	S
294.578	0.0000	0.0000	156.073	0.00000	0.00000	75765.1	37790.6	37974.5	S
300.578 306.578	0.0000 0.0000	0.0000 0.0000	156.040 156.008	0.00000 0.00000	0.00000 0.00000	75765.1 75765.1	37790.6 37790.6	37974.5 37974.5	S S
312.578	0.0000	0.0000	155.976	0.00000	0.00000	75765.1	37790.6	37974.5	S
318.578	0.0000	0.0000	155.946	0.00000	0.00000	75765.1	37790.6	37974.5	S
324.578	0.0000	0.0000	155.917	0.00000	0.00000	75765.1	37790.6	37974.5	S S
330.578	0.0000	0.0000	155.888	0.00000	0.00000	75765.1	37790.6	37974.5	S
336.578 342.578	0.0000 0.0000	0.0000 0.0000	155.860 155.833	0.00000 0.00000	0.00000 0.00000	75765.1 75765.1	37790.6 37790.6	37974.5 37974.5	S
348.578	0.0000	0.0000	155.807	0.00000	0.00000	75765.1	37790.6	37974.5	S S
354.578	0.0000	0.0000	155.781	0.00000	0.00000	75765.1	37790.6	37974.5	S
360.578	0.0000	0.0000	155.756	0.00000	0.00000	75765.1	37790.6	37974.5	S
366.578	0.0000	0.0000	155.731	0.00000	0.00000	75765.1	37790.6	37974.5	S
372.578 378.578	0.0000 0.0000	0.0000 0.0000	155.707 155.684	0.00000 0.00000	0.00000 0.00000	75765.1 75765.1	37790.6 37790.6	37974.5 37974.5	S S
384.578	0.0000	0.0000	155.661	0.00000	0.00000	75765.1	37790.6	37974.5	S
390.578	0.0000	0.0000	155.638	0.00000	0.00000	75765.1	37790.6	37974.5	S
396.578	0.0000	0.0000	155.616	0.00000	0.00000	75765.1	37790.6	37974.5	S
402.578	0.0000	0.0000	155.595	0.00000	0.00000	75765.1	37790.6	37974.5	S
408.578 414.578	0.0000 0.0000	0.0000 0.0000	155.574 155.554	0.00000 0.00000	0.00000 0.00000	75765.1 75765.1	37790.6 37790.6	37974.5 37974.5	S
420.578	0.0000	0.0000	155.534	0.00000	0.00000	75765.1	37790.6	37974.5	S S
426.578	0.0000	0.0000	155.514	0.00000	0.00000	75765.1	37790.6	37974.5	S
432.578	0.0000	0.0000	155.495	0.00000	0.00000	75765.1	37790.6	37974.5	S
438.578	0.0000	0.0000	155.476	0.00000	0.00000	75765.1	37790.6	37974.5	S
444.578	0.0000	0.0000	155.457	0.00000	0.00000	75765.1	37790.6	37974.5	S
450.578 456.578	0.0000 0.0000	0.0000 0.0000	155.439 155.421	0.00000 0.00000	0.00000 0.00000	75765.1 75765.1	37790.6 37790.6	37974.5 37974.5	S S
450.578	0.0000	0.0000	155.404	0.00000	0.00000	75765.1	37790.6	37974.5	S
468.578	0.0000	0.0000	155.386	0.00000	0.00000	75765.1	37790.6	37974.5	S
474.578	0.0000	0.0000	155.370	0.00000	0.00000	75765.1	37790.6	37974.5	S
480.578	0.0000	0.0000	155.353	0.00000	0.00000	75765.1	37790.6	37974.5	S
486.578	0.0000	0.0000	155.337	0.00000	0.00000	75765.1	37790.6	37974.5	S

Detailed Results :: Scenario 6 :: WQTV

_	Elapsed Time (hours)	Inflow Rate (ft³/s)	Outside Recharge (ft/day)	Stage Elevation (ft datum)	Infiltration Rate (ft³/s)	Overflow Discharge (ft³/s)	Cumulative Inflow Volume (ft³)	Cumulative Infiltration Volume (ft³)	Cumulative Discharge Volume (ft³)	Flow Type
	0.000	2080.5000	0.0000	152.990	0.00000	0.00000	0.0	0.0	0.0	N.A.
	0.002	2080.5000	0.0000	157.870	0.88138	0.00000	12483.0	5.3	0.0	U/P
	2.400	0.0000	0.0000	157.369	0.51210	0.00000	12483.0	7372.3	0.0	U/P
	6.000	0.0000	0.0000				12483.0	12483.0	0.0	dry
	12.000	0.0000	0.0000				12483.0	12483.0	0.0	dry
	24.000	0.0000	0.0000				12483.0	12483.0	0.0	dry
	36.000	0.0000	0.0000				12483.0	12483.0	0.0	dry
	48.000	0.0000	0.0000				12483.0	12483.0	0.0	dry
	60.000	0.0000	0.0000				12483.0	12483.0	0.0	dry
	72.000	0.0000	0.0000				12483.0	12483.0	0.0	dry
	84.000	0.0000	0.0000				12483.0	12483.0	0.0	dry
	96.000	0.0000	0.0000				12483.0	12483.0	0.0	dry

Underdrain Analysis



BACKGROUND SEEPAGE PONDS INPUTS

Aquifer Data		
Base of Aquifer:	148.7	ft
Seasonal High Water Table:	154.7	ft
Hydraulic Conductivity	5	ft/day
Fillable Porosity	20	%

Geometry: Underdrain Stage Storage

Based on the theoretical volume of water the underdrains could draw down.

ELEV.	AREA (SF)	STORAGE (CF)	STORAGE VOLUME (AC- FT)	
152.0	13,469	0	0.000	*Based on minimum Underdrain Orifice EL. 152.28'
153.0	15,494	14,482	0.332	
154.0	17,606	31,032	0.712	
155.0	0 19,819	49,744	1.142	**Set above the measured SHWT EL. 154.7'
Volumo:		40 744	of	-

Volume:	49,744	cf
Area:	19819	sf
Depth:	3.00	ft
Perimeter:	566	ft
Eq. Length:	200	ft
Eq: Width:	83	ft

Project Data

Project Name:	CRS Marvin Burnett
Simulation Description:	Background Seepage
Project Number:	23-0653
Engineer :	JHP
Supervising Engineer:	CCM
Date:	01-18-2024

Aquifer Data

Base Of Aquifer Elevation, [B] (ft datum):	148.70
Water Table Elevation, [WT] (ft datum):	154.70
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day):	5.00
Fillable Porosity, [n] (%):	20.00
Vartical infiltration was not considered	

Vertical infiltration was not considered.

Geometry Data

Equivalent Pond Length, [L] (ft):	200.0
Equivalent Pond Width, [W] (ft):	83.0

Ground water mound is expected to intersect the pond bottom

<u>Stage vs Area Data</u>

Stage	Area
(ft datum)	(ft²)
152.00	13469.0
153.00	15494.0
153.00	15494.0 17606.0
155.00	19819.0

Discharge Structures

Discharge Structure #1 is active as orifice

Structure Parameters

Description: 12" Underdrain

Orifice elevation, (ft datum):	152.27
Orifice coefficient:	4.9
Orifice area, (ft ²):	0.785
Orifice exponent:	0.5

Tailwater - disabled, free discharge

Scenario Input Data

Scenario 1 :: 12" Underdrain

Hydrograph Type: Modflow Routing:	Baseflow Routed with infiltration		
Seasonal Water Table Duration of Wet Seaso Number of Increments	0.01 120.0 240		
Initial (seasonal low) g	154.69		

Recharge is applied inside pond (in addition to outside pond)? No

Note: when this option is selected, water will be added to the pond to synchronize the rise in the pond level with the rise in the groundwater. Otherwise, no water will be added directly to the pond, and the pond water level will rise as a result of infiltration only.

Detailed Results (cont,d.) :: Scenario 1 :: 12" Underdrain

Elapsed Time (hours)	Inflow Rate (ft³/s)	Outside Recharge (ft/day)	Stage Elevation (ft datum)	Infiltration Rate (ft³/s)	Overflow Discharge (ft³/s)	Cumulative Inflow Volume (ft³)	Cumulative Infiltration Volume (ft³)	Cumulative Discharge Volume (ft³)	Flow Type
2664.000	0.0000	0.0000	152.270	-0.00331	0.00331	0.0	-178509.4	218681.4	S
2676.000	0.0000	0.0000	152.270	-0.00331	0.00331	0.0	-178652.3	218824.3	S
2688.000	0.0000	0.0000	152.270	-0.00330	0.00330	0.0	-178795.1	218967.1	S
2700.000	0.0000	0.0000	152.270	-0.00330	0.00330	0.0	-178937.7	219109.7	S
2712.000	0.0000	0.0000	152.270	-0.00329	0.00329	0.0	-179080.1	219252.1	S
2724.000	0.0000	0.0000	152.270	-0.00329	0.00329	0.0	-179222.4	219394.4	S
2736.000	0.0000	0.0000	152.270	-0.00329	0.00329	0.0	-179364.5	219536.4	S
2748.000	0.0000	0.0000	152.270	-0.00328	0.00328	0.0	-179506.3	219678.3	S
2760.000	0.0000	0.0000	152.270	-0.00328	0.00328	0.0	-179648.1	219820.1	S
2772.000	0.0000	0.0000	152.270	-0.00327	0.00327	0.0	-179789.6	219961.6	S
2784.000	0.0000	0.0000	152.270	-0.00327	0.00327	0.0	-179931.0	220103.0	S
2796.000	0.0000	0.0000	152.270	-0.00327	0.00327	0.0	-180072.2	220244.2	S
2808.000	0.0000	0.0000	152.270	-0.00326	0.00326	0.0	-180213.2	220385.2	S
2820.000	0.0000	0.0000	152.270	-0.00326	0.00326	0.0	-180354.1	220526.1	S
2832.000	0.0000	0.0000	152.270	-0.00325	0.00325	0.0	-180494.8	220666.8	S
2844.000	0.0000	0.0000	152.270	-0.00325	0.00325	0.0	-180635.3	220807.3	S
2856.000	0.0000	0.0000	152.270	-0.00325	0.00325	0.0	-180775.7	220947.7	S
2868.000	0.0000	0.0000	152.270	-0.00324	0.00324	0.0	-180915.9	221087.9	S
2880.000	0.0000	0.0000	152.270			0.0	-181055.9	221227.9	N.A.

FLOW RATE WHEN SYSTEM ACHIEVES STEADY STATE (120 DAYS) WITH SEASONAL HIGH WATER TABLE ELEVATION

Job Information

Job Name:	23-0653 CRS Marvin Burnett
Engineer:	JHP
Date:	01-18-2024

Input Data

<u>Results</u>

Computed underdrain spacing, [S]:
Computed total length of laterals, [L]:
Computed flow rate through outfall, [Q]:
Computed flow rate per lineal foot of lateral, [ql]:

106.6505	ft
185.8312	ft
2.717507E-02	ft³/sec
1.462352E-04	ft³/sec/ft

<u>Notes</u>

- 1. Laterals should be no farther than S/2 from the top of the basin.
- 2. A gravel envelope at least 3 inches thick is recommended around the underdrain pipes. If a gravel envelope is used, a filter fabric will be required around this envelope.
- 3. The underdrain pipe should have a filter fabric sock to prevent fines from moving into and clogging the perforated pipe.
- 4. Ensure outfall elevation for system will allow gravity flow without tailwater backpressure to the underdrains.
- 5. Theory is applicable where ground water flow is largely in a horizontal direction (i.e., natural gradients less than 1%).
- 6. Capped and sealed inspection and cleanout ports which extend to the ground surface are recommended at the following locations for each drain pipe:
 - a. the terminus
 - b. at every 400 feet or every bend of 45 or more degrees, whichever is shortest
- 7. Underdrain basin should be stabilized with permanent vegetative cover.

<u>Warnings</u>

None.

Job Information

Job Name:	23-0653 CRS Marvin Burnett
Engineer:	JHP
Date:	01-18-2024

Input Data

Maximum Underdrain Spacing:	55.7 ft
Provided Underdrain Spacing:	25.0 ft
Minimum Lateral Length:	355 ft
Provided Lateral Length:	375 ft

<u>Notes</u>

- 1. Laterals should be no farther than S/2 from the top of the basin.
- 2. A gravel envelope at least 3 inches thick is recommended around the underdrain pipes. If a gravel envelope is used, a filter fabric will be required around this envelope.
- 3. The underdrain pipe should have a filter fabric sock to prevent fines from moving into and clogging the perforated pipe.
- 4. Ensure outfall elevation for system will allow gravity flow without tailwater backpressure to the underdrains.
- 5. Theory is applicable where ground water flow is largely in a horizontal direction (i.e., natural gradients less than 1%).
- 6. Capped and sealed inspection and cleanout ports which extend to the ground surface are recommended at the following locations for each drain pipe:
 - a. the terminus
 - b. at every 400 feet or every bend of 45 or more degrees, whichever is shortest
- 7. Underdrain basin should be stabilized with permanent vegetative cover.

<u>Warnings</u>

None.

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Appendix B

Operation and Maintenance Requirements and Erosion and Sedimentation Control Requirements Proposed operation and maintenance and soil erosion and sediment control practices are outlined in the following paragraphs.

Surface water Management Facilities

The man-made surface water facility shall be maintained free of sediments and debris. Areas shall be inspected on a routine basis and nuisance plants shall be removed a minimum of twice annually. Grassed areas shall be mowed a minimum of 6 times per year. The natural systems shall be least disturbed as possible. Minimal maintenance is required for the natural and undisturbed areas. All ponds shall be inspected monthly. Monthly documentation shall be noted based upon the inspection findings.

Erosion Control

All erosion damage at spillways, outfall structures, and along pond side slopes shall be repaired (grading and grassing) as conditions occur. All side slopes and other areas disturbed by construction shall be stabilized by sodding, hydro-mulching or other appropriate vegetative or non-vegetative erosion control measures.

Swale/Ditch

All swales, if any, shall be maintained free of debris and sediment. Sediments shall be removed when the depth has been reduced by 20 percent. Sediments removed from swales/ditches should be evenly spread over grassed areas away from the stormwater management facilities.

Culverts, Pipes and Structures

All pipes, if any, shall be inspected bi-annually. Culverts and pipes shall be maintained free of debris and sediment. Sediments removed from culverts and pipes should be evenly spread over grassed areas away from the stormwater management facilities.

The structures and paved flow lines, if any, shall be maintained clear of debris. Remove any debris and silt collected in inlets and pipes as routine inspections dictates.

Inspection Reporting

Annual inspection reports, prepared by a properly licensed professional engineer, should be submitted to the water management district as appropriate. The engineer shall inspect the site and report on the status and function of the system. Noted deficiencies and/or maintenance requirements shall be reported to the owner with recommendations for repairs. Repairs shall be executed.

Limerock/Sinkhole

If continuous limerock is encountered during excavation of the swales/pond or if a sinkhole forms in the area of a drainage swale/pond the engineer of record shall be notified by either the contractor or the established operation and maintenance entity. The engineer of record shall inspect the repaired area upon completion of the repair.

Where continuous limerock is encountered during excavation of the swales/ponds, the limerock shall be over excavated by 2 feet and replaced with clayey soils that extend 2 feet beyond the perimeter of the limerock outcropping. The clayey soil shall have at least 20% passing the no. 200 sieve, compacted to 95% of standard proctor, and compacted in a wet condition with moisture 2% - 4% above optimum.

All swales/ponds shall be inspected monthly for sinkhole occurrence. Should a sinkhole occur, the area shall be repaired as soon as possible. Repair shall include filling (limerock such as road base material, clay/sand mixture, or concrete if necessary). A 2-foot deep cap that extends 2 feet beyond the perimeter of the sinkhole shall be constructed with clayey soils. The clayey soil shall have at least 20% passing the no. 200 sieve, compacted to 95% of standard proctor, and compacted in a wet condition with moisture 2% - 4% above optimum. The clay soil cap shall be re-graded to prevent concentration of waters (ponding) and re-vegetated.

Outfall Structures

All outfall and drawdown orifices are to be inspected bi-annually for sediment or debris in the flow line of weirs or orifices. All sediment and debris should be removed and disposed of in an approved manner.

Operation & Maintenance Entity:

Concept Development, Inc. 1449 SW 74th Drive. Suite 200 Gainesville, FL 32607

Appendix C

Geotechnical Report



SUMMARY REPORT OF A GEOTECHNICAL SITE EXPLORATION – REVISION 1

DOLLAR GENERAL – LAKE CITY SW MARVIN BURNETT LAKE CITY, COLUMBIA COUNTY, FLORIDA

GSE PROJECT NO. 16251

Prepared For:

CONCEPT DEVELOPMENT, INC.

DECEMBER 2023

December 7, 2023



Andrea Barnett Concept Development, Inc. 1449 SW 74th Drive, Suite 200 Gainesville, Florida 32607

Subject: Summary Report of a Geotechnical Site Exploration – Revision 1 **Dollar General – Lake City SW Marvin Burnett** Lake City, Columbia County, Florida GSE Project No. 16251

GSE Engineering & Consulting, Inc. (GSE) is pleased to submit this geotechnical site exploration report for the above referenced project.

Presented herein are the findings and conclusions of our exploration, including the geotechnical parameters and recommendations to assist with building foundation, pavement, and stormwater management designs. This revision includes recommended soil parameters for stormwater management design with underdrains.

GSE appreciates this opportunity to have assisted you on this project. If you have any questions or comments concerning this report, please contact us.

Sincerely,

GSE Engineering & Consulting, Inc.

Angelina X. Liu, E.I. Staff Engineer





Jason E. Gowland, P.E. Principal Engineer Florida Registration No. 66467

AXL / JEG: tlf Q:\Projects\16251 Dollar General – Lake City SW Marvin Burnett\16251 Rev.1.docx

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> GSE Engineering & Consulting, Inc. 5590 SW 64th Street, Suite B Gainesville, Florida 32608 (352) 377-3233 Phone • (352) 377-0335 Fax www.gseengineering.com

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- 1. Project Site Location Map
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1.0 INTRODUCTION

1.1 General

GSE Engineering & Consulting, Inc. (GSE) has completed this geotechnical exploration for the proposed commercial retail store located on SW Marvin Burnett Road in Lake City, Columbia County, Florida. This exploration was performed in accordance with GSE Proposal No. 2023-589 dated September 12, 2023. Ms. Andrea Barnett authorized our services on September 15, 2023.

1.2 Project Description

We understand that you are coordinating due diligence related work related to the development of this site into a commercial retail store. The site is located on the northwest corner of the State Road 47 and SW Marvin Burnett Road intersection in Lake City, Columbia County, Florida. The site is approximately +/-2.72 acres.

You provided GSE with information about the project. We understand the project will consist of an approximate 10,640 square foot building, a parking lot, and a stormwater management facility.

The structure is expected to be a single-story, high wall concrete masonry unit (CMU) and steel frame construction. Structural loads have not been provided but are expected to be on the order of 1 to 2 kips per foot for non-load bearing CMU walls, and less than 50 kips for columns. The finished floor of the structure is anticipated to be constructed within 1 to 2 feet of the existing site grades.

The building will be located in the northern portion of the site. The parking lot will be located west, south, and east of the structure. The stormwater management facility will be located on the western portion of the site.

A recent aerial photograph of the site was obtained and reviewed. The site plan and aerial photograph were used in preparation of this exploration and report.

1.3 Purpose

The purpose of this geotechnical exploration was to determine the general subsurface conditions, evaluate these conditions with respect to the proposed construction, and prepare geotechnical parameters and recommendations to assist with building foundation, stormwater management, and pavement designs.

2.0 FIELD AND LABORATORY TESTS

2.1 General Description

The procedures used for field sampling and testing are in general accordance with industry standards of care and established geotechnical engineering practices for this geographic region. This exploration consisted of performing five (5) Standard Penetration Test (SPT) borings to a depth of 20 feet below land surface (bls) within the proposed building area, five (5) auger borings to a depth of 5 feet bls in the area of the parking lot and driveways, and five (5) auger borings to depths of 15 feet bls in the area of the stormwater management facility.

The soil borings were performed at the approximate locations as shown on Figure 2. The borings were located at the site using the provided site plan, Global Positioning System (GPS) coordinates, and obvious site features as reference. The boring locations should be considered approximate. The soil borings were performed on September 20, 2023.

2.2 Auger Borings

The auger borings were performed in accordance with ASTM D1452. The borings were performed with flight auger equipment that was rotated into the ground in a manner that reduces soil disturbance. After penetrating to the required depth, the auger was retracted and the soils collected on the auger flights were field classified and placed in sealed containers. Representative samples of each stratum were retained from the auger boring. Results from the auger borings are provided in Section 5.1.

2.3 Standard Penetration Test Borings

The soil borings were performed with a drill rig employing mud rotary drilling techniques and Standard Penetration Testing (SPT) in accordance with ASTM D1586. The SPTs were performed continuously to 10 feet and at 5-foot intervals thereafter. Soil samples were obtained at the depths where the SPTs were performed. The soil samples were classified in the field, placed in sealed containers, and returned to our laboratory for further evaluation.

After drilling to the sampling depth, the standard two-inch O.D. split-barrel sampler was seated by driving it 6 inches into the undisturbed soil. The sampler was then driven an additional 12 inches by blows of a 140-pound hammer falling 30 inches. The number of blows required to produce the next 12 inches of penetration were recorded as the penetration resistance (N-value). These values and the complete SPT boring logs are provided in Section 5.2.

Upon completion of the sampling, the boreholes were abandoned in accordance with Water Management District guidelines.

2.4 Soil Laboratory Tests

The soil samples recovered from the soil borings were returned to our laboratory, and examined to confirm the field descriptions. Representative samples were then selected for laboratory testing. The laboratory tests consisted of nine (9) percent soil fines passing the No. 200 sieve, nine (9) natural moisture content determinations, two (2) Atterberg Limits tests, and three (3) constant head hydraulic conductivity tests. These tests were performed in order to aid in classifying the soils and to further evaluate their engineering properties. The laboratory tests are provided in Section 5.3.

3.0 FINDINGS

3.1 Surface Conditions

Karen Roylos with GSE visited the site on September 18, 2023 to observe the site conditions and mark the boring locations. Mr. Jason Kite with Jason Kite, LLC was retained by GSE to clear lanes to allow access to the boring locations for drilling equipment.

The majority of the site is densely vegetated with trees, scattered saw palmettos, shrubs, vines and weedy groundcover. Portions of the site were densely vegetated and more difficult to traverse. To the south of the site is SW Marvin Burnett Road. State Road 47 is located east of the site. Undeveloped wooded land borders the site to the north and west.

The topography at the site is moderately sloping from northeast towards southwest. Regional topography can be characterized as gently to moderately sloping. The Lake City West USGS Topographic Map indicates the ground surface elevations at the site are near 155 to 165 feet¹ NAVD 88.

3.2 Subsurface Conditions

The locations of the auger and SPT borings are provided on Figure 2. Complete logs for the borings are provided in Sections 5.1 and 5.2. Descriptions for the soils encountered are accompanied by the Unified Soil Classification System symbol (SM, SP-SM, etc.) and are based on visual examination of the recovered soil samples and the laboratory tests performed. Stratification boundaries between the soil types should be considered approximate, as the actual transition between soil types may be gradual.

The auger borings located within the proposed parking lot and driveways encountered relatively similar soil conditions. Auger borings A-1 to A-3 encountered poorly graded sand, and sand with silt (SP, SP-SM) to the explored depths of 5 feet bls. Auger borings A-4 and A-5 initially encountered sand with silt (SP-SM) to depths of 1.5 to 3.5 feet bls. This was underlain by clayey to very clayey sand (SC, SC/CL) to the explored depths of 5 feet bls.

The auger borings located within the stormwater management facility encountered relatively consistent soil conditions. Auger boring P-1 encountered 6 feet of silty sand, and poorly graded sand (SM, SP) overlying clayey to very clayey sand, and clay with sand (SC, SC/CL, CL/CH) to the explored depth of 15 feet bls. Auger borings P-2 to P-4 initially encountered poorly graded sand, sand with silt, and silty sand (SP, SP-SM, SM) to depths of 2 to 5 feet bls, overlying silty clayey sand, and clayey to very clayey sand (SM-SC, SC, SC/CL) to depths of 7 to 10.5 feet bls. This was underlain by sand with silt (SP-SM) to depths of 12 to 13.5 feet bls, followed by clayrich soils (CL/CH) to the explored depth of 15 feet of sand with silt (SP-SM) overlying clay with sand (CL/CH) to a depth of 12.5 feet bls. This was underlain by sand with silt (SP-SM) to the explored depth of 15 feet bls. Silt (SP-SM) to the explored depth of 15 feet bls. Auger boring P-5 initially encountered 5.5 feet of clayey sand (SC) and 5 feet of sand with silt (SP-SM) overlying clay with sand (CL/CH) to a depth of 12.5 feet bls. This was underlain by sand with silt (SP-SM) to the explored depth of 15 feet bls.

¹ United States Geological Survey, Lake City West Quadrangle, 2021.

The SPT borings located within the proposed building footprint indicate the soils across these areas are relatively consistent. SPT boring B-1 initially encountered 3 feet of sand with silt (SP-SM), and 4.5 feet of sandy clay (CL) overlying sand with clay, and poorly graded sand (SP-SC, SP) to a depth of 12 feet bls. This was underlain by clay (CL/CH) to the explored depth of 20 feet bls. SPT borings B-2 to B-5 encountered poorly graded sand, sand with silt, sand with clay, silty sand, and silty clayey sand (SP, SP-SM, SP-SC, SM-SC) with some interbedded layers of clayey to very clayey sand (SC, SC/CL) to depths of 13.5 to 17.5 feet bls. This was underlain by clay-rich (CL, CL/CH) soils to the explored depths of 20 feet bls.

The sandy soils (SP, SP-SM, SP-SC) encountered are generally in a very loose to dense condition with N-values ranging from 2 to 45 blows per foot. The silty sand, silty clayey sand, and clayey to very clayey sands (SM, SM-SC, SC, SC/CL) encountered are generally in a very loose to dense condition with N-values ranging from 4 to 38 blows per foot. The sandy clay, clay with sand, and clay (CL/CH, CL) encountered are generally in a very soft to hard condition with N-values ranging from 3 to 33 blows per foot.

Weight-of-rod strength material was encountered in SPT boring B-2 at depth range from 13.5 to 14.5 feet bls. This isolated occurrence is likely related to depositional characteristics of the soil materials and transitions between material types.

The groundwater table was encountered in the auger and SPT borings at depths of 6.1 to 8.8 feet bls at the time of our investigation.

3.3 Review of Published Data

The majority of the site is mapped as three soil series by the Soil Conservation Service (SCS) Soil Survey for Columbia County². The following soil descriptions are from the Soil Survey.

Blanton fine sand, 0 to 5 percent slopes

Map Unit Setting

- *National map unit symbol:* 2w0q2
- *Elevation:* 30 to 200 feet
- Mean annual precipitation: 51 to 59 inches
- Mean annual air temperature: 64 to 72 degrees F
- *Frost-free period:* 258 to 310 days
- *Farmland classification:* Not prime farmland

Map Unit Composition

- Blanton and similar soils: 85 percent
- Minor components: 15 percent
- Estimates are based on observations, descriptions, and transects of the map unit.

² Soil Survey of Hamilton County, Florida. Soil Conservation Service, U.S. Department of Agriculture.

Description of Blanton

Setting

- *Landform:* Knolls on marine terraces, ridges on marine terraces
- Landform position (two-dimensional): Backslope
- Landform position (three-dimensional): Side slope, interfluve, riser
- *Down-slope shape:* Convex
- Across-slope shape: Linear
- Parent material: Sandy and loamy marine deposits

Typical profile

- A 0 to 7 inches: fine sand
- *E* 7 *to 52 inches:* fine sand
- Bt 52 to 80 inches: fine sandy loam

Properties and qualities

- *Slope:* 0 to 5 percent
- Depth to restrictive feature: More than 80 inches
- Drainage class: Moderately well drained
- *Runoff class:* Negligible
- *Capacity of the most limiting layer to transmit water (Ksat):* Moderately high to high (0.20 to 6.00 in/hr)
- Depth to water table: About 42 to 72 inches
- Frequency of flooding: None
- *Frequency of ponding:* None
- *Maximum salinity:* Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
- Sodium adsorption ratio, maximum: 4.0
- Available water supply, 0 to 60 inches: Low (about 3.6 inches)

Interpretive groups

- Land capability classification (irrigated): None specified
- Land capability classification (nonirrigated): 3s
- Hydrologic Soil Group: A
- *Forage suitability group:* Sandy soils on rises, knolls, and ridges of mesic uplands (G138XA121FL)
- *Other vegetative classification:* Sandy soils on rises, knolls, and ridges of mesic uplands (G138XA121FL)
- *Hydric soil rating:* No

Summary Report of a Geotechnical Site Exploration – Revision 1 Dollar General – Lake City SW Marvin Burnett Lake City, Columbia County, Florida GSE Project No. 16251

Minor Components

Albany

- *Percent of map unit:* 6 percent
- *Landform:* Ridges on marine terraces
- Landform position (two-dimensional): Shoulder
- Landform position (three-dimensional): Interfluve, talf
- *Down-slope shape:* Convex
- Across-slope shape: Linear
- *Other vegetative classification:* Sandy soils on rises and knolls of mesic uplands (G138XA131FL), North Florida Flatwoods (R138XY004FL)
- *Hydric soil rating:* No

Troup

- *Percent of map unit:* 4 percent
- Landform: Ridges, knolls
- Landform position (two-dimensional): Summit
- Landform position (three-dimensional): Interfluve
- *Down-slope shape:* Convex
- Across-slope shape: Linear
- *Other vegetative classification:* Sandy soils on ridges and dunes of xeric uplands (G133AA111FL), Longleaf Pine-Turkey Oak Hills (R133AY002FL)
- *Hydric soil rating:* No

Chipley

- Percent of map unit: 3 percent
- *Landform:* Knolls on marine terraces, rises on marine terraces, flats on marine terraces
- Landform position (two-dimensional): Shoulder, footslope
- Landform position (three-dimensional): Interfluve
- *Down-slope shape:* Convex
- *Across-slope shape:* Linear
- *Other vegetative classification:* Sandy soils on rises and knolls of mesic uplands (G138XA131FL)
- *Hydric soil rating:* No

Alpin

- *Percent of map unit:* 2 percent
- *Landform:* Flatwoods on marine terraces, knolls on marine terraces, ridges on marine terraces
- Landform position (two-dimensional): Shoulder, backslope
- Landform position (three-dimensional): Interfluve
- *Down-slope shape:* Convex
- Across-slope shape: Linear
- *Other vegetative classification:* Sandy soils on ridges and dunes of xeric uplands (G138XA111FL), Sand Pine Scrub (R153AY001FL)
- *Hydric soil rating:* No

Ichetucknee fine sand, 5 to 8 percent slopes

Map Unit Setting

- *National map unit symbol:* vrt4
- *Elevation:* 330 to 660 feet
- Mean annual precipitation: 50 to 58 inches
- Mean annual air temperature: 64 to 72 degrees F
- *Frost-free period:* 258 to 288 days
- *Farmland classification:* Not prime farmland

Map Unit Composition

- Ichetucknee and similar soils: 80 percent
- *Minor components:* 20 percent
- *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Ichetucknee

Setting

- Landform: Hills on marine terraces, ridges on marine terraces
- Landform position (three-dimensional): Interfluve, side slope
- *Down-slope shape:* Convex
- *Across-slope shape:* Linear
- *Parent material:* Sandy and clayey marine deposits over limestone

Typical profile

- *A* 0 to 4 inches: fine sand
- E 4 to 7 inches: fine sand
- Bg 7 to 75 inches: clay
- 2*R* 75 to 79 inches: weathered bedrock

Properties and qualities

- *Slope:* 5 to 8 percent
- *Depth to restrictive feature:* 50 to 75 inches to lithic bedrock
- Drainage class: Somewhat poorly drained
- Runoff class: Negligible
- *Capacity of the most limiting layer to transmit water (Ksat):* Moderately low to moderately high (0.06 to 0.20 in/hr)
- Depth to water table: About 18 to 36 inches
- Frequency of flooding: None
- *Frequency of ponding:* None
- *Maximum salinity:* Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
- Sodium adsorption ratio, maximum: 4.0
- Available water supply, 0 to 60 inches: Moderate (about 8.4 inches)

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December 7. 2023

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Interpretive groups

- Land capability classification (irrigated): None specified
- *Land capability classification (nonirrigated):* 6e
- Hydrologic Soil Group: D
- *Forage suitability group:* Loamy and clayey soils on rises, knolls, and ridges of mesic uplands (G138XA322FL)
- *Other vegetative classification:* Loamy and clayey soils on rises, knolls, and ridges of mesic uplands (G138XA322FL)
- *Hydric soil rating:* No

Minor Components

Goldsboro

- Percent of map unit: 10 percent
- *Landform:* Knolls on marine terraces, ridges on marine terraces
- Landform position (three-dimensional): Interfluve
- *Down-slope shape:* Convex
- Across-slope shape: Linear
- *Other vegetative classification:* Loamy and clayey soils on flats and rises of mesic lowlands (G138XA331FL)
- *Hydric soil rating:* No

Ocilla

- *Percent of map unit:* 10 percent
- *Landform:* Rises on marine terraces
- Landform position (three-dimensional): Interfluve
- *Down-slope shape:* Convex
- Across-slope shape: Linear
- *Other vegetative classification:* Sandy over loamy soils on rises and knolls of mesic uplands (G138XA231FL)
- *Hydric soil rating:* No

Pelham fine sand, 0 to 2 percent slopes

Map Unit Setting

- *National map unit symbol:* 2tg56
- *Elevation:* 0 to 190 feet
- *Mean annual precipitation:* 48 to 63 inches
- Mean annual air temperature: 57 to 79 degrees F
- *Frost-free period:* 251 to 293 days
- *Farmland classification:* Not prime farmland

Map Unit Composition

- Pelham and similar soils: 75 percent
- *Minor components:* 25 percent
- *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Pelham

Setting

- Landform: Flatwoods
- Landform position (three-dimensional): Talf
- *Down-slope shape:* Linear
- Across-slope shape: Linear
- *Parent material:* Sandy and loamy marine deposits

Typical profile

- *A* 0 to 6 inches: fine sand
- Eg 6 to 26 inches: fine sand
- *Btg1 26 to 42 inches:* sandy clay loam
- Btg2 42 to 83 inches: sandy clay loam

Properties and qualities

- *Slope:* 0 to 2 percent
- Depth to restrictive feature: More than 80 inches
- Drainage class: Poorly drained
- Runoff class: High
- *Capacity of the most limiting layer to transmit water (Ksat):* Moderately high to high (0.20 to 5.95 in/hr)
- Depth to water table: About 6 to 12 inches
- Frequency of flooding: None
- *Frequency of ponding:* None
- *Maximum salinity:* Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
- *Sodium adsorption ratio, maximum:* 4.0
- Available water supply, 0 to 60 inches: Moderate (about 7.0 inches)

Interpretive groups

- Land capability classification (irrigated): None specified
- Land capability classification (nonirrigated): 3w
- *Hydrologic Soil Group:* B/D
- *Ecological site:* F153AY060NC Wet Loamy Flats and Depressions
- *Forage suitability group:* Sandy over loamy soils on flats of hydric or mesic lowlands (G153AA241FL)
- *Other vegetative classification:* Sandy over loamy soils on flats of hydric or mesic lowlands (G153AA241FL)
- *Hydric soil rating:* No

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Minor Components

Unnamed

- Percent of map unit: 13 percent
- *Landform:* Flatwoods
- Landform position (three-dimensional): Talf
- Down-slope shape: Linear
- Across-slope shape: Linear
- *Other vegetative classification:* Sandy over loamy soils on flats of hydric or mesic lowlands (G153AA241FL)
- *Hydric soil rating:* Yes

Albany

- *Percent of map unit:* 6 percent
- *Landform:* Flatwoods
- Landform position (three-dimensional): Talf
- *Microfeatures of landform position:* Rises
- *Down-slope shape:* Convex
- Across-slope shape: Convex
- Ecological site: F153AY040NC Moist Loamy Rises and Flats
- *Other vegetative classification:* Sandy soils on rises and knolls of mesic uplands (G153AA131FL)
- *Hydric soil rating:* No

Meggett

- Percent of map unit: 3 percent
- *Landform:* Flatwoods
- Landform position (three-dimensional): Talf
- Down-slope shape: Linear
- Across-slope shape: Linear
- *Ecological site:* F153AY090NC Flooded Mineral Soil Floodplains and Terraces
- *Other vegetative classification:* Loamy and clayey soils on flats of hydric or mesic lowlands (G153AA341FL)
- *Hydric soil rating:* Yes

Surrency

- *Percent of map unit:* 3 percent
- *Landform:* Drainageways, depressions
- Landform position (three-dimensional): Dip
- Down-slope shape: Linear, concave
- Across-slope shape: Convex, concave
- Ecological site: F153AY060NC Wet Loamy Flats and Depressions
- *Other vegetative classification:* Sandy over loamy soils on stream terraces, flood plains, or in depressions (G153AA245FL)
- *Hydric soil rating:* Yes

3.4 Laboratory Soil Analysis

Selected soil samples recovered from the soil borings were analyzed for the percent soil fines passing the No. 200 sieve, natural moisture content, Atterberg Limits, and hydraulic conductivity. Samples selected for laboratory testing were collected at depths ranging from near-surface to 15 feet bls. These tests were performed to confirm visual soil classification and evaluate their engineering properties. The complete laboratory report is provided in Section 5.3.

The laboratory tests indicate the tested soils consist sand with silt, silty sand, silty sand with clay, sand with clay, clayey sand, very clayey sand, and sandy clay. The tested sand with silt (SP-SM) contains approximately 11 percent soil fines passing the No. 200 sieve with a natural moisture content of about 8.7 percent. The tested silty sand, and silty sand with clay (SM, SM-SC) contains approximately 14 to 27 percent soil fines passing the No. 200 sieve with natural moisture contents of about 7.8 to 18 percent. The tested sand with clay (SP-SC) contains approximately 11 percent soil fines passing the No. 200 sieve with a natural moisture content of about 7.8 to 18 percent. The tested sand with clay (SP-SC) contains approximately 11 percent soil fines passing the No. 200 sieve with a natural moisture content of about 17 percent. The tested clayey sand (SC) contains approximately 30 percent soil fines passing the No. 200 sieve with a natural moisture content of about 13 percent. The tested very clayey sand (SC/CL) contains approximately 34 percent soil fines passing the No. 200 sieve with a natural moisture content of about 18 percent. The tested sandy clay (CL) contains approximately 56 to 62 percent soil fines passing the No. 200 sieve with natural moisture contents of about 17 to 23 percent.

Atterberg Limits tests indicate the tested sandy clay (CL) has Liquid Limit (LL) values of 35 and 41, Plastic Limit (PL) values of 15 to 18, and Plasticity Index (PI) values of 17 and 26. These values correspond to materials with low potential (LL < 50) to marginal potential (PI \leq 35) for expansive behavior³.

The constant head hydraulic conductivity test results indicate the near-surface silty sand (SM) has hydraulic conductivity values of 0.8 to 1.1 feet per day. The tested clayey sand (SC) has no flow. Tests were not conducted on the deeper very clayey sand due to the limitations of the test method on soils having moderate to high fines content, but these soils are expected to have permeability values at least one order of magnitude lower than the sandy soils.

³ U.S. Department of the Army USA, 1983, Foundations in Expansive Soils, TM 5-818-7, p. 4-1.

4.0 EVALUATION AND RECOMMENDATIONS

4.1 General

The following recommendations are made based upon our understanding of the proposed construction, a review of the attached soil borings and laboratory test data, and experience with similar projects and subsurface conditions. If plans or the location of proposed construction changes from those discussed previously, GSE requests the opportunity to review and possibly amend our recommendations with respect to those changes.

The final design of a foundation system is dependent upon adequate integration of geotechnical and structural engineering considerations. Consequently, GSE must review the final foundation design in order to evaluate the effectiveness and applicability of our initial analyses, and to determine if additional recommendations may be warranted. Without such a review, the recommendations presented herein could be misinterpreted or misapplied resulting in potentially unacceptable performance of the foundation system.

The performance of site improvements may be sensitive to their post-construction relationship to site groundwater levels, seepage zones, or soil/rock characteristics exposed at final site grades. GSE recommends that use of boring information for final design of all site improvements be predicated on proper horizontal and vertical control of borings.

In this section of the report, we present our geotechnical parameters and recommendations to assist with building foundation, stormwater management, and pavement designs as well as our general site preparation guidelines.

4.2 Groundwater

The groundwater table was encountered in the borings at depths of 6.1 to 8.8 feet bls at the time of our exploration. The Soil Survey indicates the groundwater table is typically at a depth of near-surface to 6 feet bls. We anticipate the seasonal high groundwater table will be near depths of 1 to 3.5 feet bls. Estimates for the seasonal high groundwater table are shown on the individual boring logs.

4.3 **Building Foundations**

The SPT borings located within the proposed building footprint indicate the soils across these areas are relatively consistent. SPT boring B-1 initially encountered 3 feet of sand with silt (SP-SM), and 4.5 feet of sandy clay (CL) overlying sand with clay, and poorly graded sand (SP-SC, SP) to a depth of 12 feet bls. This was underlain by clay (CL/CH) to the explored depth of 20 feet bls. SPT borings B-2 to B-5 encountered poorly graded sand, sand with silt, sand with clay, silty sand, and silty clayey sand (SP, SP-SM, SP-SC, SM-SC) with some interbedded layers of clayey to very clayey sand (SC, SC/CL) to depths of 13.5 to 17.5 feet bls. This was underlain by clay-rich (CL, CL/CH) soils to the explored depths of 20 feet bls.

Based upon the soil conditions encountered and our limited understanding of the structural loads and site grading, we recommend the building be supported by conventional, shallow strip and/or spread foundations. We recommend the shallow foundations be designed for a maximum allowable gross bearing pressure of 2,500 psf. The gross bearing pressure is defined as the soil contact pressure that can be imposed from the maximum structural loads, weight of the concrete foundations, and weight of the soil above the foundations. The foundations should be designed based upon the maximum load that could be imposed by all loading conditions.

The foundations should be embedded a minimum of 18 inches below the lowest adjacent grade. Interior foundations or thickened sections should be embedded a minimum of 12 inches. The foundations should have minimum widths of 18 inches for strip footings, and 24 inches for columns, even though the maximum soil bearing pressure may not be fully developed.

Due to the mostly sandy nature of the majority of the near-surface soils, we expect settlement to be mostly elastic in nature. The majority of the settlement will occur on application of the loads, during and immediately following construction. Using the recommended maximum bearing pressure, the assumed maximum structural loads, and the field and laboratory test data which we have correlated into the strength and compressibility characteristics of the subsurface soils, we estimate the total settlements of the structure to be 1 inch or less, with approximately half of it occurring upon load application (during construction).

Differential settlement results from differences in applied bearing pressures and the variations in the compressibility characteristics of the subsurface soils. For the building pad prepared as recommended, we anticipate differential settlement of less than 1/2 inch.

Post-construction settlement of the structures will be influenced by several interrelated factors, such as (1) subsurface stratification and strength/compressibility characteristics of the bearing soils; (2) footing size, bearing level, applied loads, and resulting bearing pressures beneath the foundation; (3) site preparation and earthwork construction techniques used by the contractor, and (4) external factors, including but not limited to vibration from off-site sources and groundwater fluctuations beyond those normally anticipated for the naturally-occurring site and soil conditions which are present.

Our settlement estimates for the structure are based upon our limited understanding of the structural loads and site grading and the use of successful adherence to the site preparation recommendations presented later in this report. Any deviation from our project understanding and/or our site preparation recommendations could result in an increase in the estimated post-construction settlement of the structure.

4.4 Flexible Pavement

Overall soil conditions encountered by our borings at this site are suitable for supporting conventional limerock base and asphalt wearing surface pavements. We have not been provided the anticipated traffic loading conditions; therefore, the following pavement component recommendations should be used only as guidelines. The below recommendations are intended to be minimums. Increasing base course and asphalt thicknesses would increase the design life of the pavement.

The seasonal high groundwater table is estimated to be approximately 12 inches to about 3.5 feet beneath existing grade across the site. We recommend a minimum of either 12 to 24 inches of separation (depending upon the pavement section design) be present between the bottom of the base course and the estimated seasonal high groundwater table. If this separation cannot be achieved by site grading, GSE recommends underdrains be used beneath the base course.

4.4.1 Stabilized Subgrade

If a crushed limerock or recycled concrete base is used, we recommend a stabilized subgrade be located beneath the base. The stabilized subgrade should have a minimum Limerock Bearing Ratio (LBR) of 40, with minimum thicknesses of 6 inches for automobile parking areas and 12 inches for driveways.

The stabilized subgrade can be imported material or a mixture of imported and on-site material. If a mix is proposed, a mix design should be performed to determine the optimum mix proportions. The stabilized subgrade should be compacted to a minimum of 98 percent of the Modified Proctor maximum dry density (ASTM D1557) for soils with less than 15 percent fines content. Soils with 15 percent or greater fines content should be compacted to 100 percent of the Standard Proctor maximum dry density (ASTM D698).

4.4.2 Base Course

The base course can consist of either crushed limerock, soil cement, or recycled concrete. If you should use a soil cement base course, a stabilized subgrade is not required.

Limerock should have an LBR of at least 100, be obtained from a FDOT approved source and meet FDOT gradation requirements. The base course thickness should be a minimum of 6 inches in automobile parking areas, and 8 inches in driveway areas. The base course should be compacted to at least 98 percent of the Modified Proctor maximum dry density (ASTM D1557). We recommend a minimum 24 inches separation between the bottom of the limerock base course and the estimated seasonal high-water table. If site grading does not allow for this separation, we recommend underdrains be considered.

Soil cement can consist of an imported material or a blend of the on-site soils and cement. A mix design should be performed to determine the optimum cement content. We recommend the soil cement have a minimum 28-day compressive strength of 500 psi. Soil cement can be blended off-site (in a pug mill) or on site. Soil cement pills should be cast from each day's production to verify the recommended compressive strength has been achieved at 28 days. We recommend the soil cement base course be a minimum of 8 inches thick throughout the project. We recommend a minimum 18 inches separation between the bottom of the soil cement base course and the estimated seasonal high-water table. If site grading does not allow for this separation, we recommend underdrains be considered.

Recycled concrete should have an LBR of at least 150, be obtained from a FDOT approved source and meet FDOT gradation requirements. The base course thickness should be a minimum of 8 inches. The base course should be compacted to at least 98 percent of the Modified Proctor maximum dry density (ASTM D1557). We recommend a minimum 12 inches separation between the bottom of the recycled concrete base course and the estimated seasonal high-water table. If site grading does not allow for this separation, we recommend underdrains be considered.

4.4.3 Wearing Surface

The asphalt-wearing surface should consist of an FDOT Type SP Hot Mix Asphalt mixture. For automobile parking areas, the thickness should be a minimum of 1.5 inches. For driveway areas, the thickness should be a minimum of 2 inches. The asphalt-wearing surface should consist of an SP-12.5 mix. The asphalt should be compacted to at least 95 percent of the mix design density.

The constructability of differing asphalt thicknesses may be difficult, and having a uniform 2-inch thick asphalt wearing surface may be more practical.

4.5 Rigid Pavement

Concrete pavement is a rigid pavement that results in smaller load transfers to the subgrade soils than flexible pavement. For concrete pavement subgrade, we recommend using the existing surficial sands or recommended clean sand (SP) fill, compacted to at least 98 percent of the Modified Proctor maximum dry density without additional stabilization with the following stipulations:

- 1. Subgrade soils must be compacted to at least 98 percent of Modified Proctor maximum dry density to a depth of at least 2 feet prior to placement of concrete.
- 2. The surface of the subgrade soils must be smooth and any disturbances or wheel rutting corrected prior to placement of the concrete.
- 3. The subgrade soils must be moistened prior to placement of concrete.
- 4. Concrete pavement thickness should be uniform throughout, with the exception of thickened edges (curb or footing).
- 5. The bottom of the pavement should be separated from the estimated seasonal high groundwater level by at least 18 inches.
- 6. Limerock or any other impermeable base is not suitable unless it meets the minimum recommended permeability of 10 ft/day.
- 7. The upper 12 inches of subgrade underlying the base course must also be "freedraining" and water that enters the base and subgrade must be allowed to seep out by gravity or if this is not possible, underdrains must be incorporated into the subgrade. A "bathtub" condition within the base/subgrade must be avoided.

Our recommendations for slab thickness for both light-duty and heavy-duty concrete pavements is based on a.) subgrade soils are compacted to 98 percent of the Modified Proctor maximum dry density, b.) modulus of subgrade reaction (k) of 200 pounds per cubic inch, c.) a 20-year design life, and d.) previously stated design parameters. For an anticipated light-duty traffic group, a minimum pavement thickness of 5.5 inches is recommended, using Table 2.4 from the ACI 330 Guide for Design and Construction of Concrete Parking Lots, ACI 330R-01. For an anticipated heavy-duty traffic group, a minimum pavement thickness of 8 inches is recommended, using Table 3.4 from the FDOT *Rigid Pavement Design Manual*, January 2019.

We recommend using concrete with a minimum 28-day compressive strength of 4,000 pounds per square inch and a minimum 28-day flexural strength (modulus of rupture) of at least 600 pounds per square inch based on the third point loading of concrete beam test samples. Maximum control joint spacing of 12.5 by 12.5 feet is suggested for light-duty concrete pavements. Maximum control joint spacing of 15 by 15 feet is suggested for heavy-duty concrete pavements. Layout of sawcut control joints should form square panels, and the depth of sawcut joint should be at least 1/4 of the concrete slab thickness. The joints should be sawed within six hours of concrete placement or as soon as the concrete has developed sufficient strength to support workers and equipment.

For further details on concrete pavement construction, refer to "Guide to Jointing Non-reinforced Concrete Pavements" published by the Florida Concrete and Products Associates, Inc. and "Building Quality Concrete Parking Areas", published by the Portland Cement Association.

4.6 Site Preparation

The soils at this site should be suitable for supporting the proposed construction using normal, good practice site preparation procedures. The following recommendations are our general guidelines for site preparation.

4.6.1 Stripping

Strip the construction limits and 10 feet beyond the perimeter of all grass, roots, topsoil, and other deleterious materials. You should expect to strip to depths of 12 or more inches. Deeper stripping will likely be necessary due to major root systems present at the site.

4.6.2 Dewatering

Temporary dewatering may be necessary for this project. If needed, we anticipate dewatering can be accomplished with sumps placed near the construction area, or with underdrains connected to a vacuum pump.

In any case, the site should always be graded to promote runoff and limit the amount of ponding. Localized ponding of stormwater is expected without proper grading during construction, and could render previously acceptable surfaces unacceptable.

4.6.3 **Proof-Rolling**

Proof-roll the subgrade with heavy rubber-tired equipment, such as a loaded front-end loader or dump truck, to identify any loose or soft zones not found by the soil borings. The proof-rolling should be monitored by a geotechnical engineer or qualified technician. Undercut or otherwise treat these zones as recommended by the geotechnical engineer in this report.

4.6.4 **Proof Compaction**

Compact the subgrade to a density of at least 95 percent of the Modified Proctor maximum dry density (ASTM D1557). The specified compaction should be obtained to a depth of 1 foot below the foundation bottoms and the existing grade prior to placing fill. Vibratory roller equipment should not be used within approximately 100 feet of existing structures. Lighter "walk-behind" compaction equipment may be used to achieve the degree of compaction.

Should clayey sand be encountered at the bearing surface, this material should be probed and visually confirmed to be unyielding in the upper 12 inches in lieu of density testing. If the foundation excavations penetrate the clayey sand, the excavation should be performed in a manner that reduces soil disturbance. Clayey sand soils (with fines content in excess of 15 percent) that are removed and replaced or appreciably disturbed need to be re-compacted to 98 percent of the Standard Proctor maximum dry density (ASTM D698).

4.6.5 Fill Placement

Imported fill placed to raise the site grades should consist of clean sand having less than 10 percent passing the No. 200 sieve. On-site soils meeting the requirements of Section 4.9 may also be used as structural fill. The fill should be placed in maximum 12-inch loose lifts that are compacted to at least 95 percent of the Modified Proctor maximum dry density (ASTM D1557). If lighter "walk-behind" compaction equipment is used, this may require lifts of 4 inches or less to achieve the required degree of compaction.

4.7 Quality Control and Construction Materials Testing

It should be noted that the geotechnical engineering design does not end with the advertisement of the construction documents. As the geotechnical engineer of record, GSE is the most qualified to perform the construction materials testing that will be required for this project. The benefits of having the geotechnical engineer of record also perform the construction materials testing are numerous. If GSE continues to be involved with the project through construction, we will be able to constantly re-evaluate and possibly alter our geotechnical recommendations in a timely and cost effective manner once final design and construction techniques are developed. This often results in cost savings for the project.

We recommend performing compaction testing beneath the concrete floor slab and the building foundations. We recommend one test be performed every 50 linear feet of continuous footing and every other column footing, per foot depth of fill or native material. We recommend a compaction test be performed for each 2,500 square feet of floor area or 10,000 square feet of pavement area per foot of fill or native material, or a minimum of three tests each, whichever is greater. Test all footing excavations to a depth of 12 inches at the frequencies stated above.

4.8 Stormwater Management

The auger borings located within the stormwater management facility encountered relatively consistent soil conditions. Auger boring P-1 encountered 6 feet of silty sand, and poorly graded sand (SM, SP) overlying clayey to very clayey sand, and clay with sand (SC, SC/CL, CL/CH) to the explored depth of 15 feet bls. Auger borings P-2 to P-4 initially encountered poorly graded sand, sand with silt, and silty sand (SP, SP-SM, SM) to depths of 2 to 5 feet bls, overlying silty clayey sand, and clayey to very clayey sand (SM-SC, SC, SC/CL) to depths of 7 to 10.5 feet bls. This was underlain by sand with silt (SP-SM) to depths of 12 to 13.5 feet bls, followed by clayrich soils (CL/CH) to the explored depth of 15 feet of sand with silt (SP-SM) overlying clay with sand (CL/CH) to a depth of 12.5 feet bls. This was underlain by sand with silt (SP-SM) to the explored depth of 15 feet bls. Silt (SP-SM) to the explored depth of 15 feet bls. Auger boring P-5 initially encountered 5.5 feet of clayey sand (SC) and 5 feet of sand with silt (SP-SM) overlying clay with sand (CL/CH) to a depth of 12.5 feet bls. This was underlain by sand with silt (SP-SM) to the explored depth of 15 feet bls.

The water table was encountered in the auger borings at depths of 7.5 to 8.8 feet bls at the time of our exploration. We anticipate the seasonal high groundwater table to be at depths of 1 to 2.5 feet bls.

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The laboratory permeability tests indicate the surficial layers of silty sand (SM) has hydraulic conductivity values of 0.8 to 1.1 feet per day, and clayey sand (SC) has no flow. The deeper very clayey sand encountered below the surficial sandy soils is friable and will have permeability values at least one order of magnitude lower than the sandy soils. The underlying dense soils and clayrich soils are expected to be confining soils.

Mr. Cole Menhennett with CHW confirmed the proposed stormwater management facility as a dry pond via email. We understand that the current design will consider underdrains. We understand that imported clean sand will be used for the backfill for the underdrains. This revision includes soil parameters considering and underdrain design with clean sand backfill.

Based upon our findings and test results, our recommended soil parameters for the stormwater management design in the explored areas are presented below. The recommended parameters consider the results of the permeability tests, wash 200 determinations, and our experience with these types of soils. The parameters below do not consider a factor of safety.

Proposed Stormwater Management Facility

- 1. Base elevation of effective or mobilized aquifer (average depth of confining layer) equal to 8 feet bls.
- 2. Unsaturated vertical infiltration rate of 10 foot per day.
- 3. Horizontal hydraulic conductivity equal to 10 feet per day.
- 4. Specific yield (fillable porosity) of 20 percent.
- 5. Average seasonal high groundwater table depth equal to 2 feet bls.
- 6. Average seasonal low groundwater table depth equal to 6 feet bls.

In areas where clay-rich soils are present at the basin bottom, we recommend these soils be undercut a minimum of 2 feet and backfilled with the on-site sands and sands with silt (SP, SP-SM) having a maximum of 12 percent soil fines passing the No. 200 sieve. This fill should also be used above the bottom of the underdrains. The intent of this undercutting and replacement is to provide a more uniform sand "blanket" at the basin bottom that allows the migration of water to the underdrains. This sand blanket will also reduce the potential for clay-fines leaching out of the soils when water is present in the basin that can result in a thin layer of confining type material on the basin bottom that can reduce the effectiveness of the basin.

4.9 Fill Suitability

The soils encountered at this site within the explored depths range from sands (SP) to clays (CL/CH). A discussion of the suitability for reuse as structural fill for each soil classification according to the Unified Soil Classification System (USCS) designation is provided below.

SP, SP/SM – Sands (SP) and sand with silt (SP/SM) have less than 5 percent and 12 percent soil fines passing the No. 200 sieve, respectively, and are typically well draining soils that are suitable for reuse as structural fill. The sands with silt may require moisture conditioning (drying) to make the material more workable. These soils will require stockpiling and drying before they are reused if they are excavated from below the water table.

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SM – Silty sands (SM) can have between 12 percent and 50 percent soil fines passing the No. 200 sieve. Silty sands are typically non-plastic or have low plasticity, and can be reused as structural fill with precautions. Silty sands can be moisture sensitive and difficult to work and compact and can rut if the moisture content is near or above the optimum moisture content. We recommend these soils be moisture content. Aerating and exposure to the sun is typically the most effective methods of drying these soils. It may not be practical to reuse these materials during the wet season, as frequent rain showers may not allow these soils to dry to a workable moisture content. Suitable silty sands are limited to soil having less than 30 percent soil fines passing the No. 200 sieve. Silty sands with more than 30 percent soil fines are especially moisture sensitive, and are not recommended for reuse as structural fill. These soils will behave more as sandy silt, and for this reason, very silty sands having more than 30 percent soil fines passing the No. 200 sieve have been assigned a dual classification of SM/ML. Silty sand soils that are excavated from below the water table are not recommended for reuse as structural fill due to the amount of time that will be required to dry these soils to a workable condition.

SC - Clayey sand (SC) soils can have between 12 percent and 50 percent soil fines passing the No. 200 sieve. Clayey sands can have a high range of plasticity, varying from a PI of 7 or greater and plotting above the A-line to highly plastic. Friable clayey sands are typically suitable for use as structural fill with precautions. Clayey sands will be moisture sensitive and difficult to work and compact and can rut during placement if the moisture content is near or above the natural moisture content. We recommend these soils be moisture conditioned (dried) so that the moisture content during use is at or below the optimum moisture content. Aerating and exposure to the sun is typically the most effective methods of drying these soils. It may not be practical to reuse these materials during the wet season, as frequent rain showers may not allow these soils to dry to a workable moisture content. Suitable clayey sands are limited to soil having less than 30 percent soil fines passing the No. 200 sieve. Clayey sands with more than 30 percent soil fines passing the No. 200 sieve are especially moisture sensitive and are typically highly plastic, and are not recommended for reuse as structural fill. These soils will behave more as sandy clay, and for this reason, very clayey sands having more than 30 percent soil fines passing the No. 200 sieve have been assigned a dual classification of SC/CH or SC/CL. Clayey sand soils that are excavated from below the water table are not recommended for reuse as structural fill due to the amount of time that will be required to dry these soils to a workable condition.

ML, MH, CL, CH – Silts and clays are not suitable materials for reuse as structural fill.

When using on-site soils as fill materials, we recommend the silty and clayey sand soils (SM, SC) be used in the lower depths of the fill. Sand and sand with silt (SP, SP-SM) should be used in the upper portions of the fill. We recommend a minimum of 2 feet of sand (SP, SP-SM) cover the silty and clayey sand fill materials to reduce the potential for soggy surface conditions due to the low permeability characteristics of the silty and clayey sand materials.

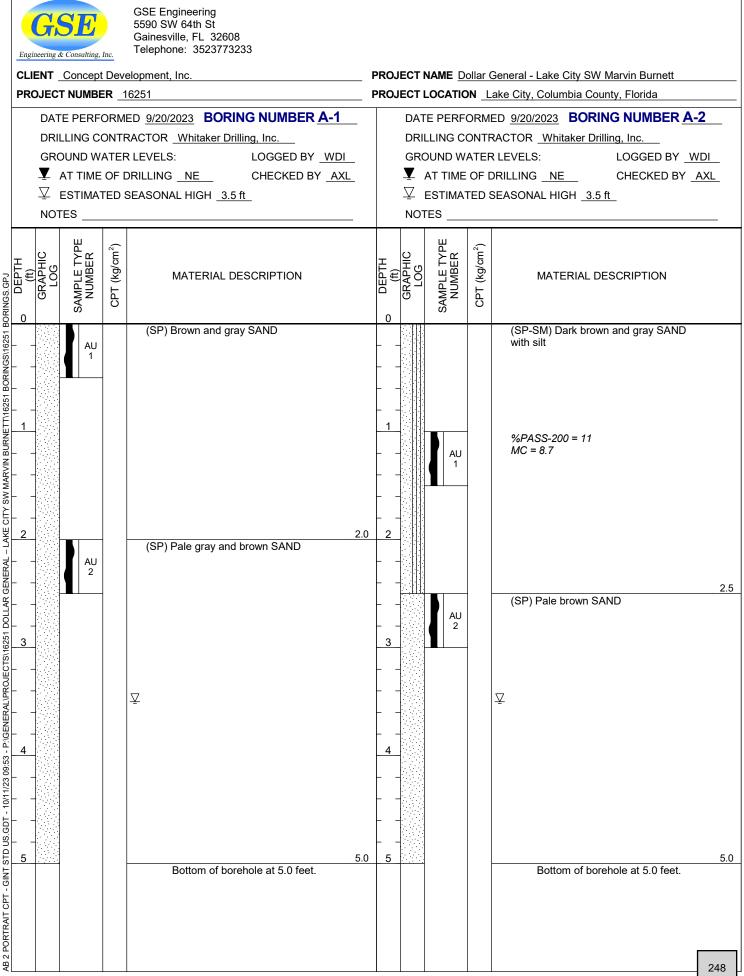
4.10 Surface Water Control and Landscaping

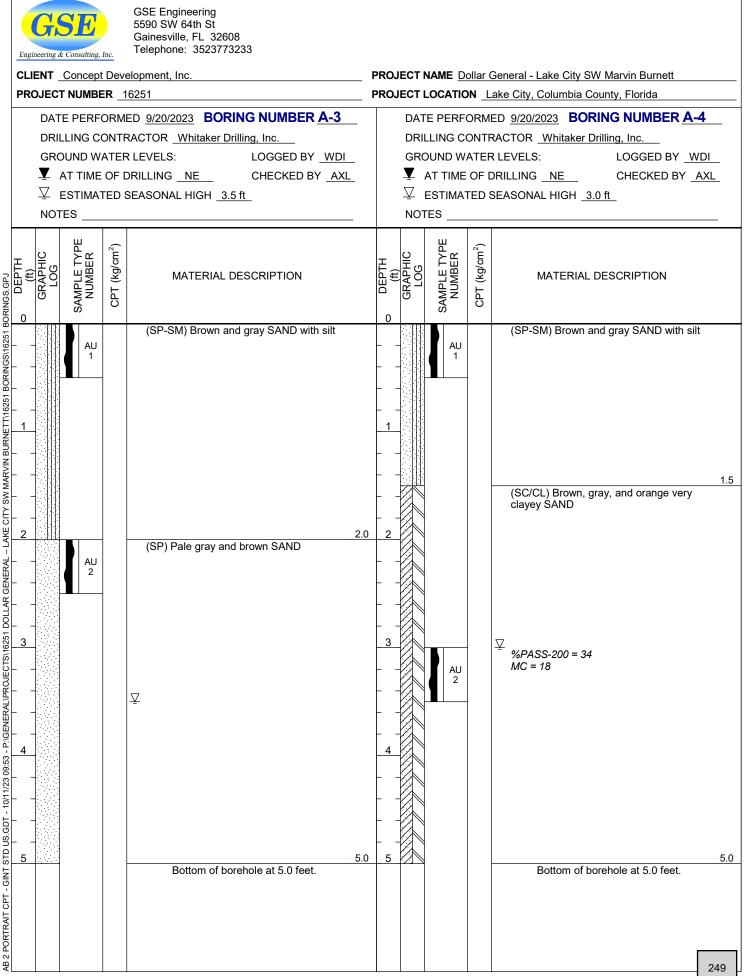
Roof gutters should be considered to divert runoff away from the building. The gutter downspouts should discharge a minimum of 10 feet from the structure to reduce the amount of water collecting around the foundations. Where possible, the gutter downspouts should discharge directly into the storm sewer system or onto the asphalt paved areas in order to reduce the amount of water collecting around the foundations. Grading of the site should be such that water is diverted away from the building on all sides to reduce the potential for erosion and water infiltration along the foundation.

With respect to landscaping, it is recommended that any trees and large "tree-like" shrubbery with potential for developing large root systems be planted a minimum distance of half their mature height, and preferably their expected final height, away from the structure. The purpose of this is to reduce the potential for foundation or slab movements from the growth of root systems as the landscaping matures.

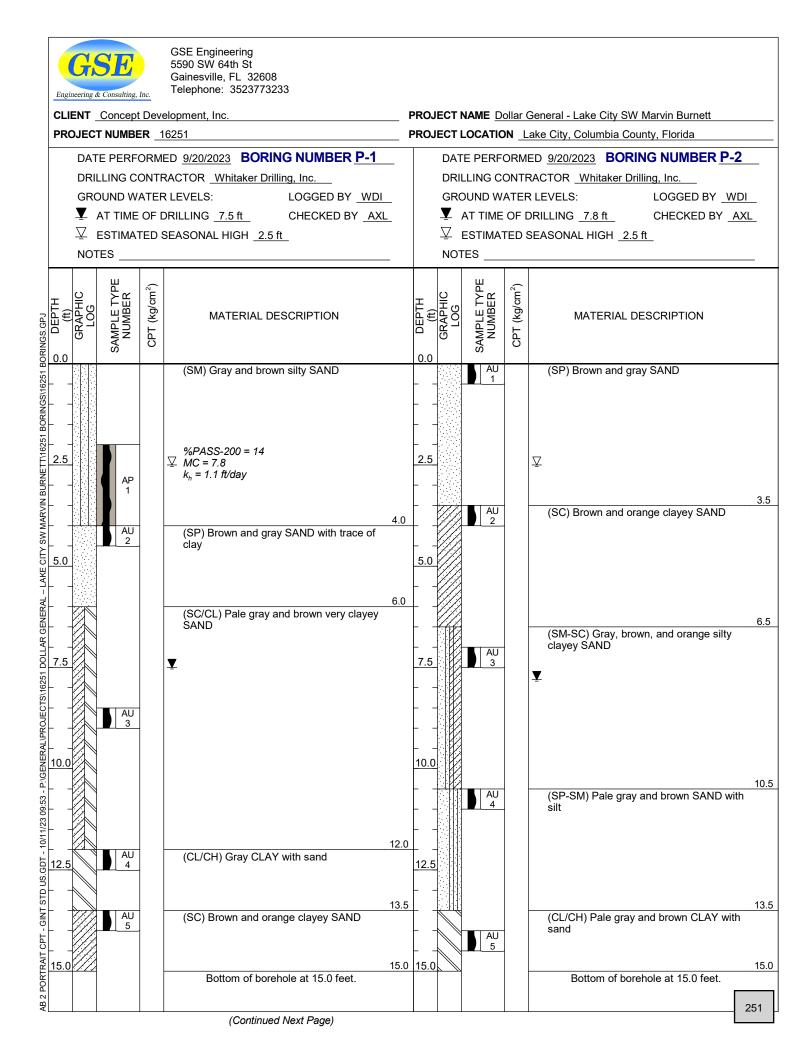
5.0 FIELD DATA

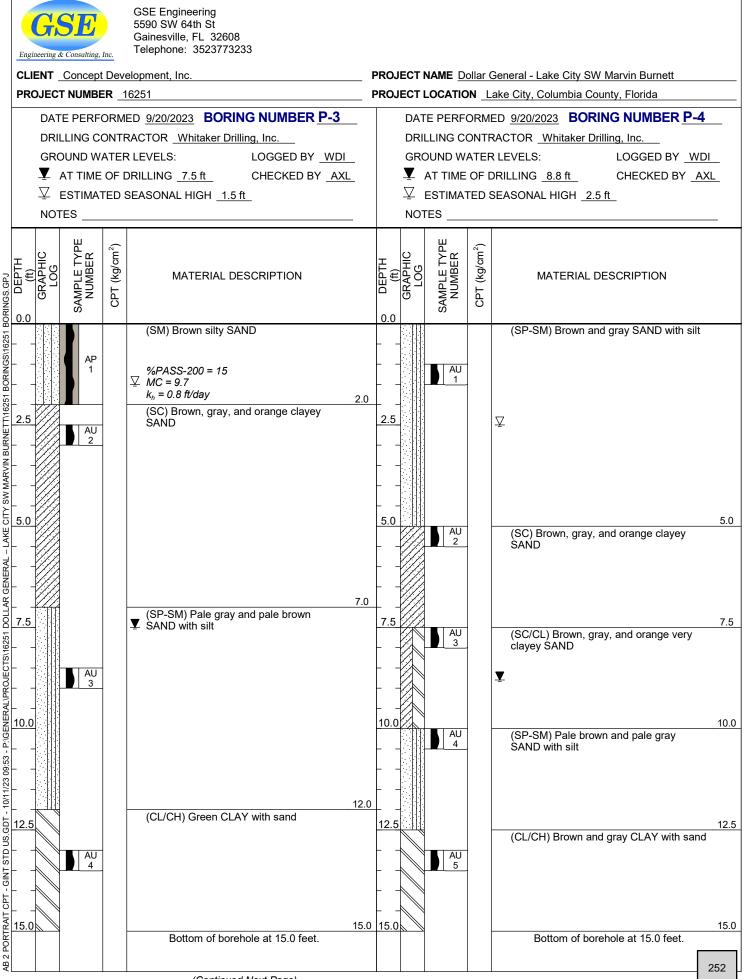
5.1 Auger Boring Logs



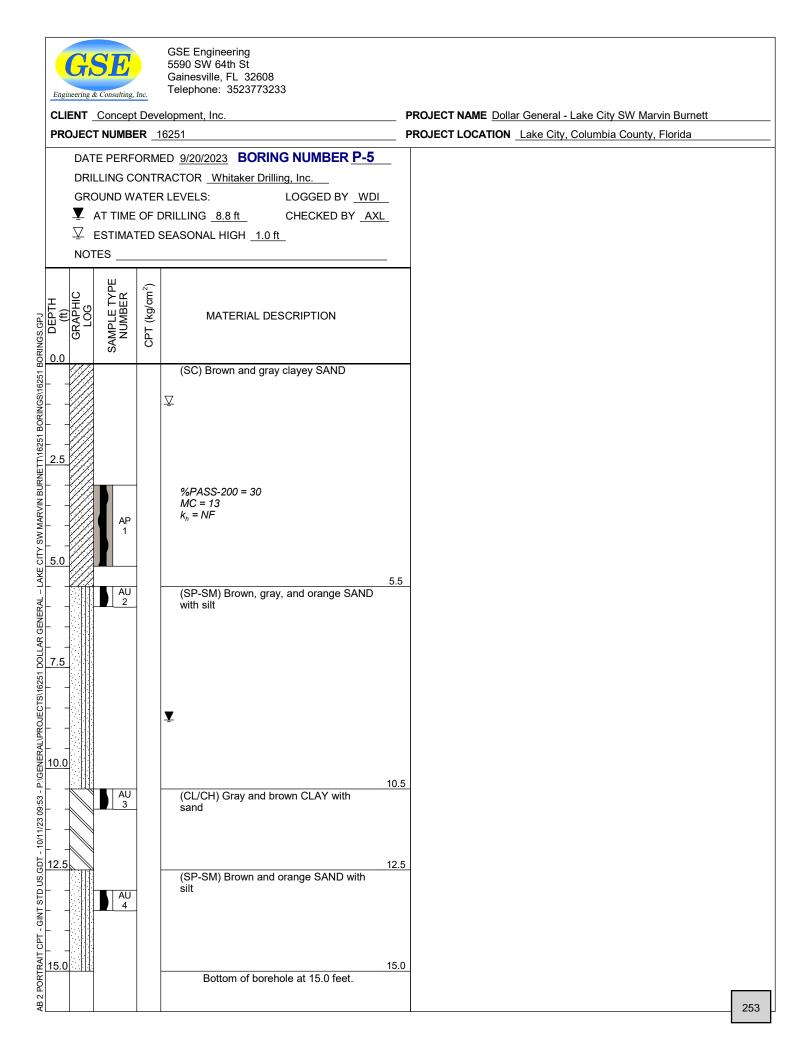


	G	SE		GSE Engineering 5590 SW 64th St Gainesville, FL 32608		
		ng & Consulting,		Telephone: 3523773233		
					PROJECT NAME Dollar General - Lake City SW Marvin Burnett PROJECT LOCATION Lake City, Columbia County, Florida	
	DATE PERFORMED <u>9/20/2023</u> BORING NUMBER <u>A-5</u>			ED <u>9/20/2023</u> BORING NUMBER <u>A-5</u>		
				RACTOR <u>Whitaker Drilling, Inc.</u>		
				R LEVELS: LOGGED BY WDI DRILLING NE CHECKED BY AXL		
				SEASONAL HIGH <u>3.0 ft</u>		
	N	OTES				
	(ft) GRAPHIC	LOG SAMPLE TYPE NUMBER	CPT (kg/cm ²)	MATERIAL DESCRIPTION		
SS/16251 BC	-	AU 1		(SP-SM) Brown and gray SAND with silt		
251 BORING	-					
	-					
	-					
V MARV	-					
2 AKE	_					
GENERAL -	-					
	-					
S/1625	_			$\bar{\Sigma}$		
	-					
RAL/PR				3.3 (SC) Brown and gray clayey SAND	5	
- GENE		AU 2				
4 4 6:53 - E						
11/23 0						
DT - 10						
				5.0 Bottom of borehole at 5.0 feet.		
CPT - C						
AB 2 PORTRAIT CPT - GINT STD US.GDT - 10/11/23 09:53 - P:/GENERALI/PROJECTS/16251 DOLLAR						
3 2 POF						_
¥						250



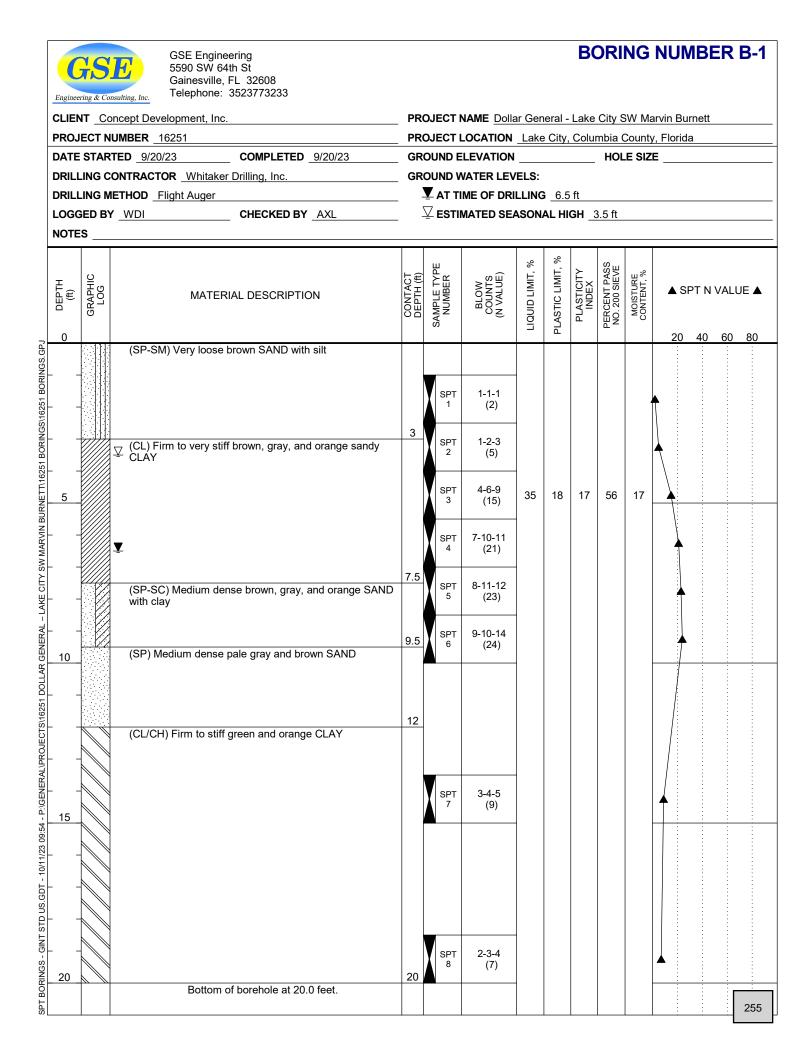


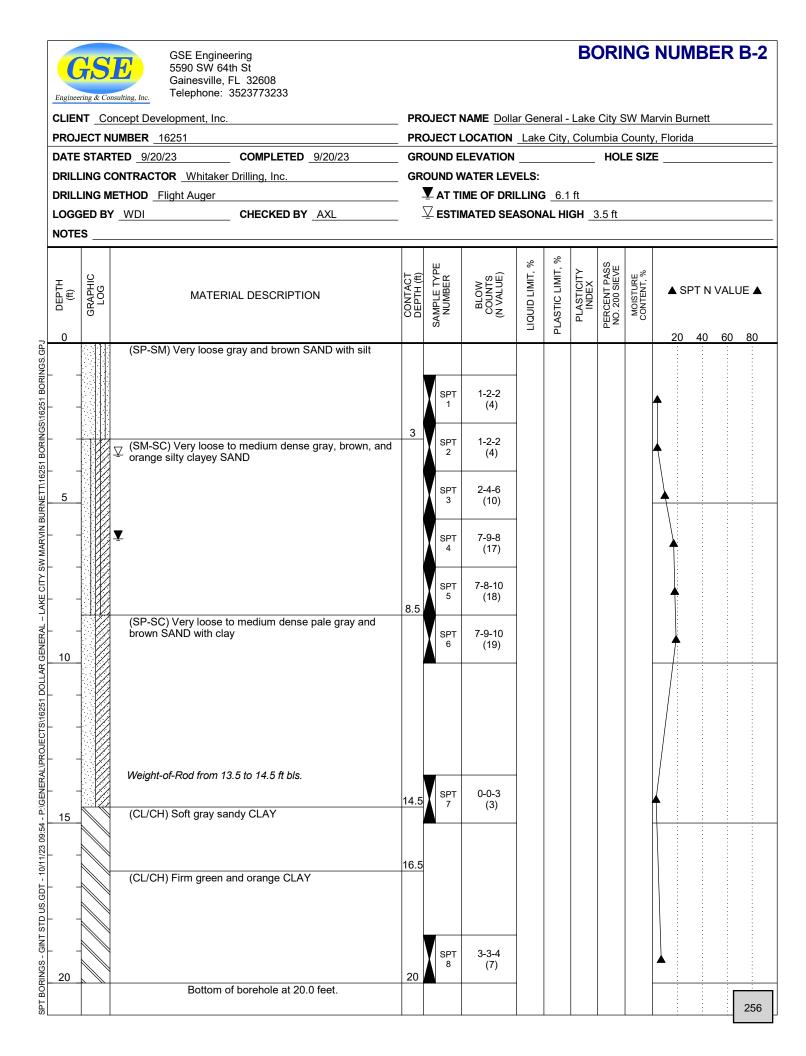
(Continued Next Page)



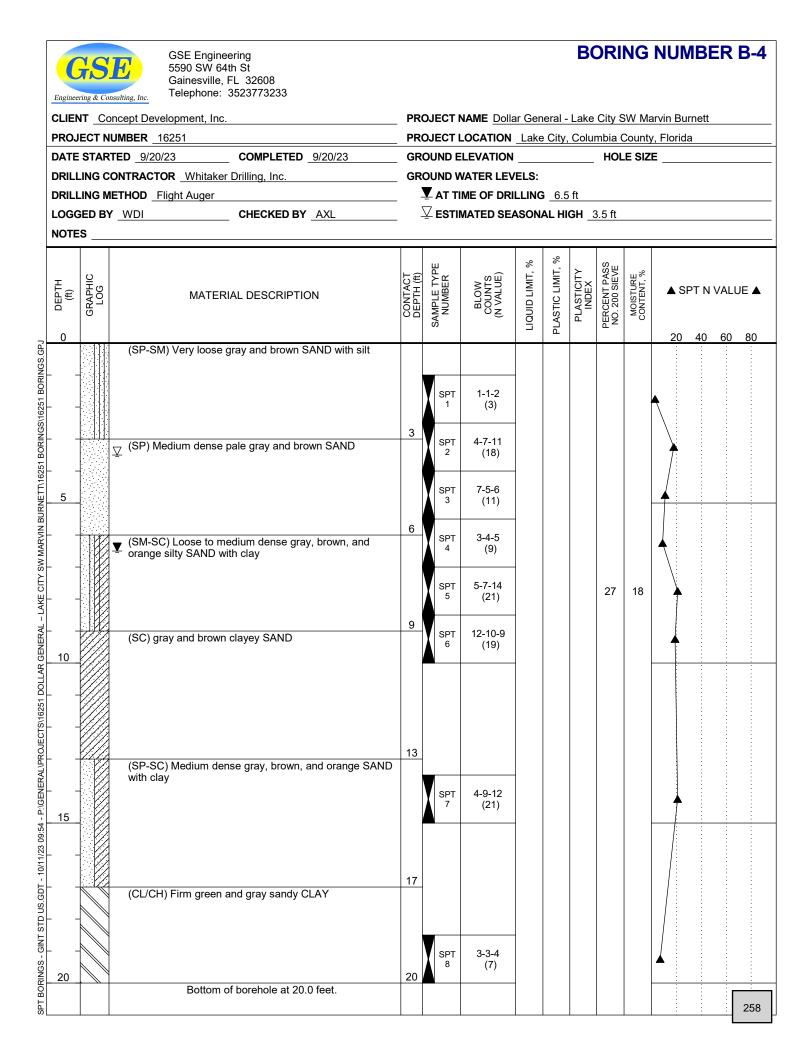
Summary Report of a Geotechnical Site Exploration – Revision 1 Dollar General – Lake City SW Marvin Burnett Lake City, Columbia County, Florida GSE Project No. 16251

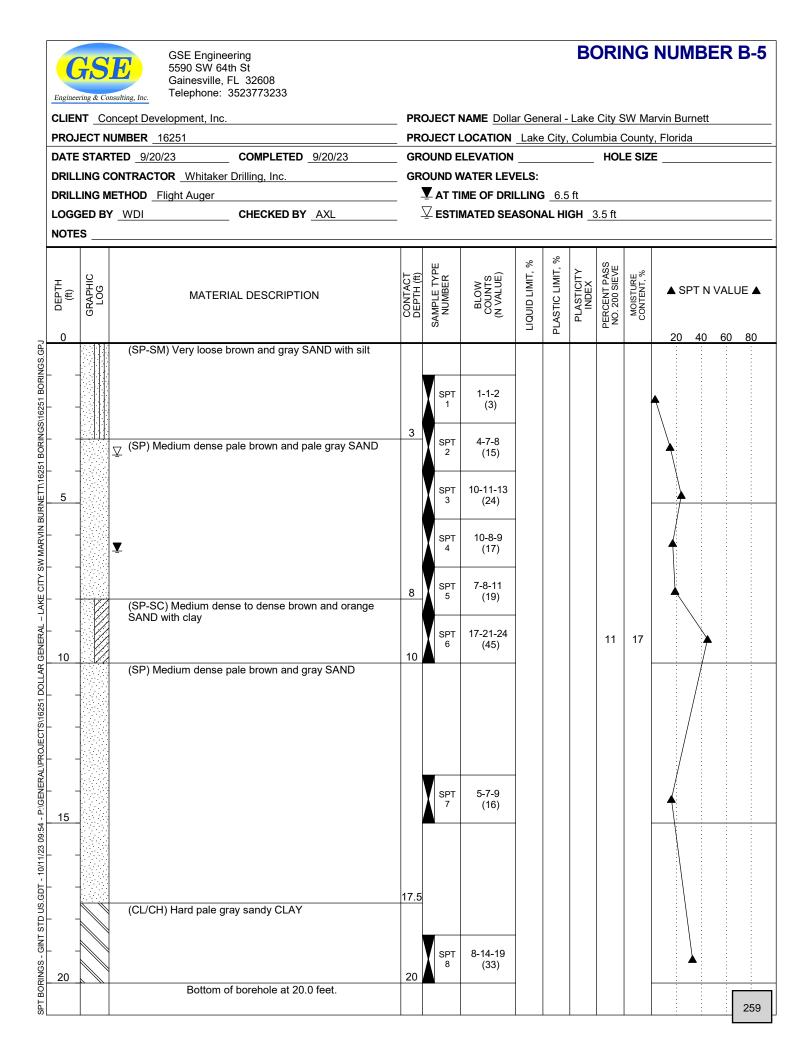
5.2 Standard Penetration Test Soil Boring Logs





Enginee		Gainesville, FL 32608 <u>sulting, Inc.</u> Telephone: 3523773233						_			NUMBER B-
		ncept Development, Inc.									
		ED 9/20/23 COMPLETED 9/20/23							HOL	LE SIZ	.E
		DNTRACTOR Whitaker Drilling, Inc.					61	ft			
								<u> </u>			
0 UETIN (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	CONTACT DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX	PERCENT PASS NO. 200 SIEVE	MOISTURE CONTENT, %	▲ SPT N VALUE ▲ 20 40 60 80
		(SP-SM) Very loose gray and brown SAND with silt									
-			2.5	SPT 1	1-1-1 (2)						
-		(SP) Loose pale gray SAND ⊈		SPT 2	1-2-4 (6)						
5		(SP-SC) Loose to gray and brown SAND with clay	4.5	SPT 3	2-4-5 (9)						
-		(SC/CL) Medium dense to dense gray, brown, and orange very clayey SAND	6	SPT 4	6-2-9 (11)						
-				SPT 5	7-9-11 (20)	-					
-				SPT 6	14-16-22 (38)	-					
-											
-		(CL) Firm gray sandy CLAY	13.5	SPT	2-3-3	-					
5				7	2-3-3 (6)	41	15	26	62	23	
-		(CL/CH) Green and orange CLAY	16								
- - 20			20								
		Bottom of borehole at 20.0 feet.									
											25





5.3 Laboratory Results

SUMMARY REPORT OF LABORATORY TEST RESULTS



GSE Engineering & Consulting, Inc.

Project Number: 16251

Project Name:

Dollar General - Lake City SW Marvin Burnett

Boring Number	Depth (ft)	Soil Description	Natural Moisture Content (%)	Liquid Limit	Plastic Limit	Plasticity Index	Percent Passing No. 200 Sieve	Organic Content (%)	Hydraulic Conductivity (ft/day)	Unified Soil Classification
A-2	1-1.5	Dark brown and gray SAND with silt	8.7				11			SP-SM
A-4	3-3.5	Brown, gray, and orange very clayey SAND	18				34			SC/CL
B-1	4-5.5	Brown, gray, and orange sandy CLAY	17	35	18	17	56			CL
B-3	13.5-15	Gray sandy CLAY	23	41	15	26	62			CL
B-4	7-8.5	Gray, brown, and orange silty SAND with clay	18				27			SM-SC
B-5	8.5-10	Pale brown and gray SAND with clay	17				11			SP-SC
P-1	2-4	Gray and brown silty SAND	7.8				14		1.1	SM
P-3	0-2	Brown silty SAND	9.7				15		0.8	SM
P-5	3-5	Brown and gray clayey SAND	13				30		NF	SC

5.4 Key to Soil Classification

Critaria fo	or Assigning Group Symbol	s and Group Names U	sing Laboratory Tests	SYM	BOLS	GROUP NAME
Cinteria io	I Assigning Group Symbol	s and Group Names Os	sing Laboratory Tests	GRAPHIC	LETTER	GROUP NAME
COARSE-GRAINED SOILS	Gravels	Clean Gravels	$Cu \ge 4$ and $1 \le Cc \le 3$		GW	Well graded GRAVEL
More than 50% retained	More than 50% of coarse	Less than 5% fines	Cu < 4 and/or 1 > Cc > 3	10000	GP	Poorly graded GRAVE
on No. 200 sieve	fraction retained on No. 4 sieve	Gravels with fines	Fines classify as ML or MH		GM	Silty GRAVEL
	sieve	More than 12% fines	Fines classify as CL or CH		GC	Clayey GRAVEL
	Sands	Clean Sands	$Cu \geq 6 \text{ and } 1 \leq Cc \leq 3$		SW	Well graded SAND
	50% or more of coarse	Less than 5% fines	Cu < 6 and/or 1 > Cc > 3		SP	Poorly graded SAND
	fraction passes No. 4 sieve	Sand with fines	Fines classify as ML or MH		SP-SM	SAND with silt
		$5\% \le \text{fines} < 12\%$	Fines classify as CL or CH		SP-SC	SAND with clay
		Sand with fines	Fines classify as ML or MH		SM	Silty SAND
		$12\% \le \text{fines} < 30\%$	Fines classify as CL or CH		SC	Clayey SAND
		Sand with fines	Fines classify as ML or MH		SM	Very silty SAND
		30% fines or more	Fines classify as CL or CH		SC	Very clayey SAND
FINE-GRAINED SOILS	Clays	inorganic	$50\% \le \text{fines} < 70\%$			Sandy CLAY
50% or more passes the	,	C	$70\% \le \text{fines} < 85\%$		CL/CH	CLAY with sand
No. 200 sieve			fines $\geq 85\%$		CL/CH	CLAY
	Silts and Clays	inorganic	PI > 7 and plots on/above "A" line		CL	Lean CLAY
	Liquid Limit less than 50	6.	PI < 4 or plots below "A" line		ML	SILT
	Enquite Ennie ress than 50	organic	Liquid Limit - oven dried			Organic clay
		organie	< 0.75 Liquid Limit - not dried		OL	Organic silt
	Silts and Clays	inorganic	PI plots on or above "A" line		СН	Fat CLAY
	Liquid Limit 50 or more	morganie	PI plots below "A" line		МН	Elastic SILT
	Equilit Emilit 50 of more	organic	Liquid Limit - oven dried		14111	Organic clay
		organie	< 0.75 Liquid Limit - not dried		ОН	Organic silt
HIGHLY ORGANIC SOILS	Drimoril	y organic matter, dark in	*	<u></u>	РТ	PEAT
No. OF BL	LOWS, N REI	LATIVE DENSITY	No	. OF BLOW	S, N CO	NSISTENCY
0 -	4	Very Loose		0 - 2		Very Soft
5 - 3	10	Loose	SILTS	3 - 4		Soft
SANDS: 11 -	30	Medium dense				
31 -	F 0	inearann aense	&	5 - 8		Firm
	50	Dense	& CLAYS:	9 - 15		Stiff
OVEI				9 - 15 16 - 30		Stiff Very Stiff
	R 50	Dense Very Dense		9 - 15 16 - 30 31 - 50		Stiff Very Stiff Hard
No. OF BL	R 50 OWS, N RELA	Dense Very Dense ATIVE DENSITY		9 - 15 16 - 30		Stiff Very Stiff
No. OF BL 0 -	R 50 OWS, N RELA 8	Dense Very Dense ATIVE DENSITY Very Soft	CLAYS:	9 - 15 16 - 30 31 - 50 OVER 50	,	Stiff Very Stiff Hard Very Hard
No. OF BL 0 - 9 - 1	R 50 OWS, N RELA 8 18	Dense Very Dense ATIVE DENSITY Very Soft Soft		9 - 15 16 - 30 31 - 50 OVER 50	,	Stiff Very Stiff Hard Very Hard
No. OF BL 0 - 9 - 1 LIMESTONE: 19 -	R 50 OWS, N RELA 8 18 32 N	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard	CLAYS: <u>SAMPLE GI</u> Location	9 - 15 16 - 30 31 - 50 OVER 50	YPE LEG	Stiff Very Stiff Hard Very Hard E ND Location
No. OF BL 0 - 9 - 1 LIMESTONE: 19 - 33 -	R 50 OWS, N RELA 8 18 32 N 50	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard	CLAYS: <u>Sample G</u>	9 - 15 16 - 30 31 - 50 OVER 50	YPE LEG	Stiff Very Stiff Hard Very Hard END AU Location of Auge
No. OF BL 0 - 9 - 1 LIMESTONE: 19 -	R 50 OWS, N RELA 8 18 32 N 50	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard	CLAYS: <u>SAMPLE GI</u> Location	9 - 15 16 - 30 31 - 50 OVER 50	YPE LEG	Stiff Very Stiff Hard Very Hard END AU 1 Location of Auge
No. OF BL 0 - 9 - 1 LIMESTONE: 19 - 33 - OVER	R 50 OWS, N RELA 8 18 32 N 50 R 50	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard	CLAYS: SAMPLE GI Location of SPT 1	9 - 15 16 - 30 31 - 50 OVER 50	YPE LEG	Stiff Very Stiff Hard Very Hard END AU 1
No. OF BL 0 - 9 - 1 LIMESTONE: 19 - 33 - OVER	R 50 OWS, N RELA 8 18 32 N 50	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard	CLAYS: SAMPLE GI Location of SPT Sample	9 - 15 16 - 30 31 - 50 OVER 50	YPE LEGI	Stiff Very Stiff Hard Very Hard END AU 1 Location of Auge Sample
No. OF BL 0 - 9 - 1 LIMESTONE: 19 - 33 - OVEI <u>PARTICLE</u>	R 50 OWS, N RELA 8 18 32 N 50 R 50	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard	CLAYS: SAMPLE GI Location of SPT Sample	9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY	YPE LEGI	Stiff Very Stiff Hard Very Hard END AU 1 Location of Auge Sample
No. OF BL 0 - 9 - 1 LIMESTONE: 19 - 33 - OVER	R 50 OWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATIO	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON	CLAYS: SAMPLE GI Location of SPT Sample	9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY	YPE LEGI	Stiff Very Stiff Hard Very Hard END AU 1 Location of Auge Sample
No. OF BL 0 - 9 - 1 LIMESTONE: 19 - 33 - 33 - OVEH <u>PARTICLE</u> BOULDERS:	R 50 OWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATIO Greater than 30 75 mm to 300	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON	CLAYS: SAMPLE GI Location of SPT Sample LABORAT	9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY	YPE LEGI	Stiff Very Stiff Hard Very Hard END AU 1 Location of Auge Sample D
No. OF BL 0 - 9 - 1 LIMESTONE: 19 - 33 - OVEI <u>PARTICLE</u> BOULDERS: COBBLES:	R 50 OWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATIO Greater than 30 75 mm to 300 - 19.0 mm to 75	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON 00 mm 0 mm 5 mm	CLAYS: SAMPLE GI Location of SPT Sample LABORAT LL =	9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY FORY TES	YPE LEGI	Stiff Very Stiff Hard Very Hard END AU 1 Location of Auge Sample D 4, %
No. OF BL 0 - 9 - 1 LIMESTONE: 19 - 33 - OVEH <u>PARTICLE</u> BOULDERS: COBBLES: GRAVEL: Coarse Fine	R 50 OWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATIO Greater than 30 75 mm to 300 - 19.0 mm to 75 - 4.75 mm to 19	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON 00 mm 0 mm 5 mm 5 mm	CLAYS: SAMPLE GI Location of SPT Sample LABORAT LL = PL =	9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY TORY TES Li Plan	YPE LEGI T LEGEN quid Limit astic Limit sticity Inde	Stiff Very Stiff Hard Very Hard END AU 1 Location of Auge Sample D ., % ., %
No. OF BL 0 - 9 - 1 LIMESTONE: 19 - 33 - OVEH <u>PARTICLE</u> BOULDERS: COBBLES: GRAVEL: Coarse Fine	R 50 OWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATIO Greater than 30 75 mm to 300 - 19.0 mm to 75 - 4.75 mm to 19 - 2.00 mm to 4.7	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON 00 mm 5 mm 5 mm .0 mm 75 mm	CLAYS: SAMPLE GI Location of SPT Sample LABORAT LL = PL = PL = PI =	9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY ECORY TES Li Pla Pla: Percent Pas	YPE LEGI T LEGEN quid Limit astic Limit sticity Inde	Stiff Very Stiff Hard Very Hard END AU 1 Location of Auge Sample D , % , % , % , % , %
No. OF BL 0 - 9 - 1 LIMESTONE: 19 - 33 - OVER PARTICLE BOULDERS: COBBLES: GRAVEL: Coarse Fine SANDS: Coarse	R 50 OWS, N RELA 8 18 32 N 50 R 50 SIZE IDENTIFICATIO Greater than 30 75 mm to 300 - 19.0 mm to 7: - 4.75 mm to 19 - 2.00 mm to 4.7 - 0.425 mm to 2.	Dense Very Dense ATIVE DENSITY Very Soft Soft Moderately Hard Hard Very Hard ON 0 mm 5 mm .0 mm 5 mm .0 mm 75 mm 00 mm	CLAYS: SAMPLE GI Location of SPT Sample LABORAT LL = PL = PL = PI = % PASS - 200 =	9 - 15 16 - 30 31 - 50 OVER 50 RAPHIC TY EXAMPLE EX	YPE LEGI T LEGEN quid Limit astic Limit sticity Inde ssing the N	Stiff Very Stiff Hard Very Hard END AU 1 Location of Auge Sample D 4, % 5, % 5, % 5, % 5, % 5, % 5, % 5, % 5

 k_h

=

SILTS & CLAYS:

Less than 0.075 mm

KEY TO SOIL CLASSIFICATION CHART

263

Horizontal Hydraulic Conductivity, ft/da

6.0 LIMITATIONS

6.1 Warranty

This report has been prepared for our client for their exclusive use, in accordance with generally accepted soil and foundation engineering practices, and makes no other warranty either expressed or implied as to the professional advice provided in the report.

6.2 Auger and SPT Borings

The determination of soil type and conditions was performed from the ground surface to the maximum depth of the borings, only. Any changes in subsurface conditions that occur between or below the borings would not have been detected or reflected in this report.

Soil classifications that were made in the field are based upon identifiable textural changes, color changes, changes in composition or changes in resistance to penetration in the intervals from which the samples were collected. Abrupt changes in soil type, as reflected in boring logs and/or cross sections may not actually occur, but instead, be transitional.

Depth to the water table is based upon observations made during the performance of the auger and SPT borings. This depth is an estimate and does not reflect the annual variations that would be expected in this area due to fluctuations in rainfall and rates of evapotranspiration.

6.3 Site Figures

The measurements used for the preparation of the figures in this report were made using the provided site plan and by estimating distances from existing structures and site features. Figures in this report were not prepared by a licensed land surveyor and should not be interpreted as such.

6.4 Unanticipated Soil Conditions

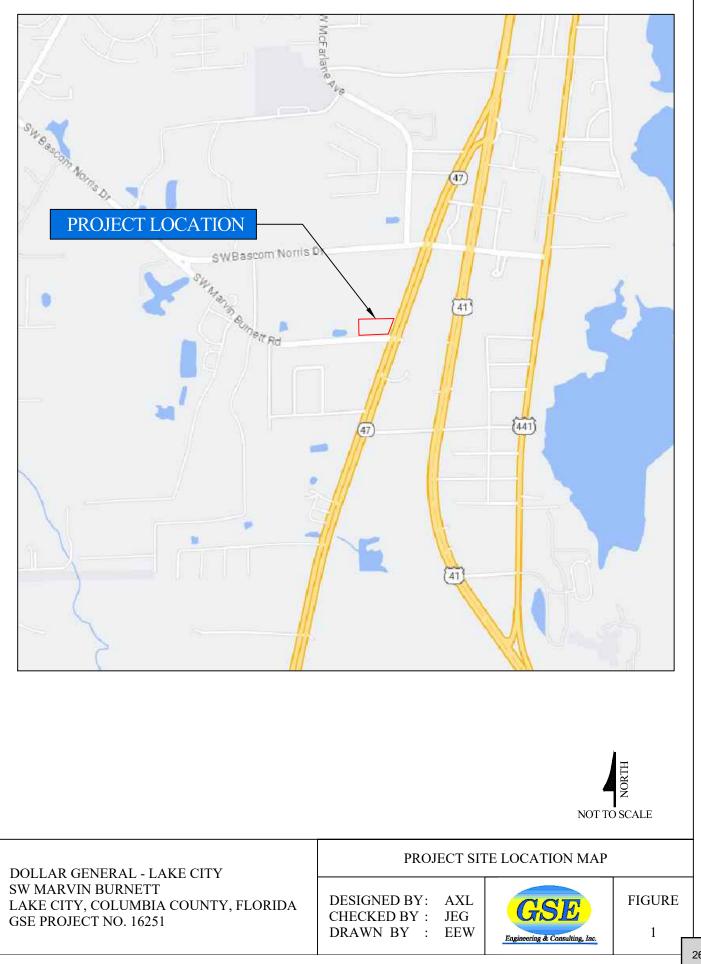
The analysis and recommendations submitted in this report are based upon the data obtained from soil borings performed at the locations indicated on Figure 2. This report does not reflect any variations that may occur between these borings.

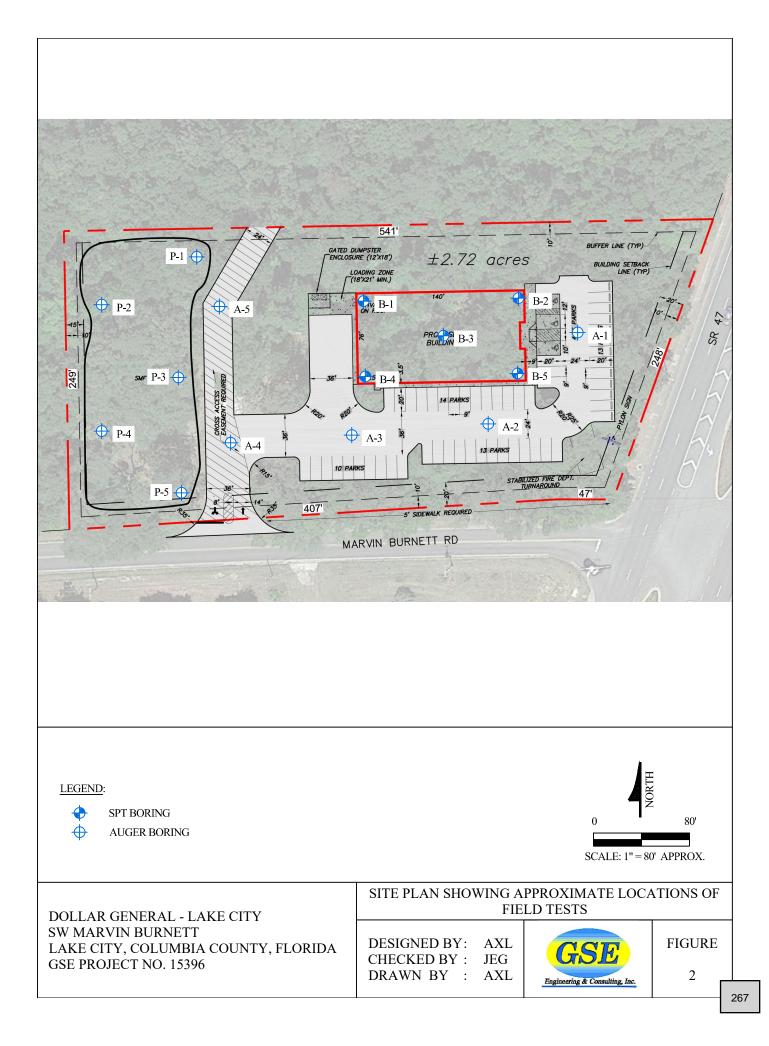
The nature and extent of variations between borings may not become known until excavation begins. If variations appear, we may have to re-evaluate our recommendations after performing on-site observations and noting the characteristics of any variations.

6.5 Misinterpretation of Soil Engineering Report

GSE Engineering & Consulting, Inc. is responsible for the conclusions and opinions contained within this report based upon the data relating only to the specific project and location discussed herein. If others make the conclusions or recommendations based upon the data presented, those conclusions or recommendations are not the responsibility of GSE.

FIGURES







DEPARTMENT OF GROWTH MANAGEMENT 205 North Marion Avenue Lake City, Florida 32055 Telephone: (386) 719-5750 growthmanagement@lcfla.com

REVIEW REPORT TO PLANNING AND ZONING, BOARD OF ADJUSTMENT AND HISTORICAL COMMITTEES' BY STAFF FOR SITE PLAN REVIEW, SPECIAL EXCEPTIONS, VARIANCES, COMPREHENSIVE PLAN AMENDMENTS/ ZONING AND CERTIFICATE OF APPROPRIATENESS

Date: ____03/21/2024

The City of Lake City staff has reviewed the application and documents provided for the above request and have determined the following.

Growth Management – Building Department, Planning and Zoning, Code Enforcement, Permitting cuSianed by: _Date: 3/22/2024 **Building Department: Reviewed by:** No comments at this time Date: 3/26/2024 Planning and Zoning: Reviewed by: Robert Angelo The property is zoned Commercial Intensive. All permitted uses in Commercial General are permitted in Commercial Intensive per section 4.13.2. Retail stores are a permitted use per section 4.12.2.1. Business License: Reviewed by: Marshall Sona will need to apply for occupational license _Date: 3/22/2024 Code Enforcement: Reviewed by: Marshall Sava No liens, codes or violations _Date: ^{3/22/2024} Permitting: Reviewed by: <u>Ann Jones</u> not at this time

Utilities – Water, Sewer, Gas, Water Distribution/Collections, Customer Service

Vater Department: Reviewed by: Mike Øskøm	Date:
None at this time	
ewer Department: Reviewed by: Usy Prilum	Date:
lone	
as Department: Reviewed by: <u>Stur Brown</u>	Date:
Cannot comment wit no address.	
— DocuSigned by:	4/2/2024
Vater Distribution/Collection: Reviewed by:	Date:
no comment at this time	
DocuSigned by:	Date: 4/9/2024
ustomer Service: Reviewed by:Slusta pulliam	Date
A tap application will need to be submitted in order request city utilities. The utility fees will be calc	to
ustomer Service: Reviewed by: <u>Slata Pillam</u> ecorrorited experies and the submitted in order request city utilities. The utility fees will be calco of the tap application.	to

Public Safety – Public Works, Fire Department, Police Department

Public Works: Reviewed by:	Date:
No comment.	
Fire Department: Reviewed by:	Date:
I have no issues	
Police Department: Reviewed by:	Date:
no concerns at this time	

NOTE: Please provide separate pages for comments that will not fit in provided spaces and please label the pages for your department and for the project.

State and County- FDOT, Suwannee River Water Management, School Board, Columbia County

FDOT: Reviewed by:	_ Date:
Suwannee River Water Management: Reviewed by:	_Date:
The project will require an ERP Permit. It is recommended applicant schedule a pre-application meeting with SRWMD so the permitting requirements.	
School Board: Reviewed by:	_Date:
No comments at this time.	
County: Reviewed by: Urad Williams	Date: 4/9/2024
A driveway permit will be required. The County is current of permitting several developments west of this location Norris Drive. For that reason, we ask that the applicar careful attention to the traffic issue. This comment is County Engineer based only on the information contained i provided. This response does not constitute the engineer' opinion with respect to the project and does not constitut committee or board for Columbia County.	along Bascom It and agencies pay provided by the n the application s professional

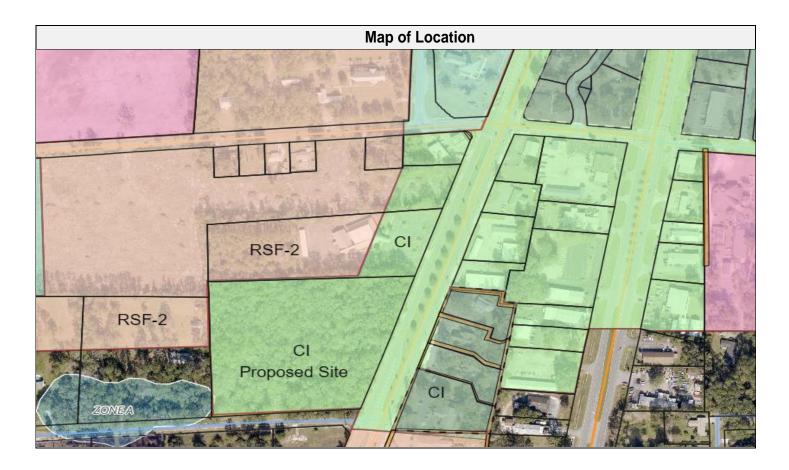
NOTE: Please provide separate pages for comments that will not fit in provided spaces and please label the pages for your department and for the project.

LAKE CITY GROWTH MANAGEMENT STAFF ANALYSIS REPORT

	Project Information
Project Name and Case No.	Dollar General site plan review
Applicant	Randall Olney, PE
Owner	Concept Companies
Requested Action	Site plan review for Dollar General, retail store, on parcel 08127-005
Hearing Date	05-14-2024
Staff Analysis/Determination	Sufficient for Review
Prepared By	Robert Angelo

	Subject Property Information				
Size	+/- 2.70 Acres				
Location	Corner of Marvin Burnett and Hwy 47				
Parcel Number	08127-000				
Future Land Use	Commercial				
Proposed Future Land Use	Commercial				
Current Zoning District	Commercial Intensive				
Proposed Zoning	Commercial Intensive				
Flood Zone-BFE	Flood Zone X and A Base Flood Elevation-N/A				

	Land Use Table						
Direction	Future Land Use	Zoning	Existing Use	Comments			
N	Residential Moderate	RSF-2	Residential				
E	Residential Moderate	RSF-2	Residential				
S	County		Vacant	County Jurisdiction			
W	Commercial	CI	Medical Office				





Summary of Request

Applicant has petitioned for a site plan review for the above parcels to build a retail store.

PUBLIC NOTICE



CITY OF LAKE CITY NOTICE LAND USE ACTION

A PUBLIC HEARING IS SCHEDULED TO CONSIDER A REQUEST FOR:

SPR24.05, a petition by Randall Olney, P.E., as agent, to request a Site Plan Review approval be granted as provided for in Section 4.13 of the Land Development Regulations, to get approval on site plan for Dollar General for a property located in the Commercial Intensive zoning district, in accordance with the submittal of the petition dated March 21, 2024, to be located on parcels 08127-005

WHEN:May 14, 2024
5:30 p.m.WHERE:City Council Meeting Room, Second Floor, City Hall, located at 205 North Marion Avenue,
Lake City, Florida.
Members of the public may also view the meeting on our YouTube channel at:
https://www.youtube.com/c/CityofLakeCity.

Copies of the site plan review application are available for public inspection by contacting the Office of Growth Management at growthmanagement@lcfla.com or by calling 386.719.5820.

At the aforementioned public hearing, all interested parties may be heard with respect to the Certificate of Appropriateness.

FOR MORE INFORMATION CONTACT ROBERT ANGELO PLANNING & ZONING TECHNICIAN AT 386.719.5820

NOTICE OF PUBLIC MEETING CITY OF LAKE CITY PLANNING AND ZONING BOARD

THIS SERVES AS PUBLIC NOTICE the Planning and Zoning Board will hold a meeting on Tuesday, May 14, 2024 at 5:30 PM or as soon after.

Agenda items-

- SPR 24-05, Petition submitted by Randall Olney, P.E., (agent) for Concept Companies, (owner), for a Site Plan Review for Dollar General, in a Commercial Intensive zoning district, and located on parcel 08127-005, which is regulated by the Land Development Regulations Section 4.13.
- LDR 24-04, Text amendment to the Land Development Regulations Sections 2.1, 4.2, 4.4, 4.5 and 4.6, to add definitions and add provisions for ADU's, Accessory Dwelling Units, and Tiny Homes for the City of Lake City.

Meeting Location: City Council Chambers located on the 2nd Floor of City Hall at 205 North Marion Avenue, Lake City, FL 32055.

Members of the public may also view the meeting on our YouTube channel at: https://www.youtube.com/c/CityofLakeCity

Pursuant to 286.0105, Florida Statutes, the City hereby advises the public if a person decides to appeal any decision made by the City with respect to any matter considered at its meetings or hearings, he or she will need a record of the proceedings, and that, for such purpose, he or she may need to ensure that a verbatim record of the proceedings is made, which record includes the testimony and evidence upon which the appeal is to be based.

SPECIAL REQUIREMENTS: Pursuant to 286.26, Florida Statutes, persons needing special accommodations to participate in this meeting should contact the City Manager's Office at (386) 719-5768.

Robert Angelo Planning and Zoning Tech

NOTICE OF PUBLIC MEETING CITY OF LAKE CITY PLANNING AND ZONING BOARD

THIS SERVES AS PUBLIC NOTICE the Planning and Zoning Board will hold a meeting on Tuesday, May 14, 2024 at 5:30 PM or as soon after.

Agenda items-

- 1. **SPR 24-05,** Petition submitted by Randall Olney, P.E., (agent) for Concept Companies, (owner), for a Site Plan Review for Dollar General, in a Commercial Intensive zoning district, and located on parcel 08127-005, which is regulated by the Land Development Regulations Section 4.13.
- 2. LDR 24-04, Text amendment to the Land Development Regulations Sections 2.1, 4.2, 4.4, 4.5 and 4.6, to add definitions and add provisions for ADU's, Accessory Dwelling Units, and Tiny Homes for the City of Lake City.

Meeting Location: City Council Chambers located on the 2nd Floor of City Hall at 205 North Marion Avenue, Lake City, FL 32055.

Members of the public may also view the meeting on our YouTube channel at: https://www.youtube.com/c/CityofLakeCity

Pursuant to 286.0105, Florida Statutes, the City hereby advises the public if a person decides to appeal any decision made by the City with respect to any matter considered at its meetings or hearings, he or she will need a record of the proceedings, and that, for such purpose, he or she may need to ensure that a verbatim record of the proceedings is made, which record includes the testimony and evidence upon which the appeal is to be based.

SPECIAL REQUIREMENTS: Pursuant to 286.26, Florida Statutes, persons needing special accommodations to participate in this meeting should contact the City Manager's Office at (386) 719-5768.

Robert Angelo Planning and Zoning Tech.

Angelo, Robert

From:	LCR-Classifieds <classifieds@lakecityreporter.com> Monday, April 29, 2024 11:20 AM</classifieds@lakecityreporter.com>
Sent: To:	Angelo, Robert
Subject:	73990 73992 73991 RE: Non-Legal Ad for P&Z, BOA, and HPA for 05-14-2024
Attachments:	73991.pdf; 73992.pdf; 73990.pdf

Robert, all are scheduled to publish on May 2. Approval due by tomorrow please P&Z: 3 col x 5.5 \$272.25 Historic: 3 col x 4.5 \$222.75 BOA: 3 col x 4 \$198

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Why Local Newsprint Advertising?

1 Newspaper readers are ENGAGED

2 Newspapers are viewed as TRUSTWORTHY

From: Angelo, Robert <AngeloR@lcfla.com> Sent: Monday, April 29, 2024 8:57 AM To: LCR-Classifieds <classifieds@lakecityreporter.com> Subject: Non-Legal Ad for P&Z, BOA, and HPA for 05-14-2024

Kym

Please publish this ad in the body of the paper as a display ad in the May 2, 2024 paper.

Thank You Robert Angelo City of Lake City Growth Management growthmanagement@lcfla.com 386-719-5820



PLEASE NOTE: Florida has a very broad public records law. Most written communications to or from City officials regarding City business are public records available to the public and media upon request. Your email communications may be subject to public disclosure.



NOTICE OF PUBLIC MEETING CITY OF LAKE CITY PLANNING AND ZONING BOARD

THIS SERVES AS PUBLIC NOTICE the Planning and Zoning Board will hold a meeting on Tuesday, May 14, 2024 at 5:30 PM or as soon after.

Agenda items-

- 1. **SPR 24-05,** Petition submitted by Randall Olney, P.E., (agent) for Concept Companies, (owner), for a Site Plan Review for Dollar General, in a Commercial Intensive zoning district, and located on parcel 08127-005, which is regulated by the Land Development Regulations Section 4.13.
- LDR 24-04, Text amendment to the Land Development Regulations Sections 2.1, 4.2, 4.4, 4.5 and 4.6, to add definitions and add provisions for ADU's, Accessory Dwelling Units, and Tiny Homes for the City of Lake City.

Meeting Location: City Council Chambers located on the 2nd Floor of City Hall at 205 North Marion Avenue, Lake City, FL 32055.

Members of the public may also view the meeting on our YouTube channel at: https://www.youtube.com/c/CityofLakeCity

Pursuant to 286.0105, Florida Statutes, the City hereby advises the public if a person decides to appeal any decision made by the City with respect to any matter considered at its meetings or hearings, he or she will need a record of the proceedings, and that, for such purpose, he or she may need to ensure that a verbatim record of the proceedings is made, which record includes the testimony and evidence upon which the appeal is to be based.

SPECIAL REQUIREMENTS: Pursuant to 286.26, Florida Statutes, persons needing special accommodations to participate in this meeting should contact the City Manager's Office at (386) 719-5768.

Robert Angelo Planning and Zoning Tech.



April 22, 2024

To Whom it May Concern

On May 14, 2024 the Planning and Zoning Board will be having a meeting at 5:30pm at 205 N. Marion. At this meeting we will be hearing a petition submitted by Randall Olaney, PE, as agent, for Concept Companies, owner, for a site plan review, SPR24-05, for parcel 08127-005, The site plan is to build a retail store-Dollar General located within the Commercial Intensive (CI) zoning district.

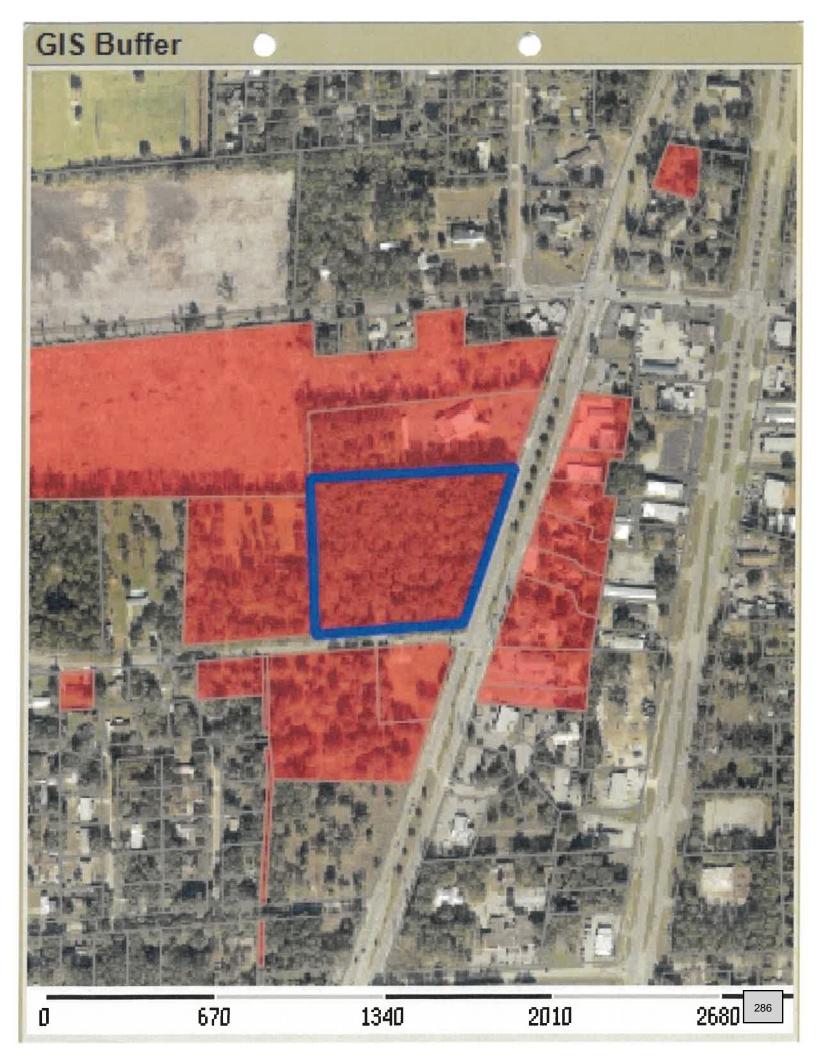
If you have any questions or concerns please call 386-752-2031 ext. 820 or email growthmanagement@lcfla.com.

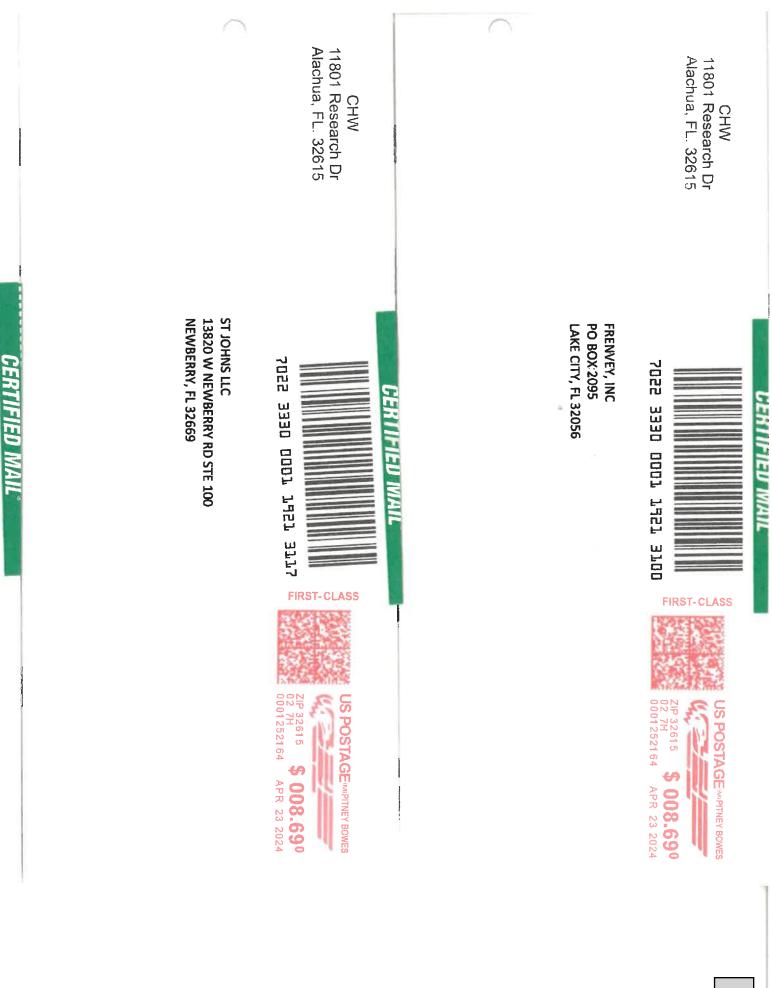
Robert Angelo

Planning and Zoning Tech City of Lake City

Columbia County Property Appraiser - Sales Report

Columbia County Property Applation Calcontepent							
Name	Address1	Address2	Address3	City	State ZI		
FRENVEY, INC	P O BOX 2095	*	LAKE CITY	FL	32056		
ST JOHNS LLC	13820 W NEWBERRY RD STE 100	9	NEWBERRY	FL	32669		
VANN SAMUEL P SR TRUST ETAL	131 W DUVAL STREET	15	LAKE CITY	FL	32055		
NFD DEVELOPERS LLC	P O BOX 2166	20	LAKE CITY	FL	32056		
GARR KENNETH	229 SW MARVIN BURNETT RD	*	LAKE CITY	FL	32024		
BAKER CHESTER	47 BURNT SWAMPP RD		EAST KINGSTON	NH	03827		
JAA INVESTMENT PROPERTIES, LLC	312 SW PILOTS WAY	2	LAKE CITY	FL	32024		
LAKE CITY CHURCH OF CHRIST INC	656 SW STATE RD 47		LAKE CITY	FL	32025		
KAMPMEYER ERVIN L LIVING TRUST	681 SW ST RD 47		LAKE CITY	FL	32025		
MARTIN CELIA S AS TRUSTEE	CELIA S MARTIN REV TRUST	973 SW STATE RD 47	LAKE CITY	FL	32025		
HAYDEN DONALD B	733 SW SR 47	ũ.	LAKE CITY	FL	32025		
POLMERSKI LAVONNA B	423 NW CLUBVIEW CR	¥.	LAKE CITY	FL	32055		
CANCER CENTERS OF NORTH FLORIDA LLC	PO BOX 80610	×	INDIANAPOLIS	IN	46280		
CIVITAN REGIONAL BLOOD CENTER INC	D/B/A LIFESOUTH COMMUNITY BLOOD CENTERS, INC	4039 NEWBERRY RD	GAINESVILLE	FL	32607		
LAKE CITY, COLUMBIA COUNTY CHAMBER OF COMMERCE, INC	875 SW SR 47	90	LAKE CITY	FL	32025		







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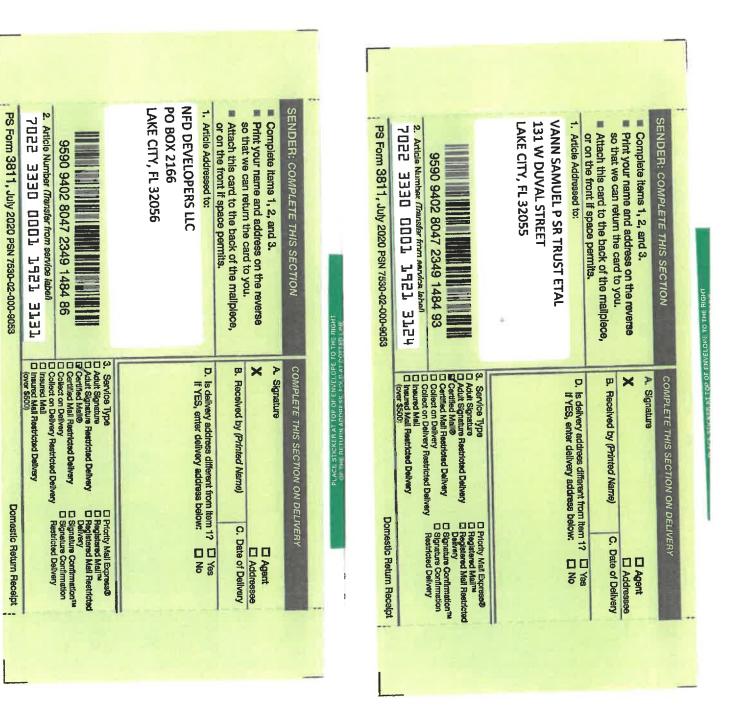
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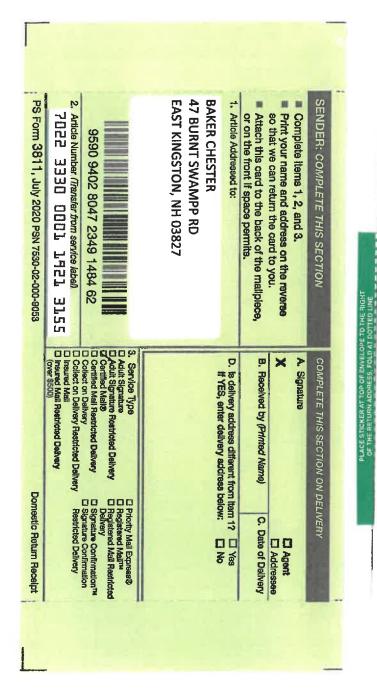
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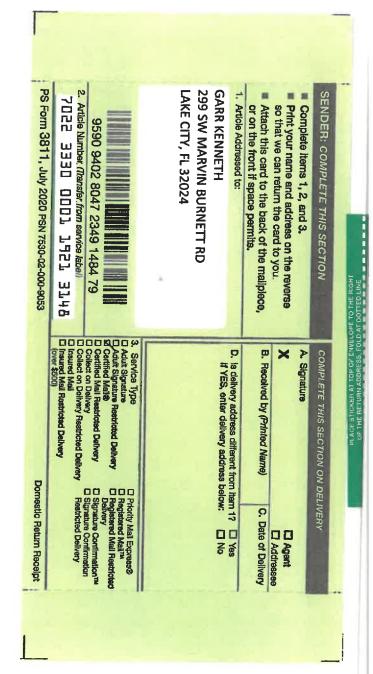


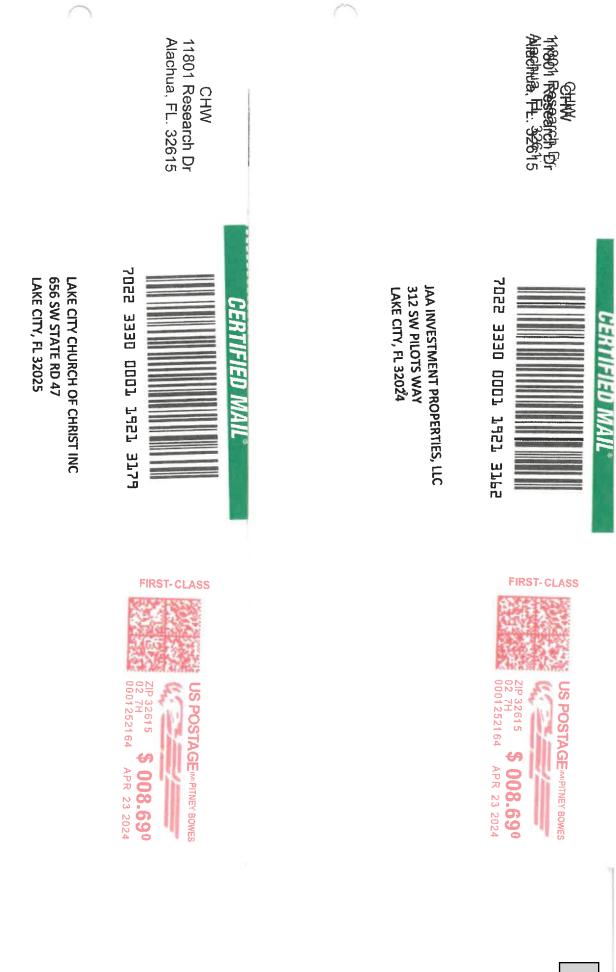




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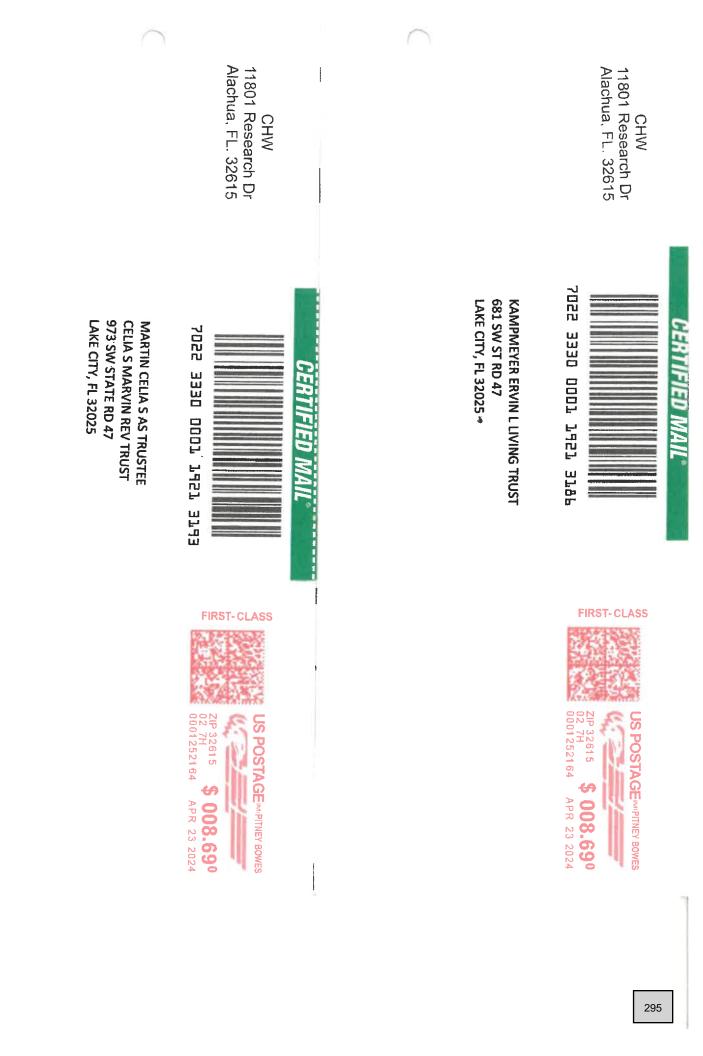


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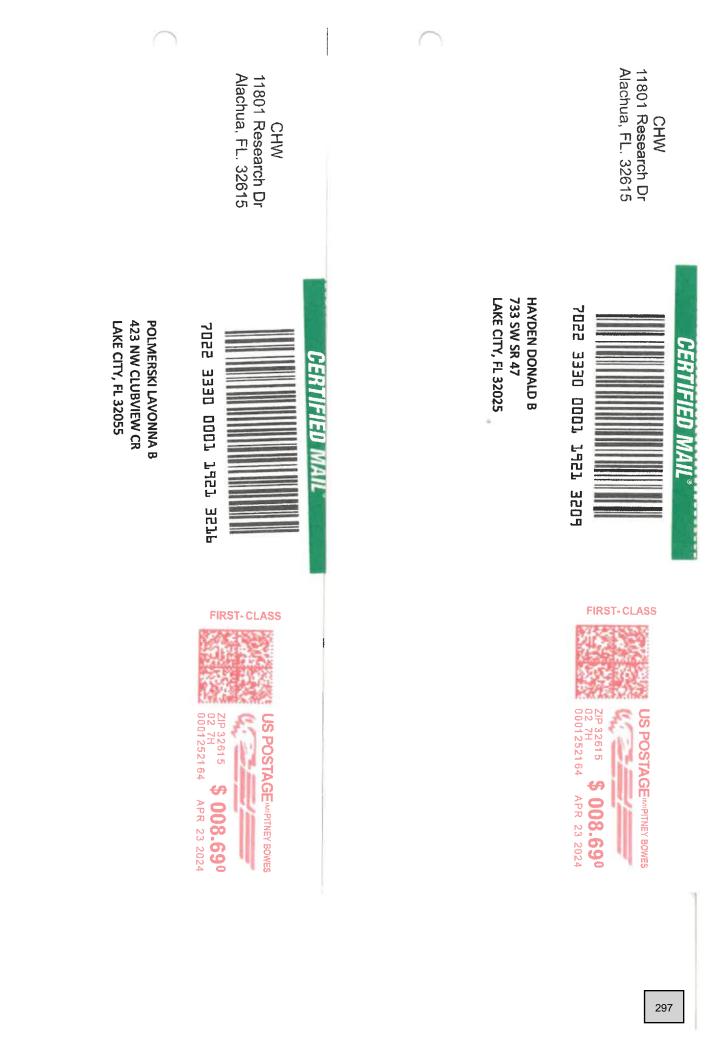


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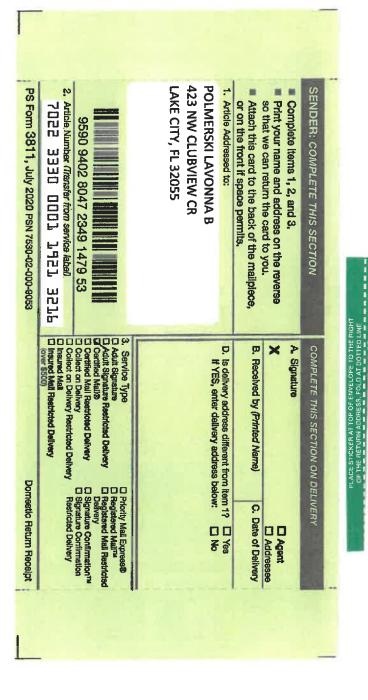
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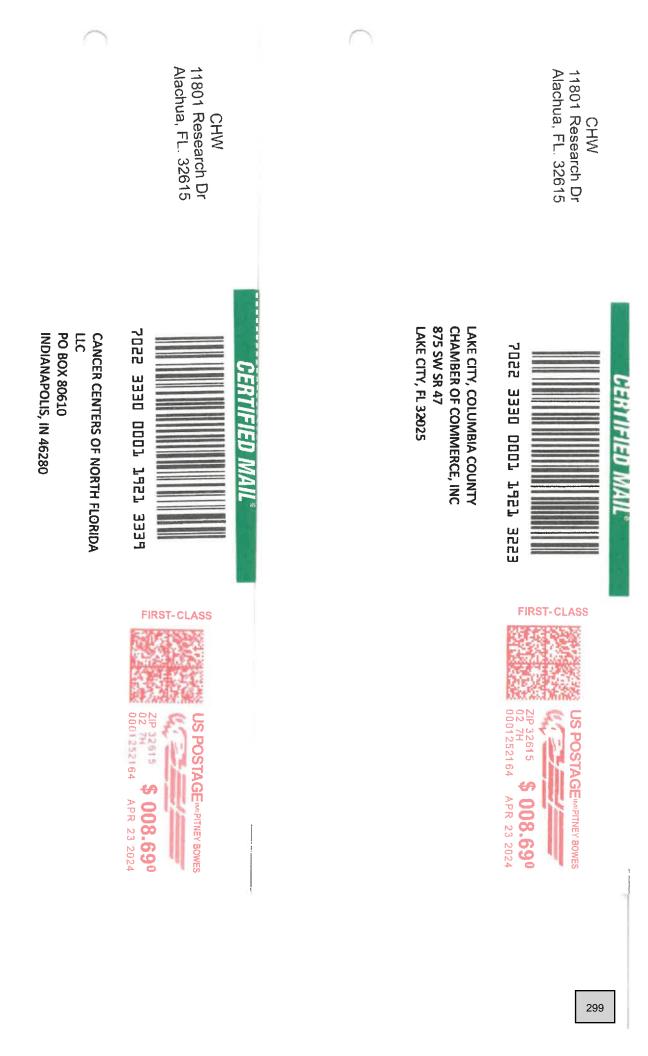
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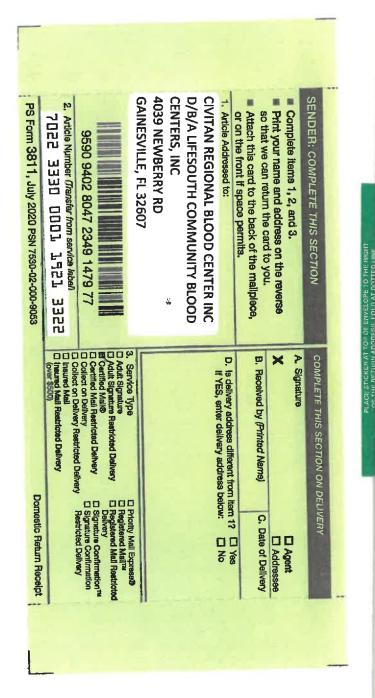
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CHW 11801 Research Dr Alachua, FL. 32615





CIVITAN REGIONAL BLOOD CENTER INC D/B/A LIFESOUTH COMMUNITY BLOOD CENTERS, INC 4039 NEWBÈRRY RD GAINESVILLE, FL 32607



File Attachments for Item:

iii. LDR 24-04; Text amendment to the Land Development Regulations Sections 2.1, 4.2, 4.4, 4.5, and 4.6, more specifically adding definitions and provisions for Accessory Dwelling Units (ADU's) and Tiny Homes for the City of Lake City.

TEXT AMENDMENT LDR 24-04

AMENDING TEXT IN SECTIONS 2.1, 4.2, 4.4, 4.5 AND 4.6 OF THE LAND DEVELOPMENT REGULATIONS OF THE CITY OF LAKE CITY

LDR 24-04, AN APPLICATION BY DAVE YOUNG TO AMEND THE TEXT SECTIONS 2.1, 4.2, 4.4, 4.5, AND 4.6 OF THE LAND DEVELOPMENT REGULATIONS BY ADDING PROVISIONS FOR TINY HOMES AND ACCESSORY DWELLING UNITS

WORDS <u>BOLDED AND UNDERLINED</u> HAVE BEEN ADDED WORDS <u>BOLDED AND STRUCK THROUGH</u> HAVE BEEN DELETED

ARTICLE TWO - DEFINITIONS

Accessory Dwelling Units (ADU). Accessory Dwelling Units (ADUs) are additional living guarters typically on single-family lots that are independent of the primary dwelling unit including a separate kitchen, bathroom, and sleeping area and are between 900 square feet and 1,100 square feet in size. All ADUs shall be permanently installed on a permanent foundation (concrete slab) or other approved foundation for the use of permanent Affordable Housing.

Infill. The allowance, by Special Exception, to place no more that two (2) tiny homes on lots that are deemed to be too small by the current Land Development Regulations to construct conventional residences upon for the use of permanent Affordable Housing.

Infill Subdivision. The allowance by Special Exception, to place two or more tiny homes, on permanent foundations, within certain zoning districts for permanent affordable housing. Each tiny home shall have a minimum of 400 square feet to 1,000 square feet of land space, depending on the square footage size of the tiny home.

<u>Tiny home (Stationary). A detached, single-family residential dwelling unit between</u> 200 SF and 900 SF set on a permanent foundation that is the primary or accessory structure and shall meets all applicable Florida Building Code standards for the use of permanent Affordable Housing.

- 1. <u>Tiny Home shall be site constructed and inspected by the local</u> jurisdiction or manufactured in a plant with an approved Florida licensed third party inspection company, recorded on each unit, during the assembly process for compliance with the Florida Building Codes and the National Electric Code
- 2. <u>Tiny Home shall be delivered on a trailer and set on a permanent</u> foundation (concrete slab) designed by a licensed Florida Design Professional.

<u>Tiny home (On Wheels for Permanent Installation). A detached, single-family</u> residential dwelling unit between 200 SF and 900 SF constructed on a trailer frame and when permanently installed for Permanent Affordable Housing and becomes the primary or accessory structure and shall meet all applicable Florida Building Code standards.

- Anchoring. Each Tiny Home shall be located on a stand permitting each unit to be sufficiently supported and anchored as in compliance with a Florida Licensed Design Professional's design. In addition, each Tiny Home shall have the wheels and axles removed, shall be placed as close to the ground as can be practically accomplished and shall have the tongue or hitch portion of the Tiny Home removed.
- 2. Skirting. Approved skirt or apron with required ventilation vents and

which is continually and properly maintained by the owner of the Tiny Home shall surround each Tiny Home between the bottom of the unit and the ground.

<u>Tiny home (On Wheels for Portable Use). A unit between 200 SF and 900 SF</u> <u>constructed on a trailer frame designed for use as temporary location shall be</u> <u>determined to be a Recreational Vehicle, and as such shall only be allowed to be</u> <u>located within campgrounds when occupied. The running gear (wheels and</u> <u>axel(s)) and trailer hitch remain in place.</u>

ARTICLE FOUR – ZONING REGULATIONS

Section 4.2 SUPPLEMENTARY DISTRICT REGULATIONS

4.2.15.16 Off-Street Parking Requirements; For all zoning districts except C-CBD Commercial Central Business District;

Tiny Home and Accessory Dwelling Units- one (1) parking space for each

4.2.36 REQUIREMENTS FOR ACCESSORY DWELLING UNITS AND TINY HOMES

The cost of rental housing has increased steadily and the cost often exceeds an amount that is affordable to extremely-low-income, very-lowincome, low-income, or moderate-income persons and has resulted in a critical shortage of affordable rentals in the City. This shortage of affordable rentals constitutes a threat to the health, safety, and welfare of the residents of the City. Therefore, the City finds that it serves an important public purpose to allow and encourage the permitting of Accessory Dwelling Units and Tiny Homes in single-family residential areas in order to increase the availability of affordable rentals for extremely-low-income, very-low-income, low-income, and moderateincome persons as defined in s.420.004(11), (12), (17), & (9).

An application for a building permit to construct or place an Accessory Dwelling Unit or Tiny Home Dwelling Unit shall include an affidavit provided by the City from the property owner which attests that the dwelling unit will be rented at an affordable rate to an extremely-lowincome, very-low-income, low-income, or moderate-income person or persons. This affidavit shall be filed with the Columbia County Clerk of the Court as part of the Property Deed.

SECTION 4.4 "A" AGRICULTURAL

Section 4.4.5 SPECIAL EXCEPTIONS

29. Tiny Homes and Accessory Dwelling Units (ADU)

The living area square footage of Tiny Homes within the LDR land use district of Agricultural (A) shall be 200 square feet minimum to 900 square feet maximum, and Accessory Dwelling Units (ADU) shall be 900 square feet minimum to 1,100 square feet maximum. Tiny Homes and Accessory Dwelling Units shall comply with all code requirements for dwelling units and/or Tiny Homes and be complete with a bathroom, kitchen, sleeping area(s) and comply with all life safety and sanitary codes. Only tiny homes and ADU's on permanent foundations or approved foundations shall be allowed for the use of permanent Affordable Housing.

4.4.7 MINIMUM YARD REQUIREMENTS (depth of front and rear yard, width of side yard) (See Section 4.2 for right-of-way setback requirements.)

1. All permitted uses and structures (unless otherwise specified):

<u>Tiny Homes and Accessory Dwelling Units:</u>

Front 30 feet

Side 10 feet

Rear 10 feet

*Note: Separation from existing structures 10 feet

SECTION 4.5 "RSF" RESIDENTIAL, SINGLE FAMILY

Section 4.4.5 SPECIAL EXCEPTIONS

a.

14. Tiny Homes and Accessory Dwelling Units (ADU)

The living area square footage of Tiny Homes within the LDR land use district of Residential, Single Family (RSF) shall be 200 square feet minimum to 900 square feet maximum, and Accessory Dwelling Units (ADU) shall be 900 square feet minimum to 1,100 square feet maximum. Tiny Homes and Accessory Dwelling Units shall comply with all code requirements for dwelling units and/or Tiny Homes and be complete with a bathroom, kitchen, sleeping area(s) and comply with all life safety and sanitary codes. Only tiny homes and ADU's on permanent foundations or approved foundations shall be allowed for the use of permanent Affordable Housing.

4.5.7 MINIMUM YARD REQUIREMENTS (depth of front and rear yard, width of side yard) (See Section 4.2 for right-of-way setback requirements.)

3. Tiny Homes and Accessory Dwelling Units (for RSF-1, RSF-2 and RSF-3)

Front 30 feet

Side 10 feet

Rear 10 feet

*Note: Separation from existing structures 10 feet

SECTION 4.6 "RSF/MH" RESIDENTIAL, (MIXED)SINGLE FAMILY/MOBILE HOME

Section 4.6.5 SPECIAL EXCEPTIONS

13. Tiny Homes and Accessory Dwelling Units (ADU)

The living area square footage of Tiny Homes within the LDR land use district of Residential, (Mixed) Single Family/Mobile Home (RSF/MH) shall be 200 square feet minimum to 900 square feet maximum, and Accessory Dwelling Units (ADU) shall be 900 square feet minimum to 1,100 square feet maximum. Tiny Homes and Accessory Dwelling Units shall comply with all code requirements for dwelling units and/or Tiny Homes and be complete with a bathroom, kitchen, sleeping area(s) and comply with all life safety and sanitary codes. Only tiny homes and ADU's on permanent foundations or approved foundations shall be allowed for the use of permanent Affordable Housing.

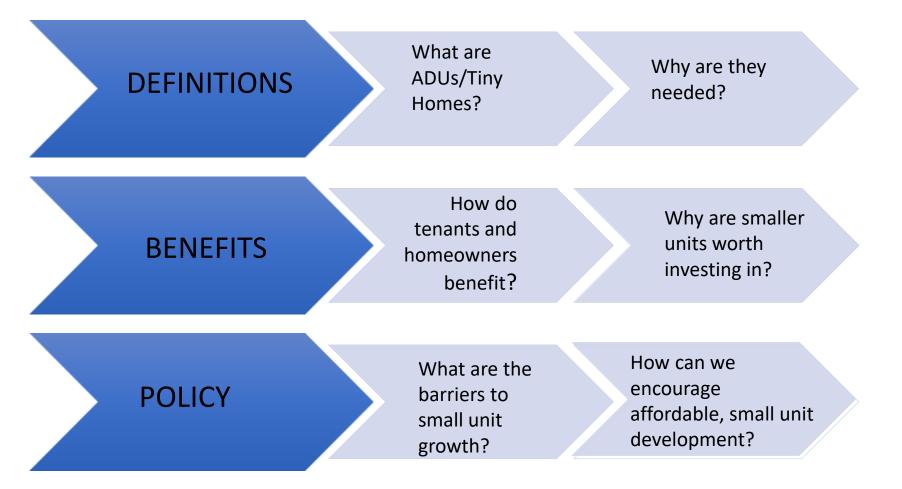
4.6.7 MINIMUM YARD REQUIREMENTS (depth of front and rear yard, width of side yard) (See Section 4.2 for right-of-way setback requirements.)

5. Tiny Homes and Accessory Dwelling Units (for RSF/MH-1, RSF/MH-2 and RSF/MH-3)

Front	25 feet	
Side	10 feet	
Rear	10 feet	
*Note: Separat	ion from existing structures	10 feet

Accessory Dwelling Units and Tiny Homes

AFFORDABLE HOUSING INITIVE by The City of Lake City David C. Young, CBO Director Growth Management



ACCESSORY DWELLING UNITS: WHAT ARE THEY?

- Accessory Dwelling Units (ADUs) are additional living quarters typically on single-family lots that are independent of the primary dwelling unit
- Can be a freestanding home on the same lot as the primary unit
- Can be owner or tenant occupied
- AKA granny flats, garden cottage, accessory apartment, etc.
- Typically 900 square feet to 1,100 square feet in size

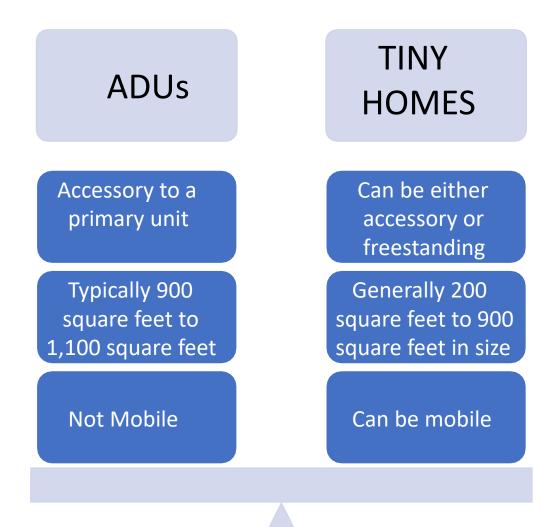


TINY HOMES: WHAT ARE THEY?

- Tiny homes are units 200 square feet to 900 square feet that can stand on a lot independently
- Can be an accessory unit, freestanding unit, and even on wheels



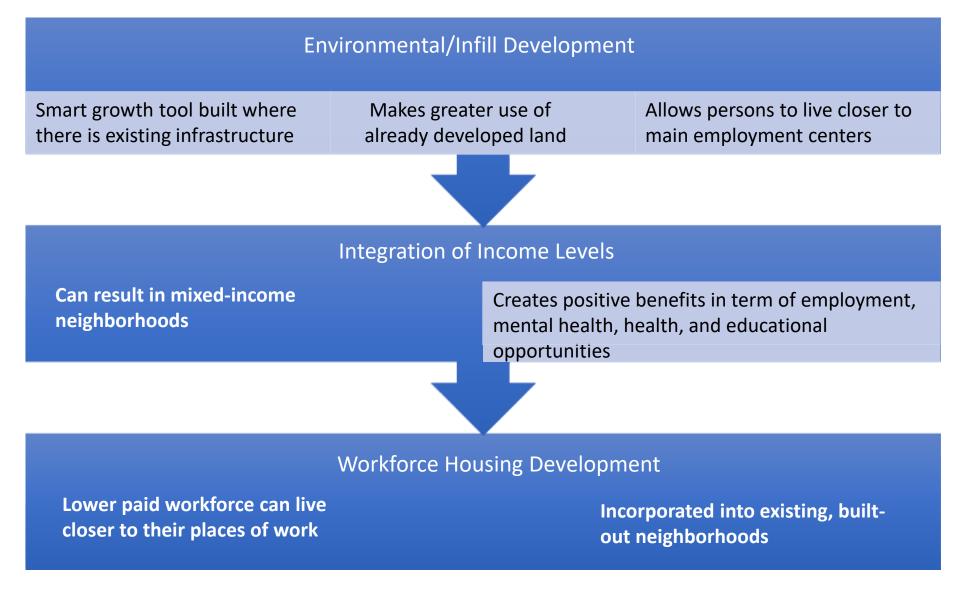
HOW DO ADUS AND TINY HOMES DIFFER?



WHY ARE SMALLER UNITS, SUCH AS ADUS AND TINY HOMES, NEEDED?

- Around 64% of occupied units in Florida, or nearly 4.8 million units, are singlefamily homes
- ADUs allow more persons to live on these lots at an affordable price
- Between 1970 and 2012, the average number of persons per household declined from 3.1 to 2.6
- With smaller households, smaller housing types are in higher demand
- Over 1.94 million, or 26% of all Florida households, are cost-burdened
- Three-quarters of low-income renters are cost-burdened
- By 2030, there will be an estimated 3.5 million more people in Florida

THE VALUE OF ADUS AND TINY HOMES



BARRIERS & SOLUTIONS TO ADU AND TINY HOME GROWTH

1. Euclidean Zoning & Single-Family District

- "Euclidean" zoning separates what are thought of as incompatible uses from being on nearby or the same lots
- Claim: ADUs are compatible with single-family homes
- Solution: Allow ADUs as a permissible use in single-family districts and use other land use mechanisms to regulate the character of development

2. Owner-Occupancy Restrictions

- Many jurisdictions in Florida currently require the homeowner to occupy the primary unit if ADU is utilized
- **Solution:** To provide flexibility, allow owners to occupy either the primary or ADU

BARRIERS & SOLUTIONS TO ADU AND TINY HOME GROWTH (CONTINUED)

3. Long-Term Rental Use Restrictions

- Some local gov'ts only allow ADUs for temporary guests, family members, caretakers, and in conjunction w/certain uses
- **Solution:** allow ADUs to be freely rented on the market

4. As-of-Right vs. Conditional Use

- The onerous, unpredictable, and costly nature of the conditional use process may discourage homeowners from constructing ADUs
- Solution: Allow ADUs as-of-right and establish transparent and predictable development requirements

5. Impact Fees

• ADUs and Tiny Homes that quality as <u>Affordable Housing</u> shall be exempt from all impact fees

BARRIERS & SOLUTIONS TO ADU AND TINY HOME GROWTH (CONTINUED)

6. Size, Density, & Other Structural Requirements

- Minimum lot size: reach a solution that allows the most possible lots to construct a lawful ADU
- Size: allow up to 900-1,100 sq. feet with additional size allowances
- Density: exempt ADUs from normal density calculations
- Setback: consider lessor lot line and other configurations that do not burden smaller lots

7. Parking Requirements

- Parking can be costly and a challenge from a planning perspective
- **Solution**: Form flexible standards that utilize on-street parking & different standards for different sizes

Housing in Lake City

Majority of construction is single family

- Reacting to demand
- Most Lake City single family housing does not fall into the Affordable Housing price range
- Greatest need in Lake City
- Housing affordable to households earning \$35,000 or less
- Housing type needed Affordable type housing for ownership and rental

Modifications to the Land Development Regulations and the Comprehensive Plan

Lake City will have to modify the Land Development Regulations and the Comprehensive Plan to allow for ADUs and Tiny Homes:

- Allow for permanently placed AHUs with a minimum square footage of 900 square feet and a maximum square footage of 1,100 square feet
- Allow for permanently placed Tiny Homes with a minimum square footage of 200 square feet and a maximum square footage of 900 square feet
- When these AHUs and Tiny Homes qualify as Affordable Housing, no impact fees shall be charged per Florida Statute 163.31801(9)

Residential Uses – ADUs, Tiny Homes for Residences

- ADUs and Tiny Homes are permitted to be rented out long term only if placed or constructed as Affordable Housing. If not placed or constructed as Affordable Housing, the primary residence shall have a Homestead Exemption
- Maximum ADU or Tiny Home size shall not exceed 40% of the conditioned floor area of the primary residence unless a variance is approved.
- The ADU or Tiny Home shall be compatible architecturally with the primary residence and, if located within a Historical District, shall be compatible with the Historic District architecturally.
- The ADU or Tiny Home shall not be attached to the primary residence.

Pros of ADUs and Tiny Homes

- 1. Extra Income. With a full time tenant in your ADU or Tiny Home along with the primary residence, it's a great source of income. And, if you sell, it will (hopefully) add value to your property and home
- 2. Usable Property. By placing no more than 2 Tiny Homes on a vacant property that is to small to build a conventional home, you will be utilizing property that would otherwise be vacant
- 3. **Create a Community**. By developing property for 3 or more Tiny Homes, you will be developing a community within a community
- 4. **Affordable Homes**. By placing or constructing ADUs or Tiny Homes, the ownership or renting costs will be less and will benefit the lower income earning citizens

Cons of ADUs and Tiny Homes

- **1. Disruption of Daily Life**. As a landlord you do have to manage the rental space (repairs and maintenance)
- **2.** Loss of yard space. With the addition of the ADU or Tiny Home and the extra vehicle to be parked
- 3. **Neighborhood**. The utilization of small vacant lots in a neighborhood to place or construct Tiny Homes may cause displeasure with the neighbors.

BENEFIT TO ALL

The greatest benefit with the addition of ADUs or Tiny Homes is that this will provide affordable housing for the veterans, lower income persons, the disabled and the elderly that reside within the City of Lake City.

These ADUs and Tiny Homes will have less energy costs to operate compared to conventional homes.

With the City of Lake City allowing the Tiny Homes to be placed or constructed on existing lots that are too small for conventional homes, the empty lots will now have residents, the lots being maintained, and the blight being removed from the neighborhood

QUESTIONS?

Accessory Dwelling Unit GUIDEBOOK

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Virtually every community in Florida is suffering from an affordable housing shortage. Of Florida's three million low-income households, over 1.94 million, or 26% of all Florida households, are cost-burdened; they spend more than 30% of their income on housing. Another 1.1 million households, or 15% of all Florida households, are severely cost burdened, spending more than 50% of their income on housing. Low-income renters are hit the hardest by the lack of affordable housing. A staggering three-quarters of these households are cost-burdened.¹ When households spend this much of their income on housing, they have little left for life's other necessities. They are typically unable to withstand a rent increase and may be one missed paycheck away from homelessness.

1 Florida Housing Coalition, Home Matters for Florida Report 9 (2018).



Intended Audience

As communities and local governments consider meeting the demand for affordable housing by tapping into the vast single-family housing stock to create accessory dwelling units (ADUs), this document will be a reference guide. Elected and appointed officials, government employees and affordable housing advocates will quickly understand the pros and cons of allowing and encouraging ADUs. They will be able to sort through the potential regulatory changes and incentives to be implemented.

Local Government Planning Staff	AHAC Members	SHIP Administrators	Local Government Administrators and Elected Officials	Developers and Builders	Affordable Housing Stakeholders



Introduction

Every county and entitlement community in Florida receives SHIP funds. Most of those communities are required to have an Affordable Housing Advisory Committee (AHAC) to make recommendations for regulatory reform at least once every three years. The Florida Housing Coalition provides training and technical assistance to counties and municipalities to help with the implementation of regulatory reform and land use planning tools to produce and preserve affordable housing.

Florida Housing Coalition also developed a guidebook, *Affordable Housing Incentive Strategies: A Guidebook for Affordable Housing Advisory Committee Members and Local Government Staff*, that provides information for each of the 11 affordable housing incentives that AHACs must consider. Permitting accessory residential units in residentially zoned areas has been on the list of statutorily enumerated items found in Section 420.9076 (4)(e), Florida Statutes, since the passage of the William E. Sadowski Act in 1992. And yet we find that, by and large, ADUs are not permitted in most residentially zoned areas. Encouragingly, what we have found, is that local government planners and affordable housing advocates would like to include ADUs in their affordable housing toolkit but could use more information about how to do it. This guidebook, produced by the Florida Housing Coalition, with funding from the Florida Housing Finance Corporation's Catalyst Program, provides local government planners and affordable housing advocates with the "How To".

Historically, ADUs were commonly used to mitigate the shortage of affordable housing, providing smaller rental dwelling units ancillary or secondary to the principal residence. In the 1950s and 1960s with the rise of suburbs catering to nuclear families, ADUs fell out of favor. However, changing demographic trends showing continuing increases in smaller households, one-person households, elderly households, and households with disabled members are creating a surging interest in ADUs.

ADUs can provide a stable affordable housing option for those in vulnerable housing situations. Persons living in ADUs benefit financially as the lower rents allow them an affordable option for decent, safe housing. Additionally, those renting out the ADUs also benefit financially from the rental income stream which often provides the additional income owners, particularly those on a fixed income, need to make ends meet.

This guidebook addresses the challenges and benefits a community might face as it considers allowing the implementation of ADUs; it presents a range of alternatives to consider and evaluate. There is a compilation of best practices and a model ordinance. A community considering implementation of regulations allowing ADUs can find suggestions for how to manage public participation. Additionally, there is a template local governments can use to help homeowners who want to create an ADU.

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Section Overview

The remaining sections of the guidebook are described below.

What are ADUs? Florida Statutes (Section 163.31771(2)(a)) define ADUs as "an ancillary or secondary living unit that has a separate kitchen, bathroom, and sleeping area existing either within the same structure, or the same lot, as the primary dwelling unit."

ADUs provide an affordable housing alternative by tapping into Florida's large stock of single-family homes. Changing demographics make ADUs an attractive alternative to the elderly, persons with disabilities, families in transition, and to others needing safe, decent housing.

Most regulatory barriers to ADUs deal with local land use regulation. This section explores those barriers and provides practical solutions to get beyond them.

IV

Local governments have the tools to fund and incentivize ADU development. Waiving impact fees and providing financial assistance can be the key to establishing ADUs.

The increasing number of short-term vacation rentals through Airbnb and similar platforms can increase community concerns about the viability of long-term ADU rentals. While ADUs can be used as short-term rentals, through deed restrictions, local governments can require ADUs to be used as long-term rentals if the unit benefits from impact fee modifications or other financial assistance.

Proposals to allow ADUs in single-family residential zoning districts may bring out neighborhood opposition. Local governments can ease community concerns through educational campaigns and by addressing legitimate objections.

ADUs and Tiny Homes are alternative housing solutions. ADUs are always accessory to the primary unit. Tiny Homes can stand alone. As a result, different regulations apply.

This section provides a best practices chart for a successful ADU program.

Local land use regulations must be devised to allow ADUs to flourish broadly as a smart growth tool. With the right local ADU ordinance, ADU construction may increase to the community's benefit. This section provides a Model Ordinance to encourage and facilitate ADU growth.

Several local governments in Florida have model ordinances for ADU development. This section highlights several local ordinances with an analysis of each.

ADU development is of great interest to local governments, policymakers, and think-tanks across the country. Other works have been written highlighting best practices and describing the benefits of ADUs.

Allowing ADUs is only half the equation; this appendix provides a template for local governments to design an ADU Manual for homeowners. With this tool, local governments can help homeowners navigate the development, design, and operation of an ADU rental.

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I. What are ADUs?

Accessory dwelling units (ADUs) are additional living quarters typically on single-family lots that are independent of the primary dwelling unit. An ADU can be an apartment within a primary residence or it can be an attached or freestanding home on the same lot as the primary residence.¹

Accessory dwelling units are commonly referred to as granny or mother-in law flats and are also sometimes referred to as accessory apartments, garage apartments, carriage houses, and backyard cottages. ADUs were a common feature of early 20th century development in America but their use dwindled with the onset of the single-family suburb. ADUs were rarely included as an eligible use in municipal codes regulating land use, zoning, and general land development standards.

Florida is one of only a few states to pass legislation that incentivizes local governments to create ADU permitting ordinances.² In 2004, the Florida Legislature passed Section 163.31771 of the Florida Statutes to "promote the use of accessory dwelling units as a tool to help local communities address deficits in the supply of affordable rental housing for very-low-, low-, and moderate-income residents."³ In enacting this statute, the Legislature found that the median price of homes in Florida had increased steadily over the last decade at a greater rate of increase than the median income in many urban areas.⁴ The Legislature also found that the cost of rental housing had increased steadily to the point that there was a "critical shortage of affordable rentals in many urban areas in the state."⁵ While the statute does not require local governments to adopt ADU ordinances, it does promote ADUs as a tool for affordable housing development for very-low, low, and moderate-income persons.

5 ld.

HIGHLIGHTS

Florida Statutes (Section 163.31771(2) (a)) define ADUs as "an ancillary or secondary living unit that has a separate kitchen, bathroom, and sleeping area existing either within the same structure, or the same lot, as the primary dwelling unit."

In this section, you'll learn about:

- Characteristics of ADUs
- ADU Regulations

¹ Jaimie Ross, Accessory Dwelling Units: A Smart Growth Tool for Providing Affordable Housing, Housing News Network Journal Vol. 32, No. 2 (July 2016).

² Sarah A. Gottlieb, Florida's Accessory Dwelling Unit Laws: Mitigating Florida's Housing Woes Through State-Encouraged Expansion of ADU Permitting, 46 Stetson L. Rev. 627, 630 (2017).

³ Fla. Department of Community Affairs, Accessory Dwelling Units: Report to the Florida Legislature 6 (2007).

⁴ Fla. Stat. § 163.31771(1) (2018).



Characteristics

ADUs are smaller in size than the primary residence and are generally located toward the rear of the parcel. Typically, the owner lives in the primary residence, but unless restricted by the local government, the owner may choose to live in the smaller unit and rent out the primary residence. The ADU is ancillary and accessory to the primary unit and is often similar in appearance to the primary. An ADU is typically for one or two persons but may house more depending on its size.

Under Section 163.31771(2)(a) of the Florida Statutes, ADUs are defined as "an ancillary or secondary living unit that has a separate kitchen, bathroom, and sleeping area existing either within the same structure, or on the same lot, as the primary dwelling unit."⁶

6 Fla. Stat. § 163.31771(2)(a) (2018).

ADU Regulations

Regulation of ADUs is within the purview of zoning and land use planning. Local governments can allow ADUs while providing helpful regulations to ensure that ADUs enhance rather than detract from the character of a neighborhood. Some examples, described more in depth later, include the following:

Occupancy

An ADU is more useful to homeowners if occupancy is not restricted to family members or temporary, non-paying guests.

Construction

Allowing the construction of ADUs concurrently with new primary residences or as part of a subdivision or master planned community maximizes the efficient use of land without needing additional infrastructure.

Parking Requirements

A successful ADU ordinance balances congestion concerns and the concern that parking may be too burdensome for a homeowner due to cost and lot configuration.

Size, Setback, Minimum Lot Size, and Other Structural Requirements

These regulations can bring desired community aesthetics while also allowing the greatest number of lots to contain lawfully permitted ADUs.

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II. The Value of Accessory Dwelling Units

In a nation dominated by single-family units, many people struggle to find suitable living arrangements.⁷ As of 2015, 64% of occupied units in the state of Florida were single-family homes.⁸ ADUs capitalize on the prominence of the single-family home by allowing more residents to live on single-family lots at an affordable price. Additionally, the small size of the ADU reflects the changing demographics and needs of those looking for housing. The number of people per household in the United States continues to decrease.⁹ Between 1970 and 2012, the average number of people per household declined from 3.1 to 2.6. With smaller households, due to a variety of factors, smaller housing options are in higher demand. For those that are not looking for a large single-family home and yet want to live in a residential neighborhood, the ADU is a great option.

Accessory dwelling units are also beneficial for elderly and disabled populations that strive for continued independence. An elderly or disabled individual could remain in their home and use an ADU for their caregiver. ADUs can also provide for family flexibility. With an ADU, a young adult could continue to live with their parents, but in a separate unit, as he or she works towards economic independence. When developed close to employment centers, an ADU can reduce a person's reliance on transportation, providing additional benefits to society through environmental and energy cost savings. ADUs also promote mixed-income communities where lower-income households can find an affordable home in an area that may have greater employment and educational opportunities.

Affordability

Accessory dwelling units are a valuable affordable housing tool for low- and moderate-income individuals. Because they do not require additional land or major new infrastructure, ADUs are cheaper to build than the traditional single-family home. Further, the rental income from the ADU can subsidize the cost of the primary unit – making ADUs an affordable housing tool for both the renter and the homeowner. When both households are spending less of their income on housing, quality of life is improved, and more money is invested in the broader local economy.

HIGHLIGHTS

ADUs provide an affordable housing alternative by tapping into Florida's large stock of single-family homes. Changing demographics make ADUs an attractive alternative to the elderly, persons with disabilities, families in transition, and to others needing safe, decent housing.

In this section, you'll learn about:

- Affordability
- Care for the Elderly and Persons with Disabilities
- Family Flexibility
- Environment/Infill Development
- Integration of Income Levels
- Workforce Housing
 Development

⁷ See Gottlieb, supra note 2, at 628-29; U.S. Census Bureau, Historical Census of Housing Tables (2011), https://www.census.gov/hhes/www/housing/census/historic/units.html.

⁸ Shimberg Center for Housing Studies, Overview of Housing in Florida 4 (2015), http://www.shimberg.ufl.edu/publications/tab2.pdf.

⁹ U.S. Census Bureau, America's Families and Living Arrangements: 2012 (2013), https://www.census.gov/prod/2013pubs/p20-570.pdf.

Care for the Elderly and Persons with Disabilities

An ADU can be utilized so that an elderly or disabled individual who wishes to remain in their home can stay in their house and have their caregiver reside in the ADU, or vice versa. Elderly and disabled individuals often struggle to live comfortably due to the traditional ways in which communities are planned.¹⁰ For these folks, ADUs can provide an opportunity to live on the same lots as their parents or other caregivers.

ADUs can assist the elderly to "age in place."¹¹ ADUs are particularly well suited for lower-income elderly persons because in addition to receiving a source of income they may not otherwise receive, the elderly homeowner may obtain companionship and needed services from the tenant in the ADU. As the state's lower-income elderly population continues to increase, ADUs can be a vital tool for meeting the increased need for elderly care. Family members may also live in the ADU or primary unit to provide this care.

In 2000, AARP worked with the American Planning Association to develop a model state act and local ordinance as a resource for meeting the affordable needs of elder Americans. Both organizations have endorsed ADUs as a valuable tool for elderly Americans.¹²

Further, if an ADU is constructed for family members of at least 62 years of age, Section 193.703, Florida Statutes, provides that a county may provide for a reduction in the assessed value of homestead property after the new construction.¹³ This section of the Florida Statutes implements section 4(f) of Article VII of the Florida Constitution.¹⁴ This section was passed to encourage municipalities to provide tax incentives to homeowners who build living spaces for a parent or grandparent.¹⁵ Thus, the Florida Statutes encourages ADUs as a housing alternative for the elderly.

Family Flexibility

ADUs can also provide for family flexibility. If a young adult is not financially able to move out and wants to maintain a semblance of independence, he or she can live in an ADU on the same lot as their parents – coming and going as they please and entertaining their own guests, while remaining tightly bound to their family.¹⁶ Once the young adult moves out, the parents can then utilize the ADU as an affordable rental unit for other individuals. An ADU may also be used by older family members as a "granny flat." In this arrangement, a family can care for their elderly parents or grandparents who are now in close proximity. ADUs allow for family flexibility in that multiple family members can live on the same lot in separate units. A family member living in an ADU also reduces the competition for the scarce inventory of affordable rental apartments in the community.

- 12 AARP Livable Communities, Creating Room for Accessory Dwelling Units (Nov. 2017), https://www.aarp.org/livable-communities/housing/info-2015/accessory-dwelling-units-model-ordinance.html.
- 13 Fla. Stat. § 193.703 (2018).
- 14 Id.

¹⁰ Gottlieb, supra note 2, at 627 (citing Robin Paul Malloy, Land Use Law and Disability: Planning and Zoning for Accessible Communities 3-5 (2015)).

¹¹ AARP Livable Communities, Making Big Sense of Small Homes (Aug. 2015) https://www.aarp.org/livable-communities/network-age-friendly-communities/info-2015/domain-3-accessory-dwelling-units-portland-oregon.html.

¹⁵ Gottlieb, supra note 2, at 646.

¹⁶ Jonathan Coppage, Accessory Dwelling Units: A Flexible Free-Market Housing Solution, R Street Policy Study No. 89 (Mar. 2017), http://www.rstreet.org/wp-content/uploads/2017/03/89.pdf.

Environment/Infill Development

For many communities, undeveloped land close to the city center is hard to come by. ADUs are a smart growth tool because they are typically infill units built where there is existing infrastructure, making greater use of the already developed land. When ADUs are built near employment centers, more people will have the opportunity to live closer to where they work – reducing transportation costs and the associated environmental impacts.

Additionally, as ADUs are smaller than single-family or even some multi-family units, their overall impact on the environment is also lessened. It takes less building material to construct an ADU and costs less in utilities for daily operation.

Integration of Income Levels

As the former Florida Department of Community Affairs, now known as, Department of Economic Opportunity, noted in its 2007 report to the Florida Legislature, ADUs can be integrated into a community resulting in the development of "mixed-income neighborhoods rather than enclaves of affordable housing."¹⁷ Integrating lower-income families within mixed-income areas can create positive benefits in terms of employment, mental health, and educational opportunities.¹⁸ With the creation of ADUs as infill development in single-family districts, lower-income households can enjoy a greater quality of life in areas of town which may have previously been closed off to them.

Workforce Housing Development

With ADUs, the lower paid workforce can live closer to their places of work. Rather than being forced to commute long distances for their jobs, people can live affordably within the community. Because ADUs do not require additional land, they can be incorporated into existing, built-out neighborhoods in parts of the community that are closer to employment centers. Proximity to employment can result in very substantial savings when it is possible for a two-person household to share one car and save the expense of owning a second car.

¹⁷ Fla. Department of Community Affairs, supra note 7, at 6.

¹⁸ Diane K. Levy et al., Effects from Living in Mixed-Income Communities for Low-Income Families, Urban Inst. (Nov. 2010), https://www.urban.org/sites/default/files/publication/27116/412292-Effects-from-Living-in-Mixed-Income-Communities-for-Low-Income-Families.PDF.

The Value of ADUs

ADUs provide an affordable housing alternative by tapping into Florida's large stock of single-family homes. Changing demographics make ADUs an attractive alternative to the elderly, persons with disabilities, families in transition, and to others needing safe, decent housing.

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Affordability

Accessory dwelling units are a valuable affordable housing tool for low- and moderate-income individuals. Because they do not require additional land or major new infrastructure, ADUs are cheaper to build than the traditional single-family home. Further, the rental income from the ADU can subsidize the cost of the primary unit – making ADUs an affordable housing tool for both the renter and the homeowner. When both households are spending less of their income on housing, quality of life is improved, and more money is invested in the broader local economy.

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Care for the Elderly & Persons with Disabilities

An ADU can be utilized so that an elderly or disabled individual who wishes to remain in their home can stay in their house and have their caregiver reside in the ADU, or vice versa. Elderly and disabled individuals often struggle to live comfortably due to the traditional ways in which communities are planned. For these folks, ADUs can provide an opportunity to live on the same lots as their parents or other caregivers.

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Family Flexibility

ADUs can also provide for family flexibility. If a young adult is not financially able to move out and wants to maintain a semblance of independence, he or she can live in an ADU on the same lot as their parents – coming and going as they please and entertaining their own guests, while remaining tightly bound to their family.



Environment/Infill Development

For many communities, undeveloped land close to the city center is hard to come by. ADUs are a smart growth tool because they are typically infill units built where there is existing infrastructure, making greater use of the already developed land. When ADUs are built near employment centers, more people will have the opportunity to live closer to where they work – reducing transportation costs and the associated environmental impacts.



Integration of Income Levels

As the former Florida Department of Community Affairs noted, now the Florida Department of Economic Opportunity, noted in its 2007 report to the Florida Legislature, ADUs can be integrated into a community resulting in the development of "mixed-income neighborhoods rather than enclaves of affordable housing." Integrating lower-income families within mixed-income areas can create positive benefits in terms of employment, mental health, and educational opportunities.



Workforce Housing Development

With ADUs, the lower paid workforce can live closer to their places of work. Rather than being forced to commute long distances for their jobs, people can live affordably within the community. Because ADUs do not require additional land, they can be incorporated into existing, built-out neighborhoods in parts of the community that are closer to employment centers.



III. ADUs in Florida: Regulatory Barriers and Practical Solutions

This section describes some of the barriers to ADU development and offers solutions to overcome these barriers. Most of the barriers relate to local land development regulations. There may be aspects of a local government's land development regulations that are so restrictive that few permitted ADUs can be built.¹⁹

As of this writing, 16 of the 67 Florida counties did not address any accessory dwelling unit – a guest house, accessory apartment, ADU, cottage house, and other similar units -- in their land development codes. For the remainder of counties that did address some type of ADU, most of them had onerous use restrictions. Of the counties that mentioned a type of ADU, at least 25 of them explicitly bar their use for long-term rental purposes or for use by persons that are not an immediate family member or worker. Only 20 counties speak of ADUs as a tool for long-term rental housing. Virtually all counties, except for a few, require the owner to occupy the principal dwelling if the ADU is used. One county requires lot sizes to be above 15,000 square feet before allowing an ADU. Further, at least 12 counties explicitly do not allow ADUs to be built in single-family zoning districts. Several jurisdictions allow ADUs only as a conditional use. These types of barriers have the effect of restricting the ADU as a tool for affordable housing development.

Florida cities tend to have more flexible ADU ordinances than counties. Of the 15 most populous cities in Florida, 11 of them explicitly allow ADUs in single-family districts (one of these cities only allows ADUs on a conditional use basis). Although Florida cities allow ADUs more broadly, issues exist regarding minimum lot size, ADU size, parking, owner-occupancy, and other standards. ADU regulations should be as flexible and open as possible to give landowners the freedom to utilize their property as a site for affordable housing development. If restrictions are too burdensome, landowners will be deterred from building ADUs to the community's detriment.

HIGHLIGHTS

Most regulatory barriers to ADUs deal with local land regulations. This section explores those barriers and provides practical solutions to get beyond them.

This section will discuss and offer recommendations for:

- Euclidean Zoning & the Single-Family District
- Owner-Occupancy Restrictions
- Long-Term Rental Use Restrictions
- As-of-Right versus Conditional Use
- Size, Density, & Other Structural Requirements
- Utility Hookup Requirements

¹⁹ Kol Peterson, Backdoor Revolution 135 (Accessory Dwelling Strategies, LLC 2018).



Barrier:

Euclidean Zoning: premise of separation of incompatible uses by zoning restriction

Solution:

F.S. 163.1777: ADUs are compatible with single family residential uses. Allow ADUs in all single-family districts.

Barrier:

ADUs permitted but overly restricted as to become impractical or impossible

Solution:

Reduce minimum lot size and amend setback and other structural requirements to allow the most possible lots to contain ADUs

Barrier:

ADUs not included as an allowable use in land development codes

Solution:

Incorporate ADUs into land use regulations by adoption of ADU specific ordinance

Barrier: Requirement for property owner to occupy the principal residence

Solution: Allow property owner to occupy the ADU by right Barrier: Prohibition of ADU for long-term rental

Solution: Allow ADUs to be rented on the long-term market

Barrier: Excessive minimum lot size requirements **Solution:** Lower minimum lot size requirements

Barrier:

Residential land uses are based on density (dwelling units/acre). When ADUs are counted as a dwelling unit the parcel might be over density and the ADU may be disallowed.

Solution:

Exempt ADUs from density calculations

Barrier:

Prohibition of non-family members from occupancy

Solution:

Allow ADUs to be rented on the long-term market to any tenant

Barrier: ADUs permitted only as conditional use

Solution: Allow ADUs as a permitted use

Barrier:

Parking requirements that may render development impractical

Solution:

Require off-street parking only if on-street parking is not available within a certain number of feet from the parcel. If off-street parking is required, utilize stacked parking (one car in front of the other) or other design solutions to allow parking in areas other than designated driveways.

Barrier:

New construction ADUs are assessed an impact fee comparable to a multi-family dwelling unit.

Solution: Waive or modify impact fees for ADUs

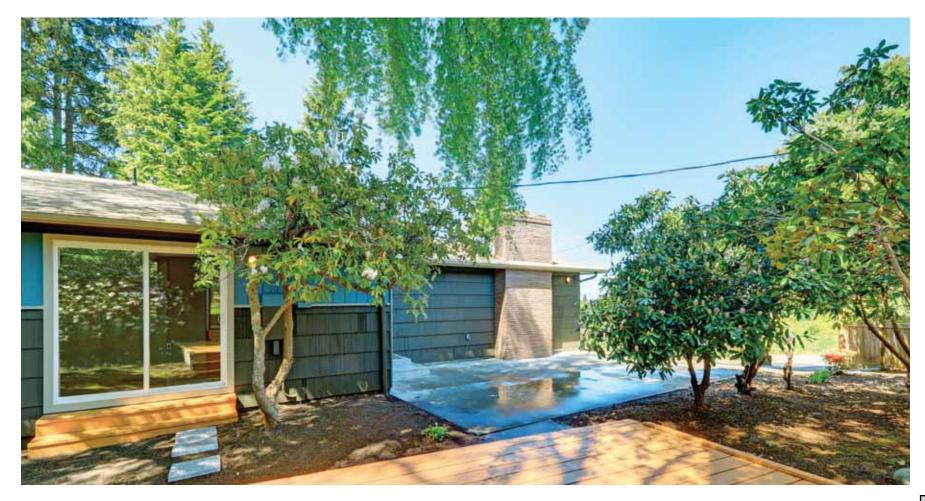
Market Type Barriers

Barrier: Perception that ADUs decrease property values

Solution: Educate residents that ADUs do not decrease property values and may increase these values.

Barrier: Vacation Rental concerns

Solution: Enter into agreements with homeowners that receive governmental incentives to rent ADUs on the long-term market



Euclidean Zoning and the Single Family District

Certain zoning and land use regulations can be detrimental obstacles to ADU development. Traditional "Euclidean" zoning separates what are thought of as incompatible land uses from being on nearby or the same lots.²⁰ For example, a local government may not consider a smaller, second housing unit to be compatible with a traditional single-family land use designation. This type of policy is a barrier to ADU development. As evidenced by the Florida Legislature²¹, ADUs are compatible with single-family homes. Local governments should treat them as such.

A neighborhood zoned as Single Family Residential, for example, would generally allow only one single-family dwelling unit per lot. Historically, without explicit allowances for ADUs, if two or more residences are situated on a single lot, they would need to be in a more intensive residential zone, such as one that permits duplexes or multi-family housing. Today, some single-family zoning districts may permit an accessory dwelling unit but mandate that certain requirements are met or that special circumstances be shown to warrant the use.

Accessory dwelling units should be permitted in all single-family zone districts. As mentioned in the above section describing the need for ADUs, as of 2015, 64% of occupied units in the state of Florida were single-family homes. However, traditional single-family zoning procedures no longer fit the needs of the newer generations of our communities as more young people are looking for smaller, affordable places to live with access to opportunity.²² These same zoning procedures restrict the needs of Florida's growing elderly population – a population that could use ADUs and other smaller units to help them age in place. ADUs capitalize on the dominance of the single-family home by providing an additional family or person's access to an affordable dwelling unit on the same lot – typically in areas of our communities that are closer to centers of opportunity. A regulatory atmosphere that increases the number of ADUs will bring a positive impact to Florida's housing stock and to our communities.²³

Barring ADUs from single-family districts severely curtails their prevalence from the outset. If local governments are concerned about ADUs changing the character of the single-family district, they should consider reasonable minimum lot size, setback requirements, or other reasonable structural regulations rather than an outright ban. Allowing ADUs in single-family districts is a necessity if the benefits of ADUs are to be realized. As already noted, many house-holds believe they need ADUs for economic or family reasons. If ADUs are not permitted, some households may erect them without pulling building permits and create potentially serious life and safety hazards for themselves and their neighbors. A local government that provides sensible ADU regulations is likely to be protecting the welfare of the community.

Recommendation

/•// Allow ADUs as a permissible use in all single-family districts.

- I FIA. Stat. 8 105.51771 (2010).
- 22 Gottlieb, supra note 2, at 633.
- 23 See David Garcia, ADU Update: Early Lessons and Impacts of California's State and Local Policy Changes, UC Berkeley Terner Ctr. for Hous. Innovation (Dec. 2017).

Owner-Occupancy Restrictions

Much has been written about the dangers of a strict owner-occupancy requirement for accessory dwelling units. A strict policy may dis-incentivize ADU development and foreclose many of the benefits they provide.²⁴ Many jurisdictions in Florida currently require that the owner occupy the primary unit if an ADU is used on the property. Others require that the ADU only be used by family members or non-paying guests. Some, however, are more flexible and allow the owner to occupy either the primary unit or the ADU.

By allowing homeowners to live in the ADU and rent out the primary dwelling, local governments grant them the option to earn more income on the primary unit and gain additional flexibility in their living arrangements.

Some cities do not require owner-occupancy at all. Portland, Oregon is one of those cities. Just as local governments do not mandate that all homeowners be on the property of single-family homes that they rent out, Portland and others take the position that local government should not mandate that owners live on the property of ADUs that they rent.

Local governments and communities may fear that a lack of restriction on owner-occupancy requirements may cause neighboring owners of single-family homes to object to having renters in their neighborhood. Communities may perceive a threat to their property values if some lots have two houses where only one is used by the homeowner. However, the addition of a lawfully permitted ADU may increase a property's value – as there is an additional unit for the homeowner to rent out for income. There are also reasonable concerns that without the homeowner present in the primary unit, ADU development may cause unwanted nuisances.

Requiring an owner to be on site may discourage ADU development by negatively impacting that homeowner's flexibility to rent their property and ultimately sell their property. If there are strict owner-occupancy requirements, a homeowner may be forced to sell their entire property instead of having the option to separately rent out the units. If a homeowner is unsure of the return on their investment before building an ADU because of the possible effect of owner-occupancy requirements, they might not build an ADU at all.

Recommendations_

- An owner-occupancy requirement should be flexible enough to encourage ADU creation. At a minimum, the owner should be allowed to occupy the ADU.
- Resolve community concerns through other land use controls and code enforcement mechanisms that are less onerous than owner-occupancy
 restrictions. Minimum lot sizes, setback requirements, and other land use controls can work to ensure that areas with ADUs are in keeping with
 the character of the community.

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Long Term Rental Use Restrictions 1200

In our survey of Florida counties, of the counties that regulate accessory dwelling units in some fashion, at least 22 do not allow ADUs to be rented longterm. These counties only allow ADUs for temporary guests, family members, caretakers, laborers, and in conjunction with certain commercial, industrial, or agricultural uses. ADUs are explicitly allowed to be rented as long-term units in only 21 counties.

lecommendations:

- Allow accessory dwelling units to be rented to whomever the homeowner chooses to live in the ADU.
- Allow accessory dwelling units to be rented long-term.

As-of-Right vs. Conditional Use

Another barrier to ADU development occurs when ADUs are only allowed as a conditional use rather than "as-of-right." If an ADU is a conditional use, a public hearing is required, and the local government undergoes a discretionary review to determine if the ADU can be constructed in a particular area. While a required public hearing may be good for educating the public on the impacts of ADU development and for providing a forum for neighborhood input, the onerous, unpredictable, and costly nature of the conditional use process may discourage homeowners from constructing ADUs. When allowed as a permitted use, the development review process is more predictable, as requirements are established up-front.

In a typical conditional use process, the homeowner may spend thousands of dollars on application fees, designs, and other requirements, and may still not be approved to add an ADU. As it is, when ADUs are rented at market-rate value, it may take years for the homeowner to break even on their investment. With the additional time and monetary burden of the conditional use process, homeowners may be dissuaded from constructing ADUs entirely or choose to construct illegal ADUs.

Recommendations

- Allow ADUs as a permitted use in all single-family residential land use classifications.
- To encourage ADUs as a tool to increase the housing stock, establish transparent and predictable requirements as opposed to a conditional use process that may be too unpredictable.

Size, Density, and Other Structural Requirements

Minimum lot size, setbacks, and other structural requirements can be used to achieve a compromise with neighborhood concerns about ADU development. Each area of the state is different and providing a one-size-fits-all policy in this area will not be feasible.

1. Minimum Lot Size

There is one county in Florida that requires a parcel of land to be a minimum of 15,000 square feet for a homeowner to lawfully construct an ADU. This effectively bars ADU development on many single-family lots. Austin, Texas, for example, changed its code in 2015 to reduce the minimum lot size requirements from 7,000 square feet to 5,750 square feet. This increased the number of lots that could have an ADU by 8,900.²⁵

Recommendations

 Local governments should study the current single-family home lot sizes of their jurisdiction and taken with public input, reach a solution that satisfies residential concerns while also allowing ADUs to flourish broadly. Minimum lot size requirements should be constructed to allow the most possible lots to contain a lawful ADU.

2. Size

In determining the allowable size of an ADU, most local governments regulate by reference to the ADU being a set maximum percentage of square footage in comparison to the primary unit. Maxing the size limit of an ADU in relation to the primary unit may have the effect of restricting the use of ADUs on smaller single-family lots. For example, if a local government restricts the size of an ADU to no more than 25% of the principal and a principal unit is 1,750 square feet, the ADU could only be roughly 440 square feet in size. This would not be enough for a two-person household to occupy the ADU safely and comfortably.

From our study of ADU ordinances and of ADU advocates across the country, it is recommended that there be around 400 square feet of living space per person. Therefore, to target ADUs as a tool for long-term affordable rental housing, a maximum square footage requirement should be from 800-1200 square feet. For sizable lots that can contain a larger ADU, local governments should make allowances for a larger unit.

Recommendations:

• Use a set number of allowable square footage rather than a rule that mandates the ADU be a certain proportion of the primary unit.

25 Tyler Whitson, Council Loosens Rules on Accessory Dwelling Units, Austin Monitor (Nov. 20, 2015), https://www.austinmonitor.com/stories/2015/11/council-loosens-rules-accessory-dwelling-units/.

• Allow ADUs up to 1,200 square feet with additional size allowances depending on lot size.

3. Density

Residential land uses are based on density. If ADUs are counted in the density calculation, this may push the parcel over the density restrictions for a particular zone and disallow an otherwise lawful ADU from being built.

Recommendations

Exempt ADUs from density calculations.

4. Setback Requirements

Any restriction on physical locational density should be dictated by setback and minimum lot size requirements. Setback requirements are a tool local governments can use to forge a compromise between neighboring landowners that may be concerned about ADU development. As with other structural regulations, setback requirements should not be designed in a manner that discourages ADU development. If a setback requirement is too stringent, the homeowner may be forced to build a smaller ADU and miss out on the opportunity to use it as a long-term rental for a two-person household. Most counties in Florida simply require the ADU to satisfy the setback requirements of the principal dwelling. Some local governments have different setback rules depending on if the door of a detached unit faces a side street or other properties. These are reasonable offerings.

Recommendations

- For maximum flexibility in setback standards, consider zero-lot line configurations in which an ADU would be allowed up to, or very near to, the edge of property lines.
 - To ensure smaller lots are not inadequately burdened by setback requirements, utilize variance procedures to amend certain setback rules.

Jtility Hookup Requirements

Requiring an ADU to hookup to its own water, sewer, or other utility may be overly burdensome and deter lawful ADU development. Local governments can facilitate an application to attach to the primary unit's utilities to save the homeowner thousands of dollars in costs.

Recommendations^{DC}

• Allow the ADU to file an application to connect to the utilities of the primary residence.

Parking Requirements

Parking requirements can be particularly burdensome to ADU development and if too stringent, may serve to discourage the construction of ADUs. Parking spaces may be very costly for a homeowner and are a challenge from a planning perspective. For smaller lots, a requirement for additional parking could render an ADU impractical – as a lot may not have enough space for both an ADU and a parking spot. These spots can cost thousands of dollars to construct – pushing the costs on to the renter and lowering the prospects for an ADU to be used as an affordable unit.

One local government in Florida does not require a parking space for ADUs that are 500 square feet or less. One county reduces parking requirements for multifamily developments that have units of 900 square foot or less. These are good compromises if residents are concerned with onstreet parking congestion. California has a law stating that local governments may not impose parking requirements for an ADU if the ADU is located "within one-half mile of public transit," is "part of the existing primary residence or an existing accessory structure," or when "on-street parking permits are required but not offered to the occupant of " the ADU or if "a car share vehicle [is] located within one block" of the ADU.²⁶ Most county ordinances in Florida that mention parking requirements have a "one spot per ADU" requirement.

In all likelihood, ADUs will be dispersed throughout neighborhoods – they will not be centered on one particular street. Therefore, it is likely that onstreet parking could satisfy the parking needs of an ADU without overly congesting the neighborhood and without burdening the homeowner with the costs of an additional parking space. Alternatively, design solutions might be considered to provide additional parking. For instance, stacked parking spaces (one in front of the other) or allowing parking in other areas of the parcel (not just the driveways) can be considered. If parking is a genuine issue, the local government should still avoid a "one spot per ADU" rule and consider requiring parking for locations where it may be impractical to park on the street. It is important to strike a balance between the cost burden placed on homeowners and genuine street congestion concerns.

Recommendations

- When devising parking requirements, study the impact that permitted ADUs have on the parking supply. A blanket "one spot per ADU" rule without an impact study may hinder ADU development. For example, require one off-street parking spot only if there is no available on-street parking within a certain number of feet from the parcel.
- If one parking space is generally required, consider exempting ADUs 500 square feet or less.
- After successful implementation of an ADU ordinance, continually monitor parking impacts to assess congestion concerns.



IV. Funding and Incentivizing ADU Development

Local governments have the tools to assist in funding and incentivizing ADU development. This section provides some ideas about how local governments can help homeowners create ADUs. As discussed throughout this Guidebook, ADUs are an excellent tool to expand and diversify a community's housing stock. To increase their prevalence, communities should consider ways to incentivize ADU development.

Impact & Applicant Review Fees

The current standard practice in Florida for assessing impact fees on an ADU is to charge the unit as a multi-family unit. If a homeowner is required to pay the same impact fee for their ADU as a developer would pay for a multi-family unit of any size, the homeowner may be discouraged from ADU development. Further, if a homeowner is required to pay the same impact fee for a 500 square foot as an 800 square foot ADU, a homeowner may be inclined to construct the larger unit instead – deterring a smaller, lower-priced ADU from being built.

A solution offered by Hillsborough County, provides for a fixed "de minimus" impact fee of \$100. If not used for long-term affordable housing and if the local government does not want to waive impact fees entirely, ADUs should be assessed by square-footage rather than by unit.²⁷ With an assessment by square-footage, a developer of a smaller ADU would pay less in impact fees than a developer of a larger ADU. Any waiver or reduction of impact fees can be paid for by the local government's affordable housing fund or other revenue sources.

Local governments can also streamline the review and permitting process to save itself administration costs and save the homeowner both time and money. By streamlining and removing certain development review processes, the cost of development should go down. For example, Leon County passed an ordinance in 2016 that eliminated several steps in the development review process which saved applicants a minimum of \$1,697 in permitting fees.²⁸ Additionally, this Ordinance had the planned effect of reducing ADU approval time by more than 45%. Similar expedited permitting processes should be considered in every local government.

HIGHLIGHTS

Local governments have the tools to fund and incentivize ADU development. Waiving impact fees and providing financial assistance can be the key to establishing ADUs.

This section will offer insight on:

- Impact & Applicant Review Fees
- Financial Assistance
- Marketing the ADU Option to Homeowners

²⁷ See Florida Housing Coalition, Affordable Housing Incentive Strategies: A Guidebook for Affordable Housing Advisory Committee Members and Local Government Staff, available at http://www.flhousing.org/wp-content/uploads/2012/03/AHAC-Guidebook-2017.pdf.

²⁸ Leon County, Florida Board of County Commissions Regular Meeting Minutes 360 (May 10, 2016), available at http://cvweb.clerk.leon.fl.us/finance/board_minutes/minutes/pdfs/20160510%20Official%20Minutes.pdf.

Recommendations

- Waive or otherwise modify impact fees for ADUs that are used for long-term affordable housing or charge a "de minimus" impact fee rate of \$100.
- If not used for long-term affordable housing, assess impact fees.
- Another possible, but less desirable alternative, is to charge an ADU in the same impact fee category as a mobile home.
- Streamline and create transparent ADU development processes to the greatest extent possible to lower administration and development costs.

Financial Assistance

Homeowners who want to create an ADU may not have all the funds they need to build the unit. Through the SHIP program, local governments could explore the possibility of establishing an affordable housing strategy to provide a subsidy for ADUs for very-low, low-, or moderate-income households. The subsidy would be secured with a recorded lien on the rental property to ensure than an affordable rent is charged for a period of at least 15 years. Residents of the ADUs would be income certified yearly. Local governments should be able to loan funds to homeowners for the construction of ADUs if the homeowner utilizes the ADU for long-term affordable housing. A loan program for creating ADUs that has a long history of implementation is found in Santa Cruz, California.

To assist homeowners develop rental ADUs for persons at 80% or below the City's median household income, the City of Santa Cruz, California has an ADU loan program by which homeowners can receive loans of up to \$100,000 at a 4 ½% interest rate for ADU construction.²⁹ The County of Santa Cruz, California allows for forgivable loans of up to \$40,000 at a 3% interest rate.³⁰ To receive the financing at the City level, the homeowner must agree to keep the rental unit affordable to low-income tenants for a period of at least 15 years. At the County, the homeowner must enter into a deed restriction for a period of 20 years that keeps the ADU or main house at a cost affordable to low-income households. If the homeowner backs out, they must repay the full amount of the loan plus interest. With loan and deed restrictions and the threat of default, local governments can ensure that ADUs they assist financially are used for long-term affordable rental housing for low- to moderate-income persons.

Recommendations

• Develop a program which loans funds to homeowners who agree to keep their ADU affordable to lower-income tenants. These funds can be derived from the local government's affordable housing funds. Upon repayment, these funds can be recycled for the ADU program or used for other affordable housing purposes. Local governments can be creative in how to raise additional revenue for their affordable housing funds to help finance ADU development.

²⁹ City of Santa Cruz, CA, Accessory Dwelling Units: Loan Program, http://www.cityofsantacruz.com/Home/ShowDocument?id=3700.

³⁰ County of Santa Cruz, CA, Accessory Dwelling Unit Forgivable Loan Program (Apr. 2018), available at http://sccoplanning.com/Portals/2/County/adu/Forgivable%20Loan%20Program.pdf.

Marketing the ADU Option to Homeowners

If a local government allows ADUs by right in all single-family zones or otherwise makes positive changes to facilitate the development of ADUs, the next critical step is to ensure that developers and homeowners are aware that they now have the option of building ADUs. An advertising campaign to educate the community about the benefits and the process for building ADUs is a key component for increasing the stock of ADUs.

Building an ADU may be one of the largest projects a homeowner undertakes on his or her property. Further, most homeowners may be unfamiliar with what it takes to build an ADU on their lot. Therefore, local governments could provide educational materials to ease the learning curve for homeowners interested in ADU development. This may include an easy-to-navigate checklist of the application development review process, development cost projections, zoning and land use regulations, and ADU design considerations.

The City of Santa Cruz, which proves to be a model for ADU regulation across the country, provides an ADU manual and a set of ADU design prototypes to encourage development.³¹ The manual connects homeowners to local architects with ADU construction experience. These materials make it easier for homeowners to construct ADUs. The current design prototypes manual offers seven working drawings by local architects to be used as templates by homeowners. The ADU manual contains a step-by-step guide on how to plan, design, and obtain permits for an ADU. Appendix A of this Guidebook contains a template Manual for local governments to use to educate homeowners.

Recommendations

- Provide user-friendly brochures and information to homeowners on the benefits of ADUs and the rules and regulations that apply to ADUs.
- Provide education on what financial resources are available to assist in developing an ADU.
- Connect homeowners to local architects with ADU expertise.
- Provide education on how to manage an ADU including landlord tenant laws, leasing, and maintenance.

³¹ City of Santa Cruz, CA, ADU Prototype Architects, http://www.cityofsantacruz.com/government/city-departments/planning-and-community-development/programs/accessory-dwelling-unit-development-program/adu-prototype-architects.



V. Concerns Over ADUs as Short-Term Vacation Rentals & Student Housing

There are justifiable concerns about the use of ADUs as short-term vacation rentals. Some critics argue that the use of ADUs for Airbnb and other vacation rental platforms poses a serious threat to their beneficial use as long-term rental units, places for elderly housing, and family flexibility. The proliferation of short-term vacation rentals may negatively affect the supply of long-term affordable housing for residents of the community.

As of this writing in 2019, local governments may not create a new law, ordinance, or regulation prohibiting vacation rentals or regulating the duration or frequency thereof.³² This statutory provision, however, does not apply to any local law, ordinance, or regulation adopted on or before June 1, 2011.³³ Thus, unless already placed in a local government's code before this grandfathered date, a local government may not prohibit ADUs as short-term vacation rentals through the zoning code. Local governments can, however, regulate short-term rentals through life safety and building codes.

For the past several Legislative sessions (including the 2019 Session), there have been bills to preempt local governments from regulating short-term rentals altogether.³⁴ Thus, local governments should be tuned in to how they may or may not regulate short-term vacation rentals.

Options for Local Governments to Regulate the Use of ADUs

One way to overcome the short-term vacation rental preemption, is by providing local government assistance that comes with a land use restriction agreement to ensure that ADUs are used for affordable housing. Land use restriction agreements, also known as deed restrictions, can be an important tool if the ADU is built using governmental assistance or through a modification of impact fees. For example, a local government could condition the reduction of impact fees on an ADU's use as a long-term affordable housing unit. In this scenario, if the ADU is used for short-term vacation rental, the homeowner will have violated the deed restriction and will have to repay the full cost of the impact fees, and perhaps suffer additional consequences imposed by the local government.

33 ld.

34 Fla. HB 987 (2018), available at https://www.flsenate.gov/Session/Bill/2019/00987; Fla. SB 1400 (2018), available at https://www.flsenate.gov/ Session/Bill/2018/01400.

HIGHLIGHTS

The increasing number of short-term vacation Airbnb and similar platforms can increase community concerns about the viability of long-term ADU rentals. While ADUs can be used as short-term rentals, through deed restrictions, local governments can require an ADU to term rental if the unit fee modifications or other financial

³² Fla. Stat. § 509.032(7)(b) (2018).



If not done already, local governments should enter into tax agreements with Airbnb and other short-term vacation rental platforms to recover Tourist Development Tax revenue. Under current law, local governments can only use this tax revenue for authorized uses. Affordable housing is not an authorized use. If the Tourist Development Tax statute is amended to allow local governments to use this revenue for affordable housing, they can use the tax revenue from short-term vacation rentals towards affordable housing purposes.³⁵ These rentals are booming, and local governments should be allowed to use this new stream of revenue for affordable housing. For example, in 2017, Broward, Brevard, Hillsborough, and Polk County received \$1.87 million, \$419,000, \$562,000, and \$610,000 in tax revenue from Airbnb, respectively.³⁶ If local governments are concerned about the proliferation of ADUs as short-term vacation rentals (and in regards to affordable housing broadly), they should be able to use the tax revenue from vacation rentals for incentivizing affordable long-term ADUs in the form of loans, reduction of impact fees, and other costs associated with development. Legislation amending the Tourist Development Tax statute would allow local governments to address this issue.

Ultimately, although strict owner-occupancy requirements are not advisable if the ADU is used for affordable housing, strict requirements can be necessary if the ADU is used as a shortterm vacation rental.

³⁵ See Fla. Stat. § 125.0104 (2018). The legislation would amend this statute to allow local governments to use revenue from a Tourist Development Tax for affordable housing purposes.

³⁶ Florida Trend, Airbnb Releases 2017 Florida Tax Report (Feb. 13, 2018), http://www.floridatrend.com/article/23942/airbnb-releases-2017-florida-tax-report.

VI. How to Combat Potential Neighborhood Opposition

The construction of new accessory dwelling units in single-family districts may bring neighborhood or community resistance. The owners of single-family homes may object to having renters in their neighborhood; they may fear increased traffic and parking, or perceive a threat to their property value.³⁷ The Not in My Backyard (NIMBY) syndrome connotes objections made to stop the development of affordable or otherwise new housing for reasons such as fear and prejudice.³⁸ NIMBYism presents an obstacle to a successful ADU regulatory structure and can result in fewer affordable housing options at a time when Florida is in desperate need of more rental housing.

Education Campaign

The first thing the local government should do to ease neighborhood opposition toward ADU development is to educate the community about the benefits of ADUs. The more informed the public, local government staff, and elected officials are about the need for affordable rental housing and how ADUs can ease that need, the more leverage advocates will have to advance the development of ADUs.

The local government should be equipped with current data about its specific needs for affordable housing and how ADUs can be used to help community members. Here are some of the questions the local government should consider:

- How many residents are cost-burdened?
- How many cost-burdened residents are forced to live far away from the places they work?
- How many of these cost-burdened residents are essential members of the lower-paid workforce, such as home health aides?
- How much of the community is zoned single-family?
- If ADUs were allowed in all single-family districts, how many new affordable rental units would be possible?

Anecdotal information about the successes of existing ADUs as sources of affordable rental housing, elderly and disabled care, and/or workforce housing can support this message.

In shaping the message, it is important to demonstrate that ADU development may not be best for everyone;

HIGHLIGHTS

Proposals to allow ADUs in single-family residential zoning districts may bring out neighborhood opposition. Local governments can ease community concerns through educational campaigns and by addressing legitimate objections.

This section will offer some solutions such as:

- Education Campaign
- Garner Support from a Broad Range of Interests
- Address All Legitimate Opposition

³⁷ Jaimie Ross, Avoiding and Overcoming Neighborhood Opposition to Affordable Rental Housing, Nat'l Low Income Hous. Coal. Advocates' Guide (2018), available at http://nlihc.org/sites/default/files/AG-2018/Ch02-S10_Avoiding-Opposition_2018.pdf.

Shape the Message

It is important to make clear that thousands of ADUs will not sprout up overnight from the successful implementation of an ADU ordinance.

- ADUs will not dramatically alter the landscape of existing neighborhoods
- ADU development will be relatively slow and scattered throughout communities
- Assure constituents that studies to assess the strengths and weaknesses of ADU development will be used to inform the decision-making process.

some people do not want to utilize their backyards for affordable rental housing. Some folks may only want to utilize their ADUs for family members, guests, or elderly housing and not have their ADUs on the public marketplace. Sensible ADU regulations would go a long way to help households help themselves to solve their own affordable housing problems by providing additional living quarters to family members. It is important to make clear that thousands of ADUs will not sprout up overnight from the successful implementation of an ADU ordinance.

The local government should share these points with the community and help residents understand that ADUs will not dramatically alter the landscape of existing neighborhoods. ADU development will be relatively slow, scattered throughout communities, and if a successful ordinance is implemented, local governments can assure their constituents that they will undergo a study to assess the strengths and weaknesses of ADU development.

The City of Boston, Massachusetts provides a good method by which to study ADU impacts. Several years ago, Boston began allowing what are called "micro-units" – units with a minimum size of 350 square feet -- in a limited area of the city. Simultaneously, the City teamed up with Harvard University's Rappaport Institute to study the impacts of the first batch of units.³⁹ Local governments in Florida might consider a similar type of study with University partners in Florida to measure the results of an ADU program.

Garner Support from a Broad Range of Interests

Local governments should partner with local organizations that are interested in affordable housing development. They should look for members of the business community, clergy, social services agencies, and others who are outspoken about the need for affordable housing and form partnerships to support ADU development. The media can also be a crucial ally. Local governments should contact the media so the public can better understand ADUs and their development processes, their public purpose, and the population served.

With these allies, the local government will be in a better position to convince their community that ADUs are a beneficial housing tool. For instance, nurses and public safety workers can attest to the need for housing closer to the places in which they work – a need which ADUs in single-family districts can address. Elderly individuals can describe how an ADU may have helped them age in place. With allies from a broad range of interests, more connections between ADU development and community concerns can be voiced.

³⁹ Casey Ross, Housing-Starved Cities Seek Relief in Micro-Apartments, Boston Globe (Mar. 26, 2013), https://www.bostonglobe.com/business/2013/03/25/micro-apartments-tight-squeeze-but-livable/vDRdMnChgdhCdFOrmupnyN/story.html.

Address All Legitimate Opposition

The key to overcoming community opposition to establishing a regulatory structure for ADUs is to address the community's legitimate concerns. The local government should be prepared to describe the numerous community benefits of ADUs and willingness to address legitimate concerns. For example, ADUs architectural and design compatibility with the neighborhood may be an issue. Local governments could include a modest and simple set of design guidelines to assure compatibility with the surroundings. For instance, the guidelines could deal with mass, scale, height, and site position of the ADUs to gain community support. Guidelines would make the overall design of the ADU more predictable and compatible with the principal structure and neighborhood.

Parking

Parking may be an issue a local government will need to address. Some community members may oppose ADU development specifically in terms of parking. However, requiring new parking may be too costly to homeowners looking to build an ADU. It is unlikely that 1) dozens of ADUs will sprout up overnight after implementation of a flexible code; and 2) even if they did sprout up overnight, it is unlikely they would all be located on the same block or in the immediate vicinity. As mentioned previously, the parking problem for ADUs in single-family areas can be solved through innovative design solutions. Local governments should be prepared to advocate for their methods.

The City of Orlando provides a potential compromise in this area. Orlando requires parking for ADUs 500 square feet or more but does not require parking to be built for ADUs less than 500 square feet. This solution was designed to encourage smaller units and in recognition of the complexity of building a new parking space on a parcel while meeting setback, maximum lot coverage, and other structural requirements.

Garner Support

Partner with local organizations interested in affordable housing such as:

- Business community,
- Clergy, and
- Social services agencies.

Contact the media to inform the public so that they can learn more about:

- How ADUs are developed,
- Their public purpose, and
- Populations served



VII. ADUs and Tiny Homes

Tiny homes are increasing in popularity; local governments may be asked how tiny homes and ADUs differ. ADUs and tiny homes have many similarities. Both are relatively small in size compared to traditional dwelling units, are flexible in where and how they are built, and cause relatively little impact on the environment and existing infrastructure. However, there are differences in the two housing types which require different rules and regulations from a zoning and land use standpoint.

Simply put, ADUs can be tiny homes and tiny homes can be ADUs. Yet, this is not always the case. Here are some main distinctions between the two housing types:

1. By Definition

By definition, ADUs are accessory to a primary unit and under the same ownership. An ADU cannot exist on a lot by itself. This contrasts with a tiny home which can stand on a lot independently. Because of this, local governments regulate the location, size, and structural requirements of tiny homes differently from ADUs.

A tiny home can be an ADU if built in the backyard of a single-family home and under the same ownership. An ADU can be considered a tiny home based the size of the unit. If a tiny home is built as a backyard unit, it will need to follow ADU regulations. Otherwise, local governments tend to regulate tiny homes separately.

2. Size

Tiny homes are generally smaller in size than the typical ADU. A tiny home is usually defined as a habitable structure of less than 500 square feet. This square footage definition depends on the jurisdiction. ADUs, by contrast, are typically up to 1,000 square feet or larger in some circumstances.

Thus, when local governments regulate stand-alone tiny homes without reference to a primary unit, they tend to max the size requirement at 400 or 500 square feet. If it is considered an accessory dwelling unit, the tiny home can be larger in size.

3. Mobility

One main distinction between the two housing types is that tiny homes can be built on wheels. Tiny homes on wheels (THOW) are typically allowed in areas zoned for mobile homes. If a tiny home is on wheels, it likely cannot be an ADU as local governments generally require ADUs to be on a foundation. THOWs will need to be registered with the Florida Department of Highway Safety and Motor Vehicles.

HIGHLIGHTS

ADUs and Tiny Homes are alternative housing solutions. ADUs are always accessory to the primary unit. Tiny homes can stand alone. As a result, different regulations apply.

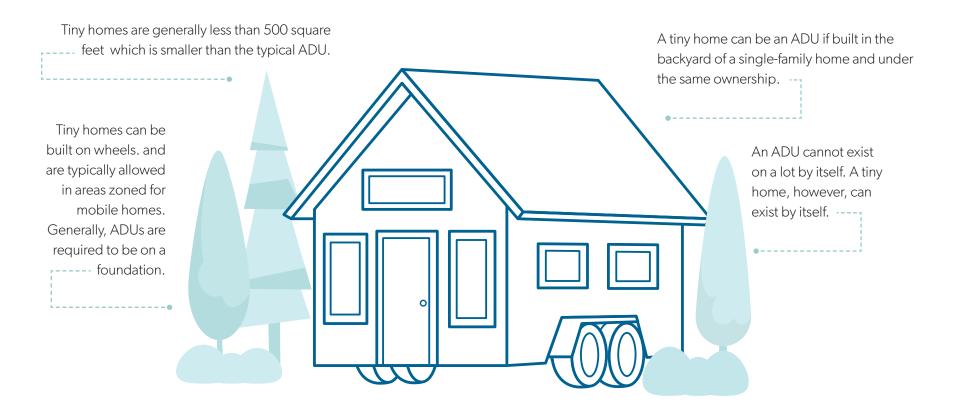
Tiny homes and ADUs differ by:

- Definition
- Size
- Mobility

If the tiny home is an on-site structure, it will be subject to the same zoning requirements as a single-family home, ADU, or clustered site, depending on the circumstances.

In sum, a tiny home can be an accessory dwelling unit and an ADU can be considered a tiny home. Different rules and regulations apply whether the tiny home is a backyard unit, whether it is a stand-alone unit, and whether it is on wheels. If a backyard unit, the tiny home will need to follow the relevant ADU regulations. If a tiny home is a stand-alone unit on a single-family site, multi-family cluster site, or on wheels within a mobile home park, different standards apply based on zoning districts and location.

A tiny home can be an accessory dwelling unit and an ADU can be considered a tiny home. However, different rules and regulations often apply.



VIII. Best Practices

Below you'll find best practices chart for a successful ADU program.

CATEGORY	BEST PRACTICES
Zoning	 Allow ADUs in all single-family districts as an accessory use Owner must occupy either the primary or accessory dwelling unit No rental restrictions No parking requirement if there is on-street parking available 375-1200 sq. feet with allowances for an increased maximum if lot a certain size Must meet district setback requirements Exempt from density calculations Shall connect to existing utility connections
Development Review, Fees, & Incentives	 Waiver of impact fees if used as affordable rental; if not, "de minimis" impact fee of \$100 or by square footage Streamlined and transparent permitting process ADU Loan Program for affordable rental construction w/funds from local housing trust or other revenue pool
Administration	 Monitoring system to study local ADU impact on parking, nuisances, property values, etc. Homeowner & Community Education program

HIGHLIGHTS

This section provides a best practices chart for a successful ADU program, including:

- Zoning
- Development Review, Fees, & Incentives
- Administration



IX. Model Ordinance

This Model Ordinance combines our findings with the recommendations as provided in Section 163.31771 of the Florida Statutes. Certain requirements will depend on the unique nature of each community. This Model Ordinance contains the baseline of requirements to ensure an ADU-friendly regulatory structure. Local ordinances may contain greater or fewer requirements than what is provided here. At minimum, local governments should allow ADUs in all single-family districts and adhere to owner-occupancy flexibility regulations.

After creating an ADU regulatory structure, it is essential for the local government to have a system in place to track the total number and location of each permitted ADU. For an ADU system to work, the local government ought to continuously monitor the progression of the program.

The numbers provided here, especially in reference to lot size and size of the ADU overall, are reflective of what are considered best practices. Fundamentally, when devising an ADU ordinance, it is essential that local government regulations do not hinder the potential of ADUs as a source of affordable housing.

Accessory Dwelling Units

- (a) Purpose The intent and purpose of this section is to allow accessory dwelling units to be permitted in all single-family districts and other zone districts as ______ (City/County) finds necessary. It is also the intent and purpose of this section to create a regulatory framework that encourages the development of accessory dwelling units that are rented on the local housing market to members of the community. ______ (City/County) adopts the view of the Florida Legislature as stated in Section 163.31771 of the Florida Statutes pertaining to the need to encourage the permitting of accessory dwelling units in single-family residential areas in order to increase the availability of affordable rentals for extremely-low-income, very-low-income, low-income, or moderate-income persons.
 - (1) Accessory dwelling units are intended to provide additional housing that is incidental to a primary use. Accessory dwelling units are intended to be used as a necessary smart growth tool to increase the supply of affordable housing, elderly and disabled care units close to family members and caretakers, and/or workforce housing development. Accessory dwelling units are unique housing tools that provide for infill development with low environmental impacts that can connect to existing infrastructure.

HIGHLIGHTS

This section includes a Model Ordinance with baseline requirements to ensure an ADUfriendly regulatory structure.

- (2) With surging housing costs and lack of affordable housing stock, accessory dwelling units capitalize on the prominence of the single-family home by providing an additional family or persons access to an affordable dwelling unit on the same lot typically in areas of our community that are closer to areas of greater opportunity. Creating a regulatory atmosphere that encourages increasing the number of accessory dwelling units will have a positive impact on our community's housing shortage and on the property rights of homeowners.
- (3) These standards are devised to ensure that the development of accessory dwelling units do not cause negative impacts on the character or stability of single-family neighborhoods.

(b) Definitions

- "Accessory dwelling unit" means an ancillary or secondary living unit that has a separate kitchen, bathroom, and sleeping area existing within the same structure, or on the same lot, as the primary dwelling unit. The accessory dwelling unit may be a separate and detached unit, an attached unit to the principal structure, a repurposed existing space within the principal structure, an apartment over a garage, or a similar structural form.
- (2) "Affordable rental" means that monthly rent and utilities do not exceed 30 percent of that amount which represents the percentage of the median adjusted gross annual income for extremely-low-income, very-low-income, low-income, or moderate-income persons.
- (3) "Lot requirements" means restrictions on lot size, setbacks, building coverage, and similar zoning requirements.
- (4) "Short-term rental" means the rental of a primary or accessory unit for thirty days or less.

(c) Standards

- (1) Accessory dwelling units are to be permitted as accessory uses to single-family homes in all residential districts and all other districts as _____ (City/County) deems necessary.
- (2) Unless the accessory dwelling unit is used as a short-term rental, the owner must occupy either the principal or accessory dwelling unit.
 - (A) If used as a short-term rental, the owner must occupy the primary unit.
- (3) No more than one accessory dwelling unit shall be allowed on any residential lot or within any principal nonresidential structure.
- (4) An accessory dwelling unit may be constructed with or after the construction of the primary unit.
- (5) The establishment of a new accessory dwelling unit shall only be allowed if the lot area of the principal building is at least 5,000 square feet.
- (6) The accessory dwelling unit shall be subordinate to the principal building as to location, height, square footage, and building coverage. The design of the accessory dwelling unit shall be uniform, compatible, or complementary in appearance to the primary residence.
- (7) The floor area of the accessory dwelling unit shall be no less than 300 square feet and no greater than 1,200 square feet. A variance to increase this amount may be requested provided that the total building coverage does not exceed district standards.

- (8) All accessory dwelling units shall meet the applicable zoning district setbacks. Total building coverage on the lot shall not exceed district standards. The accessory dwelling unit shall comply with the requirements of all applicable housing or buildings codes.
 - (9) No additional parking spaces are required if there is on-street parking available within ______ feet of the parcel. If there is no on-street parking available, one off-street space is required unless the ADU is 500 square feet or less.
 - (10) Accessory dwelling units are exempt from zone district density calculations.
 - (11) The accessory dwelling unit may connect to existing water, sewer, and other existing utility connections.

(d) Development Review Procedures

- (1) Applications for accessory dwelling unit development shall be streamlined to the greatest extent possible.
- (2) Applicants may seek a variance from all structural and lot requirements.

(e) Impact Fees

- (1) If used for affordable rental, impact fees shall be waived. An application for a building permit to construct an affordable rental must include an affidavit from the applicant which attests that the unit will be rented at an affordable rate to an extremely-low-income, very-low-income, low-income or moderate-income person or persons. (City/County) will enter into deed restrictions or other agreements as necessary to ensure that the ADU is used for affordable housing purposes.
- (2) If not used for affordable rental or the application does not include an affidavit which attests to the accessory dwelling unit as an affordable rental, impact fees will be assessed at a "de minimis" impact fee of \$100.



X. Examples of ADU Policies in Florida

Orlando

The City of Orlando recently adopted an ADU ordinance with a clear intent to promote the use of ADUs. The ordinance allows ADUs in all single-family districts, does not require parking if the ADU is 500 square feet or less, and does not have a strict owner-occupancy requirement. The staff report presented in support of the ordinance demonstrates the local government's understanding of ADUs as a tool for affordable housing and the need to create a regulatory atmosphere that encourages their use.⁴⁰ The staff report includes an excellent description of the benefits ADUs provide, a survey of comparative local governments and their ADU policies, and a comprehensive analysis of how the new ADU ordinance lessens the land-use restrictions on local governments.

Elements of the Ordinance⁴¹:

- Type of Use: Accessory
- Zone Districts Allowed: All residential districts as well as mixed use and office districts.
- Size: Maximum of 50% of the size of the principal unit and can be no larger than 1,000 square feet.
- Minimum Lot Size: Correlated with the size of the ADU and depends on the zoning district. Residential districts require a lot size of a minimum of 5,500 square feet for an ADU of up to 500 square feet and 8,250 square feet minimum for an ADU of up to 1,000 square feet.
- Parking: No required parking for ADUs of 500 square feet or less. One additional off-street parking space is required for ADUs above 500 square feet.
- Owner-Occupancy: Not explicit in the ordinance.

Pinellas County

Pinellas County's ordinance has an important element that is worth showcasing: ADUs are exempt from density calculations. This is a best practice as it allows more single-family lots to construct lawful ADUs. Further, Pinellas County allows the owner of the property to occupy either the primary unit or ADU. This flexibility in owner-occupancy is essential to a successful ADU Ordinance.

HIGHLIGHTS

This section provides examples of ADU policies.

Examples are from the following jurisdictions:

- City of Orlando
- Pinellas County
- Alachua County

⁴⁰ City of Orlando, Staff Report to the Municipal Planning Board, LDC Amendment – Accessory Dwelling Units (ADUs) (May 15, 2018), available at http://www.cityoforlando.net/city-planning/wp-content/uploads/sites/27/2018/05/MPBStaffReport2018-05_LDC2018-10004.pdf.

⁴¹ Orlando, Fla. Code of Ordinances CH 58, Part 3A (2018).

Elements of the Ordinance⁴²:

- Type of Use: Accessory
- Zone Districts Allowed: All single-family districts and multi-family residential
- Density: ADUs are exempt from density calculations
- Size: Shall not exceed 750 square feet or 50% of the living area of the primary, whichever is less
- Owner-Occupancy: Owner must occupy either the primary unit or ADU

Alachua County

As with Pinellas County, Alachua County does not include the size of an ADU in gross residential density calculations and allows the homeowner to live in either the primary unit or ADU. The Alachua County ordinance is similar to Pinellas' in many respects and is also a model for local governments around the state. A change a county like Alachua could make is to consider zero-lot line configurations when establishing setback requirements. A relaxed setback requirement can encourage healthy ADU development on lots that may be otherwise unable to build a lawful ADU.

Elements of the Ordinance⁴³:

- Type of Use: Accessory
- Zone Districts Allowed: Single-family districts and agricultural districts
- Density: ADUs are exempt from density calculations
- Size: Maximum of 50% of principal residence or 1,000 square feet, whichever is greater
- Setbacks: Must meet applicable zoning district setback requirements
- Owner-Occupancy: Owner must occupy either the primary unit or ADU

⁴² Pinellas County Land Development Code § 138-1 (2018).

⁴³ Alachua County Code § 404.24 (2018).

EXAMPLES OF ADU POLICIES IN FLORIDA			
Elements of the Ordinance	City of Orlando	Pinellas County	Alachua County
Type of Use	Accessory	Accessory	Accessory
Zone Districts	All residential districts as well as mixed use and office districts.	All single-family districts and multi-family residential	Single-family districts and agricultural districts
Density	-	ADUs are exempt from density calculations	ADUs are exempt from density calculations
Size	Maximum of 50% of the size of the principal unit and can be no larger than 1,000 square feet	Shall not exceed 750 square feet or 50% of the living area of the primary, whichever is less	Maximum of 50% of principal residence or 1,000 square feet, whichever is greater
Minimum Lot Size	Correlated with the size of the ADU and depends on the zoning district. Residential districts require a lot size of a minimum of 5,500 square feet for an ADU of up to 500 square feet and 8,250 square feet minimum for an ADU of up to 1,000 square feet.	-	-
Parking	No required parking for ADUs of 500 square feet or less. One additional off- street parking space is required for ADUs above 500 square feet.	-	-
Setbacks	-	-	Must meet applicable zoning district setback requirements
Owner-Occupancy	Not explicit in the ordinance	Owner must occupy either the primary unit or ADU	Owner must occupy either the primary unit or ADU



XI. Other Resources for ADU Models

Santa Cruz, California Accessory Dwelling Unit Program

- Santa Cruz offers its residents assistance through loans, an ADU Manual, and ADU design prototypes.
 - http://www.cityofsantacruz.com/government/city-departments/planning-and-community-development/accessory-dwelling-units-adus

Family Housing Fund - Twin Cities ADU Guidebook for Homeowners

- Family Housing Fund is an affordable housing organization based in Minneapolis, Minnesota that has released ADU Guidebooks for Homeowners, ADU Developers, and Policy Leaders.
 - http://www.fhfund.org/adu/

Decatur, Georgia

- Decatur allows ADUs on all single-family lots and recognizes the use of ADUs as a tool to supply the "missing middle" of the housing stock.
 - http://www.decaturga.com/city-government/city-departments/planning-and-zoning-redesign/permits-and-zoning/accessory-dwelling-units

Urban Land Institute Study - Jumpstarting the Market for Accessory Dwelling Units: Lessons Learned from Portland, Seattle and Vancouver

- This study describes in detail how these three cities removed barriers to ADU development and the increase in construction that occurred.
 - http://ternercenter.berkeley.edu/uploads/ADU_report_4.18.pdf

NYU Furman Center – Responding to Changing Households: Regulatory Challenges for Micro-Units and Accessory Dwelling Units

- This work dives through several cities and their ADU regulations and discusses some barriers to ADU development.
 - http://furmancenter.org/files/NYUFurmanCenter_RespondingtoChangingHouseholds_2014_1.pdf

R Street Policy Study No. 89

- This study provides an introductory overview to ADU development, discusses ADU benefits and their barriers to full implementation.
 - http://www.rstreet.org/wp-content/uploads/2017/03/89.pdf

Department of Housing and Urban Development Accessory Dwelling Units: Case Study

- This 2008 study by HUD is outdated in some respects but does provide examples of how local governments have regulated ADUs around the country.
 - https://www.huduser.gov/portal/publications/adu.pdf



Appendix: ADU Manual for Homeowners

This document is intended to be a template for local governments to assist homeowners who may want to create an ADU.

Table of Contents

- What are ADUs? Introduction to ADU development
- Zoning and Design Standards Land Use/Zoning Regulations and Local Assistance
- Designing your ADU Neighborhood compatibility, ADU planning, financing, and design
- Permitting and Building your ADU Navigating the Local Development Process
- Managing your ADU Landlord/Tenant laws, leasing, and maintenance
- More Resources

Chapter One: What are ADUs?

Introduction

Walking around your neighborhood, you may have seen windows and a door above a garage or a cottage sized home in the backyard of your neighbor's house. What you have seen is likely an accessory dwelling unit. Interested, you may be wondering how the unit was built, if it is lawful, and how you can build your own for your elderly relative, collegiate son or daughter, or as a rental unit.

Accessory dwelling units (ADUs) are additional living quarters typically on single-family lots that are independent of the primary dwelling unit. An ADU can be an apartment within a primary residence or it can be an attached or freestanding home on the same lot as the primary residence.

Accessory dwelling units were formerly referred to as granny or mother-in law flats and are also sometimes referred to as accessory apartments, garage apartments, carriage houses, and backyard cottages. ADUs were a common feature of early 20th century development in America but their use dwindled with the onset of single-family suburb. ADUs were rarely included as an eligible use in municipal codes regulating land use, zoning, and general land development regulations.

The tide is changing. Increasingly, local governments around the State of Florida see the benefits that ADUs provide and are changing their zoning codes to allow ADUs as a lawful use in single-family neighborhoods. CITY/COUNTY allows ADUs as-of-right in single-family neighborhoods. This Manual answers questions you may have about ADU development and how you can construct a lawful unit on your property.

What are the benefits of an ADU?

ADUs provide many benefits for the homeowner and the community. If rented on the long-term market (typically, with a minimum six-month lease), an ADU can provide a homeowner additional income to help pay down a mortgage, meet other expenses, or provide income for investment. Due to the relatively small size of the unit and because it does not require additional land or major new infrastructure, an ADU can be a valuable affordable housing tool for lowto moderate-income individuals. ADUs promote mixed-income communities where lower-income households can find an affordable home in an area that may have greater employment and educational opportunities.

If not rented, an ADU can provide numerous other benefits. ADUs can be used by elderly or disabled individuals that strive for continued independence. An elderly or disabled individual could remain in their home and use an ADU for their caregiver. ADUs can also provide for family flexibility. The ADU can be used as a "granny flat" for elderly members of a family to help them age-in-place near the comfort of the family unit. With an ADU, a young adult could continue to live with their parents, but in a separate unit, as he or she works towards economic independence.

Further, when developed close to employment centers, an ADU can reduce a person's reliance on transportation, providing additional benefits to society through environmental and energy cost savings.

Who can build an ADU in (CITY/COUNTY)?

This Section should contain the basics of your ADU ordinance. Include basic details about minimum lot size, zoning, maximum lot coverage, owner-occupancy, and setback requirements. Below is an example.

Any homeowner within CITY/COUNTY who has a lot that is DESCRIBE MINIMUM LOT SIZE REGULATION or more in an area that is zoned for single-family dwellings may be able to build an ADU. An ADU must meet setback, lot coverage, and other land use regulations as described in Chapter Two of this Manual. The homeowner must live in either the main house or the ADU and only one ADU per single-family lot is allowed. The ADU may be detached from the main dwelling or attached.

What do I need to know to build an ADU?

Building an ADU may be one of the largest projects a homeowner undertakes on their property. First, decide whether you want to utilize the ADU as a long-term rental unit or for family members or other guests. If you choose the former, be aware of the landlord-tenant legal obligations and financial implications of leasing an ADU. Then, assess your finances and utilize this Manual to see if your lot is suitable for ADU development. Be sure that developing an ADU on your lot will meet zoning standards. If unsure that ADU development is right for you, CITY/COUNTY can assist in making this decision. TEMPLATE FOR LOCAL GOVERNMENT USE: ADU Manual for Homeowners

Chapter Two: Navigating ADU Development

This Chapter should describe the zoning and design standards as described in the local government's ADU Ordinance. It should provide easy-to-read charts on what properties are eligible to build a lawful ADU.

CITY/COUNTY has developed zoning standards for ADUs. These standards were established with community input to allow ADUs on the most possible lots. The table below provides a summary of CITY/COUNTY standards for an ADU located in a single-family zone.

The Table can contain more zoning standards as the local government finds necessary.

Zoning Standard	Requirement for ADUs	Other Comments
Minimum Lot Size		
Side-yard Setback		
Front-yard Setback		
Rear-yard Setback		
ADU Size		
Parking		
Owner-Occupancy		
Maximum Lot Coverage		
Impact Fees		
Density Calculations		
Maximum Height		
ADU Entrance		

It is important to make sure that your lot can contain a lawful ADU. CITY/ COUNTY can provide this guidance. You can also contact a local engineer to inspect your property for compatibility with these regulations. If you have further questions, please contact the RELEVANT DEPARTMENT at PHONE NUMBER/OTHER CONTACT INFORMATION to schedule an appointment to discuss the possibility of including an ADU on your property.

Local Government Assistance

This section should describe, in detail, any assistance that the local government offers for ADU development. It can include items such as an ADU loan program, impact fee reduction for long-term affordable units, technical assistance, and other financial assistance.

Chapter Three: Designing your ADU

Once I figure out the zoning standards for ADU development, what should I do next?

For this portion of the Manual, the local government should consider partnering with local architects and provide information on who has expertise in ADU development.

As with any construction or remodeling in CITY/COUNTY, appropriate building permits are required to develop an ADU. Chapter Four of this Manual provides information on how to navigate the permitting requirements. The permitting process will require drawings and models of your ADU. This Chapter discusses how to design your ADU.

Once you are sure that you can build a lawful ADU on your property, contact a local architect to begin designing the ADU. It will be beneficial to work with a qualified designer, builder, or engineer to make sure your project meets your needs as well as CITY/COUNTY permitting requirements. It is important to select professionals that are familiar with local development processes to ensure maximum ease of development. Local professionals can better anticipate the types of technical and regulatory issues you will need to address.

How should I begin designing the ADU?

First, it is important for your ADU to be a good fit with your home and the surrounding neighborhood. Consider talking to your neighbors to see how your ADU can best fit on your site and into your neighborhood. You should walk around your neighborhood and gather as much information as you can to make sure the ADU is compatible with the surrounding environment. Here are some good questions to consider before designing your ADU:

- What is the predominant height of homes in the neighborhood?
- How much space is there between homes?

- How many neighboring properties have accessory units in their backyard?
- Do these accessory units blend in with the surrounding buildings? Are they attached or detached?
- Is there one material or color that is predominately used for the homes on your block?
- Where do most of the homes have their garages? Are they detached or attached?
- What do the backyards in your neighborhood typically contain?
- How private are the backyards in the neighborhood? Does vegetation exist on the sides or rear of homes?

Answering these questions will help you design an ADU that can blend in with the neighborhood. Understanding this fit will allow the ADU to exist within the fabric of the existing community.

Privacy of Adjoining Properties. It is also important to understand the privacy aspects of building an ADU. Your neighbors may not want a dwelling in the backyard next to theirs that can potentially see into their home. You can resolve privacy issues with additional vegetation, careful planning, and communication with your neighbors. The orientation of an ADU can solve privacy issues. You may think about which way your unit faces and where the windows and doors are located.

Privacy for ADU residents. When designing your ADU, there is the opportunity to plan for which parts of the parcel will be used exclusively for the homeowner, the tenant, and for shared use. You will need to consider how tenants can access the ADU to limit passing by private rooms on route to the ADU. The location of parking and the ADU can also have a noise and physical impact on the primary unit and surrounding properties. You may

want to be sure that tenants of the ADU need not walk near surrounding dwelling units on the way to the ADU.

Design Compatibility. You will also need to consider the architectural compatibility with your primary unit. The ADU should be similar in appearance to the primary unit to create an aesthetic and ownership connection between the main house and the ADU. You should also be careful in designing the ADU in a manner that restricts the view of the primary unit or neighboring units. A larger ADU, for example, may restrict visual and/or physical access to a lake or other natural spaces. At a fundamental level, it is important that the ADU blend into the surrounding neighborhood and not be cause for concern from a design and planning standpoint.

Fundamentally, you will need to decide:

- Where the ADU will be located your property
- The size of the ADU
- Which direction the ADU faces
- How to access the ADU with the least impact on surrounding properties
- How to minimize privacy concerns
- Design compatibility with the primary unit and surrounding neighborhood
- When you are going to schedule the work

All these decisions should be made with the underlying goal to design your ADU in a way that fits into the existing community. Work with your site engineer/architect or contact CITY/COUNTY for more information on designing your ADU.

How much will an ADU cost?

At this point in process, you will also need to figure out the financing and development costs for your ADU. If you plan to use the ADU as a long-term rental unit, you may want the rent to cover the cost of development while keeping the monthly rent low enough to be attractive to renters. If you are building the ADU for other reasons, such as to house a caregiver, you may weigh the costs and benefits of building the ADU in comparison to the costs and benefits of moving to an assisted living facility, for example.

First, you will need to consider the "hard costs" of ADU development. These costs are expenses directly related to the physical construction of the building. These costs cover the material and labor that will go into ADU development. The material hard costs include items such as cement, drywall, carpet, windows, and doors. Labor hard costs can include landscaping, site excavation, carpentry, and general building of the ADU.

To lower your hard costs, you have some control over your destiny. Rather than building a detached ADU, for example, you can save money converting your garage into an apartment or by building an attached ADU. You can also choose the materials that you use to build the ADU. If parking is not required and you are able to connect to existing utilities, you can save costs there as well. You can also decide to do part of the work yourself instead of hiring additional labor. Below is an example ADU budget provided by the City of Santa Cruz, California. This is only a sample of what tools you will be dealing with as the prices will likely be different based on material selection, your customization needs, and the current pricing of these supplies in Florida.

Торіс		Total Dollars
Off Site Improvements	Water Service	\$3,500
Foundation	Grading/Excavating/Backfill/Compaction Concrete & Rebar, Anchoring	\$2,500 \$7,500
Framing	Studs, joists, rafters, sheathing, beams, headers, connectors	\$24,500
Plumbing	Rough Finish	\$2,500 \$900
Roofing	Asphalt shingle	\$3,500
Doors	Interior, exterior, shower encl.	\$3,500
Windows	Wood	\$4,500
Finishes	Drywall Carpeting Resilient Flooring Countertops (laminate) Cabinets Ceramic Tile Painting (interior and exterior)	\$3,250 \$900 \$800 \$750 \$1,200 \$1,200 \$5,000
Metalwork	Piperail Guardrails (Int.) Gutters, downspouts	\$2,500 \$1,000
Mechanical	Tankless Water Heater Gas Fired Wall Heaters Garbage Disposal	\$750 \$800 \$200
Landscaping	Allowance	\$500
Total Preliminary Estimation of Construction Cost		\$76,000

Next, you will need to consider the "soft costs" of ADU development. These costs are expenses indirectly related to the construction of the ADU. These include development fees, planning costs, utility hook-up fees, and professional design and engineering services. If you work with a local engineer with experience with the local development process, these costs may be easy to calculate.

Other soft costs include the maintenance of the ADU. Be sure to consider ongoing repairs as a part of your cost calculation and decide on materials up-front that may bring less maintenance costs down the road.

How can I finance my ADU?

If you do not have enough cash on hand, traditional mortgage products are regularly used to construct ADUs. First, you could seek a Home Equity Line of Credit (HELOC) or a Home Equity Loan. Both of these products are essentially second mortgages backed by the equity you own in your home. A Home Equity Loan provides a fixed amount of cash on a fixed repayment schedule backed by the equity in your home. A HELOC is similar but is structured as revolving lines of credit, like a credit card, that has shorter repayment terms and only charges interest on the balance you have drawn. You can typically borrow up to 85% of the value of your home minus the amount you owe. This product typically has a 10-year draw period followed by a 20-year repayment period.

Similarly, you can seek cash-out refinancing. This method is similar to home equity financing except that it replaces your current mortgage, has a fixed

interest rate over the life of the loan (instead of an adjustable interest rate) that is typically lower than a HELOC, has greater initial payments, and is typically more cumbersome to receive. This method allows you refinance your current mortgage for more than what you currently owe in order to receive a lump-sum of cash to build your ADU. An advantage to this option is you can set the loan term for thirty years, lowering the monthly payments by spreading the cost of the ADU over a longer period.

A construction loan can also be used. This loan can be utilized if you do not have sufficient equity based on your current home value. This type of loan looks at the improved value of the home rather than the current home value, allowing you to receive a greater loan if you lack necessary home equity. The closing costs and interest rates for a construction loan are typically higher than a standard refinance.

If the local government offers a loan program for ADUs used as long-term affordable housing units, include that information here. For instance, the local SHIP program could be used for a loan program for ADUs, and the additional benefit of using SHIP would be the assurance that the ADU would serve an income eligible renter (could not be used for tourist vacation rental) and would be monitored for compliance.

Contact your financial advisor, lender, or RELEVANT DEPARTMENT at PHONE NUMBER/OTHER CONTACT INFORMATION for more information on the best financing options for your ADU.

Chapter Four: Permitting and Building Your ADU

The Land Development Process

Once you have your ADU design and financing figured out as described in Chapter 3, you will need to begin navigating the local development process. Contact RELEVANT DEPARTMENT at PHONE NUMBER/ OTHER CONTACT INFORMATION for more information on starting the development process for your ADU.

In this section, include information on the local land development process with in-depth information on how a homeowner can navigate relevant procedures.

Building Your ADU

Once your permits are finalized, you can begin building your ADU! First, you will want to hire a licensed and insured residential building contractor. You should ask two or three contractors to bid on your ADU. All bids should be based on the same set of plans and specifications and with the same materials, appliances, windows, and similar tools. Discuss the bids in detail with each contractor and gather as much as you can about the success and reputation of each. It is important to choose a contractor that is perfect for you. Ask the contractor for local references to see if former clients were satisfied with the work.

Construction Contract

Once you have a contractor in place, make sure you have a written contract in place and do not sign anything unless you completely understand what you are signing. Consult with an attorney if possible. Be as specific as possible and be sure the terms of the contract are clear. The contract should include the total price, when payments will be made, and whether there is a cancellation penalty. Include all aspects of the work that you consider important, including complete cleanup, removal of debris and materials, and when the work shall be done.

After the contract is signed, be aware that modifications can be made with mutual agreement. Always use a signed "change order" if you add or delete work, substitute materials or equipment, or change the completion date. It is very important to have all modifications signed by both parties.

Inspections

This section should contain information on the local inspection process.

Chapter Five: Managing Your ADU

Renting your ADU

This section applies if you decide to rent your ADU. If you intend to rent your ADU, you will be a landlord and there are many items you will need to consider.

Choosing a tenant for your ADU may be the most important thing you do as a landlord. You will be choosing a person or household that will be living on your property. To ensure the right tenant, you can first establish a screening process to attract responsible and honest applicants. Choose criteria by which to judge applicants and apply the criteria consistently for all applicants. Here are some potential screening points:

- Require contact information for most recent landlords
- Require submittal of a complete application
- Run a credit and criminal background check
- Personal references

It is important to use a written rental application when selecting tenants. A good application gives you access to verifiable information. Contact a local rental housing association or legal counsel for copies of sample rental applications. There are many resources at your disposal in this context. Before potential tenants submit their application, it is a good time to distribute your tenant selection criteria as well as specific information about security deposits, vehicles, pet policy, maximum occupancy, and other issues related to the rental of the ADU. If the applicant rides a bicycle, consider providing a secure location for the bike.

After receiving applications, request a credit check on each tenant who will be signing the lease. Credit checks reveal information about installment and revolving credit lines, court records, collection accounts, judgments, liens, and may be used to determine whether you think an applicant has the ability to pay rent. You can also check with the applicant's previous landlords to determine whether the applicant will be a tenant who pays in a timely fashion and keeps the property in good order. If the applicant is local, you can also ask permission to visit their current residence to assess their housekeeping. In choosing your ADU tenant, be sure to use a process that is simple and fair. Follow all relevant civil rights laws which are designed to prevent discrimination based on issues that are unrelated to a person's qualifications to be a good tenant.

Once you have chosen the tenant, execute a written lease. First, decide how long the lease-term will be. If the lease term is for six months or less, you must remit Florida's 6% sales tax plus any applicable discretionary sales surtax. Lease terms of longer than six months are exempt from sales tax. The lease agreement is vital to forming the understanding between the two parties. Responsibilities should be comprehensive and as clear and concise as possible, and spell out all expectations and responsibilities of each party. Consult with an attorney when devising a lease agreement. Finally, consult with your insurance agent to make sure you have adequate coverage for your ADU.

Obligations as a Landlord

Being a landlord in Florida brings responsibilities. In exchange for receiving rent and the right to have the ADU returned to you undamaged at the end of the lease term, you must satisfy your duties as a landlord. If unsure of your obligations, consult with an attorney before renting your ADU.

As a landlord, you have the duty under Section 83.51 of the Florida Statutes to provide a home that is safe and meets applicable housing, building, and health codes. You must make reasonable repairs as necessary to make sure the structural components of the ADU are in good repair and capable of resisting normal forces and loads. This may include fixing broken pipes, windows, doors, and other items that impair the safety of the home. You must make sure the plumbing is in reasonable working condition and provide for functioning facilities for heat during winter, running water, and hot water. Florida law also proscribes affirmative disclosures you must make to your tenant.

It is also your duty to respect the tenant's rights as defined in Chapter 83 of the Florida Statutes and pursuant to the Lease. One of the most important tenant rights is the right of peaceful possession. You must not interfere with the tenant's leasehold without first consulting the tenant and providing reasonably timed notice. You have the right to protect your ADU through inspection, but you must give a reasonable notice of at least 12 hours. You may not show prospective buyers or tenants the ADU without notice to and with the agreement of the existing tenants.

Further, it is unlawful to increase or decrease services in a discriminatory manner or threaten to bring an action for possession in retaliation. Retaliation may be presumed if it occurs after a tenant has complained about housing conditions. It is also unlawful to lock the tenant out, shut off utilities, or remove tenant's property from the ADU.

A landlord must follow all lease terms in accordance with the termination of the lease. If there is no written rental agreement or if the lease does not state otherwise and unit is rented on a month-to-month basis, you must give at least 15 days- notice in writing to end the tenancy. A week-to-week rental period requires seven days- notice. The notice may be posted on the door of the ADU if the tenant is absent from the premises.

If the lease agreement is violated by the tenant, certain circumstances must be met before the tenant can be evicted. Section 83.20 of the Florida Statutes lists the causes for removal of tenants. If the tenant fails to pay rent or refuses to move out, you may evict the tenant, but only after you have taken the proper steps to commence an action for possession. These include notifying the tenant and if the tenant does not cure the violation within three days after receiving notice, the landlord may file for eviction. Other steps follow. Because these steps are so technical, you should consult with an attorney when engaging in the eviction process.

The purpose of this information is not to dissuade you from creating and renting an ADU, but rather to provide a full picture of the landlord obligations that come with renting any home or apartment.

Maintaining the ADU

The ADU must be maintained in accordance with housing, building, and health codes.

If your ADU is a rental unit, be sure to respond to any tenant complaints in a swift manner. Follow the lease terms as to maintenance of the ADU. Most leases will state a procedure for repairs and damages in the event of a breach of contract. Under Section 83.201 of the Florida Statutes, if the lease is silent on the procedure to be followed to effect repair or maintenance and the tenant places the obligation on the landlord, the tenant may withhold rent after notice to the landlord if the landlord fails to repair the unit. If the landlord does not fix the issue within 20 days, the tenant may withhold rent until the repair has been performed. Once the repair is completed, the tenant shall then pay the amounts of rent withheld. The lease may provide for a longer period of time for repair or maintenance.

Chapter Six: More Resources

In this section, include resources as the local government finds necessary to round out this educational material. This section should include a copy of the ADU ordinance and other applicable laws including, but not limited to, landlord-tenant laws and civil rights laws. This section may include local contractors, engineers, and architects that have expertise in ADU development as well as the contact information of all relevant departments of the local government. It may contain permit fees, a local ADU development checklist, other building codes, and other useful websites for homeowner education. If you would like assistance in developing your local government's Homeowner ADU Manual, please contact the Florida Housing Coalition.

Notes



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we make housing affordable

ACCESS AN ELECTRONIC VERSION OF THE ACCESSORY DWEILING UNIT GUIDEBOOK

AND OTHER VALUABLE RESOURCES UNDER THE PUBLICATIONS TAB ON THE FLORIDA HOUSING COALITION'S WEBSITE AT: FLhousing.org



NOTICE OF PUBLIC MEETING CITY OF LAKE CITY PLANNING AND ZONING BOARD

THIS SERVES AS PUBLIC NOTICE the Planning and Zoning Board will hold a meeting on Tuesday, May 14, 2024 at 5:30 PM or as soon after.

Agenda items-

- SPR 24-05, Petition submitted by Randall Olney, P.E., (agent) for Concept Companies, (owner), for a Site Plan Review for Dollar General, in a Commercial Intensive zoning district, and located on parcel 08127-005, which is regulated by the Land Development Regulations Section 4.13.
- LDR 24-04, Text amendment to the Land Development Regulations Sections 2.1, 4.2, 4.4, 4.5 and 4.6, to add definitions and add provisions for ADU's, Accessory Dwelling Units, and Tiny Homes for the City of Lake City.

Meeting Location: City Council Chambers located on the 2nd Floor of City Hall at 205 North Marion Avenue, Lake City, FL 32055.

Members of the public may also view the meeting on our YouTube channel at: https://www.youtube.com/c/CityofLakeCity

Pursuant to 286.0105, Florida Statutes, the City hereby advises the public if a person decides to appeal any decision made by the City with respect to any matter considered at its meetings or hearings, he or she will need a record of the proceedings, and that, for such purpose, he or she may need to ensure that a verbatim record of the proceedings is made, which record includes the testimony and evidence upon which the appeal is to be based.

SPECIAL REQUIREMENTS: Pursuant to 286.26, Florida Statutes, persons needing special accommodations to participate in this meeting should contact the City Manager's Office at (386) 719-5768.

> Robert Angelo Planning and Zoning Tech.

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Robert Angelo Planning and Zoning Tech.



From:	LCR-Classifieds <classifieds@lakecityreporter.com></classifieds@lakecityreporter.com>
Sent:	Monday, April 29, 2024 12:02 PM
To:	Angelo, Robert
Subject:	RE: 73990 73992 73991 RE: Non-Legal Ad for P&Z, BOA, and HPA for 05-14-2024

Confirmed

Thank you much, **Kymberlee Harrison 386-754-0401** Support your local news source while reaching our community of loyal subscribers *Screing:*

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1086 SW Main Blvd. Ste 103, Lake City, FL 32055 PH 386-754-0401

Why Local Newsprint Advertising?

1 Newspaper readers are ENGAGED

2 Newspapers are viewed as TRUSTWORTHY

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Subject: RE: 73990 73992 73991 RE: Non-Legal Ad for P&Z, BOA, and HPA for 05-14-2024

Looks good.

Thank You Robert Angelo City of Lake City Growth Management growthmanagement@lcfla.com 386-719-5820



PLEASE NOTE: Florida has a very broad public records law. Most written communications to or from City officials regarding City business are public records available to the public and media upon request. Your email communications may be subject to public disclosure.

From: LCR-Classifieds <<u>classifieds@lakecityreporter.com</u>> Sent: Monday, April 29, 2024 11:20 AM To: Angelo, Robert <<u>AngeloR@lcfla.com</u>> Subject: 73990 73992 73991 RE: Non-Legal Ad for P&Z, BOA, and HPA for 05-14-2024

Robert, all are scheduled to publish on May 2. Approval due by tomorrow please P&Z: 3 col x 5.5 \$272.25

Historic: 3 col x 4.5 \$222.75 BOA: 3 col x 4 \$198

Thank you much, **Kymberlee Harrison 386-754-0401** Support your local news source while reaching our community of loyal subscribers *Serving:* **COLUMBIA • SUWANNEE • HAMILTON • LAFAYETTE** 1086 SW Main Blvd. Ste 103, Lake City, FL 32055 PH 386-754-0401 **Why Local Newsprint Advertising?** <u>1</u> Newspaper readers are ENGAGED <u>2</u> Newspapers are viewed as TRUSTWORTHY

From: Angelo, Robert <<u>AngeloR@lcfla.com</u>> Sent: Monday, April 29, 2024 8:57 AM To: LCR-Classifieds <<u>classifieds@lakecityreporter.com</u>> Subject: Non-Legal Ad for P&Z, BOA, and HPA for 05-14-2024

Kym

Please publish this ad in the body of the paper as a display ad in the May 2, 2024 paper.

Thank You Robert Angelo City of Lake City Growth Management growthmanagement@lcfla.com 386-719-5820



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> Robert Angelo Planning and Zoning Tech.





Angelo, Robert

From: Sent: To: Subject: LCR-Classifieds <classifieds@lakecityreporter.com> Monday, April 29, 2024 10:59 AM Angelo, Robert RE: 813653 RE: Legal ad for LDR24-04

Confirmed

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From: Angelo, Robert <AngeloR@lcfla.com> Sent: Monday, April 29, 2024 10:28 AM To: LCR-Classifieds <classifieds@lakecityreporter.com> Subject: RE: 813653 RE: Legal ad for LDR24-04

Looks good.

Thank You Robert Angelo City of Lake City Growth Management growthmanagement@lcfla.com 386-719-5820



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From: LCR-Classifieds <<u>classifieds@lakecityreporter.com</u>> Sent: Monday, April 29, 2024 9:19 AM To: Angelo, Robert <<u>AngeloR@lcfla.com</u>> Subject: 813653 RE: Legal ad for LDR24-04

Please see attached for approval

Thank you much,

Kymberlee Harrison 386-754-0401

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1086 SW Main Blvd. Ste 103, Lake City, FL 32055 PH 386-754-0401

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From: Angelo, Robert <<u>AngeloR@lcfla.com</u>> Sent: Monday, April 29, 2024 8:53 AM To: LCR-Classifieds <<u>classifieds@lakecityreporter.com</u>> Subject: Legal ad for LDR24-04

Kym

Please publish in the legal section of the Lake City Reporter on May 2, 2024.

Thank You Robert Angelo City of Lake City Growth Management growthmanagement@lcfla.com 386-719-5820



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ORDER CONFIRMATION

Salesperson: KYM HARRISON	Printed at 04/29/24 09:18 by kharr-cn
Acct #: 45150	Ad #: 813653 Status: New WHOLD
CITY OF LAKE CITY ATTN: FINANCE 205 N MARION AVE LAKE CITY FL 32055	Start: 05/02/2024 Stop: 05/02/2024 Times Ord: 1 Times Run: *** STD 1.00 X 11.79 Words: 426 Total STD 11.79 Class: 8000 LEGAL COLUMBIA CO Rate: LG Cost: 194.54
Contact: AP CHERYL 719-5794 Phone: (386)719-5804 Fax#: Email: Agency:	# Affidavits: 1 Ad Descrpt: LDR24-04
PUB ZONE EDT TP RUN DATES LCR A 96 S 05/02	

AUTHORIZATION

Under this agreement rates are subject to change with 30 days notice. In the event of a cancellation before schedule completion, I understand that the rate charged will be based upon the rate for the number of insertions used.

Name (print or type)

Name (signature)

(CONTINUED ON NEXT PAGE)

This ad has been reformatted for proofing purposes. Column breaks are not necessarily as they will appear in publication.

NOTICE OF PUBLIC HEAR-INGS CONCERNING AMEND-MENTS TO THE CITY OF LAKE CITY LAND DEVELOP-MENT REGULATIONS BY THE PLANNING AND ZON-

BY THE PLANNING AND ZON-ING BOARD OF THE CITY OF LAKE CITY, FLORIDA, SERV-ING ALSO AS THE LOCAL PLANNING AGENCY OF THE CITY OF LAKE CITY, FLORI-DA, NOTICE IS HEREBY GIV-EN that, pursuant to Section 163.3161 through 163.3248, Florida Statutes, as amended, and the City of Lake City Land Development Regulations, as amended, objections, recommendations and comments concerning the amendments, as described below, will be heard by the Planning and Zoning Board of the City of Lake City, Florida, serving also as the Local Planning Agency of the City of Lake City, Florida, at public hearings on May 14, 2024 at 5:30 p.m., or as soon thereafter as the matters can be heard in the City Council Meeting Room, Second Floor, City Hall, located at 205 North Marion Avenue, Lake City, Florida and via communications

(1) LDR 24-04, Text amendmedia technology. (1) LDR 24-04, Text amendment to the Land Development Regulations Sections 2.1, 4.2, 4.4.5, 4.5.5, and 4.6.5, to amend the text in section 2.1 adding a definitions for Accessory Dwelling Units (ADU), infill, infill subdivision, Tiny Homes (On Wheels for Permanent Installation), Tiny Home (On Wheels for Portable Use), to amend section 4.2 adding section 4.2.36, entitled Requirements for Accessory Dwelling Units and Tiny Homes, and amending the text in sections 4.4.5, 4.5.5, and 4.6.5 adding text for ADUs and Tiny Homes

Tiny Homes. Members of the public may also view the meeting on our YouTube channel at: https://www.youtube.com/c/City ofLakeCity.

Those attendees wishing to share a document must email the item to submissions@lcfla.com no later than noon on the day of the meeting.

Copies of the amendments are available for public inspection by contacting the Office of Growth Management at growthmanagement@lcfla.com or by calling 386.719.5746. At the aforementioned public

At the aforementioned public hearings, all interested parties may appear and be heard with respect to the amendments.

All persons are advised that if they decide to appeal any decision made at the above referenced public hearings, they will need a record of the proceedings, and that, for such purpose, they may need to ensure that a verbatim record of the proceedings is made, which record includes the testimony and evidence upon which the appeal is to be based. Persons with disabilities requesting reasonable accommo-

Persons with disabilities requesting reasonable accommodations to participate in these proceedings should contact the Office of City Manager, 386.719.5768 at least 48 hours prior to the proceedings. If you are hearing or speech impaired, please contact the Florida Relay Service at 800.955.8770 (voice) or 800.955.8771 (TTY).

813653 May 2, 2024 NOTICE OF PUBLIC HEARINGS CONCERNING AMENDMENTS TO THE CITY OF LAKE CITY LAND DEVELOPMENT REGULATIONS

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